# Palestine Polytechnic University



# College of Engineering & Technology Electrical & Computer Department

**Graduation Project** 

Sign Language Coach

Project Team:
Hanan Ahmad Shroukh
Heba Mosa Al\_Dababseh
Tahreer Qaher Mohammad

Project Supervisor Eng. Hiba Tamimi Eng.Amal Dwaik

Hebron-Palestine June, 2008

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جامعة بوليتكنك فلسطين الخليل- فلسطين كلية الهندسة والتكنولوجيا دانرة الهندسة الكهربانية والحاسوب

اسم المشروع: Sign Language Coach

أسماء الطلبة: حنان أحمد الشروخ هبه موسى الدبابسه تحرير قاهر محمد

بناء على نظام كلية الهندسة والتكنولوجيا وإشراف ومتابعة المشرف المباشر على المشروع وموافقة أعضاء اللجنة الممتحنة تم تقديم هذا المشروع إلى دائرة الهندسة الكهربائية وذلك للوفاء بمتطلبات درجة البكالوريوس في الهندسة تخصص هندسة أنظمة الحاسوب

توقيع المشرف توقيع اللجنة الممتحنة توقيع رنيس الدائرة

#### Abstract

The Sign Language Coach (SLC) is an embedded system that translates the movement of the fingers that represent the American Sign Language (ASL) into letters.

ASL is a visual language, meaning that the information is expressed not with combination of sound but with combination of hand shapes, palm orientations, movements of the hands, arms and body, location in relation to the body, and facial expressions.

The system was implemented using statistical approach which called nearest neighbor algorithm, and it uses a glove to recognize the hand positions and outputs letters onto LCD.

The goal is achieved and the system was able to recognize 26 letters at PC phase.

#### الملخص

معلم لغة الاشارة هونظام يقوم بترجمة حركة الاصابع الممثلة بلغة الاشارة الامريكية الى حروف. لغة الاشارة الامريكية هي عبارة عن لغة مرئية وهذا يعني ان المعلومات لا يعبر عنها بالصوت وانما يعبر عنها بحركة اليد وشكلها ودوران الكف وحركة الذراع والجسم ، وموقع الكف بالنسبة للجسم، وتعابير الوجه.

تم تمثيل النظام باستخدام طريقة احصائية تسمى خوارزمية الجار الاقرب ، ويستخدم كف للتعرف على مواقع اليد ويخرج النتيجة على LCD.

الهدف من النظام تحقق؛ فالنظام قادر على التعرف على 26 حرف في مرحلة الكمبيوتر.

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### **List of Abbreviations**

ASL American Sign Language

DC Direct Current

EEPROM Electrically Erasable Programmable Read Only Memory

LCD Liquid Crystal Display

LABVIEW Laboratory Virtual Instrument Engineering workbench

MCU Microcontroller Unit

MSSP Managed Security Service Provider

OpAmp Operational Amplifier

PC Personal Computer

PGSI Power Glove Serial Interface

PIC Peripheral Interface Controller

SLC Sign Language Coach

SVM Support Vector Machine

SRAM Static Random Access Memory

USART Universal Synchronous Asynchronous Receiver Transmitter

T Task

# **CHAPTER**

1

### **INTRODUCTION**

Introduction

General idea about project and its importance

Project objectives

Literature review

Time plane / project schedule

Estimated cost and budget break down

Project risk management

Report contents

### Chapter one

### Introduction

#### 1.1 Introduction

This chapter presents the general idea about project, its importance, literature review and estimated cost.

### 1.2 General idea about project and its importance

Sign Language Coach (SLC) is an embedded system that translates the movement of the fingers of a glove into the American Sign Language (ASL). The system is portable and stands alone.

This system consists of an ordinary glove and movement sensors, a microcontroller unit (MCU). The system outputs letters on an LCD.

### 1.2.1 Importance of project

- 1. Help deaf people to explain what they need in their society.
- 2. The Sign Language Coach (SLC) helps people to understand the American Sign Language(ASL) by translating the sign into letters.

### 1.3 Project objectives

- 1. Create a glove that senses a user's finger position.
- 2. Translate the American Sign Language into letters that appear on the LCD.
- 3. Match each sign with the appropriate letter.

#### 1.4 Literature review

This section mentions previous projects that done in this domain.

### The AcceleGlove [1]

The AcceleGlove is a portable system, designed as an assistive device that translates hand and gesture based languages into written and spoken language. The AcceleGlove consists of a group of sensors and accelerometers that are strapped to the hand, arm and shoulder and a set of algorithms that decipher and categorize the movements of the hand and arm. The accuracy of this system is 89%.

# Arabic Sign Language recognition using an instrumented Glove[2]

This system recognizes Arabic Sign Language using an instrumented glove as interfacing device and the support vector machine algorithm as classification Algorithm, this instrumented glove is the power glove. The accuracy of this system is 85%.

• Mehdi and Khan proposed a glove. It used a seven sensors form 5 dimensions and a multi-layer perception neural network to recognize the alphabet of the American Sign Language (ASL). The glove that used provides only measurements for the bend of each finger and measures the tilt and the rotation of the hand. The neural network that used had 7 neurons in the input layer, 54 neurons in the hidden layer and 26 neurons in the output layer. The system was able to achieve an accuracy of around 88% [3].

Yoon and Jo designed a vision-based system for recognizing the Korean Sign Language alphabet, which consists of 16 consonants and 14 vowels. The system consists of a video camera connected to a computer with an image capturing board

To aid the system in extracting the hand shape form images, the user of the system wears gloves with different colors for each hand. Moment invariance was used for recognition and experiments with one person showed a recognition rate of 97% [4]

### 1.5 Time plane / project schedule

The project time needed is 32 weeks.

### 1.5.1. The main activities in this project:

T: Task.

T1: Collecting information and theoretical issues.

At the beginning; the requirements collected from the stakeholders and then a feasibility study will be written.

T2: Analyzing and specifying the concepts.

In this activity the requirements will be analyzed very well to make decisions regarding what the new system will be according to users and stakeholders defining user and system requirements.

#### T3: System modeling and design.

After collecting the requirements and writing the feasibility study, the system modeled .

#### T4: Learning American Sign Language.

In this task the designer will learn how to represent the letters using American Sign Language.

T5: System implementation.

T6: System testing.

T7: System documentation.

The following tables display the duration of each task

Table (1.1): The tasks duration for first semester

| Activities (Tasks)                     | Symbol | Duration(week) |  |  |  |
|--|--------|----------------|--|--|--|
| Collecting information and theoretical | T1     | 8              |  |  |  |
| issues                                 |        |                |  |  |  |
| Analyze the concepts.                  | T2     | 6              |  |  |  |
| System modeling and design             | Т3     | 6              |  |  |  |
| Learning American sign Language        | T4     | 6              |  |  |  |
| System documentation.                  | T7     | 15             |  |  |  |

Table (1.2): The tasks duration for the second semester

| Activities(Tasks)      | Symbol | Duration(week) |
|------------------------|--------|----------------|
| System implementation. | Т5     | 8              |
| System testing         | Т6     | 7              |
| System documentation.  |        | 15             |
| Final project          |        | 32 week        |

The time chart of each semester is shown below:

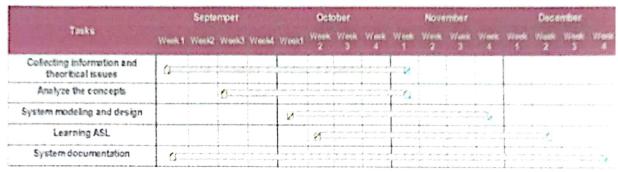


Figure 1.1. Project scheduling & time plan (First semester)

|                       | February |       | March |       |                        | April     |           |           |           | May  |           |           |           |           |  |           |
|-----------------------|----------|-------|-------|-------|------------------------|-----------|-----------|-----------|-----------|------|-----------|-----------|-----------|-----------|--|-----------|
| Tasks                 | Week 1   | Week2 | Week3 | Week4 | Week1                  | Week<br>2 | Week<br>3 | Week<br>4 | Week<br>1 | Week | Week<br>3 | Week<br>4 | Week<br>1 | Week<br>2 | Week 3   | Work<br>4 |
| System implementation | 0=       |       |       |       |                        | -         |           | -         | I         | -    | K         | -         |           | -         | The same of the sa |           |
| System testing        |          |       |       |       |                        | O         |           |           | 1         |      | -         |           |           | 3         |  |           |
| System documentation  | Q=       |       |       | -     | in a second control of |           | -         | -         | I         |      |           |           |           |           |  | -V        |

Figure 1.2. Project scheduling & time plan (second semester)

### 1.5.1 Project management

This section presents the members of the project and their job.

### 1.5.1.1 Allocation of rules of system developers

- Collecting information and theoretical issues (T1)→Tahreer + Hanan+Hiba.
- Analyzing and specifying of the concepts (T2)→Hanan.
- -System modeling and design (T3)→Hiba.
- -Learning American Sign Language (T4)→Hanan+Hiba+Tahreer.
- -System implementation (T5)→ Hanan + Hiba + Tahreer.
- -Testing (T6)→ Hanan + Hiba +Tahreer.
- -Documentation (T7)→ Hanan+Hiba+Tahreer.

#### 1.6. Estimated cost

This section presents the hardware cost and the software cost.

### 1.6.1. Hardware Component

This section mentions the cost of hardware components.

Table (1.3): Hardware cost

| Component                                   | Cost   |
|---|--------|
| Accelerometer<br>sensor(ADXL202AQC)<br>(#5) | 153\$  |
| LCD 2X16                                    | 10\$   |
| Capacitor 0.1MF(# 5) + 0.47MF(# 10)         | 2\$    |
| Resistor ( 25K +100k)(#5)                   | 1\$    |
| Board                                       | 15\$   |
| LM358                                       | 3(1)\$ |
| Wires                                       | 20\$   |
| Regulator 7807                              | 1\$    |
| PC  |        |
| DAQ   |        |

### 1.6.2. Software Component

This section mentions the cost of software components.

Table (1.4): Software cost

| Component    | Cost |
|--------------|------|
| Flash memory | 15\$ |
|              | 20\$ |
| PIC 18f4550  | 204  |

## 1.6.3. Human Development Resources

The development of project will be implemented by a team of 3 developers.

### **Human resources cost estimation**

The project team works through 32 week, 5 days per week, and 5 hours a day. Total number of hours:

32 week\*5 days\*5 hour=800hour.

800 hour\*\$10=\$8000 per individual

Total human cost=\$8000\*3=\$24000

Internet:

Total internet cost=7week\*5hour\*\$1=\$ 35

#### 1.6.4. Total cost

The following table shows the total cost of the whole component:

Table (1.5): Total cost

| Resource | Estimated cost |
|----------|----------------|
| Hardware | 203\$          |
| Software | 35\$           |
| Human    | 24000\$        |
| Internet | 35\$           |

### 1.7. Project risk management

In this project the team may faces the following risks:

- Some activities may not be made on time for some reasons, such as one of the team members might become ill.
- The system may fail in the operation stage.
- Political situation may affect the time schedule like suspensions in university.

### Nonfunctional risks:

Project component may not found.

#### **Functional risks:**

Some requirements might be changed.

### Operational risk:

Appearance of new requirement after or during development stage.

### 1.8. Report contents

The report consists of seven chapters; this is a brief description of the main topics of each chapter.

Chapter (2): Introduces and illustrates the idea of the project, describes the component used in the project, software component and hardware component.

Chapter (3): Introduces the design concepts, the project objectives, and the general block diagram of the system and explains how system works.

Chapter (4): Outlines formal procedure for design, and the overall system design.

Chapter (5): Contains the software.

Chapter (6): Contains the system implementation and testing.

Chapter (7): Contains the conclusion and future work.

# **CHAPTER**

2

### THEORETICAL BACKGROUND

Introduction.

Theoretical background of the project.

Hardware and Software component.

Project integrity.

#### Chapter two

### Theoretical background

### 2.1 Introduction

This chapter focuses on theoretical subjects related to the main idea of the project, and information about the components used in the project.

### 2.2 Theory

Sign language can be represented using different sign languages such as Arabic sign Language, British Sign Language, and American Sign Language (ASL). This project deals with American Sign Language (ASL).

#### 2.2.1 American Sign Language (ASL)

ASL is a natural language contains semantic, syntax and pragmatics just like spoken language.

It is a manual language or visual language, meaning that the information is expressed not with combination of sound but with combination of hand shapes, palm orientations, movements of the hands, arms and body, location in relation to the body, and facial expressions.

While spoken language are produced by the vocal cords only, and can thus be easily written in linear pattern, ASL uses the hands, head and body, with constantly changing

movements and orientation. ASL is used natively and predominantly by the deaf and hard-of-hearing.

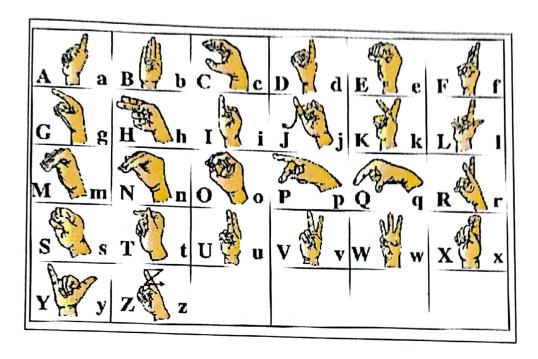


Figure 2.1: ASL (letters and its associated sign using one hand) [5]

### 2.3 Components

There are two kinds of components hardware component and software component.

### 2.3.1 Hardware Component

This section mentions and explains the hardware that are used in this project

### 2.3.1.1 Accelerometer sensor

Piezo- electric crystals are man made or naturally occurring crystals that produce a charge output when they are compressed, flexed or subjected to shear forces, the word piezo is a corruption of the Greek word for squeeze.

In a piezo –electric accelerometer a mass is attached to a pizo –electric crystal, which is in turn mounted to the case of the accelerometer.

When the body of the accelerometer is subjected to vibration the mass mounted on the crystal wants to stay in space due to inertia and so compresses and stretches the pizo electric crystal. This force causes a charge to be generated and due to Newton low F=ma (F: force, m: mass, a: acceleration) this force is in turn proportional to acceleration.

The charge output is either converted to a low impedance voltage output by the use of integral electronic or made available as a charge output.



Figure 2.2 Accelerometer sensors [6]

#### 2.3.1.1.1 ADXL202 AOC

The ADXL202 is low cost, low power, complete 2\_axis accelerometer with a measurement range of either +-2g/+-10g. It can measure both dynamic acceleration (e.g vibration) and static acceleration (e.g gravity).

The outputs are digital signals whose duty cycles (ratio of pulse-width to period) are proportional to the acceleration in each of the 2 sensitive axes. These outputs may be measured directly with a microprocessor counter, requiring no A/D converter. The output period is adjustable from 0.5 ms to 10 ms via a single resistor (Rset). If a voltage output is desired, a voltage output proportional to acceleration is available from the Xfilt and Yfilt pins, or may be reconstructed by filtering the duty cycle outputs.

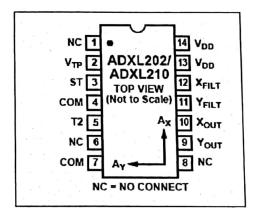


Figure 2.3: ADXL202AQC Pin configuration [7]

#### Features:

- 2\_axis acceleration sensor on a single IC chip measures static acceleration as well as dynamic acceleration.
- Duty cycle output with used adjustable period .

- Low power <0.6mA.</li>
- Faster response than electrolytic, mercury or thermal tilt sensors.
- Bandwidth adjustment with a single capacitor per axis.
- 5mg resolution at 60 Hz bandwidth.
- +3v to +5.25v single supply operation.

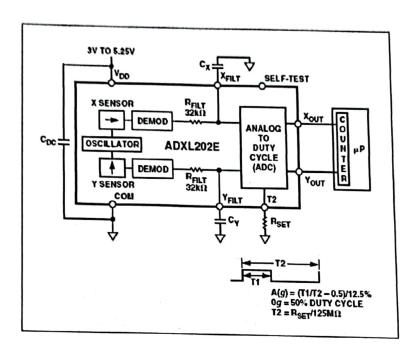


Figure 2.4:ADXL202AQC Functional block diagram [8]

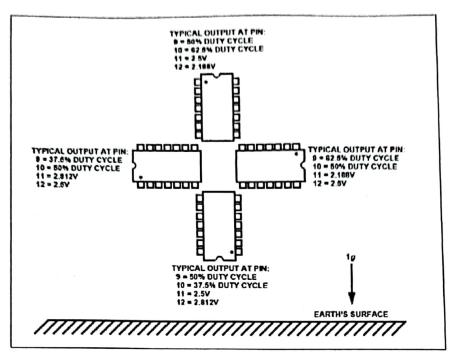


Figure 2.5: Earth Orientations [9]

### **Application**

- 2\_axis tilt sensing.
- Computer peripherals.
- Inertial navigation.
- Seismic monitoring.
- Vehicle security systems.
- Battery powered motion sensing.

In this project the designer uses the analog output, because the system needs five of these sensors and if the designer uses the digital output (which appears as duty cycle pulse), he needs counter to count the number of pulses and the PIC18f4550 has only one pin for counter and also the Data Acquisition(DAQ) which uses to enter data to the

computer has only two. So the designer chooses the analog output because the DAQ has 16 channels for analog input, and PIC18f4550 has 12 channels.

### 2.3.1.2 LM358 Operational Amplifier

LM358 consists of two independent, high gain, internally frequency compensated operational amplifiers which were designed specifically to operate from a single power supply over a wide range of voltages. Operation from split power supplies is also possible and the low power supply current drain is independent of the magnitude of the power supply voltage.

#### **Features**

Internally frequency compensated for unity gain

- Large dc voltage gain: 100 dB
- Wide bandwidth (unity gain): 1 MHz
- (temperature compensated)
- Wide power supply range:
  - Single supply: 3V to 32V
  - or dual supplies:  $\pm 1.5$ V to  $\pm 16$ V
- Very low supply current drain (500  $\mu$ A)—essentially independent of supply voltage
- Low input offset voltage: 2 mV
- Input common-mode voltage range includes ground
- Differential input voltage range equal to the power supply voltage
- Large output voltage swing: 0V to V+- 1.5V

#### Advantages

- Two internally compensated op amps
- Eliminates need for dual supplies
- Allows direct sensing near GND and VOUT also goes to GND
- Compatible with all forms of logic
- Power drain suitable for battery operation
- Pin-out same as LM1558/LM1458 dual op amp.

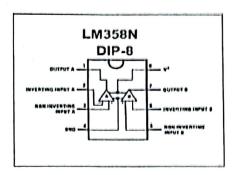


Figure 2.6: LM358 Pin Diagram[10]

#### 2.3.1.3 2X16 LCD

This project needs this 2X16 LCD to show the output letters of this system. This LCD can show 32 chars which are enough for this product which needs to appear 26 letters. Also 2X16 LCD is suitable to use with the glove because of its size which is small.

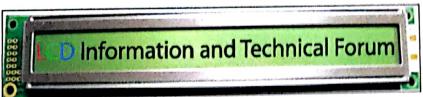


Figure 2.7:2X16 LCD [11]

## 2,3,1,4 Data Acquisition (DAQ)

This device is used for acquiring, analyzing, output data. DAQ characteristics:

- 16 channels for analog input.
- 8 bit digital input
- Max voltage entered =+,- 10 volts

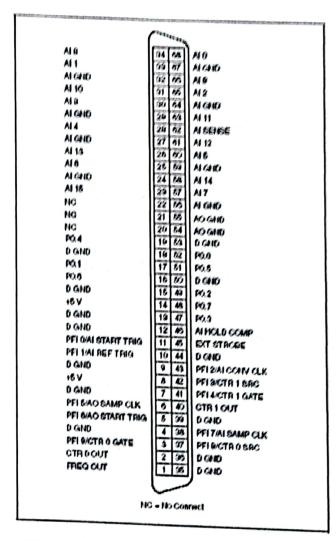


Figure 2.8: Pin diagram of 6034E [12]

### 2.3.2 Software Components

This section contains the software components that used in this system.

### 2.3.2.1 PIC Microcontroller (PIC18f4550)

Microcontroller is a device which integrates a number of the components of a microprocessor system onto a single microchip and optimized to interact with the outside world through on-board interfaces.

It is a little gadget that house a microprocessor, ROM, RAM, I/O, and various other specialized circuits all in one package.

The PIC that used in this project is PIC18f4550, the designer chooses this type because it has the feature that is suitable for this product such that:

- It contains 256 byte data EEPROM, 2kbyte SRAM byte,32k flash byte; this system needs to store 26 letter so it enough(26letter \* 5sensor \* 8 bit).
- It has 32 I/O lines to the PIC I/O ports so it suitable.
- 8 bit Microcontroller.
- Non volatile program and data memory.
- High performance, low power.
- High speed Flash/EEPROM technology.
- 12 channel 10 bit A/D.

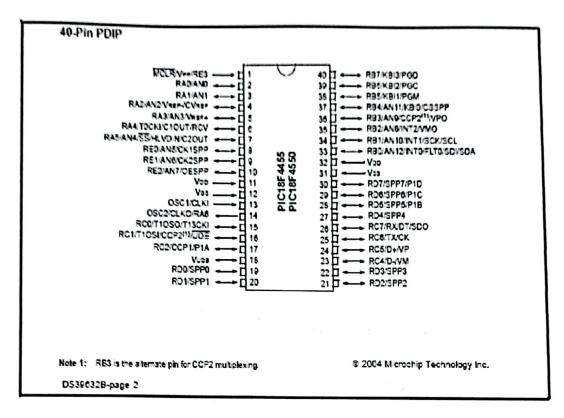


Figure 2.9: PIC18F4550 Pin Diagram[13]

#### 2.4 Project integrity

This system does not cause any problem either for the human or for the environment, on the opposite it has humanistic helpful.

## **CHAPTER**

3

## PROJECT CONCEPTUAL DESIGN

Introduction

Detailed project objectives.

Design options.

Project design block diagram.

Project interaction with the surrounding environment.

Design realization approach.

#### Chapter three Project conceptual design

#### 3.1 Introduction

This chapter shows the design concepts and the block diagram of the system.

#### 3.2 Objectives

Read the movement of the fingers.

This is done by fixing a movement sensor on the glove; one for each finger. This sensor can sense the movement of each finger.

Matching each movement with its associated letter.

The value of the movement and its associated letter will be stored in the EPROM of the MCU and when the user represents a letter in ASL, this value and its letter will be matched from those that previously stored in the EEPROM.

#### 3.3 Design options

Depending on the requirements of the system there are various options for the design as the following.

- The designer can use potentiometer instead of the flex sensor but it is costly because the designer must use one for each knuckle.
- The designer can use camera to take photo for each sign and this photo will interpret into its associated letter but this will make the design not portable..

- The designer can use P5 glove(Power of five), but this will make the design not portable because it has a receiver and it does not work without it.
- The designer can use Arabic Sign Language, but there is a problem (there is no Arabic LCD).
- The designer can use British Standard Sign Language but this language uses 10 fingers and this will be costly because it needs 10 sensor while American Sign Language uses 5 fingers (so it needs 5 sensor).

## 3.4 Project design block diagram

This system works on two phases; computer phase and MCU phase.

#### 3.4.1 Computer phase:

This phase composed of three units:

- Glove unit: This unit reads the value of hand movement and this value enters to the DAQ unit.
- DAQ unit: This unit used to read the signals that come from the sensors through analog channels and enter these signals into computer.
- PC unit: This unit used to process the signals that come from the DAQ unit, and the result will appear on the computer screen.



Figure 3.1: Block diagram of the system in computer phase

#### 3.4.2 MCU phase:

This system composed of three units:

- Glove unit: This unit reads the value of hand movement and this value enters to the MCU.
- MCU unit: This unit reads this value and makes match between this value and its associated letter.
- LCD unit: This unit displays the letter that matched.



Figure 3.2: Block diagram of the system in MCU phase

### 3.5 Project interaction with the surrounding environment

The input of this system comes from a movement sensor (Accelerometer) fixed on the glove that will sense the movement of the fingers, and the output will appear on LCD.

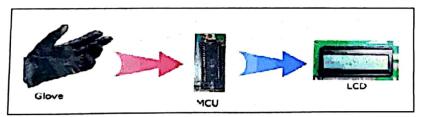


Figure 3.3: Interaction with the surrounding environment [14]

## 3.6 Design realization approach

This section contains the details of the system. The glove unit contains accelerometer sensor and accelerometer sensor circuit.

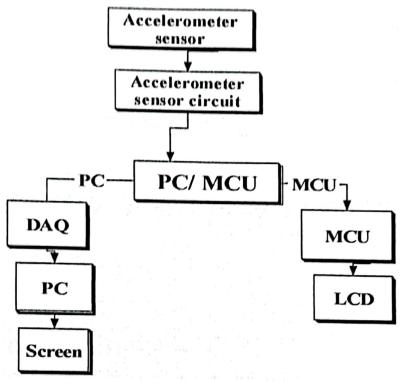


Figure 3.4: Detailed system flowchart

When the designer represents the signal of the letter in ASL, a movement will happen and an acceleration results from this movement, and this acceleration will change to voltage.

The output which comes from the sensor circuit is analog, so analog to digital converter will be used and the value that comes from it compared with the database that stored in the EEPROM to make match. LCD used to interface with the user.

## **CHAPTER**

4

### **DETAILED TECHNICAL PROJECT DESIGN**

#### Introduction

Detailed descriptions of the project phases.

Subsystem detailed design (characteristics, specifications).

Overall system design (schematic diagram).

User system interface (hardware, software).

# Chapter four Detailed technical project design

#### 4.1 Introduction

This chapter outlines formal procedure for design and the overall system design.

## 4.2 Detailed description of the project phases

This system works in two modes, train mode and operational mode.

Train mode: In this mode the user trains the MCU ASL using hand gestures.

To prevent data corruption A/D converter outputs and the associated user specified alphabet are saved in EEPROM.

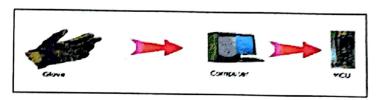


Figure 4.1: Train mode [15]

 Operational mode: In this mode the user chooses a letter and represents it and so the MCU compares between the value of this representation and the database stored in the EEPROM to make match.



Figure 4.2: Operational mode [16]

### 4.3 Subsystem detailed design

This section contains detailed description of the subsystems.

#### 4.3.1 ADXL202 connections

The circuit consists of five modules one for each finger, each module contained an accelerometer sensor. The output of each module is a voltage

The following figure shows the accelerometer sensor circuit, this module is repeated to each finger.

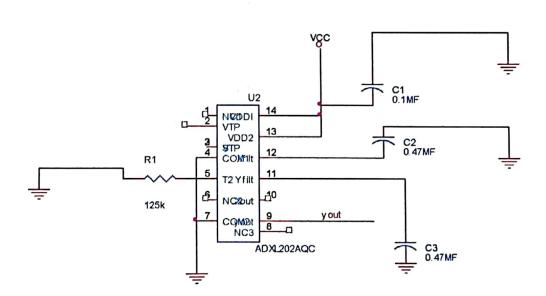


Figure 4.3: ADXL202AQC sensor circuit

 0.1MF capacitor will decouple the accelerometer from signal and noise on the power supply, this capacitor will be placed between VDD and COM.

- Pin4 and pin7: These two pins are commons and they should be connected directly together and pin7 grounded.
- Pin 12 analog output for x axis.
- Pin 11 analog output for y axis.
- 125k (Reset): It will set the duty cycle repetition rate to approximately 1 kHZ, or 1ms.

Note: Reset should always be included, even if only an analog output is desired.

#### 4.3.2 MCU Connection

The output of the accelerometer sensor is analog signal; these signals are entered into the MCU which contains Analog to Digital converter (A/D) to convert the analog signals into digital signals.

Also it contains EEPROM that used to store the value of voltage for each letter in train mode so that the value of the voltage in operational mode will compare with the values that are stored in train mode in this memory.

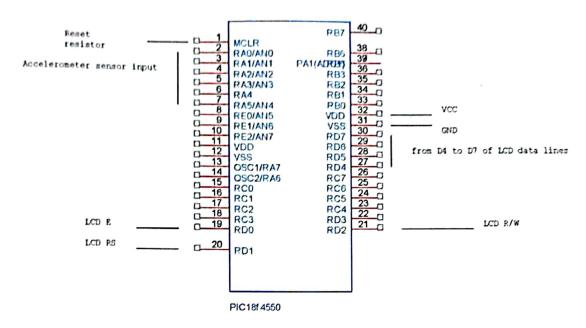


Figure 4.4: MCU connection

#### 1.3.3 Operational amplifier connection

The output of the accelerometer sensor is analog signal; these signals are entered nto PIC18f4550 which needs at least current in milliampere(mA), and accelerometer has urrent in microampere(MA) at most so the PIC cant read this analog input so the designer leeds an operational amplifier circuit to make the current larger.

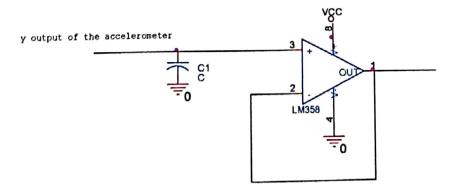


Figure 4.5: Operational amplifier connection

## 4.4 Overall system design

The system design is shown in the following figure:

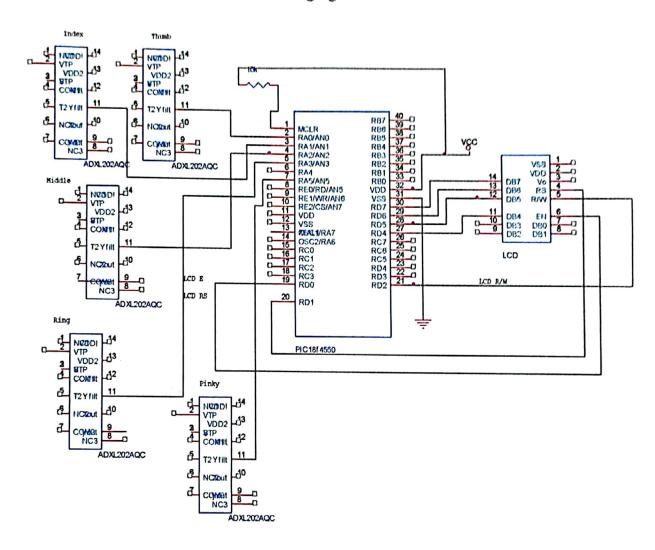


Figure 4.6: Overall system design

## 4.5 User System interface

This section contains the hardware and the software used for the interface.

#### 4.5.1 Hardware

The following components will be used:

- The movement sensors called Accelerometer sensor.
- The LCD is 2X16 LCD.
- The glove is an ordinary glove used just to fix the sensors on it, but the designer must choose one that is durable.

#### 4.5.2 Software

The user uses MPLAB C18 program to program the PIC in the different hand positions of the alphabet in MCU phase, and LABVIEW program in PC phase.

## **CHAPTER**

5

## PROJECT SOFTWARE

Introduction

Software needed for the Project.

Algorithms and Flowcharts.

#### Chapter five

#### **Project software**

#### 5.1 Introduction

This chapter contains the software needed for the design and the flow charts of the system.

### 5.2 Software needed for the project

The language that will use in this project is C language because it is very familiar language and easy to use and program, also this language can be used to program PIC18f4550, this will be used in MCU phase while the computer phase will use the LABVIEW.

#### 5.3 Algorithms and Flowcharts

#### 1. Train mode

```
for(i=0 to 26) // number of letters
```

for(j=0 to 20) // number of samples for each letter

// Choose a letter and represent it .

for(k=0 to 5) // number of fingers

// Read the output of accelerometer sensor and store it in array [20][5] for each letter .

for (j=0 to 20)

for (k=0 to 5)

```
array1[j][k]=array[k];

// calculate the mean of the 20 samples
for(j=0 to 20)
for(k=0 to 5)
mean[k]=array1[j][k]/20;

// store the mean for each letter in array[26][5] called sign
for(i=0 to 26)
for(k=0 to 5)
sign[i][k]=mean[k];
```

#### 2. Operational mode

for(i=0 to 26)

Choose a letter and represent it in ASL.

for (i=0 to 5).

Read the output of the accelerometer sensor.

Compare between the values that is read and those that are stored in sign[26][5] depends on nearest neighbor algorithm.

if match

Display the matched letter.

### 5.3.1 Computer phase:

This section contains the system flowcharts and LABVIEW blocks description.

### 5.3.1.1 System flowcharts

This section talks about the flowcharts of the system phases train and operation, the following are the symbols used in the flowcharts.

CountL: represents the counter that counts the letters.

CountS: represents the counter that counts the samples.

Va : represents the voltage of accelerometer sensor.

Vavg : represents the average voltage.

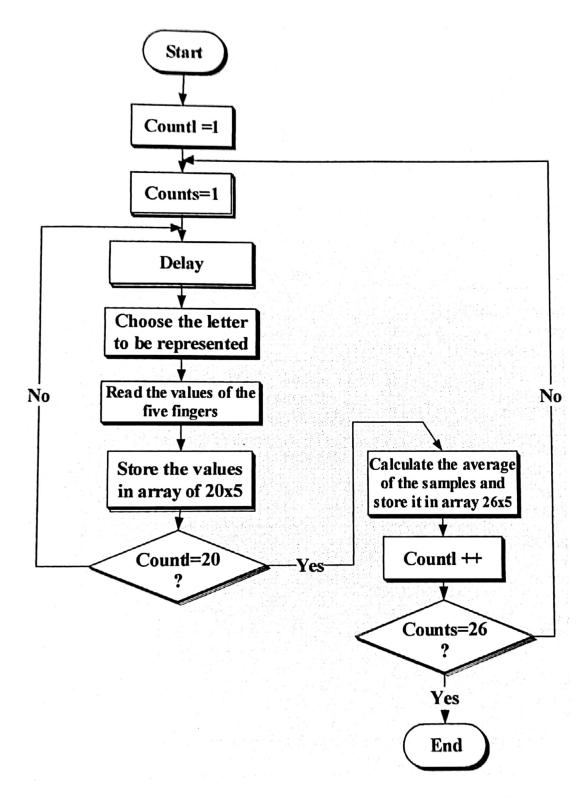


Figure 5.1: Train mode flow chart in computer phase

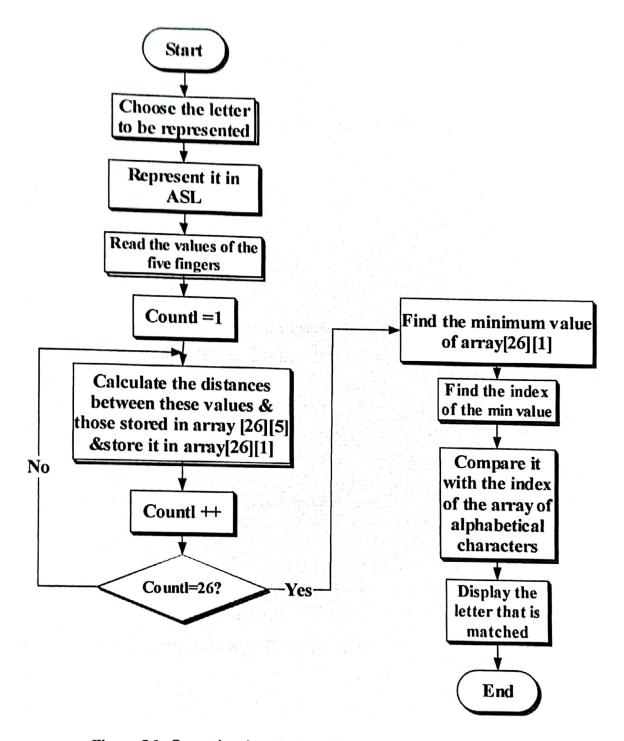


Figure 5.2: Operational mode flow chart in computer phase

#### 5.3.2 MCU phase

- Train mode: The values of train mode are taken and stored statically through array [26][5].
- Operational mode:

```
for(i=0 to 26)

// Choose a letter and represent it.

for(j=0 to 5)

// Read the output of the accelerometer sensor for thumb, index, middle, Ring, Pinky;

Calculate_N(thumb, index, middle, Ring, Pinky);

Nearest_N(distance);

match(index);

LCD_display(letter);
```

The following section explains the methods that are called above.

#### 5.3.2.1 Calculate\_N(arg1,arg2,arg3,arg4,arg5) method

```
arg1=thumb, arg2=index, arg3=middle, arg4=Ring, arg5=Pinky.

for(i=0 to 26)

for(j=0 to 5)

D=sqrt(pow(thumb-sign[i][0],2)+ pow(thumb-sign[i][1],2)+ pow(thumb-sign[i][2],2)+

pow(thumb-sign[i][3],2) + pow(Pinky-sign[i][4]),2));

Distance[i]=D;
```

To know more go to the code in the appendices

### 5.3.2.2 Nearest \_N(arg) method

```
arg=distance[26];
min=distance[0];
for(i=0 to 26)
if(distance[i]<min)
min=distance[i];
count=i; // the index of the minimum value
```

To have more details go to the code in the appendices.

#### 5.3.2.3 Match (arg) method

```
arg=count // index of the minimum values.
Letter=Character[count];
```

To have more information go to the code in the appendices.

#### 5.3.2.4 LCD\_display(arg) method

```
arg=letter
lcd_init();
lcd_gotoyx(1,1);
lcd_putc(letter);
```

To have more information go to the code in the appendices.

## **CHAPTER**

6

## SYSTEM IMPLEMENTATION AND TESTING

Introduction.

Implementation.

Testing.

# Chapter six System implementation and testing

#### 6.1 Introduction

This chapter introduces the system implementation and component testing, subsystem testing and integrated testing related to SLC system.

#### 6.2 Implementation

In this section the circuits was built and the code was built.

#### 6.2.1 Sensor circuit

The ADXL202AQC sensor circuit which mentions in chapter 4 was built . This circuit is repeated for the five fingers.



Figure 6.1: Sensor circuit for each finger.

### 6.2.2 Sensor circuit for the five fingers

The circuit shown in figure 6.1 was repeated for the five fingers, the five modules for the five fingers are connected together through VCC and GND.

The following figure represents the sensor circuit for all the glove.

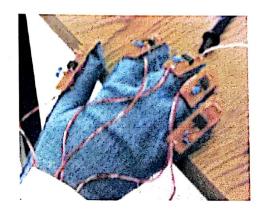


Figure 6.2: The created glove

#### 6.2.3 PC phase train mode

The glove are connected to the PC through DAQ and the letters are represented in ASL and the result are stored in array[20][5]{ 20:number of samples for each letter, 5:number of fingers}.



Figure 6.3: Glove connected to PC through DAQ.

#### 6.2.4 PIC phase

This section mentions the circuits that used for LCD section, ADC section.

#### 6.2.4.1 LCD implementation

There are two modes in LCD connection, the first mode uses 4 data lines for data and the data are transfer in two phases and the designer uses this mode in this system in order to use less data lines, and the second mode uses 8 data lines for data, and so the data are transfer in one phase.

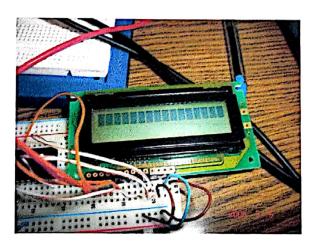


Figure 6.4: LCD connected in PIC mode.

#### 6.3 Testing

This section contains the result of the circuits that are implemented in the previous section.

### 6.3.1 Sensor circuit result

The circuit which shown in figure 6.1 is tested on the oscilloscope, it tested for its digital output x and y (pin9 and pin10) and the result was as follow:



Figure 6.5: Result of x and y on pin9 and pin10.

### 6.3.2 Sensor circuit result for all hand

The letters are implemented in ASL and the results for the five fingers are taken from five digital multimeter at the first time.



Figure 6.6: Voltages of letters represented in ASL using five digital multimeter.

The result which the designer took it from the five digital multimeter for the 26 letter are shown in the following table.

Table (6.1): Voltage values for the letters measured using 5 digital multimeter.

| Letter | Thumb | Index | Middle | Ring | Pinky |
|--------|-------|-------|--------|------|-------|
| A      | 2.14  | 2.95  | 2.52   | 2.93 | 1.96  |
| В      | 2.27  | 2.50  | 2.08   | 2.41 | 2.2   |
| С      | 2.28  | 2.77  | 2.34   | 2.67 | 1.95  |
| D      | 2.39  | 2.53  | 2.37   | 2.42 | 2.11  |
| E      | 2.55  | 2.74  | 2.41   | 2.82 | 1.97  |
| F      | 2.21  | 2.70  | 2.10   | 2.53 | 2.02  |
| G      | 2.43  | 2.66  | 2.41   | 2.59 | 2.22  |
| Н      | 2.46  | 2.59  | 2.15   | 2.92 | 2.19  |
| I      | 2.40  | 2.96  | 2.57   | 2.81 | 2.35  |
| J      | 2.50  | 2.89  | 2.43   | 2.41 | 2.15  |
| K      | 2.26  | 2.51  | 2.07   | 2.42 | 2.9   |
| L      | 2.16  | 2.48  | 2.54   | 2.87 | 2.86  |
| M      | 2.47  | 2.87  | 2.61   | 2.92 | 2.22  |
| N      | 2.48  | 3.23  | 2.50   | 2.76 | 2.67  |
| 0      | 2.41  | 3.91  | 2.45   | 2.67 | 2.32  |
| P      | 2.70  | 2.91  | 2.58   | 2.46 | 2.42  |
| Q      | 2.71  | 3     | 2.23   | 2.91 | 1.9   |
| R      | 2.46  | 2.55  | 2.04   | 2.82 | 1.7   |
| S      | 2.32  | 2.96  | 2.58   | 2.41 | 1.86  |
| T      | 2.27  | 2.73  | 2.53   | 2.43 | 1.98  |
| U      | 2.32  | 2.48  | 2.06   | 2.42 | 1.96  |
| V      | 2.30  | 2.48  | 2.06   | 2.63 | 2.2   |
| W      | 2.34  | 2.49  | 2.11   | 2.92 | 2.582 |
| X      | 2.57  | 2.70  | 2.48   | 2.44 | 2.43  |
| Y      | 2.14  | 2.93  | 2.55   | 2.45 | 2.53  |
| Z      | 2.55  | 2.62  | 2.47   | 2.66 | 2.6   |

#### 6.3.3 PC train mode

Figure 6.3 was implemented for each letter and this section contains the values of train mode for each letter.

The code of train mode was implemented and the letters was implemented in ASL.

The values for each finger stored in array[20][5].

The following figure represents the values of 20 samples for representation of A letter in ASL.

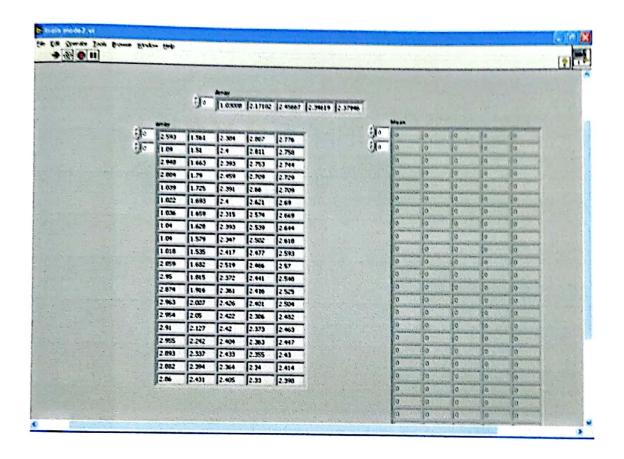


Figure 6.7: A letter train mode at PC phase.

he following figure shows the representation of letter A in ASL.

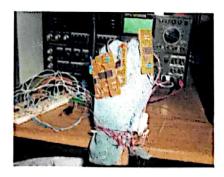


Figure 6.8: Representation of A letter in ASL.



The following figure represents the values of 20 samples for representation of B letter in ASL.

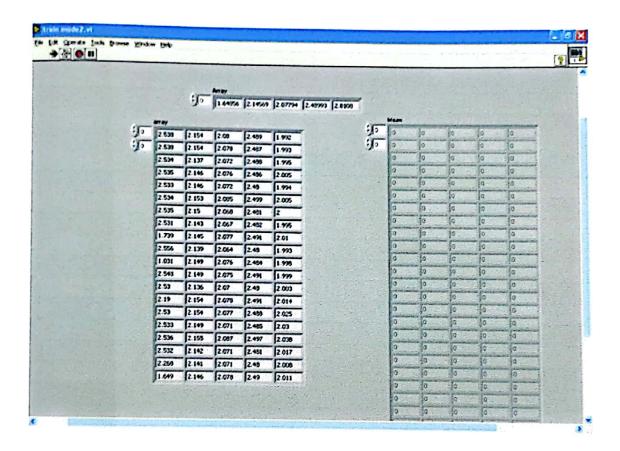


Figure 6.9: B letter train mode at PC phase.

The following figure shows the representation of B letter in ASL.



Figure 6.10: Representation of B letter in ASL.

The following figure represents the values of 20 samples for representation of C letter in ASL.

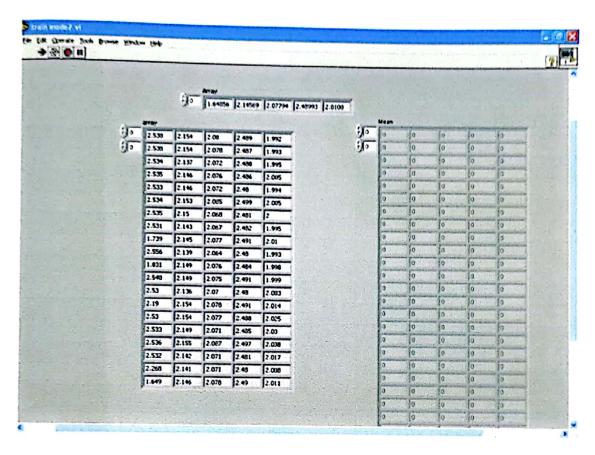


Figure 6.11: C letter train mode at PC phase.

he following figure shows the representation of C letter in ASL.

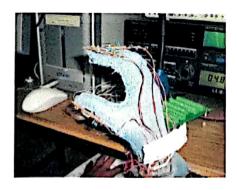


Figure 6.12: Representation of C letter in ASL.

The following figure represents the values of 20 samples for representation of D letter in ASL.

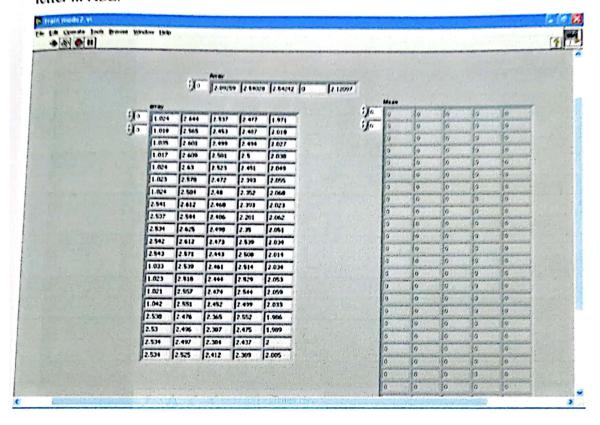


Figure 6.13: D letter train mode at PC phase.

The following figure shows the representation of D letter in ASL.



Figure 6.14: Representation of D letter in ASL.

The following figure represents the values of 20 samples for representation of E letter in ASL.

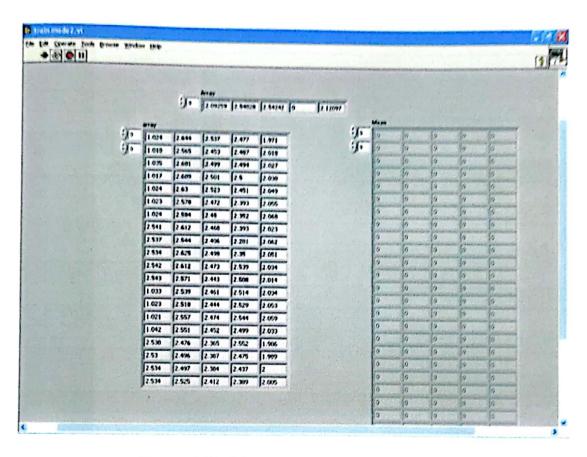


Figure 6.15: E letter train mode at PC phase.

The following figure shows the representation of E letter in ASL.



Figure 6.16: Representation of E letter in ASL.

The following figure represents the values of 20 samples for representation of F letter in ASL.

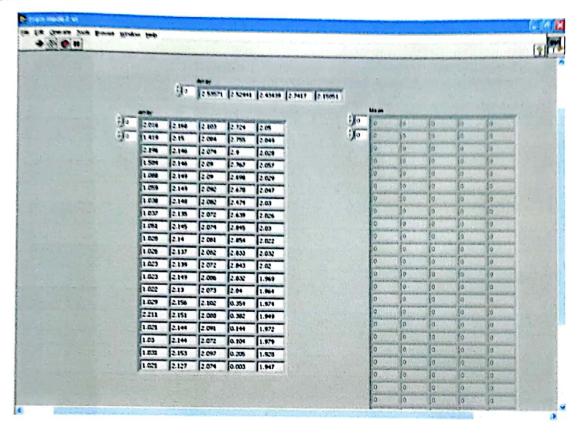


Figure 6.17: F letter train mode at PC phase.

The following figure shows the representation of F letter in ASL.

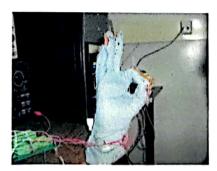


Figure 6.18: Representation of F letter in ASL.

The following figure represents the values of 20 samples for representation of G letter in ASL.

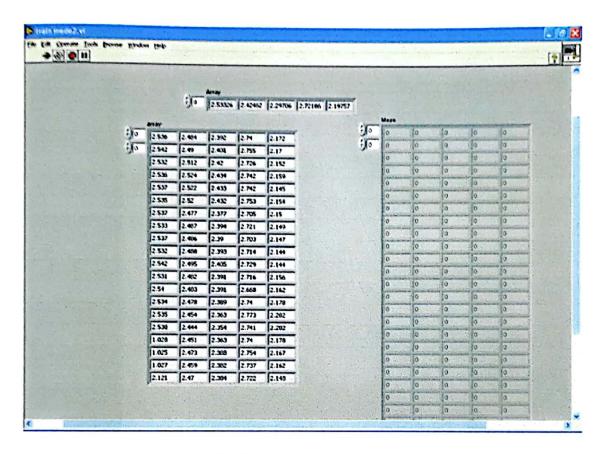


Figure 6.19: G letter train mode at PC phase.

The following figure shows the representation of G letter in ASL.



Figure 6.20: Representation of G letter in ASL.

The following figure represents the values of 20 samples for representation of H letter in ASL.

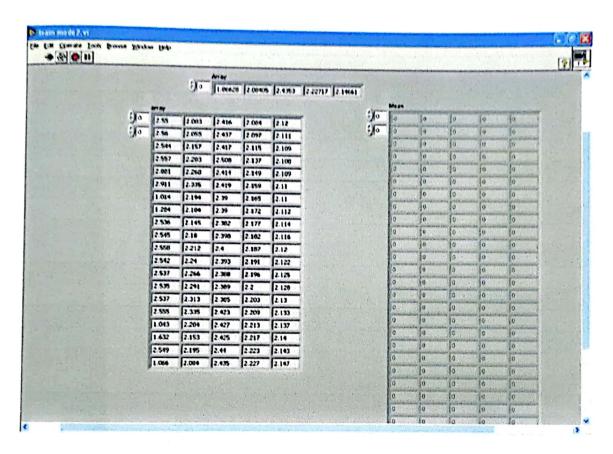


Figure 6.21: H letter train mode at PC phase.

he following figure shows the representation of H letter in ASL.



Figure 6.22: Representation of H letter in ASL.

The following figure represents the values of 20 samples for representation of I letter in ASL.

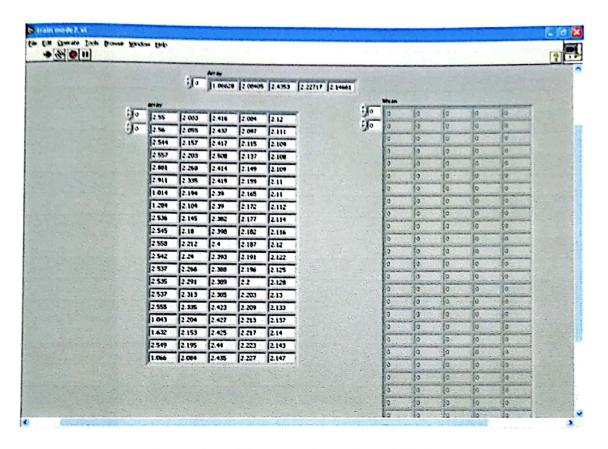


Figure 6.23: I letter train mode at PC phase.

he following figure shows the representation of I letter in ASL.



Figure 6.24: Representation of I letter in ASL.

The following figure represents the values of 20 samples for representation of J letter in ASL.

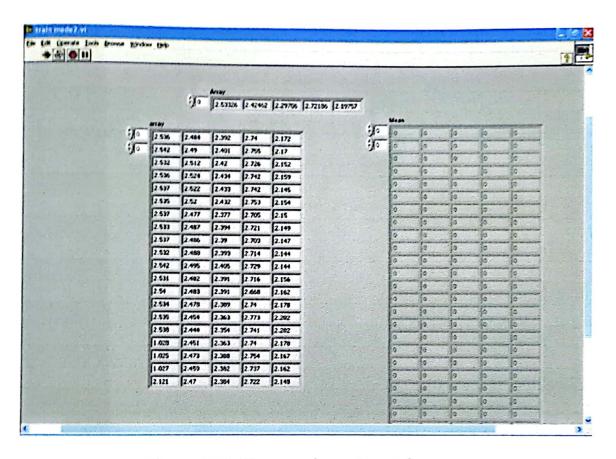


Figure 6.25: J letter train mode at PC phase.

he following figure shows the representation of J letter in ASL.

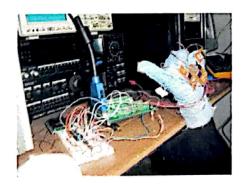


Figure 6.26: Representation of J letter in ASL.

The following figure represents the values of 20 samples for representation of K letter in ASL.

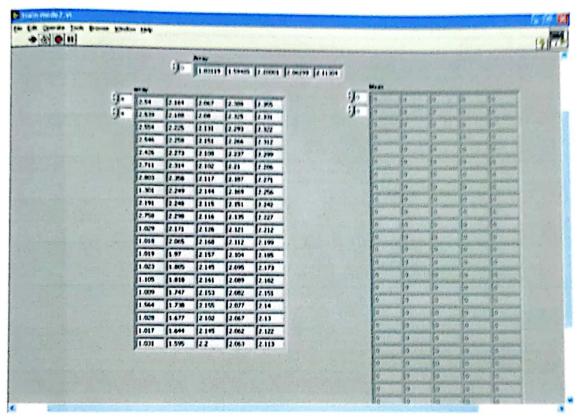


Figure 6. 27: K letter train mode at PC phase.

The following figure shows the representation of K letter in ASL.

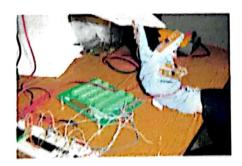


Figure 6.28: Representation of K letter in ASL.

The following figure represents the values of 20 samples for representation of L letter in ASL.

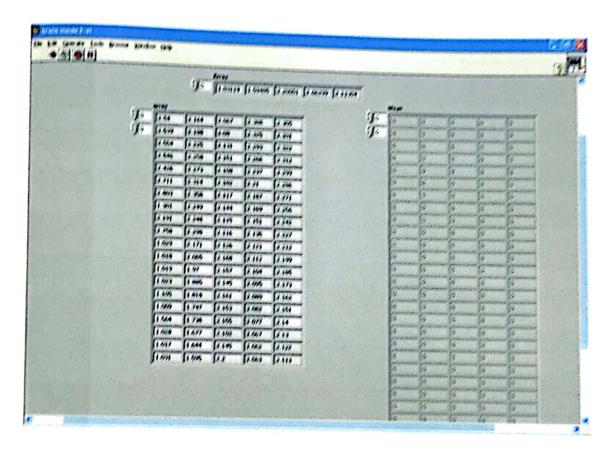


Figure 6.29: L letter train mode at PC phase.

The following figure shows the representation of L letter in ASL.



Figure 6.30: Representation of L letter in ASL.

The following figure represents the values of 20 samples for representation of M letter in ASL.

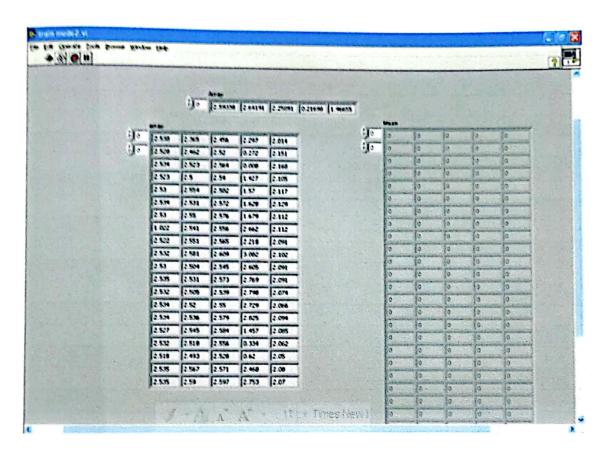


Figure 6.31: M letter train mode at PC phase.

he following figure shows the representation of M letter in ASL.



Figure 6.32: Representation of M letter in ASL

The following figure represents the values of 20 samples for representation of O letter in ASL.

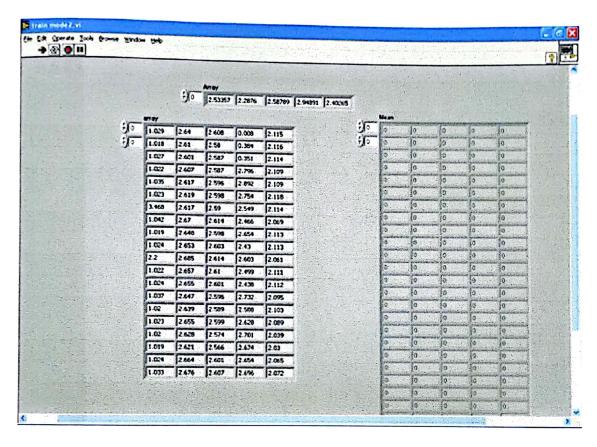


Figure 6.35: O letter train mode at PC phase.

The following figure shows the representation of O letter in ASL.



Figure 6.36: Representation of letter O in ASL

The following figure represents the values of 20 samples for representation of P letter in ASL.

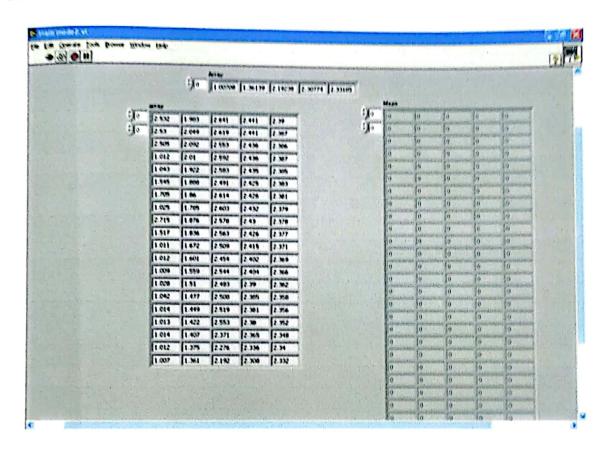


Figure 6.37: P letter train mode at PC phase.

The following figure shows the representation of P letter in ASL.



Figure 6.38: Representation of letter P in ASL

The following figure represents the values of 20 samples for representation of R letter in ASL.

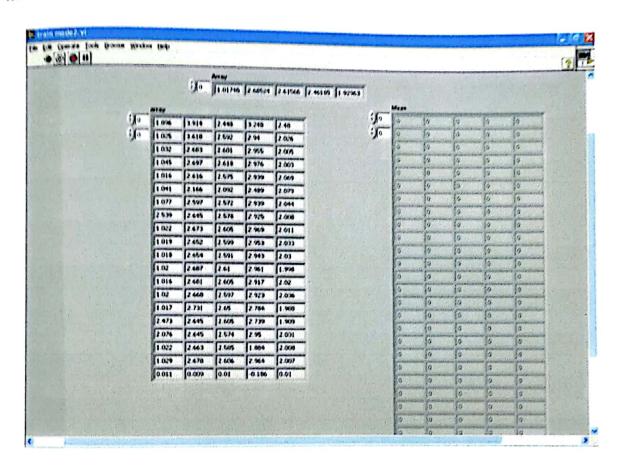


Figure 6.41: R letter train mode at PC phase.

The following figure shows the representation of R letter in ASL.



Figure 6.42: Representation of letter R in ASL

The following figure represents the values of 20 samples for representation of T letter in ASL.

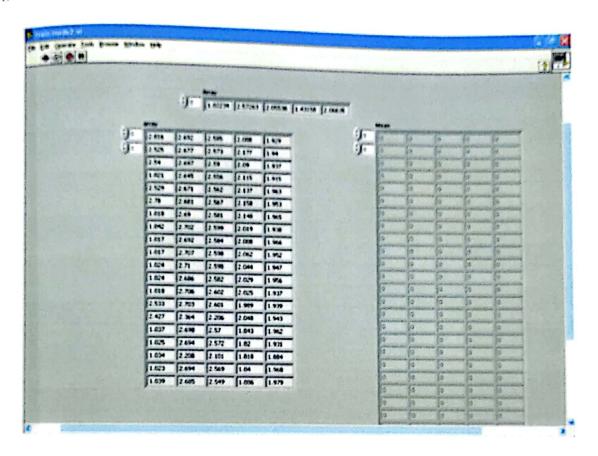


Figure 6.45: T letter train mode at PC phase.

The following figure shows the representation of T letter in ASL.



Figure 6.46: Representation of letter T in ASL

The following figure represents the values of 20 samples for representation of U  $_{\text{letter}}\,\text{in}$  ASL.

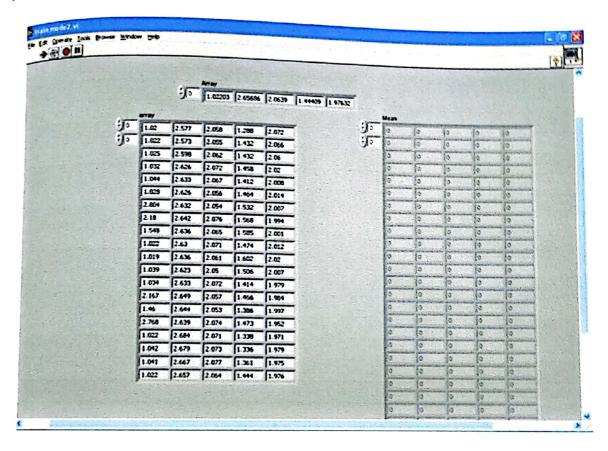


Figure 6.47: U letter train mode at PC phase.

following figure shows the representation of U letter in ASL.

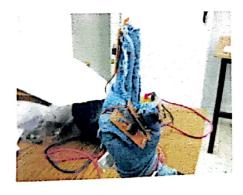


Figure 6.48: Representation of letter U in ASL

The following figure represents the values of 20 samples for representation of  $V_{1}ASL$ .

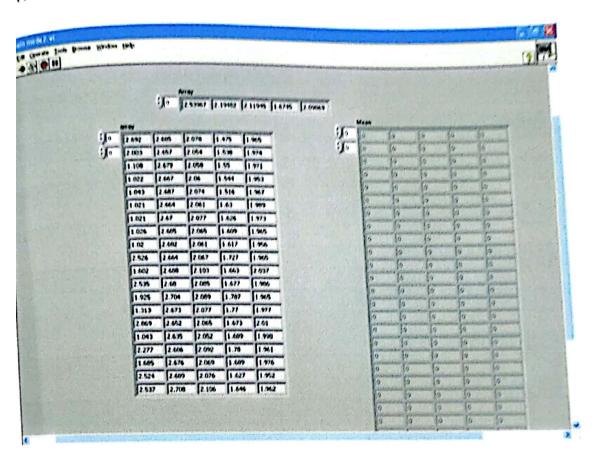


Figure 6.49: V letter train mode at PC phase.

he following figure shows the representation of V letter in ASL.

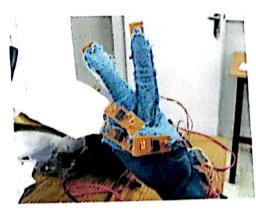


Figure 6.50: Representation of letter V in ASL

The following figure represents the values of 20 samples for representation of W  $_{\mbox{\scriptsize letter}}$  in ASL.

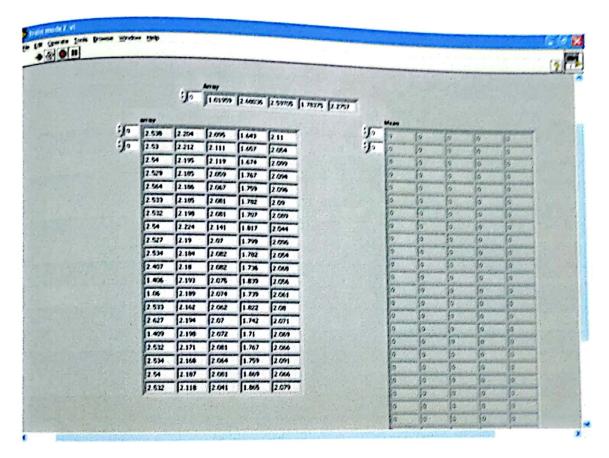


Figure 6.51: W letter train mode at PC phase.

The following figure shows the representation of W letter in ASL.



Figure 6.52: Representation of letter W in ASL

The following figure represents the values of 20 samples for representation of X letter in ASL.

| ### ### ##############################                                      |
|---|
| To  |
| \$\begin{array}{c c c c c c c c c c c c c c c c c c c                       |
| \$\begin{array}{c c c c c c c c c c c c c c c c c c c                       |
| 2.891   2.551   2.498   2.379   2.666   0   0   0   0   0   0   0   0   0   |
| 1.049   2.399   2.459   2.364   2.401   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| 1.037   2.276   2.439   2.352   2.392   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| 1.001   2.171   2.457   2.346   2.379   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| 1.099 2.003 2.352 2.351 2.37  |
| 1.046   2.01   2.516   2.752   2.361   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  |
| 1.017   1.922   2.503   2.75   2.553   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  |
| 1.045   1.505   2.483   2.349   2.346   0   0   0   0   0   0   0   0   0   |
| 1.019   |
| 1.249   1.826   2.496   2.343   2.336   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| 2.852   1.953   2.465   2.343   2.332   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| 1.001   1.861   2.347   2.328   2.324                                       |
| 1.016   1.779   2.417   2.323   2.317   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| 1.02  |
| 1.017 1.63 2.377 2.304 2.302  |
|   |
|   |
| 1.018 1.515 2.384 2.29 2.29   |
| 1.014 1.468 2.385 (2.283 (2.283 0 0 0 0                                     |
| 0 10 0 0  |
| 0 0 10  |
| 0 0 0   |

Figure 6.53: X letter train mode at PC phase.

The following figure shows the representation of X letter in ASL.

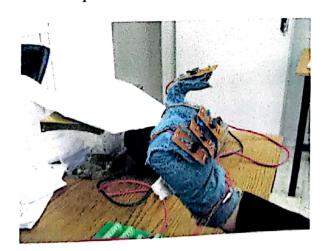


Figure 6.54: Representation of letter X in ASL

The following figure represents the values of 20 samples for representation of Y letter in ASL.

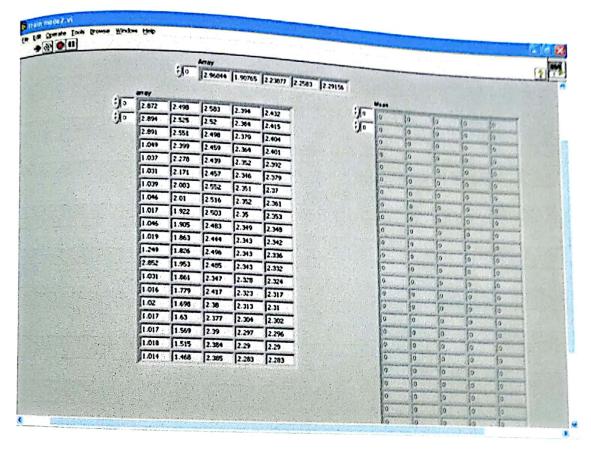


Figure 6.55: Y letter train mode at PC phase.

The following figure shows the representation of Y letter in ASL.



Figure 6.56: Representation of Y letter in ASL.

The following figure represents the values of 20 samples for representation of Z  $_{letter}$  in ASL.

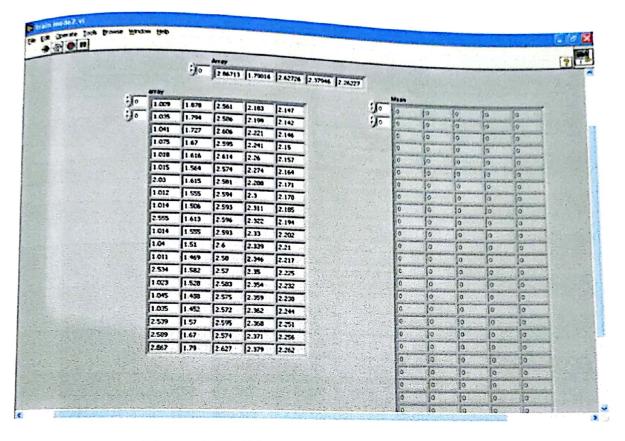


Figure 6.57: Z letter train mode at PC phase.

The following figure shows the representation of Z letter in ASL.



Figure 6.58: Representation of letter Z in ASL

....uy[20][5] which is shown below:

| )   | 2.4459   | 2.6866   | 2 Energy   | AND DESCRIPTION OF THE PERSON NAMED IN   | OJ[5] whi  |            |
|-----|--|--|--|--|--|------------|
| 0   | 2.4459   | 2.11345  | 2.0250   | 2.93905  | 1,68665  | Commence   |
|     | 2.45195  | 2.11345  | 12.0359  | 2.41275  | 1.9606   |            |
|     | Townson to the last of the las | A CONTRACTOR OF THE PARTY OF TH | 14.39135   | 2 47000  | William Marketon   |            |
|     | the second section and the section of the  |  | 1 2 9 2000   | -  | The state of the s |            |
|     | Control of the Contro |  | 12.4 ULA   |  | The second second second second  |            |
| T   | and the property of the second   | 1 4 7 7 7 7  | IZ.1276  | 0.00   | -  | -          |
| 11  | Market and the Control of the Contro | 141702   | 12.3937¢   | 2 50.0   | THE RESIDENCE OF   |            |
| 1   |  | 14,70335   | 12,23915   | 2 5000-  | _  |            |
| 11  | CONTRACTOR OF STREET   | 12.00015   | 2.59145  | 2.9275   | 1.0700   | 1          |
| 1   | 1211002  | 12.55015   | 2,47965  | 2 81405  | Tana .   | Ť.         |
|     | 12,71175   | 12.63505   | 2.112  | 2,4098   | 1.8946   |            |
|     | 12.7246  | 12.6878  | 2.5908   | 2.42215  | 1,9003   | 1          |
|     | 2.4884   | 2.55505  | 2.5541   | 2.8784   | 2 07025  |            |
|     | 2.51845  | 2.662  | 2.5366   | 2,92965  | 2.05005  | 1          |
|     | 12.42735   | 2.43015  | 2.33595  | 2.7098   | 1.9946   |            |
|     | 2.537  | 2.44885  | 2.65175  | 2.76695  | 2.45215  |            |
|     | 2.5852   | 2.3282   | 2.27575  | 2.6758   | 2.4787   |            |
|     | 2.4661   | 2.6482   | 2.06225  | 2.46085  | 2.01085  |            |
|     | 2.4517   | 2.6838   | 2.5855   | 2.917  | 1.95645  |            |
|     | 2.47825  | 2.6685   | 2.5746   | 2.82895  | 1.86825  |            |
|     | 2.4754   | 2.66815  | 2.05315  | 2.4152   | 2.02605  |            |
|     |  | 2.5478   |  |  |  |            |
|     | The second secon | 2.1272   | A CONTRACTOR OF THE PARTY OF TH |  |  | The Park   |
| 1   | 2.42995  | 2.64965  | 2.55155  | 2.6318   | 2.2821   |            |
| 14. | 2.4848   | 2.68175  | 2.58825  | 2.9234   | 1.86935  | - Carolina |
| 11  |  | 2.66585  | the second second second   | A STATE OF THE PARTY OF THE PAR |  | -          |

## 13.4 PC test mode

After the train mode was done the designer test the system, and the system was able precognize to all the letters.

This section contains the results of the test mode for all letters.

The following figure shows the A letter after it was tested successfully on the PC

Figure 6.60: A letter test mode at PC phase.

The following figure shows the B letter after it was tested successfully on the PC

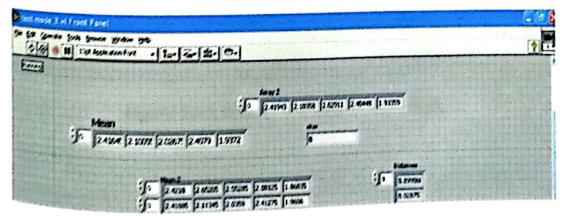


Figure 6.61: B letter test mode at PC phase.

The following figure shows the C letter after it was tested successfully on the PC

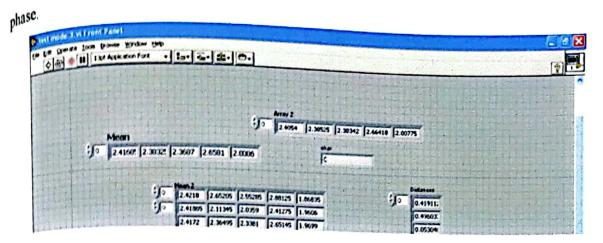


Figure 6.62: C letter test mode at PC phase.

The following figure shows the D letter after it was tested successfully on the PC phase.

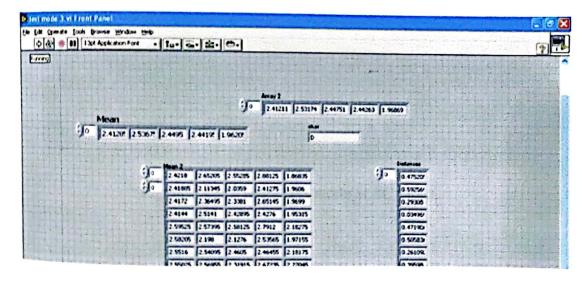


Figure 6.63: D letter test mode at PC phase.

The following figure shows the E letter after it was tested successfully on the PC

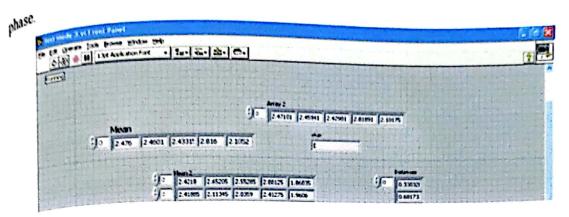


Figure 6.64: E letter test mode at PC phase.

The following figure shows the F letter after it was tested successfully on the PC

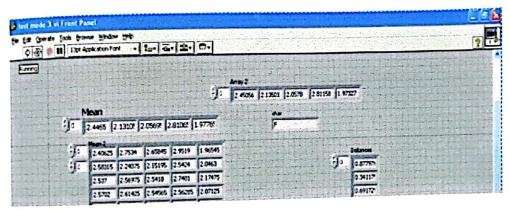


Figure 6.65: F letter test mode at PC phase.

The following figure shows the G letter after it was tested successfully on the PC

Figure 6.66: G letter test mode at PC phase.

The following figure shows the H letter after it was tested successfully on the PC

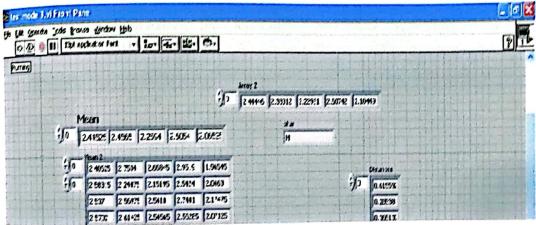


Figure 6.67: H letter test mode at PC phase.

The following figure shows the I letter after it was tested successfully on the PC

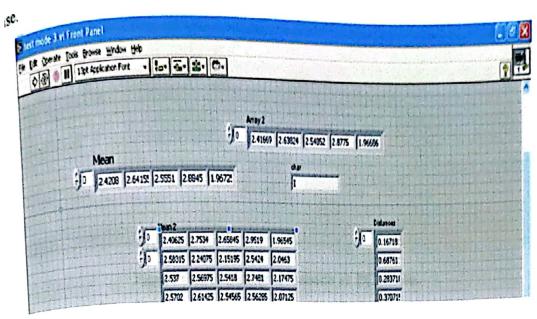


Figure 6.68: I letter test mode at PC phase.

The following figure shows the J letter after it was tested successfully on the PC

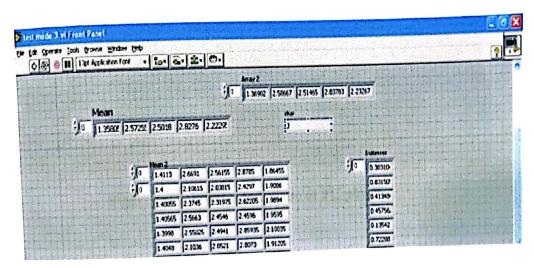


Figure 6.69: J letter test mode at PC phase.

The following figure shows the K letter after it was tested successfully on the PC

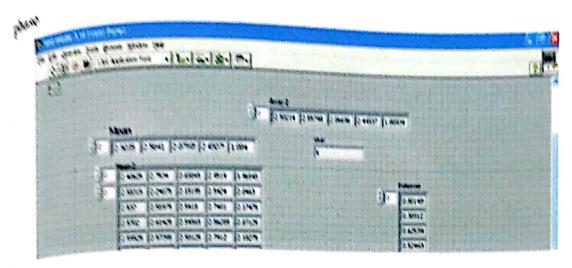


Figure 6.70: K letter test mode at PC phase.

The following figure shows the L letter after it was tested successfully on the PC

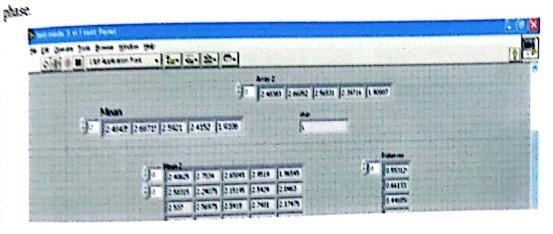


Figure 6.71: L letter test mode at PC phase.

The following figure shows the M letter after it was tested successfully on the PC

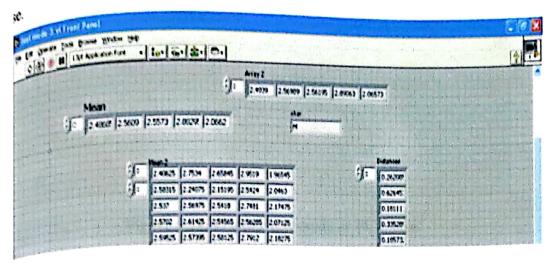


Figure 6.72: M letter test mode at PC phase.

The following figure shows the N letter after it was tested successfully on the PC

se.

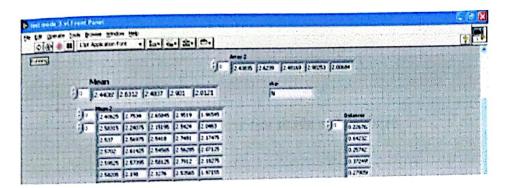


Figure 6.73: N letter test mode at PC phase.

The following figure shows the O letter after it was tested successfully on the PC

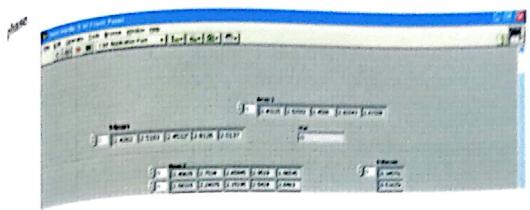


Figure 6.74: O letter test mode at PC phase.

The following figure shows the P letter after it was tested successfully on the PC

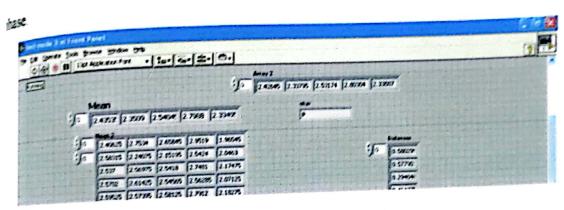


Figure 6.75: P letter test mode at PC phase.

The following figure shows the Q letter after it was tested successfully on the PC  $_{\rm hlase}$ .

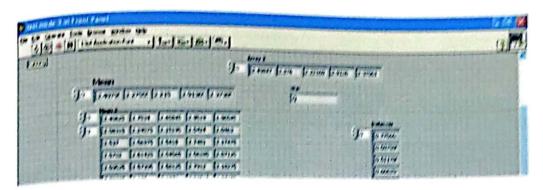


Figure 6.76: Q letter test mode at PC phase.

The following figure shows the R letter after it was tested successfully on the PC

hase

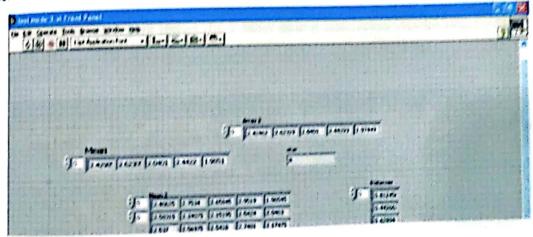


Figure 6.77: R letter test mode at PC phase.

The following figure shows the U letter after it was tested successfully on the PC

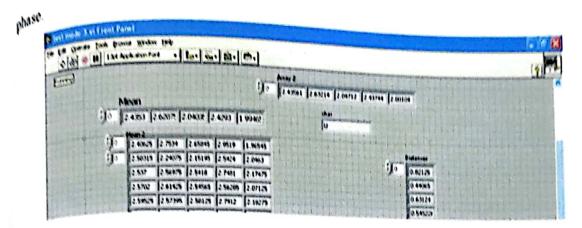


Figure 6.80: U letter test mode at PC phase.

The following figure shows the V letter after it was tested successfully on the PC phase.

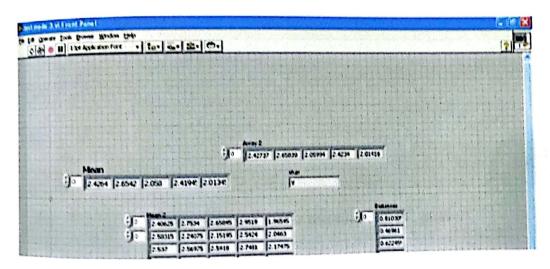


Figure 6.81: V letter test mode at PC phase.

The following figure shows the W letter after it was tested successfully on the PC

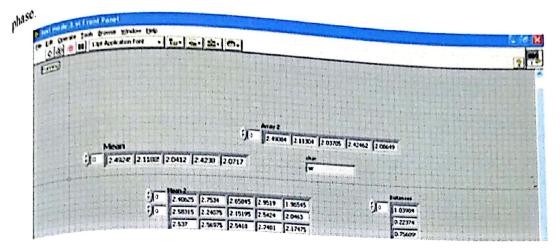


Figure 6.82: W letter test mode at PC phase.

The following figure shows the X letter after it was tested successfully on the PC

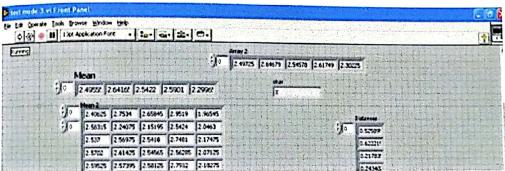


Figure 6.83: X letter test mode at PC phase.

The following figure shows the Y letter after it was tested successfully on the PC

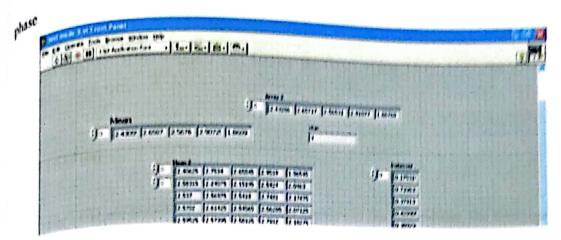


Figure 6.84: Y letter test mode at PC phase.

The following figure shows the Z letter after it was tested successfully on the PC phase.

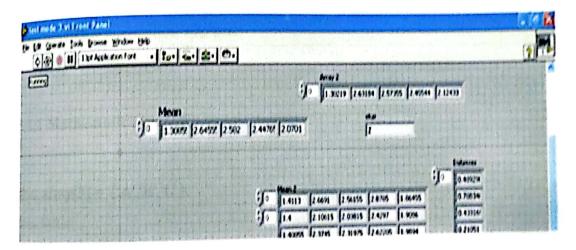


Figure 6.85: Z letter test mode at PC phase.

# 6.3.5 PlC phase

In this section the designer will display the result of test LCD, ADC, the whole  $\mathfrak{g}^{slem}$ 

### 6.3.5.1 LCD test

The LCD are tested for the code which appears in the appendices, the designer stored 3 letters in array of char, he supposed values for voltage for the five fingers and stored them in array[3][5], and he stored values as constant in thumb, index, middle, ring, pinky variables instead of reading these values from sensors.

The designer made calculations using nearest neighbor algorithm and he expected that the LCD will display A, and after he tested the LCD, it displayed A, so the code was true and the LCD connection was true.

#### 6.3.5.1.1 Mathematical proof

```
char array[3] = {'A','B','C'};
char letter;
float sign_values[3][5];
sign_values[3][5]={{1.1,1.2,1.3,1.4.1.44},{1.1,1.3,1.4,1.44,1.5},{1.2,1.35,1.5,1.45,
2.5}};
float thumb=1.12;
float index= 1.3;
float middle=1.1.
```

```
float ring=1.6;
float pinky=1.5;
float distance[3];
```

Note: the values which stores in 2 dimension array are stored in alphabetical order, this means that the first row is for A letter, the second for B and so on.

Steps of the nearest neighbor algorithm:

 Calculate the distance between the first point(thumb, index, middle, ring, pinky) and the rows of the 2 dimension array.

For(i=0;i<3;i++)
D=sqrt(pow(thumb-sign[i][0],2)+ pow(thumb-sign[i][1],2)+ pow(thumb-sign[i][2],2)+ pow(thumb-sign[i][3],2) + pow(Pinky-sign[i][4]),2));

Substitute in the above formula.

$$D1=(((1.12)-(1.1))^2 + (1.3-1.2)^2+(1.1-1.3)^2+(1.6-1.4)^2+(1.5-1.44)^2)^(1/2)=0.306594194.$$

• Find the minimum value.

D1 is the minimum, so A is the nearest neighbor and the LCD must display A.

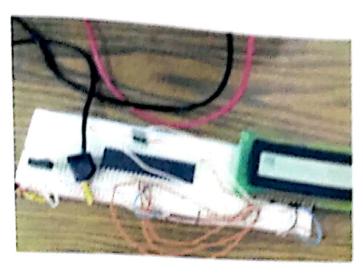


Figure 6.86: LCD displays letter A.

#### 6.3.5.2 ADC code test

The code of analog to digital converter was tested on the PIC, but in the first the designer took the input from VCC and GND and connected it to channel zero of port A of the PIC which is used for analog input.

The result was displayed on LCD, when connected to GND it displayed 0 and when connected to VCC it displayed 1023.

The following figure shows the analog input when connected to GND and it displayed 0.



Figure 6.87: ADC tested through connecting analog input to GND.

The following figure shows the analog input when connected to VCC and it displayed 1023.

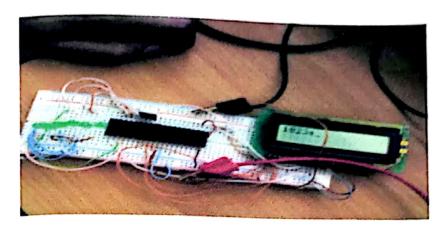


Figure 6.88: ADC tested through connecting analog input to VCC.

When the designer used the input from the sensor, the PIC was unable to read from the sensor because the signal was so small and it displayed only either 0 or 1023 (the values of VCC and GND), so the designer used Operational amplifier to make the signal larger and after that the PIC was able to read from sensor.

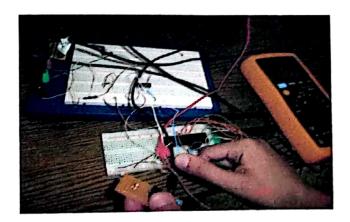


Figure 6.89: ADC tested through connecting sensor to the analog input.

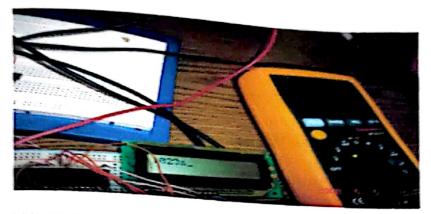


Figure 6.90: ADC tested through connecting sensor to analog input without using operational amplifier.

In the previous figure the PIC was unable to read from the accelerometer sensor without using operational amplifier, while in the following figure the PIC was able to read from accelerometer sensor after using operational amplifier.

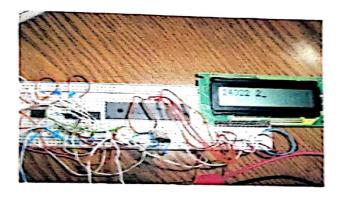


Figure 6.91: ADC tested through connecting analog input to sensor using operational amplifier.

#### الكرية Nearest neighbor algorithm code test

In this section the code for the nearest neighbor was tested on C language before it was applied on the MPLAB C18 which used to program the PIC.

The code was tested for the following methods:

- Calculate\_N().
- Nearest\_N().
- Match().
- LCD\_display().

The designer entered constant array with values which were supposed from the designer, and he entered values through using scanf() for thumb, index, middle, ring, pinky; and so the code was tested successfully.

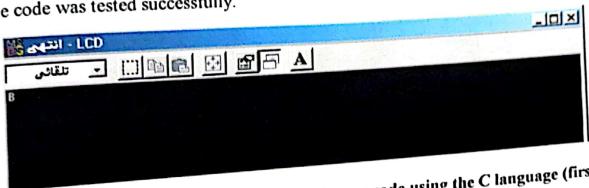


Figure 6.92: The output of testing the software code using the C language (first trial displayed B letter).

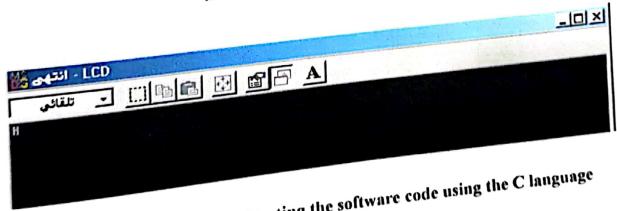


Figure 6.93: The output of testing the software code using the C language (second trial displayed H letter).

## 6.3.5.4 PIC train mode

The 26<sup>th</sup> letters were represented using ASL (10 trials for each letter and then the average was calculated), and the values of voltage were read from LCD after the train mode

Note: the value of voltage is multiplying by 5000.

Table (6.2): The displayed values of all letters in train mode at PIC phase.

| T    |  |   |  | mode at PIC <sub>I</sub>   |
|------|--|---|--|--|
| -    |  |   |  |  |
| 9625 | 7625   | M   | R  | Р  |
| 9274 |  | 19300   | 18750  | 89250  |
| 9350 |  |   | 18700  | 87250  |
| 9250 |  |   | 18750  | 87250  |
| 9274 |  |   | 18775  | 87255  |
|      |  |   | 18600  | 87000  |
|      |  |   | 18600  | 87000  |
|      |  |   |  | 88255  |
|      |  |   |  | 86495  |
|      |  |   |  | 86755  |
|      |  |   |  | 78651  |
| _    | ·  |   |  | Р  |
|      |  |   |  | 89250  |
|      |  |   | 18650  | 87500  |
|      |  |   | 18625  | 87505  |
|      |  | 19350   | 18650  | 87500  |
|      |  | 19175   | 18700  | 87500  |
| 9274 | 7625   | 19175   | 18600  | 87250  |
| 9250 | 7700   | 19300   | 18600  | 87250  |
| 9325 | 7924   | 19275   | 18600  | 87500  |
| 9274 | 7700   | 19250   | 18550  | 87250  |
| 9274 | 7700   | 19200   | 18700  | 87000  |
|      |  | 40070   | 40057.5  | 97550 6  |
|      | 7757.4   |   |  | 87550.5<br>P   |
|      |  |   |  | <u> </u>   |
| 8024 | 5675   |   |  | 73240  |
| 7299 | 5899   |   |  | 69005  |
| 7249 | 5875   |   |  | 68505  |
| 7249 | 5875   |   |  | 68750  |
|      | 5875   | 20100   |  | 68500  |
|      | 5875   | 20050   |  | 68500  |
|      |  | 19925   | 19575  | 66995  |
| 7249 | 5875   | 20100   | 19425  | 68505  |
|      | 9350<br>9250<br>9274<br>9299<br>9250<br>9299<br>10450<br>9452.333<br>T<br>9025<br>9325<br>9375<br>9425<br>9250<br>9274<br>9250<br>9274<br>9274<br>9274<br>9274<br>9274 | 9274 7675 9350 7600 9250 7650 9274 7725 9299 7650 9250 7874 9299 7650 10450 7650 9452.333 6909.9 T   9025 8075 9325 7725 9375 7725 9425 7675 9250 7725 9274 7625 9274 7625 9274 7625 9274 7700 9325 7924 9274 7700 9325 7924 7700 9379 7757.4 T   8024 5675 7299 5899 7249 5875 7224 5875 7224 5875 7224 5875 | 9274         7675         19225           9350         7600         19125           9250         7650         19150           9274         7725         19225           9299         7650         19350           9250         7874         19250           9299         7650         19300           10450         7650         19225           9452.333         6909.9         17315           T         I         M           9025         8075         19425           9325         7725         19350           9425         7675         19350           9250         7725         19175           9274         7625         19175           9250         7700         19300           9325         7924         19275           9274         7700         19200           9274         7700         19200           9274         7700         19200           9279.7         7757.4         19270           T         I         M           8024         5675         20150           7299         5899         20125 | 9274         7675         19225         18700           9350         7600         19125         18700           9250         7650         19150         18775           9274         7725         19225         18600           9299         7650         19350         18600           9250         7874         19250         18575           9299         7650         19300         18575           10450         7650         19225         18675           9452.333         6909.9         17315         16800           T         I         M         R           9025         8075         19425         18900           9325         7725         19200         18650           9375         7725         19350         18650           9375         7725         19350         18650           9250         7725         19175         18600           9274         7625         19175         18600           9274         7625         19175         18600           9274         7700         1920         18500           9274         7700         19250         18 |

| 200  | 7224   | 5875   | 20076 (  |  |  |  |
|--|--|--|--|--|--|--|
| years a series and   | 7400   | 6999   | 20076  | 19376  | 68505  |  |
| positive twee or an arm  |  | and the state of t | 19925  | 19550  | 66990  |  |
| Avg  | 7354,2   | 5884.7   | 20000  |  | Carlotte Control of the Control of t |  |
| D letter   | T  |  | 20070  | 19477.5  | 68749.5  |  |
| a Mush is this tens  | 8600   | 6900   | M  | R  | P  |  |
|  | 8576   | 6875   | 19425  | 19050  | 77000  |  |
| described by the second  | 8700   | 6649   | 19400  | 19150  | 77990  |  |
| CONTRACTOR OF THE REAL   | 8700   | The second secon | 19375  | 19050  | 81750  |  |
| 100 FEB. 1-01 72   | 8600   | 6800   | 19625  | 18860  | 78240  |  |
| conduct the designation  | 8750   | 6875   | 19625  | 19000  | 77500  |  |
| and the transfer and   | 8700   | 6875   | 19525  | 19000  | 75500  |  |
|  | 8750   | 6900   | 19500  | 18950  | 80500  |  |
| A COLUMN TO A STATE OF THE PARTY OF THE PART | THE RESERVE THE PERSON NAMED IN  | 6950   | 19325  | 18925  | 79995  |  |
| manufacture of   | 8750   | 7025   | 19500  | 18925  | 77505  |  |
| A LAG  | 0000 550   | The state of the state of  | and the same of th | Print Block Statement of the State of  | 7700   |  |
| Avg<br>E letter  | 8680,556<br>T  | 6872.111   | 19477.7  | 8 18990  | 78442.22   |  |
| C lotte  | THE R. LEWIS CO., LANSING, MICH.   |  | M  | R  | P  |  |
|  | 8875   | 7000   | 19425  | 19050  | 85250  |  |
| 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1  | 8825   | 7125   | 19550  | 18775  | 98995  |  |
| NOT AND A SECURE ASSESSMENT  | 8675   | 6975   | 19400 18925  |  | 85505  |  |
| COLUMN TO A STATE OF THE STATE  | 8800   | 7075   | 19550  | 18750  | 78740  |  |
|  | 8675   | 6975   | 19375  | 18850  | 75750  |  |
| NAME OF TAXABLE PARTY.   | 8649   | 6975   | 19325 18925  |  | 77005  |  |
|  | 8700   | 6950   | 19300 18750  |  | 78990  |  |
|  | 8825   | 7050   | 19450 18900  |  | 85000  |  |
|  | 8825   | 6950   | 19325  | 18875  | AND REAL PROPERTY AND PERSONS ASSESSMENT OF THE PERSON NAMED IN COLUMN TWO PERSONS ASSESSMENT OF THE PERSON NAMED IN COLUMN TWO PERSONS ASSESSMENT OF THE PERSON NAMED IN COLUMN TWO PERSONS ASSESSMENT OF THE PERSON NAMED IN COLUMN TWO PERSONS ASSESSMENT OF THE PERSON NAMED IN COLUMN TWO PERS |  |
|  | A STATE OF THE PARTY OF THE PAR | With the Real Property lies  | THE REAL PROPERTY AND ADDRESS OF THE PARTY AND | 10070  | 84255  |  |
| avg  | 8761   | 7008,333   | 19411.1  | 1 18866.6  | 83276.67   |  |
| F Letter   | T  | CA STREET, STATE OF THE STREET, STATE AND  | M  | R  | P 03270,07   |  |
|  | 9625   | 7374   | 19700  | 19175  | 83505  |  |
| Control to State S | 8700   | 6975   | 19400  | 18875  | THE RESERVE ASSESSMENT OF THE PARTY ASSESSMENT OF THE  |  |
| Control of the Control of the  | 8649   | 6900   | 19425  | 19050  | 78745  |  |
| SE-SENS CREATED TO COMPANY SE  | 8675   | 6950   | Non-April 1975-0752-1-10   | A STATE OF THE PARTY OF THE PAR | 78490  |  |
| <b>美国大学 大学 大学 大学 大学</b>  | 8675   | TO AN ADVANCED VALUE OF  | 19450  | 19000  | 75000  |  |
| February States Subdivision and the  | White the County of the County of the  | 6925   | 19600  | 18800  | 79240  |  |
| The state of the s | 8649   | 6925   | 19450  | 18850  | 79740  |  |
| S APPLIES THE REPORT OF THE  | 8825   | 7149   | 19525  | 18900  | 77740  |  |
| THE RESERVE TO THE PROPERTY OF | 8675   | 6925   | 19350  | 18750  | 77990  |  |
| THE RESERVE AND ADDRESS OF THE PARTY.  | 8775   | 6850   | 19600  | 19050  | 79490  |  |
| Mary Commission of the Commiss | 8800   | 7050   | 19600  | 18775  | 85005  |  |
| Ava  | 0004.0   | 7000 0   | 40540  | 40000 5  | 70404 5  |  |
| Avg  | 8804.8   | 7002.3   | 19510  | en i la president production de la constitución de  | 79494.5  |  |
| G Letter   | T  | 7040   | M 40000  | R 10076  | Р  |  |
| Or other desired to the owner, where   | 9625   | 7249   | 19800  | THE RESIDENCE AND ADDRESS OF THE PERSON NAMED IN   | 85255  |  |
| Section 4 man discountry   | 8750   | 7025   | 19600  | HER CHILDREN STONE AND THE THE THE   | 83505  |  |
| Constitution of the land of th | 8875   | 6925   | 19550  | COST COST BOTH AND ADDRESS OF THE PARTY OF T | 77000  |  |
|  | 8800   | 6875   | 19375  | 19000  | 77000  |  |

|          | 8700   | 6850   | 19350   |         |    |         |
|----------|--------|--------|---------|---------|----|---------|
|          | 8825   | 6800   | 19350   | 19025   |    | 85005   |
|          | 8850   | 7125   | 19400   | 19000   |    | 75500   |
|          | 8800   | 7149   | 19500   | 19025   |    | 77745   |
|          | 8775   | 7174   | 19500   | 18950   |    | 77740   |
|          | 8800   | 6975   | 19300   | 18950   |    | 82500   |
|          |        |        | 19300   | 18850   |    | 77500   |
| Avg      | 8880   | 7014.7 | 19485   |         |    |         |
| H letter | T      | 1      | M 19405 | 18950   |    | 79875   |
|          | 9625   | 7400   | 19650   | R       | Р  |         |
|          | 8925   | 7000   |         | 19000   |    | 88250   |
|          | 8825   | 7025   | 19600   | 19000   |    | 85250   |
|          | 8775   | 7075   | 19625   | 18775   |    | 78995   |
|          | 8900   | 7050   | 19600   | 18925   |    | 85255   |
|          | 8775   | 7025   | 19450   | 18800   |    | 79740   |
|          | 8775   | 7025   | 19600   | 19025   |    | 79495   |
|          | 8850   | 7000   | 19450   | 18950   |    | 80750   |
|          | 8875   | 6925   | 19650   | 18900   |    | 80750   |
|          | 8750   | 7025   | 19375   | 18825   |    | 77505   |
|          |        | 1025   | 19575   | 18775   |    | 84005   |
| Avg      | 8907.5 | 7055   | 100     |         |    | 04003   |
| l letter | T      | 1000   | 19557.5 | 18897.5 |    | 81999.5 |
|          | 9625   | •      | M       | R       | P  | 01999.5 |
|          | 8850   | 7400   | 19575   | 10175   |    | 96405   |
|          | 8900   | 7050   | 19450   | 18850   |    | 86495   |
|          | 8775   | 6950   | 19400   | 18800   |    | 86000   |
|          | 8775   | 6925   | 19425   | 18850   |    | 78990   |
|          |        | 7224   | 19325   | 1890    |    | 81500   |
|          | 8675   | 6925   | 1 7730  | 1890    |    | 77990   |
|          | 8775   | 7149   | 19525   |         |    | 77990   |
|          | 8750   | 7100   | 19400   | .003    |    | 84000   |
|          | 8725   | 7149   | 19500   | .003    |    | 78740   |
|          | 8850   | 7050   |         |         |    | 79990   |
| Ave      |        |        | 19375   | 1882    | 5  | 79745   |
| Avg      | 8870   | 7092.2 | 10400   | -       |    |         |
| J letter | T      | 1      | 102.0   |         | 5  | 81144   |
|          | 7750   | 7000   | M       | R       | P  | 01144   |
|          | 8950   |        |         | 100     | 75 | 88505   |
|          | 8875   | 7125   |         | 5 1867  |    |         |
|          | 8900   | 0000   |         |         | _  | 83005   |
|          |        | 7025   | 070     | 0 187   |    | 79245   |
|          | 8750   |        |         |         |    | 80505   |
|          | 8850   |        |         | 00      |    | 79245   |
|          | 8800   | , , ,  |         | 07      |    | 78240   |
|          | 8900   | 722    |         | - 100   |    | 81250   |
|          | 8800   | 722    |         |         | _  | 79240   |
|          | 8900   | 122.   | - 1040  |         | 75 | 7774    |
|          | 100    | 702    | 1937    | 75 187  | 00 |         |
|          |        |        | 1       |         | -  | 7899    |

| Avg             | 8747.5 | 7034.8   | 19422.5  |           |          |
|-----------------|--------|----------|----------|-----------|----------|
| K Letter        | T      |          | M        | 18790     | 80597    |
|                 | 8675   | 7475     |          | R         | P        |
|                 | 8975   | 7174     | 19575    | 19150     | 87250    |
|                 | 8900   | 6950     | 19450    | 18775     | 86755    |
|                 | 8875   | 7075     | 19525    | 18950     | 81250    |
|                 | 8900   | 7274     | 19475    | 19000     | 79490    |
|                 | 8875   | 7050     | 19600    | 18900     | 80750    |
|                 | 8900   | 7125     | 19575    | 18800     | 79990    |
|                 | 8800   | 7075     | 19400    | 18700     | 79240    |
|                 | 8900   | 7050     | 19500    | 18925     | 81755    |
|                 | 8825   | 7274     | 19300    | 18950     | 78990    |
|                 |        | 1214     | 19375    | 18625     | 85255    |
| Avg             | 8862.5 | 7152.2   | 40       |           | 00200    |
| L letter        | T      | 1132.2   | 19477.5  | 18877.5   | 82072.5  |
|                 | 8975   |          | М        | R         | P        |
|                 | 8925   | 7075     | 1957     |           | 00 85250 |
|                 | 8850   | 7025     | 1947     | 1882      |          |
|                 | 9000   | 7050     | 1942     | 1900      |          |
|                 | 8825   | 7100     | 1942     | 187       | - 00200  |
|                 |        | 7299     | 19500    | 1882      | - 00200  |
|                 | 8975   | 6900     | 19550    |           | 01000    |
|                 | 9000   | 7100     | 19650    |           | 01100    |
|                 | 8875   | 7075     | 1937     | 5 1890    |          |
|                 | 8900   | 7149     | 1937     |           | 01100    |
| ۸۰۰۰            |        |          |          |           | 03230    |
| Avg<br>M Letter | 8925   | 7085.889 | 19483.33 | 3 37763.8 | 84086.11 |
| M Letter        | T      | 1        | M        | R         | P        |
|                 | 9625   | 7525     | 19550    | 19000     | 87250    |
|                 | 9025   | 7224     | 19300    | 18875     | 84255    |
|                 | 8925   | 7174     | 19300    | 19075     | 84505    |
|                 | 9000   | 7224     | 19375    | 18850     | 84250    |
|                 | 9000   | 7149     | 19350    | 18750     | 83750    |
|                 | 8975   | 7224     | 19400    | 18900     | 84250    |
|                 | 8975   | 7249     | 19325    | 18650     | 84500    |
|                 | 8975   | 7100     | 19375    | 18825     | 85505    |
|                 | 9000   | 7450     | 19450    | 18750     | 84000    |
|                 | 9025   | 7450     | 19225    | 18675     | 85505    |
|                 |        |          |          | 10070     | 65505    |
| Avg             | 9052.5 | 7276.9   | 19365    | 18835     | 84777    |
| N letter        | T      | 1        | M        | R         | P 04///  |
|                 | 9625   | 7650     | 19600    | 18950     |          |
|                 | 9050   | 7349     | 19350    | 18700     | 87750    |
| -               | 9100   | 7249     | 19550    |           | 87250    |
|                 | 8975   |          |          | 18750     | 85500    |
|                 |        | 7224     | 19325    | 18775     | 85005    |
|                 | 9050   | 7274     | 19300    | 18850     | 85000    |
|                 | 9000   | 7199     | 19350    | 18725     | 85005    |

| R letter   | T 9150       | 7274         | -                                       | 5 1                                    | 8700   | 86250          |
|--|--------------|--------------|---|--|--|----------------|
| Avg  | 18972.22     | 1            | M                                       | R                                      |  | P              |
| Aver   | 40070 00     | 68611.11     | 20111.1                                 | 11 199                                 | 944.44   | 25485.67       |
|  | 19000        | 69000        | 2010                                    | -                                      | 10075  | 2000           |
|  | 18900        | 69250        |   | AND DESCRIPTION OF THE PERSON NAMED IN | 20000<br>19875   | 25500          |
|  | 19075        | 69005        |   | -                                      | 20050  | 25525<br>25474 |
|  | 18900        | 67240        |   | THE RESERVE TO SHAREST PROPERTY.       | 19925  | 25400          |
|  | 19050        | 68750        | -                                       | -                                      | 20050  | 25474          |
|  | 19000        | 68750        | -                                       | COLUMN THE PERSON                      | 19875  | 25474          |
|  | 19000        | 68750        | -                                       | man pulsar and advantage with          | 19875  | 25600          |
| ~  | 18925        | 67505        | and the same of the same of the same of | AND DESCRIPTION OF THE PERSON NAMED IN | 19925  | 25474          |
|  | 18900        | 69250        | 2009                                    | 50                                     | 19925  | 25450          |
| Q letter   | T            | []           | M                                       | R                                      | mose file on the   | P              |
| Avg  | 9093         | 7634.7       | 5479.5                                  | 18667                                  | .5   | 86251.5        |
|  |              |              | a secondo de la constanção              |  |  | 00000          |
|  | 9100         | 7450         | 5449                                    | 186                                    | CONTRACTOR STATE   | 85505          |
|  | 9005         | 7799         | 5449                                    | 185<br>187                             | the last of the last   | 85500<br>85500 |
|  | 9150         | 7575<br>7525 | 5424<br>5449                            | 187                                    | ecological based on the  | 85255          |
|  | 9100         | 7774         | 5500                                    | 185                                    | elemental property was   | 85755          |
|  | 9125<br>9200 | 7550         | 5449                                    | 186                                    | CALL STREET, CO.   | 86250          |
|  | 9150         | 7575         | 5525                                    | 185                                    | And State Of the Asset   | 86495          |
|  | 9175         | 7575         | 5500                                    | 185                                    | STREET, SQUARE, SQUARE,  | 87505          |
|  | 9200         | 7625         | 5475                                    | 187                                    | 50   | 86250          |
|  | 8725         | 7899         | 5575                                    | 189                                    | NAME OF STREET   | 88500          |
| P letter   | T            |              | M                                       | R                                      | P  | 0002010        |
| Avg  | 9125         | 7299.3       | 19387.5                                 | 18762                                  |  | 85526.5        |
|  |              |              |   | None and Publisher                     | VV   | 00000          |
|  | 9075         | 7249         | 19450                                   | 187                                    |  | 85250<br>85000 |
|  | 9025         | 7299         | 19300                                   | 100                                    | Section of the last of the las | 85000          |
| THE RESERVE OF THE PERSON  | 9125         | 7075         | 19325                                   | 107<br>187                             | Control of the Contro | 85005          |
|  | 9075         | 7274         | 19450                                   | 100                                    | AND RESIDENCE AND RESIDENCE AND  | 05266          |
|  | 9050         | 7274         | 19300                                   | 107                                    |  | 05250          |
|  | 9125         | 7240         | 19475<br>19450                          | 107                                    |  | 00000          |
|  | 9050         | 7500         | 19350                                   | 100                                    |  | 05750          |
| and the same of th | 9050         | 7274         | 19325                                   | 189                                    | 26   | 05255          |
|  | 9050         | 7274         | 19450                                   | 100                                    | 00   | 87500          |
|  | 9625         | 7525         | M                                       | R                                      | В  | 00021          |
| O letter   | *            | 7200.0       | 19302.5                                 | 107                                    | 05   | 05527          |
| AVQ  | 9090         | 7300 0       |   | 101                                    | 20   | 04755          |
|  | -            | 7274         | 19325                                   | 107                                    | 96   | 84500          |
| parameter of the second  | 8975         | 7240         | 19275                                   | 107                                    | 90   | 84250          |
| and the second second  | 9000         | 7100         | 19450                                   | 188                                    | 29   | 66266          |
| and the second   | 9125         | 7100         | 19300                                   | 188                                    | ne I   |                |

|  | 9200   | 727      | . 1                          |         |                             |    |          |
|--|--|----------|------------------------------|---------|-----------------------------|----|----------|
| CONTRACTOR NO.   | 9075   | 7274     | STATE OF THE PERSON NAMED IN | 60      | 1885                        | :n |          |
| Maria de la companya  | 9075   | 7249     | 1923                         | 25      | 1885                        |    | 86000    |
| THE PARTY OF THE PARTY   | 9050   | 7274     | 1947                         | 15      | 1875                        |    | 85500    |
| the second second  | A STATE OF THE PERSON NAMED IN COLUMN 2 IN | 7125     | 1927                         |         | THE RESERVE OF THE PARTY OF | _  | 86000    |
| A CARROL IN COLUMN   | 9050   | 7500     | 1920                         |         | 1870                        |    | 85000    |
| S to the same of the same of the   | 9050   | 7174     | 1927                         |         | 1862                        |    | 86495    |
| 100000000000000000000000000000000000000  | 9150   | 7324     | 1942                         |         | 1855                        |    | 87000    |
| the factor and the state of the state of the   | 9025   | 7248     |                              |         | 1865                        |    | 85500    |
| State with the land of the lan | And the second second second second  |          | 1021                         | _       | 1880                        | 00 | 85750    |
| Avg  | 9091.667   | 7271.444 | 1000                         | _       |                             | -  |          |
| S letter   | Т  |          | 1932<br>M                    | _       | 18719.4                     | 4  | 85943.89 |
| Service of the latest of the l | 9625   | 7500     | -                            | 1       | ₹                           | P  |          |
| A second state of the latest to  | 9125   | 7374     | 19450                        | _       | 18900                       | _  | 88250    |
| per transfer of the last of th | 9200   | 7349     | 19275                        | _       | 18675                       |    | 85755    |
|  | 9125   | 7324     | 19425                        | _       | 18700                       |    | 85500    |
| No. of Street, Street, St.   | 9075   |          | 19425                        | 1       | 18650                       |    | 85500    |
|  | 9100   | 7324     | 19225                        | $\perp$ | 18800                       |    | 85500    |
|  | A STATE OF THE PARTY OF THE PAR | 7425     | 19275                        | $\perp$ | 18600                       |    | 86750    |
| Marked Laboratory  | 9050   | 7274     | 19250                        |         | 18550                       |    | 85250    |
| Control Complete Street  | 9025   | 7324     | 19175                        |         | 18825                       |    | 85255    |
|  | 9050   | 7324     | 19200                        |         | 18775                       |    | 85505    |
|  | 9075   | 7500     | 19175                        |         | 18625                       |    | 85255    |
| Avg  | 9145   | 7371.8   | 19287.5                      | +       | 19710                       |    | 05050    |
| Tletter  | T  | 1        | M                            | +,      | 18710<br>R                  | _  | 85852    |
| 1 101101   | 9625   | 7600     |                              | +'      |                             | Р  |          |
| atura and recovery a we  | 9225   | 7675     | 5575                         | +       | 18775                       |    | 87755    |
|  |  |          | 5500                         | ╀       | 18425                       |    | 86255    |
|  | 9299   | 7650     | 5475                         | +       | 18575                       |    | 86495    |
| -  | 9175   | 7650     | 5475                         | +       | 18600                       |    | 86490    |
| ***  | 9200   | 7675     | 5475                         | +       | 18500                       |    | 87250    |
|  | 9200   | 7600     | 5475                         | _       | 18625                       |    | 86255    |
|  | 9150   | 7675     | 5475                         |         | 18675                       |    | 87005    |
|  | 9175   | 7725     | 5475                         |         | 18600                       |    | 86490    |
|  | 9125   | 7625     | 5475                         | $\perp$ | 18300                       |    | 86750    |
|  | 9150   | 7849     | 5449                         | 4       | 18725                       |    | 86255    |
|  |  |          |                              | _       |                             |    | 00700    |
| Avg  | 9232.4   | 7672.4   | 5484.9                       | 1       | 18580                       | _  | 86700    |
| U letter   | Т  | 1        | M                            | +       | R                           | Р  | 00500    |
|  | 9625   | 7625     | 19500                        | _       | 18900                       |    | 89500    |
|  | 9125   | 7525     | 19325                        | _       | 18700                       |    | 87250    |
|  | 9125   | 7274     | 19450                        | 1       | 18725                       | _  | 85505    |
| -  | 9050   | 7274     | 19450                        |         | 18725                       |    | 85255    |
|  | 9050   | 7274     | 19400                        | $\prod$ | 18650                       |    | 85000    |
|  | 9075   | 7274     | 19450                        | -       | 18725                       |    | 84755    |
|  |  | 7249     | 19450                        | _       | 18725                       |    | 84755    |
|  | 9100   | 7249     | 19275                        | _       | 18800                       |    | 84250    |
|  | 9000   | 1248     |                              |         |                             |    |          |

|  |  | 9000  | 7274   | 19325  |  |  |
|--|--|---|--|--|--|--|
| Avg 9125 7321.7 19410 18762.5 85507  V letter T  | Control of the Contro | 9100  |  | 10476  | 18825  | 84050  |
| Violitier         T         I         M         R         P           9625         7475         19450         18760         86250           8975         7224         19325         18725         8505           9100         7174         19475         18850         84750           9025         7140         19325         18750         84500           8975         7224         19350         18725         86255           8950         7199         19375         18900         83500           8900         7025         19400         18600         85250           8925         7174         19225         18775         79995           8925         7050         19450         18900         82500           Avg         9037.5         7186.8         19372.5         18772.5         76425.5           W letter         T         I         M         R         P           4 letter         T         I         M         R         P           8025         7124         19425         18825         83255           8875         7374         19425         18825         83255   | THE RESERVE OF THE PARTY OF THE |   | and the other ball of the  | MA / D   | 18850  | 84750  |
| Vietter   T  | Avg  | 9125  | 7321.7   | 10440  | Service and the service of the servi |  |
| 9625   |  | T   |  |  |  |  |
| 8975   7224   19325   18726   86250     9100   7174   19476   18850   84750     9025   7140   19325   18750   84560     8975   7224   19350   18725   86255     8975   7190   19375   18900   83500     8900   7025   19400   18800   82550     8925   7174   19350   18775   79955     8925   7050   19450   18900   82500     Avg   9037.5   7186.8   18372.5   18772.5   76425.5     W letter   T   I   M   R   P     8825   7299   19800   18825   83255     8875   7174   19450   18800   85250     8875   7374   19425   18825   83255     8875   7174   19450   18900   85250     8875   7174   19450   18900   85250     8875   7025   19525   18825   85255     88850   7075   19800   18800   34255     88775   7025   19350   18800   34255     88800   7174   19450   18900   79240     88775   7000   19500   18850   8175     Avg   8860   7157   19480   18862.5   83399     letter   T   I   M   R   P     9625   7400   19600   189745   79241     88900   70749   19400   18750   83500     8850   7050   19400   18750   83500     8850   7050   19400   18750   83500     8850   7050   19400   18750   83500     8850   7050   19400   18750   83500     8850   7050   19400   18750   83500     8850   7050   19400   18750   83500     8850   7050   19450   18750   83500     8850   7050   19450   18750   8075     8850   7050   19550   18725   8400     8875   7174   19425   18850   8100     8876   7050   19550   18725   8400     88775   6975   19450   19000   7949     88775   6975   19450   19000   7949     88775   6975   19450   19000   7949     88775   6975   19450   19000   7949     88775   6975   19450   19000   7949     88775   6975   19450   19000   7949     88775   6975   19450   19000   7949     88775   6975   19450   19000   7949     88775   6975   19450   19000   7949     88775   6975   19450   19000   7949     88775   7040   19442.5   35942   8204     409   16942.5   7142.1   19442.5   35942   8204     409   16942.5   7142.1   19442.5   35942   8204     409   16942.5   7142.1   19442.5   35942   8204     409   16942.5   7142.1   19442.5   3   | A School Service College College   | 9625  | 7475   | Part Company of the Company  | WORLS OF STREET  | P  |
| 9100 7174 19475 18650 84750 9025 7140 19325 18750 84500 8975 7224 19350 18725 86255 8950 7199 19375 18900 83300 8975 7174 19225 18750 82750 8900 7025 19400 18800 85250 8925 7174 19350 18775 79995 8925 7050 19450 18900 82500  Avg 9037.5 7186.8 19372.5 18772.5 76425.5  W letter T I M R P 8825 7299 19600 19150 87500 8975 7374 19425 18825 83255 8875 7174 19450 18900 85250 8875 7025 19525 18825 85255 88850 7075 19600 18850 84500 8775 7025 19350 18800 79240 8800 7174 19450 18700 77990 8775 7000 19500 18850 81750  Avg 8860 7157 19480 18862.5 83399. letter T I M R P 9625 7400 19600 18750 83399. letter T I M R P 9625 7400 19600 18750 83399. letter T I M R P 9625 6950 19400 18750 83500 8850 7075 19480 18862.5 83399. letter T I M R P 9625 7400 19500 18850 84500 8850 7075 19480 18862.5 83399. letter T I M R P 9625 8400 7850 19400 18750 83500 8850 7050 19500 18750 8050 8850 7050 19500 18750 8050 8850 7050 19400 18750 83500 8850 7050 19350 18750 8050 8850 7050 19350 18750 80750 8850 7050 19350 18750 80750 8850 7050 19350 18750 80750 8850 7050 19350 18750 80750 8850 7050 19350 18750 80750 8850 7050 19350 18750 80750 8850 7050 19350 18750 80750 8850 7050 19350 18750 80750 8850 7050 19550 18725 8400 8800 7249 19475 18950 7899 88775 6975 19450 19000 7949 8800 7249 19375 18950 7899 88775 6975 19450 19000 7949 88000 7249 19375 18950 7899 88775 6975 19450 19000 7949 88900 7249 19375 18950 8050  | AND THE PERSON NAMED IN COLUMN   | 8975  | Secure of the Part | THE RESERVE OF THE PARTY OF THE | Committee of the Commit | 86250  |
| 9025   | Service Servic | 9100  | THE RESERVE AND ADDRESS OF THE PARTY OF THE  | THE PERSON NAMED IN COLUMN TWO   | Company of the Party and State of the Party a | 8505   |
| 8975   7224   19350   18725   86255   8850   7199   19375   18900   83500   8975   7174   19225   18750   82750   8925   7174   19350   18775   79995   8925   7050   19450   18900   82500   82500   8925   7050   19450   18900   82500   82750   8925   7050   19450   18900   82500   82   | produced to be desired.  | 9025  | WATER TOTAL PROPERTY.  |  | THE RESERVE AND PERSONS ASSESSED.  | And the state of the second se |
| 8950   7199   19375   18900   83500  |  | 8975  |  |  | THE RESERVE THE PARTY OF THE PARTY OF THE PARTY.   | CALCON DESCRIPTION OF STREET,  |
| 8975         7174         19225         18750         83500           8900         7025         19400         18800         85250           8925         7174         19350         18775         79995           8925         7050         19450         18900         82500           Avg         9037.5         7186.8         19372.5         18772.5         76425.5           W letter         T         I         M         R         P           8825         7299         19600         19150         87500           8975         7374         19425         18825         83255           8875         7174         19450         18900         85250           8875         7124         19450         18900         85250           8875         7025         19525         18825         85255           8875         7025         19525         18825         85255           8875         7025         19525         18825         85255           8875         7025         19350         18800         34250           8925         7299         19300         18800         7924           800 </td <td></td> <td>8950</td> <td></td> <td></td> <td>The state of the s</td> <td>A STATE OF THE PARTY OF THE PAR</td> |  | 8950  |  |  | The state of the s | A STATE OF THE PARTY OF THE PAR |
| 8900         7025         19400         18600         82750           8925         7174         19350         18775         79995           8925         7050         19450         18900         82500           Avg         9037.5         7186.8         19372.5         18772.5         76425.5           W letter         T         I         M         R         P           8825         7299         19600         19150         87500           8975         7374         19425         18825         83255           8875         7174         19450         18900         85250           8875         7025         19600         18825         85005           8875         7025         19525         18825         85255           8850         7075         19800         18950         84500           8775         7025         19350         18800         7924           8800         7174         19450         18700         77990           8775         7000         19500         18850         81750           Avg         8860         7157         19480         18862.5         83399.   |  | 8975  | STATE OF THE PERSON NAMED IN   | THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN THE OWNER, THE PERSON NAMED | THE RESIDENCE OF THE PERSON AS   | A RESIDENCE OF THE PROPERTY OF THE PERSON NAMED IN   |
| 8925         7174         19350         18800         85250           8925         7050         19450         18900         82500           Avg         9037.5         7186.8         19372.5         18772.5         76425.5           W letter         T         I         M         R         P           8825         7299         19600         19150         87500           8975         7374         19425         18825         83255           8875         7174         19450         18900         85250           8875         7125         19600         18825         85005           8875         7025         19525         18825         85255           8850         7075         19600         18950         84500           8775         7025         19350         18800         34250           8800         7174         19450         18700         7994           8775         7002         19350         18800         79240           8800         7174         19450         18860         81750           Avg         8860         7157         19480         18862.5         83399.   |  | 8900  | NAME AND ADDRESS OF THE OWNER, WHEN  | を から 日本  | THE RESERVE OF THE PARTY OF THE | CARL STREET, STREET, STREET, SALES STREET, S |
| Avg         9037.5         7186.8         19372.5         18775         79995           Veletter         T         I         M         R         P           8825         7299         19600         19150         87500           8975         7374         19425         18825         83255           8875         7174         19450         18900         85250           8875         7125         19600         18825         85250           8875         7025         19525         18825         85250           8875         7025         19525         18825         85255           8850         7075         19600         18950         84500           8775         7025         19350         18800         7924           8800         7174         19450         18700         77990           8775         7000         19500         18850         8175           Avg         8860         7157         19480         18862.5         83399.           letter         T         I         M         R         P           9625         7400         19600         19000         87000   | A CONTRACTOR OF THE PARTY OF TH | AND DESCRIPTION OF THE PERSON | DESCRIPTION OF THE RESERVE OF THE PERSON OF  | 1 日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日   | The second secon | The same of the sa |
| Avg         9037.5         7186.8         19372.5         18772.5         76425.5           W letter         T         I         M         R         P           8825         7299         19600         19150         87500           8975         7374         19425         18825         83255           8875         7174         19450         18900         85250           8875         7025         19525         18825         85005           8875         7025         19525         18825         85250           8850         7075         19600         18950         84500           8775         7025         19350         18800         7924           8800         7174         19450         18700         77990           8775         7000         19500         18850         8175           Avg         8860         7157         19480         18862.5         83399.           letter         T         I         M         R         P           9625         7400         19600         19000         87000           8850         6950         19400         18750         83500 <td>And the same of th</td> <td></td> <td>THE RESERVE THE PERSON NAMED IN</td> <td>THE PERSON NAMED IN</td> <td>CONTRACTOR OF THE PERSON NAMED IN COLUMN 1</td> <td>the large his section at a little process with the large</td>   | And the same of th |   | THE RESERVE THE PERSON NAMED IN  | THE PERSON NAMED IN  | CONTRACTOR OF THE PERSON NAMED IN COLUMN 1   | the large his section at a little process with the large   |
| W  letter   T  |  |   | 7000   | 19450  | 18900  | 82500  |
| 8825   7299   19600   19150   87500  | Avg  | 9037.5  | 7186.8   | 19372.5  | 18772.5  | 78425.5  |
| 8825   7299   19600   19150   87500  | 10/1-44  | _   |  |  |  |  |
| 8975       7374       19425       18825       83255         8875       7174       19450       18900       85250         8925       7125       19600       18825       85005         8875       7025       19525       18825       85255         8850       7075       19600       18950       84500         8775       7025       19350       18800       84250         8925       7299       19300       18800       79240         8800       7174       19450       18700       77990         8775       7000       19500       18850       81750         Avg       8860       7157       19480       18862.5       83399.         letter       T       I       M       R       P         8850       6950       19400       18750       83500         8850       7050       19425       18725       81500         8850       7050       19350       18750       8075         8950       7050       19350       18750       8075         8950       7050       19350       18755       8400         8975       7174   | Wietter  | -   | -  | SECRETARIAN PROPERTY.  | THE RESERVE AND ADDRESS OF THE PARTY OF THE  | Р  |
| 8875       7174       19450       18900       85250         8925       7125       19600       18825       85005         8875       7025       19525       18825       85255         8850       7075       19600       18950       84500         8775       7025       19350       18800       84250         8925       7299       19300       18800       79240         8800       7174       19450       18700       77990         8775       7000       19500       18850       81750         Avg       8860       7157       19480       18862.5       83399.         letter       T       I       M       R       P         8850       6950       19400       18750       83500         8800       7249       19400       189745       79244         8900       7075       19425       18725       81506         8850       7050       19350       18750       8075         8850       7050       19350       18725       8400         8900       7249       19375       18950       7899         8875       7174 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>87500</td></td<>   |  |   |  |  |  | 87500  |
| 8925       7125       19600       18825       85005         8875       7025       19525       18825       85255         8850       7075       19800       18950       84500         8775       7025       19350       18800       84250         8925       7299       19300       18800       79240         8800       7174       19450       18700       77990         8775       7000       19500       18850       81750         Avg       8860       7157       19480       18862.5       83399.         letter       T       I       M       R       P         9625       7400       19600       19000       87000         8850       6950       19400       18750       83500         8800       7249       19400       189745       79244         8900       7075       19425       18725       8150         8950       7050       19350       18725       8400         8975       7174       19425       18850       8100         8775       6975       19450       19000       7949         88900       7249 <td< td=""><td></td><td></td><td>-</td><td>and the second section in the second</td><td></td><td>83255</td></td<>  |  |   | -  | and the second section in the second   |  | 83255  |
| 8875       7025       19525       18825       85255         8850       7075       19600       18950       84500         8775       7025       19350       18800       84250         8925       7299       19300       18800       79240         8800       7174       19450       18700       77990         8775       7000       19500       18850       81750         Avg       8860       7157       19480       18862.5       83399.         letter       T       I       M       R       P         9625       7400       19600       19000       87000         8850       6950       19400       18750       83500         8800       7249       19400       189745       79249         8850       7050       19350       18750       8075         8950       7050       19550       18725       8400         8900       7249       19375       18850       7899         8875       7174       19425       18850       8100         88900       7249       19450       18925       8500         Avg       16942.5 <t< td=""><td></td><td>-</td><td></td><td></td><td>18900</td><td>85250</td></t<>  |  | -   |  |  | 18900  | 85250  |
| 8850       7075       19800       18950       84500         8775       7025       19350       18800       84250         8925       7299       19300       18800       79240         8800       7174       19450       18700       77990         8775       7000       19500       18850       81750         Avg       8860       7157       19480       18862.5       83399.         letter       T       I       M       R       P         9625       7400       19600       19000       87000         8850       6950       19400       18750       83500         8800       7249       19400       189745       79248         8850       7050       19350       18750       8075         8950       7050       19550       18725       8400         8900       7249       19375       18950       7899         8875       7174       19425       18850       8100         88900       7249       19450       18925       8500         Avg       16942.5       7142.1       19442.5       35942       8204         Avg   |  |   |  |  | 18825  | 85005  |
| 8775   7025   19350   18800   84250  |  |   |  |  |  | 85255  |
| 8925       7299       19300       18800       79240         8800       7174       19450       18700       77990         8775       7000       19500       18850       81750         Avg       8860       7157       19480       18862.5       83399.         letter       T       I       M       R       P         9625       7400       19600       19000       87000         8850       6950       19400       18750       83500         8800       7249       19400       189745       79249         8950       7050       19350       18725       81500         8950       7050       19550       18725       8400         8975       7174       19425       18850       7899         8875       7174       19425       18850       8100         8775       6975       19450       19000       7949         88900       7249       19450       18925       8500         Avg       16942.5       7142.1       19442.5       35942       8204         Y letter       T       I       M       R       P  |  |   | and the same of the case of  | -  | 18950  | 84500  |
| 8800       7174       19450       18700       77990         8775       7000       19500       18850       81750         Avg       8860       7157       19480       18862.5       83399.         letter       T       I       M       R       P         9625       7400       19600       19000       87000         8850       6950       19400       18750       83500         8800       7249       19400       189745       79248         8850       7050       19350       18750       8075         8950       7050       19550       18725       8400         8900       7249       19375       18950       7899         8875       7174       19425       18850       8100         8775       6975       19450       19000       7949         88900       7249       19450       18925       8500         Avg       16942.5       7142.1       19442.5       35942       8204         Y letter       T       I       M       R       P   |  |   |  |  | 18800  | 84250  |
| Avg       8860       7157       19480       18850       81750         letter       T       I       M       R       P         9625       7400       19600       19000       87000         8850       6950       19400       18750       83500         8800       7249       19400       189745       79245         8900       7075       19425       18725       81500         8850       7050       19350       18750       8075         8950       7050       19550       18725       8400         8900       7249       19375       18950       7899         8875       7174       19425       18850       8100         88900       7249       19450       19000       7949         88900       7249       19450       18925       8500         Avg       16942.5       7142.1       19442.5       35942       8204         Y letter       T       I       M       R       P   |  | 8925  | 7299   | 19300  | 18800  | 79240  |
| Avg         8860         7157         19480         18862.5         83399.           letter         T         I         M         R         P           9625         7400         19600         19000         87000           8850         6950         19400         18750         83500           8800         7249         19400         189745         79248           8900         7075         19425         18725         81500           8850         7050         19350         18750         8075           8950         7050         19550         18725         8400           8875         7174         19425         18850         8100           8875         7174         19425         18850         8100           88900         7249         19450         18925         8500           Avg         16942.5         7142.1         19442.5         35942         8204           Y letter         T         I         M         R         P  |  | 8800  | 7174   | 19450  | 18700  | 77990  |
| letter         T         I         M         R         P           9625         7400         19600         19000         87000           8850         6950         19400         18750         83500           8800         7249         19400         189745         79245           8900         7075         19425         18725         81500           8950         7050         19350         18750         8075           8990         7249         19375         18950         7899           8875         7174         19425         18850         8100           8775         6975         19450         19000         7949           88900         7249         19450         18925         8500           Avg         16942.5         7142.1         19442.5         35942         8204           Y letter         T         I         M         R         P   |  | 8775  | 7000   | 19500  | 18850  | 81750  |
| letter         T         I         M         R         P           9625         7400         19600         19000         87000           8850         6950         19400         18750         83500           8800         7249         19400         189745         79245           8900         7075         19425         18725         81500           8950         7050         19350         18750         8075           8990         7249         19375         18950         7899           8875         7174         19425         18850         8100           8775         6975         19450         19000         7949           88900         7249         19450         18925         8500           Avg         16942.5         7142.1         19442.5         35942         8204           Y letter         T         I         M         R         P   |  |   |  |  |  |  |
| letter         T         I         M         R         P           9625         7400         19600         19000         87000           8850         6950         19400         18750         83500           8800         7249         19400         189745         79245           8900         7075         19425         18725         81500           8950         7050         19350         18750         8075           8900         7249         19375         18950         7899           8875         7174         19425         18850         8100           88900         7249         19450         19000         7949           88900         7249         19450         18925         8500           Avg         16942.5         7142.1         19442.5         35942         8204           Y letter         T         I         M         R         P  | Avg  | 8860  | 7157   | 19480  | 18862.5  | 83399.5  |
| 8850       6950       19400       18750       83500         8800       7249       19400       189745       79249         8900       7075       19425       18725       81500         8850       7050       19350       18750       8075         8950       7050       19550       18725       8400         8900       7249       19375       18950       7899         8875       7174       19425       18850       8100         8775       6975       19450       19000       7949         88900       7249       19450       18925       8500         Avg       16942.5       7142.1       19442.5       35942       8204         Y letter       T       I       M       R       P   |  | T   | Ī  | M  | R  | P  |
| 8850     6950     19400     18750     83500       8800     7249     19400     189745     79245       8900     7075     19425     18725     81505       8850     7050     19350     18750     8075       8950     7050     19550     18725     8400       8900     7249     19375     18950     7899       8875     7174     19425     18850     8100       8775     6975     19450     19000     7949       88900     7249     19450     18925     8500       Avg     16942.5     7142.1     19442.5     35942     8204       Y letter     T     I     M     R     P   |  | 9625  | 7400   | 19600  | 19000  | 87000  |
| 8800       7249       19400       189745       79245         8900       7075       19425       18725       81505         8850       7050       19350       18750       8075         8950       7050       19550       18725       8400         8900       7249       19375       18950       7899         8875       7174       19425       18850       8100         8775       6975       19450       19000       7949         88900       7249       19450       18925       8500         Avg       16942.5       7142.1       19442.5       35942       8204         Y letter       T       I       M       R       P   |  |   |  | 19400  | 18750  | 83500  |
| 8900       7075       19425       18725       8150         8850       7050       19350       18750       8075         8950       7050       19550       18725       8400         8900       7249       19375       18950       7899         8875       7174       19425       18850       8100         8775       6975       19450       19000       7949         88900       7249       19450       18925       8500         Avg       16942.5       7142.1       19442.5       35942       8204         Y letter       T       I       M       R       P   |  |   |  | 19400  | 189745   | 79245  |
| 8850       7050       19350       18750       8075         8950       7050       19550       18725       8400         8900       7249       19375       18950       7899         8875       7174       19425       18850       8100         8775       6975       19450       19000       7949         88900       7249       19450       18925       8500         Avg       16942.5       7142.1       19442.5       35942       8204         Y letter       T       I       M       R       P  |  |   |  |  | 18725  | 81505  |
| 8950     7050     19550     18725     8400       8900     7249     19375     18950     7899       8875     7174     19425     18850     8100       8775     6975     19450     19000     7949       88900     7249     19450     18925     8500       Avg     16942.5     7142.1     19442.5     35942     8204       Y letter     T     I     M     R     P   |  |   |  |  | 18750  | 80750  |
| 8900     7249     19375     18950     7899       8875     7174     19425     18850     8100       8775     6975     19450     19000     7949       88900     7249     19450     18925     8500       Avg     16942.5     7142.1     19442.5     35942     8204       Y letter     T     I     M     R     P  |  |   |  |  |  | 84005  |
| 8875 7174 19425 18850 8100<br>8775 6975 19450 19000 7949<br>88900 7249 19450 18925 8500<br>Avg 16942.5 7142.1 19442.5 35942 8204<br>Y letter T I M R   |  |   |  |  |  | 78990  |
| 8875 6975 19450 19000 7949 88900 7249 19450 18925 8500  Avg 16942.5 7142.1 19442.5 35942 8204  Y letter T I M R P  |  |   |  |  |  | 81000  |
| 8775 6975 19450 18925 8500  88900 7249 19450 18925 8500  Avg 16942.5 7142.1 19442.5 35942 8204  Y letter T I M R   |  |   |  |  |  | 79490  |
| Avg     16942.5     7142.1     19442.5     35942     8204       Y letter     T     I     M     R     P       5525     19175     8775   |  |   |  |  |  | 2500   |
| Avg   16942.5   7142.1   19442.5   33342   P<br>Y letter   T   I   M   R   P   |  | 88900   | 7249   | 19450  | 10020  |  |
| Y letter T I M R P   | Ava  | 16042.5   | 7142 1   | 19442.5  | 35942  |  |
| Tieller   1   5525   19175   8775  |  |   |  |  | R  |  |
|  | Y letter   | 9625  | 7450   |  | 5 1917   | 5 8775   |

|          | 8950   | 7374   | F445 1 |         |         |
|----------|--------|--------|--------|---------|---------|
|          | 8925   | 7299   | 5449   | 18725   | 86755   |
|          | 8950   | 7349   | 5424   | 18925   | 83755   |
|          | 8900   | 7274   | 5424   | 18875   | 84005   |
|          | 8900   | 7349   | 5424   | 18875   | 80755   |
|          | 8875   | 7299   | 5449   | 18925   | 81505   |
|          | 9000   | 7274   | 5399   | 18925   | 83505   |
|          | 8825   | 7299   | 5424   | 18875   | 80505   |
|          | 8850   | 7199   | 5374   | 18850   | 81500   |
|          |        | 7199   | 5424   | 18850   | 84750   |
| Ava      | 8980   | 7316.6 |        |         |         |
| Avg      | 0000   | 7310.0 | 5431.6 | 18900   | 83479   |
| Z letter | Т      | 1      | М      | R       | Р       |
|          | 9625   | 7620   | 19325  | 18675   | 87255   |
|          | 9274   | 7425   | 19300  | 18600   | 86000   |
|          | 9250   | 7725   | 19275  | 18600   | 86490   |
|          | 9200   | 7575   | 19200  | 18700   | 87500   |
|          | 9200   | 7525   | 19150  | 18575   | 86255   |
|          | 9225   | 7774   | 19200  | 18550   | 88500   |
|          | 9250   | 7575   | 19250  | 18575   | 86755   |
|          | 9299   | 7500   | 19300  | 18600   |         |
|          | 9225   | 7700   | 19150  | 18750   | 86750   |
|          | 9325   | 7899   | 19300  |         | 87000   |
|          | 5525   | 7000   | 19300  | 18650   | 87500   |
| Aug      | 9287.3 | 7621 0 | 10045  | 40007.5 | 07000 5 |
| Avg      | 9207.3 | 7631.8 | 19245  | 18627.5 | 87000.5 |

The previous trials was able to recognize only one letter (C letter), so the designer repeat the train mode.

The 26<sup>th</sup> letters were represented again using ASL (10 trials for each letter and then the average was displayed on the LCD), then the averages were read from LCD after the train mode code was put on the PIC, the averages were in the following table.

Table (6. 3): displayed values for the letters taken from the LCD (10 trials for each letter).

| Letter | Thumb | Index | Middle | Ring | Pinky |
|--------|-------|-------|--------|------|-------|
| A      | 772   | 229   | 817    | 810  | 249   |
| В      | 778   | 229   | 821    | 815  | 251   |
| C      | 777   | 232   | 822    | 813  | 248   |

|    | T 776 | 229 |     |     |      |
|----|-------|-----|-----|-----|------|
| 0  | 776   |     | 819 | 816 | 251  |
| D  | 776   | 233 | 821 | 813 | 250  |
| E  | 775   | 234 | 820 |     |      |
| F  | 776   | 234 | 821 | 813 | 251  |
| 6  | 773   | 231 |     | 813 | 251  |
| H  |       |     | 817 | 811 | 251  |
| 1  | 777   | 234 | 821 | 814 | 251  |
| Ī  | 777   | 244 | 205 | 818 | 257  |
|    | 776   | 232 | 821 | 815 | 255  |
| K  | 770   | 825 | 826 | 192 | 1017 |
| [L | 771   | 233 | 817 |     |      |
| M  |       |     |     | 812 | 255  |
| N  | 775   | 232 | 819 | 815 | 254  |
| 0  | 775   | 234 | 821 | 813 | 252  |
| P  | 776   | 233 | 820 | 814 | 255  |
| Q  | 773   | 233 | 817 | 811 | 253  |
| R  | 777   | 236 | 821 | 814 | 253  |
| S  | 775   | 234 | 818 | 814 | 254  |
| T  | 777   | 235 | 821 | 812 | 253  |
| Ü  | 773   | 234 | 817 | 810 | 253  |
| V  | 777   | 235 | 821 | 811 | 253  |
| W  | 772   | 236 | 817 | 810 | 254  |
| X  | 773   | 235 | 818 | 811 | 254  |
| Y  | 776   | 235 | 821 | 815 | 256  |
| Z  | 773   | 249 | 206 | 816 | 262  |
|    |       |     | _   |     |      |

Note: the previous values were taken and stored statically in array in test mode code, and after the letters were tested, the PIC was able to recognize only 4 letters from 26(A, K,L and C letters).

So the designer repeated the previous work and took 20 trials for each letter.

(6.4): displayed values for the letters taken from the LCD(20 trials for each letter).

| Jan.   |       |       | <u>letter)</u> . |      | (20 (11111) |
|--------|-------|-------|------------------|------|-------------|
| 108    | Thumb | Index | Middle           | Ring | Pinky       |
| Letter | 775   | 230   | 1020             | 8250 | 8250        |
| A      | 778   | 227   | 1019             | 8289 | 8289        |
| В      | 778   | 226   | 1017             | 8277 | 1077        |
| c      | 777   | 227   | 1019             | 8299 | 7299        |
| 0      | 771   | 825   | 1015             | 1895 | 1017        |
| E      | 768   | 824   | 1015             | 1905 | 1016        |
| F      | 776   | 232   | 1020             | 8310 | 8310        |
| 6      | 777   | 230   | 1018             | 8278 | 7278        |
| H      | 775   | 226   | 1013             | 8253 | 8253        |
| 1      | 778   | 226   | 1016             | 8286 | 8286        |
| I<br>K | 777   | 227   | 1018             | 8278 | 7278        |
| L      | 775   | 226   | 1014             | 8244 | 7244        |
| M      | 778   | 228   | 1019             | 8309 | 8309        |
| N      | 775   | 226   | 1015             | 8255 | 8255        |
| 0      | 778   | 228   | 1019             | 8279 | 7279        |
| P      | 778   | 228   | 1018             | 8288 | 8288        |
| Q      | 777   | 225   | 1015             | 8295 | 9295        |
| R      | 777   | 227   | 1018             | 8288 | 7288        |
| S      | 779   | 224   | 1016             | 8296 | 8296        |
| T      | 779   | 227   | 1019             | 8299 | 8299        |
| U      | 778   | 225   | 1018             | 8298 | 7298        |
| V      | 777   | 227   | 1018             | 8278 | 7278        |
| W      | 773   | 827   | 1015             | 1895 | 1017        |
| X      | 778   | 230   | 1018             | 8298 | 9298        |
| Y      |       |       | 1013             | 8263 | 8263        |
| Z      | 775   | 227   | 1016             | 1916 | 1917        |
|        | 771   | 830   | 1010             |      |             |

## 63.5.5 PIC test mode

This section contains the result of test mode for the letters after they tested on the plC in the second trial.

The following figure shows the K letter after it was tested successfully in PIC phase.

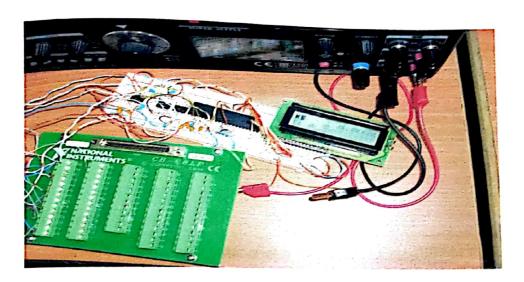


Figure 6.94: K letter test mode at PIC phase.

The following figure shows the L letter after it was tested successfully in PIC phase.

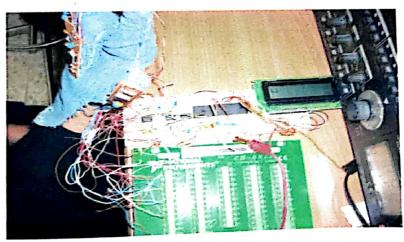


Figure 6.95: L letter test mode at PIC phase.

The following figure shows the J letter after it was tested successfully in PIC phase.

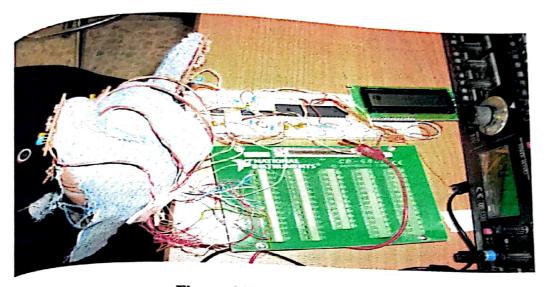


Figure 6.96 J letter test mode at PIC phase.

The following figure shows the F letter after it was tested successfully in PIC phase.

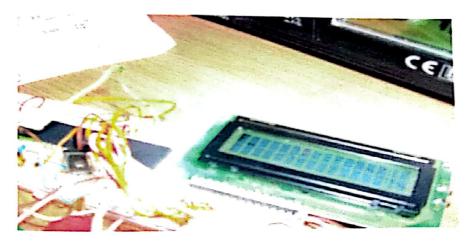


Figure 6.97 F letter test mode at PIC phase

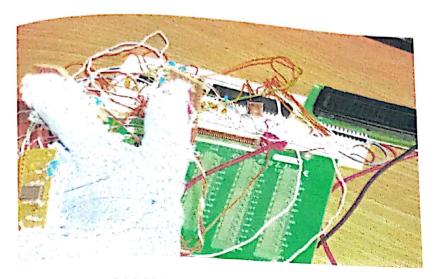


Figure 6.98 V letter test mode at PIC test mode

The following figure shows the V letter after it was tested successfully in PIC phase.



Figure 6.99 V letter at PIC test mode

## **CHAPTER**

7

### CONCLUSION AND FUTURE WORK

Introduction.

Conclusion.

Future works.

### Chapter Seven Conclusion and future work

## : I Introduction

This chapter represents the future works and conclusions related to the SLC system.

## 2 Conclusions

In this system many conclusions that are concluded after working with this project nd in this section a description of the resulted conclusions will be pointed:

- The SLC system recognizes 26 letters at computer phase.
- . Working on this system increases the knowledge of PIC programming.
- Working on this system increases the knowledge of sign language.
- Working on this system increases the knowledge of working with a new sensor called accelerometer sensor (new technology).
- In test mode the designer must represent the letter in the same way he did in train mode from the side of hand position.
- If the designer stores an array statically in ROM he can retrieve any value depends on the index in the same way as if it was stored in ram.
- If the designer stores an array dynamically at runtime in ROM and he tries to retrieve value depends on index this will return 0, so to solve this problem the designer uses external EEPROM to write on it at runtime and after that to read from it.

## i future work

pis system could be improved and modified, and the following points can be implemented to the system could be improved so that it becomes

- The system could be improved so that it becomes able to implement sound by using speaker to pronounce the sound of each letter.
- The system could be improved so that it becomes able to implement words instead of letters, by using PIC with larger memory like AVR PIC microcontroller.

## Resources

## Books:

- S.Mehdi and Y.khan, "Sign Language recognition using sensors gloves" in proceeding of the 9th international conference in neural information processing.(ICON1P'02),2002,pp,2204\_22\_6.
- Y.Yoon and k.Jo "hand shape recognition using moment invariant for the Korean sign language recognition" in proceedings of the 7th korea\_Russia international symposium, KORUS, 2003, pp, 308\_313.
- Barbara Bernstein Fant, Betty Miller, Lou Fant "The American Sign Language phrase book" ISBN 0071497137/9780071497138, format paperback, 416 pages, 2003.

#### Papers:

 Omar Al\_Jarrah, Alaa Halawani, "Recognition of gestures in Arabic Language using neuro\_fuzzy systems", Artifical Inteligence ,133(2001) 117\_138.

#### Links:

[1]:http://www.gwu.edu/~research/accele.htm.
Research at George Washington University.
By jose Hernandez\_Rebollar.

[2]: A thesis presented to the deanship of graduate studies King Fahd University of petroleum and minerals. By Salah Mohammad Saeed Al\_Buraiky, Master of science in electrical engineering, September 2004.

[3]:S.Mehdi and Y.khan, "Sign Language recognition using sensors gloves" in Proceeding of the 9<sup>th</sup> international conference in neural information processing. (ICONIP'02),2002,pp,2204\_22\_6.

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y, younger recognition" in proceedings of the 7th korea_Russin interests.
Y, Youn and Room in proceedings of the 7th korea_Russia international
in proceedi in pro
(f/en.wikipedia.org/wiki/American_Manual_Alphabet.
|| http://www.futurlec.com/AnalogDevices/ADXL202AQCa.shtml.
 ||||: http://www.eio.com/public/LCD.2004.
 ||1||: http://www.mines.edu/Academic/courses/physics/phgn317/labview06/6034E_and_
 M35E_User_Manual.pdf.
 |35E_Use.
|13|: http://ww1.microchip.com/downloads/en/DeviceDoc/39632D.pdf
 ||||:http://home.gwu.edu/~jreboll/news.htm.
  ||5|:http://home.gwu.edu/~jreboll/news.htm.
 ||5||:http://home.gwu.edu/~jreboll/news.htm.
```

# APPENDIX A DATA SHEET



## Low Cost $\pm 2 g/\pm 10 g$ Dual Axis *i*MEMS® Accelerometers with Digital Output

## ADXL202/ADXL210

2-Axis Acceleration Sensor on a Single IC Chip 2-AXIS ACCELERATION AS WELL AS Dynamic Acceleration

Duty Cycle Output with User Adjustable Period Low Power < 0.6 mA

Faster Response than Electrolytic, Mercury or Thermal

Bandwidth Adjustment with a Single Capacitor Per Axis 5 mg Resolution at 60 Hz Bandwidth +3 V to +5.25 V Single Supply Operation

1000 g Shock Survival

**APPLICATIONS** 2-Axis Tilt Sensing Computer Peripherals Inertial Navigation Seismic Monitoring Vehicle Security Systems Battery Powered Motion Sensing

### GENERAL DESCRIPTION

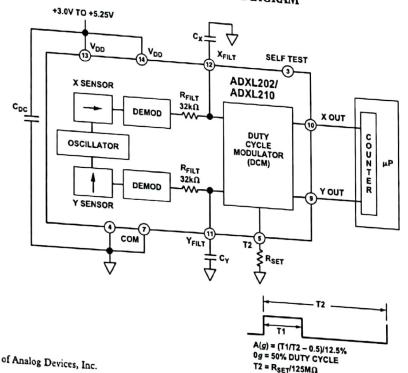
The ADXL202/ADXL210 are low cost, low power, complete 2-axis accelerometers with a measurement range of either  $\pm 2$  g/ $\pm 10$  g. The ADXL202/ADXL210 can measure both dynamic acceleration (e.g., vibration) and static acceleration (e.g.,

The outputs are digital signals whose duty cycles (ratio of pulsewidth to period) are proportional to the acceleration in each of the 2 sensitive axes. These outputs may be measured directly with a microprocessor counter, requiring no A/D converter or glue logic. The output period is adjustable from 0.5 ms to 10 ms via a single resistor ( $R_{SET}$ ). If a voltage output is desired, a voltage output proportional to acceleration is available from the  $X_{FILT}$  and  $Y_{FILT}$  pins, or may be reconstructed by filtering the

The bandwidth of the ADXL202/ADXL210 may be set from 0.01 Hz to 5 kHz via capacitors  $C_X$  and  $C_Y$ . The typical noise floor is 500  $\mu g/\sqrt{Hz}$  allowing signals below 5 mg to be resolved for bandwidths below 60 Hz.

The ADXL202/ADXL210 is available in a hermetic 14-lead Surface Mount CERPAK, specified over the 0°C to +70°C commercial or -40°C to +85°C industrial temperature range.

## FUNCTIONAL BLOCK DIAGRAM



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## DXL202/ADXL210—SPECIFICATIONS ( $T_A = T_{MIN}$ to $T_{MAX}$ , $T_A = +25^{\circ}$ C for J Grade only, $Y_{p0} = +5$ V, $R_{SET} = 125$ k $\Omega$ , Acceleration = 0 g, unless otherwise noted)

| UNEL  |   |                             | SET = 125                              | K12, Acce           | leration = 0                | g, unless                                 | otherwise           | noted)                                  |
|---|---|-----------------------------|--|---------------------|-----------------------------|---|---------------------|---|
|   | Conditions  | ADXL2<br>Min                | 02/JQC/A                               | QC                  | ADXL2                       | 10/JQC/A                                  | QC                  |   |
| arameter INPUT  | Each Axis   | Wilh                        | Тур                                    | Max                 | Min                         | Тур                                       | Max                 | Units                                   |
| Measurement Range I Nonlinearity Alignment Error Alignment Error Transverse Sensitivity 3                                     | Best Fit Straight Line X Sensor to Y Sensor   | ±1.5                        | ±2<br>0.2<br>±1<br>±0.01               |                     | ±8                          | ±10<br>0.2<br>±1<br>±0.01                 |                     | g<br>% of FS<br>Degrees<br>Degrees<br>% |
| ENSITIVITY Duty Cycle per g Sensitivity, Analog Output Temperature Drift <sup>4</sup>   | Each Axis<br>T1/T2 @ +25°C<br>At Pins X <sub>FILT</sub> , Y <sub>FILT</sub><br>Δ from +25°C | 10                          | 12.5<br>312<br>±0.5                    | 15                  | 3.2                         | 4.0<br>100<br>±0.5                        | 4.8                 | %/g<br>mV/g<br>% Rdg                    |
| IERO & BIAS LEVEL  Of Duty Cycle Initial Offset Of Duty Cycle vs. Supply Of Offset vs. Temperature <sup>4</sup>               | Each Axis<br>T1/T2<br>Δ from +25°C  | 25                          | 50<br>±2<br>1.0<br>2.0                 | 75<br>4.0           | 42                          | 50<br>±2<br>1.0<br>2.0                    | 58<br>4.0           | %<br>%/V<br>m <sub>g</sub> °C           |
| NOISE PERFORMANCE<br>Noise Density <sup>5</sup>   | @ +25°C   |                             | 500                                    | 1000                |                             | 500                                       | 1000                | µg/√Hz                                  |
| FREQUENCY RESPONSE 3 dB Bandwidth 3 dB Bandwidth Sensor Resonant Frequency  | Duty Cycle Output At Pins X <sub>FILT</sub> , Y <sub>FILT</sub>                             |                             | 500<br>5<br>10                         |                     |                             | 500<br>5<br>14                            |                     | Hz<br>kHz<br>kHz                        |
| FILTER R <sub>FILT</sub> Tolerance Minimum Capacitance  | 32 kΩ Nominal<br>At X <sub>FILT</sub> , Y <sub>FILT</sub>                                   | 1000                        | ±15                                    |                     | 1000                        | ±15                                       | j.                  | %<br>pF                                 |
| SELF TEST Duty Cycle Change   | Self-Test "0" to "1"  |                             | 10                                     |                     |                             | 10  |                     | %                                       |
| DUTY CYCLE OUTPUT STAGE  F_SET F_SET Tolerance Output High Voltage Output Low Voltage T2 Drift vs. Temperature Rise/Fall Time | R <sub>SET</sub> = 125 kΩ<br>I = 25 μΑ<br>I = 25 μΑ   | 0.7<br>V <sub>s</sub> - 200 | MΩ/R <sub>SET</sub><br>mV<br>35<br>200 | 1.3                 | 0.7<br>V <sub>s</sub> - 200 | 5 MΩ/R <sub>SE</sub><br>0 mV<br>35<br>200 | 200                 | kHz<br>mV<br>mV<br>ppm/°C<br>ns         |
| POWER SUPPLY Operating Voltage Range Specified Performance Quiescent Supply Current   |   | 3.0<br>4.75                 | 0.6<br>C <sub>FILT</sub> + 0           | 5.25<br>5.25<br>1.0 | 2.7<br>4.75                 | 0.6<br>0 C <sub>FILT</sub> +              | 5.25<br>5.25<br>1.0 | V<br>V<br>mA<br>ms                      |
| Turn-On Time <sup>6</sup> IEMPERATURE RANGE Operating Range Specified Performance   | JQC<br>AQC  | 0<br>-40                    |  | +70<br>+85          | 0<br>-40                    |   | +70<br>+85          | °C                                      |

NOTES

For all combinations of offset and sensitivity variation.

Alignment error is specified as the angle between the true and indicated axis of sensitivity errors.

Inawere sensitivity is the algebraic sum of the alignment and the inherent sensitivity errors.

Specification references in parameter from its initial at +25 °C to its worst the sensitivity is the algebraic sum of the alignment and the inherent sensitivity is the algebraic sum of the alignment and the inherent sensitivity is the algebraic sum of the alignment and the inherent sensitivity is the algebraic sum of the alignment and the inherent sensitivity.

In any one is specified as the angle between the true and indicated axis of selectivity errors.

Specification refers to the maximum change in parameter from its initial at +25°C to its worst case value at TMIN to TMAX.

Noise density (µg/√Hz) is the average noise at any frequency in the bandwidth of the part.

Car in µF. Addition of filter capacitor will increase turn on time. Please see the Application section on power cycling.

All min and max specifications.

All min and max specifications are guaranteed. Typical specifications are not tested or guaranteed.

Specifications subject to change without notice.

| AFERICAN (Any Axis, Unpowered for 0.5 ms)  |
|--|
| June Unpowered for 0.5 ms) 1000 g  |
| Any Axis, Compered for 0.5 ms) 500 g   |
| Any Axis, I diversify a contract of the contra |
| AN ERCOND  |
| Ve Coont Duration  |
| Short Circuit  |
| Short Circuit Duration  Indefinite  Fin to Common)  Temperature  |
| (A) Find   |
| Temperature 11500C   |

Of to +120°C to +150°C

This is a street rating only the formation of the desire. This is a street rating only the formation of the desire. and a three or any other conditions above those in a the desire at these or any other conditions above those indicated in the operational string of this specification is not implied. Exposure to absolute maximum rating eminims for extended periods may affect device reliability.

Drops onto hard surfaces can cause shocks of greater than 1000 g and exceed the absolute maximum rating of the device. Care should be exercised in handling to avoid damage.

### PIN FUNCTION DESCRIPTIONS

| Fin                 | Name   | Description   |
|---------------------|--|---|
| 1 1 1 1 1 2 1 3 1 4 | NC V <sub>TP</sub> ST COM T2 NC COM NC Y <sub>OUT</sub> X <sub>OUT</sub> Y <sub>FILT</sub> X <sub>FILT</sub> V <sub>DD</sub> V <sub>DD</sub> | No Connect Test Point, Do Not Connect Self Test Common Connect R <sub>SET</sub> to Set T2 Period No Connect Common No Connect Y Axis Duty Cycle Output X Axis Duty Cycle Output Connect Capacitor for Y Filter Connect Capacitor for X Filter +3 V to +5.25 V, Connect to 14 +3 V to +5.25 V, Connect to 13 |

### ACKAGE CHARACTERISTICS

| ACKAGE CHARACTI      | θ <sub>IC</sub> | Device Weight |
|----------------------|-----------------|---------------|
| ackage $\theta_{JA}$ | 20°C/V          | 5 Grams       |
| 4-Lead CERPAK 11     | 0°C/W 30°C/W    |               |

#### PIN CONFIGURATION

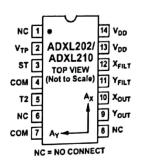


Figure 1 shows the response of the ADXL202 to the Earth's gravitational field. The output values shown are nominal. They are presented to show the user what type of response to expect from each of the output pins due to changes in orientation with respect to the Earth. The ADXL210 reacts similarly with output changes appropriate to its scale.

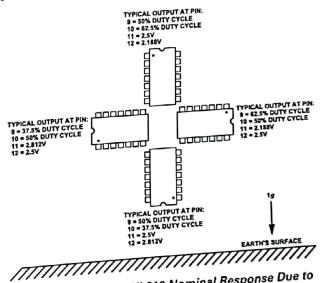


Figure 1. ADXL202/ADXL210 Nominal Response Due to Gravity

### ORDERING GUIDE

|   |                                   | Temperature   | Package<br>Description   | Package<br>Option                |
|---|-----------------------------------|---|--|----------------------------------|
| Model  ADXL202JQC  ADXL202AQC  ADXL210JQC  ADXL210AQC | £ Range<br>±2<br>±2<br>±10<br>±10 | Range  0°C to +70°C  -40°C to +85°C  0°C to +70°C  -40°C to +85°C | 14-Lead CERPAK<br>14-Lead CERPAK<br>14-Lead CERPAK<br>14-Lead CERPAK | QC-14<br>QC-14<br>QC-14<br>QC-14 |
| ADALL   |                                   |   |  |                                  |

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily ESD (electrostatic discharge) seasons to the equipment and can discharge without detection.

Escumulate on the human body and test equipment and can discharge without detection. Although the ADXL202/ADXL210 features proprietary ESD protection circuitry, permanent Although the ADXL 2022 ADXL 2022 projection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper damage may occur on the recommended to avoid performance degradation or leave the recommended to avoid performance degradation d damage may occur on devices adopted to avoid performance degradation or loss of functionality.



## <sub>IDXL2</sub>02/ADXL210

## The second of the second content of the sec

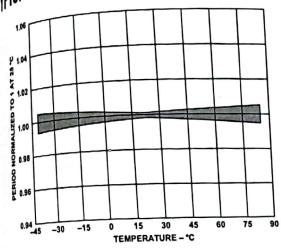


Figure 2. Normalized DCM Period (T2) vs. Temperature

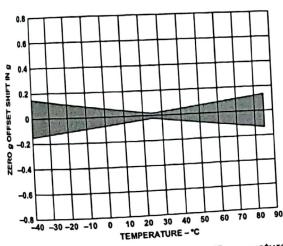


Figure 3. Typical Zero g Offset vs. Temperature

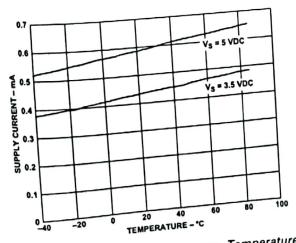


Figure 4. Typical Supply Current vs. Temperature

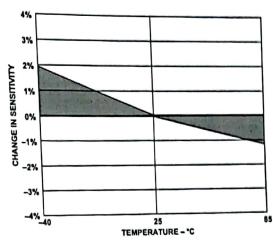


Figure 5. Typical X Axis Sensitivity Drift Due to Temperature

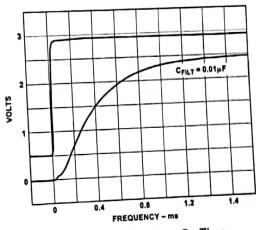


Figure 6. Typical Turn-On Time

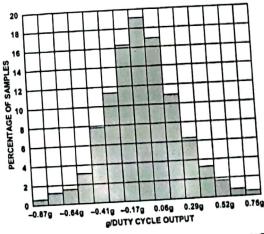


Figure 7. Typical Zero g Distribution at +25°C

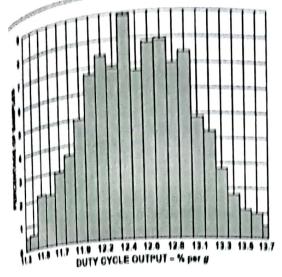


Figure 8. Typical Sensitivity per g at +25°C

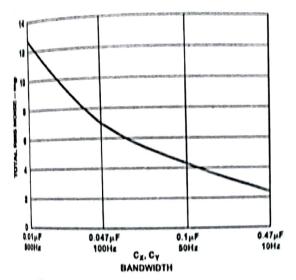


Figure 9. Typical Noise at X<sub>FILT</sub> Output

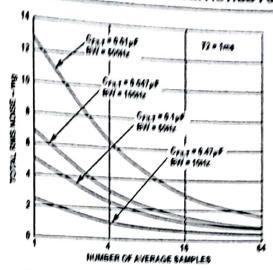


Figure 10. Typical Noise at Digital Outputs

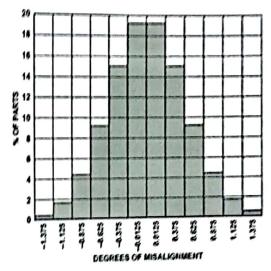


Figure 11. Rotational Die Alignment

## 1202/ADXL210

NS Length of the "on" portion of the cycle.

Length of the total cycle.

Ratio of the "on" time (T1) of the cycle to the total orde (T2). Defined as T1/T2 for the Angele (T2). Rand of 2). Defined as T1/T2 for the ADXL202/

Time period of the "on" pulse. Defined as T1 for the ADXL202/ADXL210.

ORY OF OPERATION DXL202/ADXL210 are complete dual axis acceleration truent systems on a single monolithic IC. They contain a armen surface-micromachined sensor and signal conditioninding to implement an open loop acceleration measureachirecture. For each axis, an output circuit converts the signal to a duty cycle modulated (DCM) digital signal be decoded with a counter/timer port on a micropror. The ADXL202/ADXL210 are capable of measuring positive and negative accelerations to a maximum level of w±10 g. The accelerometer measures static acceleration ssuch as gravity, allowing it to be used as a tilt sensor.

sensor is a surface micromachined polysilicon structure on top of the silicon wafer. Polysilicon springs suspend the mme over the surface of the wafer and provide a resistance Macceleration forces. Deflection of the structure is meadusing a differential capacitor that consists of independent plates and central plates attached to the moving mass. The plates are driven by 180° out of phase square waves. An tration will deflect the beam and unbalance the differential citor, resulting in an output square wave whose amplitude oportional to acceleration. Phase sensitive demodulation inques are then used to rectify the signal and determine the

Output of the demodulator drives a duty cycle modulator M) stage through a 32 k $\Omega$  resistor. At this point a pin is lable on each channel to allow the user to set the signal dwidth of the device by adding a capacitor. This filtering Toyes measurement resolution and helps prevent aliasing.

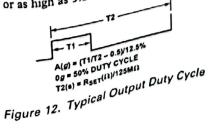
Theing low-pass filtered, the analog signal is converted to a Veycle modulated signal by the DCM stage. A single resistor the period of the period for a complete cycle (T2), which can be set beth 0.5 ms and 10 ms (see Figure 12). A 0 g acceleration duces a receleration sign duces a nominally 50% duty cycle. The acceleration signal be determined by the deter be determined by measuring the length of the T1 and T2

tes with a court les with a counter/timer or with a polling loop using a low

analog output voltage can be obtained either by buffering the al from the XFILT and YFILT pin, or by passing the duty cycle that through an RC State Construct the dc value. through an RC filter to reconstruct the dc value.

\*\* ADXL202/ADXL210 will operate with supply voltages as yas 3.0 V

vas 3.0 V or as high as 5.25 V.



#### **APPLICATIONS**

#### POWER SUPPLY DECOUPLING

For most applications a single 0.1 µF capacitor, CDC, will adequately decouple the accelerometer from signal and noise on the power supply. However, in some cases, especially where digital devices such as microcontrollers share the same power supply, digital noise on the supply may cause interference on the ADXL202/ ADXL210 output. This is often observed as a slowly undulating fluctuation of voltage at XFILT and YFILT. If additional decoupling is needed, a 100  $\Omega$  (or smaller) resistor or ferrite beads, may be inserted in the ADXL202/ADXL210's supply line.

### DESIGN PROCEDURE FOR THE ADXL202/ADXL210

The design procedure for using the ADXL202/ADXL210 with a duty cycle output involves selecting a duty cycle period and a filter capacitor. A proper design will take into account the application requirements for bandwidth, signal resolution and acquisition time, as discussed in the following sections.

The ADXL202/ADXL210 have two power supply (V<sub>DD</sub>) Pins: 13 and 14. These two pins should be connected directly together.

The ADXL202/ADXL210 have two commons, Pins 4 and 7. These two pins should be connected directly together and Pin 7 grounded.

-6-

This pin is to be left open; make no connections of any kind to this pin.

### Decoupling Capacitor CDC

A 0.1  $\mu F$  capacitor is recommended from  $V_{DD}$  to COM for power supply decoupling.

The ST pin controls the self-test feature. When this pin is set to  $V_{\rm DD}$ , an electrostatic force is exerted on the beam of the accelerometer. The resulting movement of the beam allows the user to test if the accelerometer is functional. The typical change in output will be 10% at the duty cycle outputs (corresponding to 800 mg). This pin may be left open circuit or connected to common in normal use.

The ADXL202/ADXL210's digital output is a duty cycle modulator. Acceleration is proportional to the ratio T1/T2. The nominal output of the ADXL202 is:

0 g = 50% Duty Cycle

Scale factor is 12.5% Duty Cycle Change per g

The nominal output of the ADXL210 is:

0 g = 50% Duty Cycle

## Scale factor is 4% Duty Cycle Change per g

These nominal values are affected by the initial tolerance of the device including zero g offset error and sensitivity error.

T2 does not have to be measured for every measurement cycle. It need only be updated to account for changes due to temperature, (a relatively slow process). Since the T2 time period is shared by both X and Y channels, it is necessary only to measure it on one channel of the ADXL202/ADXL210. Decoding algorithms for various microcontrollers have been developed. Consult the appropriate Application Note.

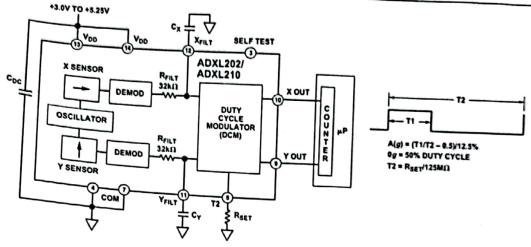


Figure 13. Block Diagram

## Setting the Bandwidth Using $C_X$ and $C_Y$

The ADXL202/ADXL210 have provisions for bandlimiting the X<sub>FILT</sub> and Y<sub>FILT</sub> pins. Capacitors must be added at these pins to implement low-pass filtering for antialiasing and noise reduction. The equation for the 3 dB bandwidth is:

$$F_{-3\,dB} = \frac{1}{\left(2\,\pi\,(32\,k\Omega)\times C(x,y)\right)}$$

or, more simply, 
$$F_{-3dB} = \frac{5 \,\mu F}{C_{(X,Y)}}$$

The tolerance of the internal resistor (R<sub>FILT</sub>), can vary as much as  $\pm 25\%$  of its nominal value of 32 k $\Omega$ ; so the bandwidth will vary accordingly. A minimum capacitance of 1000 pF for C(X, Y) is required in all cases.

Table I. Filter Capacitor Selection,  $C_X$  and  $C_Y$ 

|                                    | , -A C                          |
|------------------------------------|---------------------------------|
| Bandwidth                          | Capacitor<br>Value              |
| 10 Hz<br>50 Hz<br>100 Hz<br>200 Hz | 0.47 µF<br>0.10 µF<br>0.05 µF   |
| 500 Hz<br>5 kHz                    | 0.027 µF<br>0.01 µF<br>0.001 µF |

### Setting the DCM Period with R<sub>SET</sub>

The period of the DCM output is set for both channels by a single resistor from R<sub>SET</sub> to ground. The equation for the period

$$T2 = \frac{R_{SET} (\Omega)}{125 M\Omega}$$

A 125 kΩ resistor will set the duty cycle repetition rate to ap-Proximately 1 kHz, or 1 ms. The device is designed to operate at duty cycle periods between 0.5 ms and 10 ms.

Table II. Resistor Values to Set T2

| T2    | R <sub>SET</sub> |
|-------|------------------|
| 1 ms  | 125 kΩ           |
| 2 ms  | 250 kΩ           |
| 5 ms  | 625 kΩ           |
| 10 ms | 1.25 ΜΩ          |

Note that the  $R_{\text{SET}}$  should always be included, even if only an analog output is desired. Use an R<sub>SET</sub> value between 500  $k\Omega$ and 2 M $\Omega$  when taking the output from  $X_{FILT}$  or  $Y_{FILT}$ . The R<sub>SET</sub> resistor should be place close to the T2 Pin to minimize parasitic capacitance at this node.

#### Selecting the Right Accelerometer

For most tilt sensing applications the ADXL202 is the most appropriate accelerometer. Its higher sensitivity (12.5%/g allows the user to use a lower speed counter for PWM decoding while maintaining high resolution. The ADXL210 should be used in applications where accelerations of greater than  $\pm 2$  g are expected.

#### MICROCOMPUTER INTERFACES

The ADXL202/ADXL210 were specifically designed to work with low cost microcontrollers. Specific code sets, reference designs, and application notes are available from the factory. This section will outline a general design procedure and discuss the various trade-offs that need to be considered.

The designer should have some idea of the required performance of the system in terms of:

Resolution: the smallest signal change that needs to be detected. Bandwidth: the highest frequency that needs to be detected. Acquisition Time: the time that will be available to acquire the signal on each axis.

These requirements will help to determine the accelerometer bandwidth, the speed of the microcontroller clock and the length of the T2 period.

When selecting a microcontroller it is helpful to have a counter timer port available. The microcontroller should have provisions for software calibration. While the ADXL202/ADXL210 are highly accurate accelerometers, they have a wide tolerance for

initial offset. The easiest way to null this offset is with a calibration factor saved on the microcontroller or by a user calibration for zero g. In the case where the offset is calibrated during manufacture, there are several options, including external EEPROM and microcontrollers with "one-time programmable" features.

## DESIGN TRADE-OFFS FOR SELECTING FILTER CHARACTERISTICS: THE NOISE/BW TRADE-OFF

The accelerometer bandwidth selected will determine the measurement resolution (smallest detectable acceleration). Filtering can be used to lower the noise floor and improve the resolution of the accelerometer. Resolution is dependent on both the analog filter bandwidth at X<sub>FILT</sub> and Y<sub>FILT</sub> and on the speed of the microcontroller counter.

The analog output of the ADXL202/ADXL210 has a typical bandwidth of 5 kHz, much higher than the duty cycle stage is capable of converting. The user must filter the signal at this point to limit aliasing errors. To minimize DCM errors the analog bandwidth should be less than 1/10 the DCM frequency. Analog bandwidth may be increased to up to 1/2 the DCM frequency in many applications. This will result in greater dynamic error generated at the DCM.

The analog bandwidth may be further decreased to reduce noise and improve resolution. The ADXL202/ADXL210 noise has the characteristics of white Gaussian noise that contributes equally at all frequencies and is described in terms of  $\mu g$  per root Hz; i.e., the noise is proportional to the square root of the bandwidth of the accelerometer. It is recommended that the user limit bandwidth to the lowest frequency needed by the application, to maximize the resolution and dynamic range of the accelerometer.

With the single pole roll-off characteristic, the typical noise of the ADXL202/ADXL210 is determined by the following equation:

Noise (rms) = 
$$\left(500 \, \mu g / \sqrt{Hz}\right) \times \left(\sqrt{BW \times 1.5}\right)$$

At 100 Hz the noise will be:

Noise 
$$(rms) = (500 \,\mu g/\sqrt{Hz}) \times (\sqrt{100 \times (1.5)}) = 6.12 \,mg$$

Often the peak value of the noise is desired. Peak-to-peak noise can only be estimated by statistical methods. Table III is useful for estimating the probabilities of exceeding various peak values, given the rms value.

Table III. Estimation of Peak-to-Peak Noise

| Nominal Peak-to-Peak<br>Value | % of Time that Noise<br>Will Exceed Nominal<br>Peak-to-Peak Value |
|-------------------------------|---|
| 2.0 × rms                     | 32%   |
| $4.0 \times \text{rms}$       | 4.6%  |
| $6.0 \times rms$              | 0.27%   |
| $8.0 \times \text{rms}$       | 0.006%  |

The peak-to-peak noise value will give the best estimate of the uncertainty in a single measurement.

Table IV gives typical noise output of the ADXL202/ADXL210 for various  $C_X$  and  $C_Y$  values.

Table IV. Filter Capacitor Selection,  $C_{\boldsymbol{x}}$  and  $C_{\boldsymbol{y}}$ 

|  |  | , , ,   |   |
|--|--|---|---|
| Bandwidth                                    | C <sub>x</sub> , C <sub>y</sub>                      | rms Noise                                       | Peak-to-Peak Noise<br>Estimate 95%<br>Probability (rms × 4) |
| 10 Hz<br>50 Hz<br>100 Hz<br>200 Hz<br>500 Hz | 0.47 μF<br>0.10 μF<br>0.05 μF<br>0.027 μF<br>0.01 μF | 1.9 mg<br>4.3 mg<br>6.1 mg<br>8.7 mg<br>13.7 mg | 7.6 mg<br>17.2 mg<br>24.4 mg<br>35.8 mg<br>54.8 mg          |

## CHOOSING T2 AND COUNTER FREQUENCY: DESIGN TRADE-OFFS

The noise level is one determinant of accelerometer resolution. The second relates to the measurement resolution of the counter when decoding the duty cycle output.

The ADXL202/ADXL210's duty cycle converter has a resolution of approximately 14 bits; better resolution than the accelerometer itself. The actual resolution of the acceleration signal is, however, limited by the time resolution of the counting devices used to decode the duty cycle. The faster the counter clock, the higher the resolution of the duty cycle and the shorter the T2 period can be for a given resolution. The following table shows some of the trade-offs. It is important to note that this is the resolution due to the microprocessors's counter. It is probable that the accelerometer's noise floor may set the lower limit on the resolution, as discussed in the previous section.

Table V. Trade-Offs Between Microcontroller Counter Rate, T2 Period and Resolution of Duty Cycle Modulator

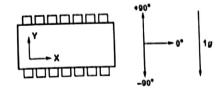
| T2 (ms) | R <sub>SET</sub><br>(kΩ) | ADXL202/<br>ADXL210<br>Sample<br>Rate | Counter-<br>Clock<br>Rate<br>(MHz) | Counts<br>per T2<br>Cycle | Counts<br>per g | Resolution<br>(mg) |
|---------|--------------------------|---------------------------------------|------------------------------------|---------------------------|-----------------|--------------------|
| 1.0     | 124                      | 1000                                  | 2.0                                | 2000                      | 250             | 4.0                |
| 1.0     | 124                      | 1000                                  | 1.0                                | 1000                      | 125             | 8.0                |
| 1.0     | 124                      | 1000                                  | 0.5                                | 500                       | 62.5            | 16.0               |
| 5.0     | 625                      | 200                                   | 2.0                                | 10000                     | 1250            | 0.8                |
| 5.0     | 625                      | 200                                   | 1.0                                | 5000                      | 625             | 1.6                |
| 5.0     | 625                      | 200                                   | 0.5                                | 2500                      | 312.5           | 3.2                |
| 10.0    | 1250                     | 100                                   | 2.0                                | 20000                     | 2500            | 0.4                |
| 10.0    | 1250                     | 100                                   | 1.0                                | 10000                     | 1250            | 0.8                |
| 10.0    | 1250                     | 100                                   | 0.5                                | 5000                      | 625             | 1.6                |

## STRATEGIES FOR USING THE DUTY CYCLE OUTPUT STRATION NOT CONTROLLERS

WITH out outlining various strategies for using the duty Application with low cost microcontrollers are available from acceptance. the factory.

## USING THE ADXL202/ADXL210 AS A DUAL AXIS TILT

SENSOR
One of the most popular applications of the ADXL202/ADXL210 One of the measurement. An accelerometer uses the force of gravity is in input vector to determine orientation of an object in space. An accelerometer is most sensitive to tilt when its sensitive axis An acceptance of gravity, i.e., parallel to the specification its sensitivity to changes in earth shighest. When the accelerometer is oriented on axis to gravity, i.e., near its +1 g or -1 g reading, the change in output acceleration per degree of tilt is negligible. When the accelerometer is perpendicular to gravity, its output will change nearly 17.5 mg per degree of tilt, but at 45° degrees it is changing only at 12.2 mg per degree and resolution declines. The following table illustrates the changes in the X and Y axes as the device is tilted ±90° through gravity.



|   | X OUTP   | UT  | Y OUTPUT  |  |
|---|--|---|---|--|
| X AXIS<br>ORIENTATION<br>TO HORIZON (*)                             | X OUTPUT ( <i>g</i> )  | Δ PER<br>DEGREE OF<br>TILT (mg)                         | Υ Ο <b>υ</b> ΤΡ <b>υ</b> Τ ( <i>g</i> )   | Δ PER<br>DEGREE OF<br>TILT (mg)  |
| -90<br>-75<br>-60<br>-45<br>-30<br>-15<br>0<br>15<br>30<br>45<br>60 | -1.000<br>-0.966<br>-0.866<br>-0.707<br>-0.500<br>-0.259<br>0.000<br>0.259<br>0.500<br>0.707<br>0.866<br>0.966 | -0.2 4.4 8.6 12.2 15.0 16.8 17.5 16.9 15.2 12.4 8.9 4.7 | 0.000<br>0.259<br>0.500<br>0.707<br>0.866<br>0.966<br>1.000<br>0.966<br>0.866<br>0.707<br>0.500 | 17.5<br>16.9<br>15.2<br>12.4<br>8.9<br>4.7<br>0.2<br>-4.4<br>-8.6<br>-12.2<br>-15.0<br>-16.8 |
| 90  | 1.000  | 0.2   | 0.000   | -17.5  |

Figure 14. How the X and Y Axes Respond to Changes in Tilt

#### A DUAL AXIS TILT SENSOR: CONVERTING ACCELERATION TO TILT

When the accelerometer is oriented so both its X and Y axes are parallel to the earth's surface it can be used as a two axis tilt sensor with a roll and a pitch axis. Once the output signal from the accelerometer has been converted to an acceleration that varies between -1 g and +1 g, the output tilt in degrees is calculated as follows:

Pitch = 
$$ASIN (Ax/1 g)$$
  
 $Roll = ASIN (Ay/1 g)$ 

Be sure to account for overranges. It is possible for the accelerometers to output a signal greater than ±1 g due to vibration, shock or other accelerations.

#### MEASURING 360° OF TILT

It is possible to measure a full 360° of orientation through gra ity by using two accelerometers oriented perpendicular to one another (see Figure 15). When one sensor is reading a mazimum change in output per degree, the other is at its minimus

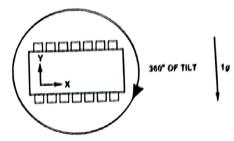


Figure 15. Using a Two-Axis Accelerometer to Meas 360° of Tilt

USING THE ANALOG OUTPUT USING 111202/ADXL210 was specifically designed for use with The ADAL designed for use with its digital outputs, but has provisions to provide analog outputs ss well.

Duty Cycle Filtering Duty Of the polymer of the duty An analog output can be reconstructed by filtering the duty An analog the duty cycle output. This technique requires only passive components. The duty cycle period (T2) should be set to 1 ms. An RC filter The day 3 dB point at least a factor of 10 less than the duty cycle with a 3 dB point at least a factor of 10 less than the duty cycle frequency is connected to the duty cycle output. The filter resisfrequency for should be no less than 100 kΩ to prevent loading of the tor should stage. The analog output signal will be ratiometric to the supply voltage. The advantage of this method is an output scale factor of approximately double the analog output. Its disadvantage is that the frequency response will be lower than when using the XFILT, YFILT output.

XFILT, YFILT Output The second method is to use the analog output present at the  $X_{FILT}$  and  $Y_{FILT}$  pin. Unfortunately, these pins have a 32 k $\Omega$ output impedance and are not designed to drive a load directly. An op amp follower may be required to buffer this pin. The advantage of this method is that the full 5 kHz bandwidth of the accelerometer is available to the user. A capacitor still must be added at this point for filtering. The duty cycle converter should be kept running by using  $R_{SET}$  <10 M $\Omega$ . Note that the accelerometer offset and sensitivity are ratiometric to the supply voltage. The offset and sensitivity are nominally:

2.5 V at +5 V  $0 g \text{ Offset} = V_{DD}/2$ ADXL202 Sensitivity =  $(60 \text{ mV} \times \text{V}_S)/g$ 300 mV/g at +5 V,  $V_{DD}$ 100 mV/g at +5 V,  $V_{DD}$ ADXL210 Sensitivity =  $(20 \text{ mV} \times \text{V}_s)/g$ 

#### USING THE ADXL202/ADXL210 IN VERY LOW POWER APPLICATIONS

An application note outlining low power strategies for the ADXL202/ADXL210 is available. Some key points are presented here. It is possible to reduce the ADXL202/ADXL210's average current from 0.6 mA to less than 20 µA by using the following techniques:

- 1. Power Cycle the accelerometer.
- 2. Run the accelerometer at a Lower Voltage, (Down to 3 V).

#### Power Cycling with an External A/D

Depending on the value of the X<sub>FILT</sub> capacitor, the ADXL202/ ADXL210 is capable of turning on and giving a good reading in 1.6 ms. Most microcontroller based A/Ds can acquire a reading in another 25 µs. Thus it is possible to turn on the ADXL202/ ADXL210 and take a reading in <2 ms. If we assume that a 20 Hz sample rate is sufficient, the total current required to take 20 samples is 2 ms × 20 samples/s × 0.6 mA = 24  $\mu$ A average current. Running the part at 3 V will reduce the supply current from 0.6 mA to 0.4 mA, bringing the average current down to 16 µA.

The A/D should read the analog output of the ADXL202/ ADXL210 at the X<sub>FILT</sub> and Y<sub>FILT</sub> pins. A buffer amplifier is recommended, and may be required in any case to amplify the analog output to give enough resolution with an 8-bit to 10-bit converter.

#### Power Cycling When Using the Digital Output

An alternative is to run the microcontroller at a higher clock rate and put it into shutdown between readings, allowing the use of the digital output. In this approach the ADXL202/ ADXL210 should be set at its fastest sample rate ( $\Gamma 2 = 0.5 \text{ ms}$ ), with a 500 Hz filter at  $X_{\rm PHT}$  and  $Y_{\rm PHT}$ . The concept is to acquire a reading as quickly as possible and then shut down the ADXL202/ADXL210 and the microcontroller until the next sample is needed.

In either of the above approaches, the ADXL202/ADXL210 can be turned on and off directly using a digital port pin on the microcontroller to power the accelerometer without additional components. The port should be used to switch the common pin of the accelerometer so the port pin is "pulling down."

#### CALIBRATING THE ADXL202/ADXL210

The initial value of the offset and scale factor for the ADXL202/ ADXL210 will require calibration for applications such as tilt measurement. The ADXL202/ADXL210 architecture has been designed so that these calibrations take place in the software of the microcontroller used to decode the duty cycle signal. Calibration factors can be stored in EEPROM or determined at turn-on and saved in dynamic memory.

For low g applications, the force of gravity is the most stable, accurate and convenient acceleration reference available. A reading of the 0 g point can be determined by orientating the device parallel to the earth's surface and then reading the output.

A more accurate calibration method is to make a measurements at +1 g and -1 g. The sensitivity can be determined by the two measurements.

To calibrate, the accelerometer's measurement axis is pointed directly at the earth. The 1 g reading is saved and the sensor is turned 180° to measure -1 g. Using the two readings, the sensitivity is:

Let A = Accelerometer output with axis oriented to +1 g Let B = Accelerometer output with axis oriented to -1 g then: Sensitivity = [A - B]/2 g

For example, if the +1 g reading (A) is 55% duty cycle and the -1 g reading (B) is 32% duty cycle, then:

Sensitivity = [55% - 32%]/2 g = 11.5%/g

These equations apply whether the output is analog, or duty

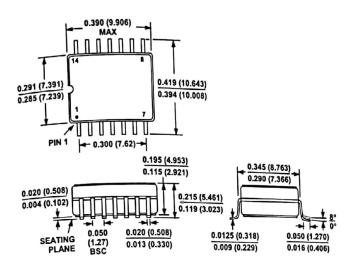
Application notes outlining algorithms for calculating acceleration from duty cycle and automated calibration routines are available from the factory.

REV. E -10-

### OUTLINE DIMENSIONS

Dimensions shown in inches and (mm).

#### 14-Lead CERPAK (QC-14)



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## NI 6034E/6035E/6036E Family Specifications

This document lists the I/O terminal summary and specifications for the devices that make up the N16034E/6035E/6036E family

- NI PCI-6034E
- NI PCI-6035E
- NI DAQCard-6036E
- NI PCI-6036E

#### I/O Terminal Summary



Note With NI-DAQmx, National Instruments revised its terminal names so they are easier to understand and more consistent among NI hardware and software products. The revised terminal names used in this document are usually similar to the names they replace. For a complete list of Traditional NI-DAQ (Legacy) terminal names and their NI-DAQmx equivalents, refer to Terminal Name Equivalents of the E Series Help.

Table 1. I/O Terminals

| Terminal Name     | Terminal<br>Type and<br>Direction | Impedance<br>Input/<br>Output        | Protection<br>(V) On/Off   | Source<br>(mA at V) | Sink<br>(mA at V) | Rise<br>Time<br>(ns) | Bias    |
|-------------------|-----------------------------------|--------------------------------------|----------------------------|---------------------|-------------------|----------------------|---------|
| A1<015>           | Al                                | 100 GΩ in parallel with 100 pF       | 25/15                      | _                   | -                 |                      | ±200 pA |
| AI SENSE          | Al                                | 100 GΩ in<br>parallel<br>with 100 pF | 25/15                      | _                   | _                 | _                    | ±200 pA |
| AI GND            | _                                 | _                                    |                            | _                   | _                 | name.                | -       |
| AO 0†             | AO                                | 0.1 Ω                                | Short-circuit<br>to ground | 5 at 10             | 5 at -10          | -                    | _       |
| AO 1 <sup>†</sup> | AO                                | 0.1 Ω                                | Short-circuit<br>to ground | 5 at 10             | 5 at -10          |                      | 1000    |
| AO GND            | _                                 | _                                    | _                          | _                   | _                 | ****                 | Comma   |
| D GND             | _                                 | _                                    | _                          | _                   | _                 |                      | Name .  |



Table 1. 10 formosis (Contraed)

| Names Vann   | Distriction<br>Distriction<br>Distriction<br>Distriction | Impedance<br>Imput:<br>Online | Protection<br>(V) On/Off | vinuit.                           | Sink<br>(mA at V)  | Rise<br>Time<br>(us) | Htas     |
|--|--|-------------------------------|--------------------------|-----------------------------------|--|----------------------|----------|
| Haming   |  | 93.63                         | Shar-vicus<br>to ground  | 1 A flood                         | The Control of Control | -                    | 10.73    |
| Mark &   | 1980   | -                             | Ver+0.5                  | 13 at<br>(V <sub>CC</sub> = 0.4)  | 24 at 0.4  | 1,1                  | 50 kO pu |
| MINN DEAMS.  | 180  |                               | 700                      | 3.5 at<br>(V <sub>CC</sub> = 0.4) | S at 0.4   | 1,5                  | 50 kΩ pu |
| ELTSTHINE.   | 100  | _                             | Vite.                    | 3.5 at<br>(V <sub>CC</sub> = 0.4) | S at 0.4   | 1.3                  | 50 kΩ p4 |
| MAN'<br>(Alstart Irki)   | 080  | -                             | Ver+0.5                  | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 5 at 0.4   | 1.5                  | 50 kΩ pu |
| (Alstant<br>Mal/<br>(Alstatiski)   | DIO  | -                             | Ver+0.5                  | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 5 21 0.4   | 1.5                  | 50 kΩ pu |
| MASH<br>MONVCLK)*  | DIO  | -                             | Vec + 0.5                | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 5 at 0.4   | 1.5                  | 50 kΩ pu |
| MCONTENTS OF STATE OF | DIO  | -                             | V <sub>cc</sub> + 0.5    | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 3 at 0.4   | 1.5                  | 50 kΩ pu |
| MACTE I GATE   | Dio  |                               | V <sub>CC</sub> + 0.3    | 3.5 at $(V_{CC} - 0.4)$           | 5 # 0.4  | 1.5                  | 50 kΩ pu |
| CTRIOUT  | 100  | -                             | _                        | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 5 at 0.4   | 1.5                  | 50 kΩ pu |
| PF1.5/   | DIO  |                               | Vec + 0.5                | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 5 at 0.4   | 1.5                  | 50 kΩ pu |
| (AO SAMP CLK)*   | DIO  | _                             | Vec + 0.5                | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 5 at 0.4   | 1.5                  | 50 kΩ ps |
| (AO START TRIG)  | DIO  | -                             | Vec + 0.5                | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 5#0.4  | 1.5                  | 50 kΩ p  |
| (ALSAMP CLK) PFLS/   | DIO  | -                             | Vec + 0.5                | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 5 at 0.4   | 1.5                  | 50 kΩ p  |
| CTR 0 SOURCE   | D10  |                               | V <sub>cc</sub> + 0.5    | 3.5 at<br>(V <sub>CC</sub> = 0.4) | 5 at 0.4   | 1.5                  | 50 kΩp   |
| CTR 0 GATE   | DO   | -                             | _                        | 3.5 at<br>(Vcc - 0.4)             | 5 21 0.4   | 1.5                  | 50 kΩ į  |

Table 1. I/O Terminals (Continued)

| Company of the State of the Sta | The second second second      | a reminale (C)                                      | intinued)  |   |   |  |
|--|-------------------------------|---|--|---|---|--|
| Terminal<br>Type and<br>Direction  | Impedance<br>Input/<br>Output | Protection<br>(V) On/Off                            | Source<br>(mA at V)  | Sink<br>(mA at V)   | Rise<br>Time<br>(ns)  | Blas   |
| DO   | Pi-s                          | Princip   | 3.5 at (V <sub>CC</sub> = 0.4)                                 | 5 at 0.4  | 1.5   | 50 kΩ pu   |
|  | Type and<br>Direction         | Terminal Impedance Type and Input/ Direction Output | Terminal Impedance Type and Input/ Direction Output (V) On/Off | Type and Direction Output Protection (V) On/Off Source (mA at V)  DO 3.5 at | Terminal Type and Direction Output Protection (V) On/Off Source (mA at V)  DO 3.5 at 5 at 0.4 | Terminal Type and Direction Output Protection (V) On/Off Source (mA at V) (mA at V)  DO Source (mA at V) (mA at V) (ns)  3.5 at 5 at 0.4 1.5 |

<sup>·</sup> Indicates active low.

Al = Analog Input

DIO = Digital Input/Output

pu = pull-up

AO = Analog Output

DO = Digital Output

Note: The tolerance on the 50 k $\Omega$  pull-up resistors is large. Actual value might range between 17 k $\Omega$  and 100 k $\Omega$ .

## Specifications

The following specifications are typical at 25 °C unless otherwise noted.

### **Analog Input**

### Input Characteristics

Number of channels ...... 16 single-ended or 8 differential (software-selectable per channel)

Type of A/D converter (ADC)...... Successive approximation

Resolution ...... 16 bits, 1 in 65,536

Max sampling rate .......200 kS/s guaranteed

Input signal ranges

| Range<br>(Software-Selectable) | Bipolar Input Range |
|--------------------------------|---------------------|
| 20 V                           | ±10 V               |
| 10 V                           | ±5 V                |
| 1 V                            | ±500 mV             |
| 100 mV                         | ±50 mV              |

Input coupling ...... DC

Max working voltage

(signal + common mode) ...... Each input should remain within ±11 V of ground

#### Overvoltage protection

| Signal             | Powered<br>On (V) | Powered<br>Off (V) |
|--------------------|-------------------|--------------------|
| AI <015>, AI SENSE | ±25               | ±15                |

FIFO buffer size

NI DAQCard-6036E ......1,024 samples (S)

NI 6034E, NI 6035E,

NI PCI-6036E ......512 S

DMA (PCI only)

Channels.....1

Data sources/destinations......Analog input, analog output, counter/timer 0, or counter/timer 1

Data transfers......Direct memory access (DMA)1, interrupts, programmed I/O

DMA1 modes......Scatter-gather (single transfer, demand transfer)

Configuration memory size.....512 words

NI 6035E/6036E only,

<sup>&</sup>lt;sup>1</sup> DMA is not available on the NI DAQCard-6036E.

Accuracy Information (NI 6034E, NI 6035E, NI PCI-6036E Only)

|                        |          |   | ₹  | Absolute Accuracy           | ,  | - Committee Committee Committee | Committee of the second state of the second  | Retains heering  | Longins  |
|------------------------|----------|---|--|-----------------------------|--|---------------------------------|--|--|--|
|                        |          | A Commence of the commence of | And the second s | Noise + Quantization (It V) | tization (µV)  |                                 | Absolute   | Residentian (47)   | 100  |
| Nominal                | N 10 %   | % of Reading  |  |                             | Contract of the same of the sa |                                 | Accuracy at  | THE PROPERTY OF THE PROPERTY O |  |
| Range at<br>Full Scale |          |   | Offset (uV)  | Single Pt.                  | Averaged   | Temp Drift<br>(%,FC)            | Full Seale<br>(mV)   | Singe Pt.  | paceally   |
| 3                      | Z4 Hours | , Ica   | / diameter   |                             |  |                                 | 4.61   | 1000   | 102.5  |
|                        | 0.0546   | 0.0588  | 1001   | ±933                        | ±#2.4  | 01000                           | 7.36   | t Marie  | The state of the s |
| *10                    | 0,0340   |   |  |                             |  | 90000                           | 1.79   | 242  | \$2.24   |
|                        | 0.0146   | 0.0188  | ±811   | ±467                        | 2,11,2   | UNAKD                           |  |  |  |
| a                      | 0.00     |   |  |                             | 70.37  | 01000                           | 0.399  | 64.3   | 6630   |
| * 0*                   | 0.0546   | 0.0588  | ±100   | ±56,2                       | 23.74  |                                 |  |  | 3171   |
| E.N.E.                 |          |   |  | 600                         | 27.00  | 01000                           | 1190'0   | 20.5   | Sind   |
| 30.0                   | 0.0546   | 0.0588  | £28.9  | 7.077                       |  |                                 | The second secon | A de de  | and sendines   |
| COVER                  | 2000     |   | The second secon |                             |  | Lichard Lichard                 | ton and mersone  | Ashering and mergered of 100 sange-manners   | The state of the s |

NI recommends a one-year calibration interval. The Abaclute Accuracy at Full Scale calculations were performed for a maximum range input voltage (for example, 10 V to a NI recommends a one-year calibration interval.) Measurement accuracies are listed for operational temperatures within ±1 °C of internal calibration temperature and ±10 °C of external or factory-calibration temperature. Note: Accuracies are valid for measurements following an internal E Series calibration. Averaged numbers assume dithering and averaging of 100 the ±10 V range) after one year, assuming 100 points of averaged data. Go to n.k., com/info and enter info code raspec for example calculations.

Accuracy Information (NI DADCard-6036E Only)

| Accuracy morning      |              |   |              | •  | Absolute Accuracy | <b>5</b>   |                |                      | Retains                             | Relative Accuracy  |
|-----------------------|--------------|---|--------------|--|-------------------|--|----------------|----------------------|-------------------------------------|--|
|                       |              |   |              |  |                   |  |                | Absolute             | Render                              | Resolutions (p.V.)   |
| Nominal Range at Full | inge at Full | 0.00  | malina       |  | Noise + Quan      | Noise + Quantization (µV)  |                | Accuracy             |                                     |  |
| Scale (V)             | :<br>:       | W 10 %  | % Of Reading |  |                   |  | Termo Drift    |                      | ano and                             |  |
|                       |              |   |              |  |                   | Patriciana   | (%FC)          | Scale (mV)           | Single Pt.                          | Aprilage   |
| Doctrive              | Negative     |   | 1 Vans       | Offset (µV)                                  | Single FL.        | Meren  | Ħ              |                      | -                                   | 230.081  |
| 1                     | V. II Scale  | 24 Hours  | J real       |  |                   |  | 0.000          | 8,653                | 1,000,1                             |  |
| Full Scale            | T UII CAN    |   |              |  | 1 500.21          | 137.329  | 1              | 1                    | -                                   | 200 000  |
|                       |              | 0.0549  | 1650'0       | C07007                                       | ١                 | Γ  |                | 2337                 | W 18                                | 100  |
| 410                   | 97           | NAME OF THE PARTY |              | 27.  | 260 10            | 595.89   | cocco          |                      |                                     | 20.000   |
|                       |              | 07100   | 16100        | 1,311.33                                     |                   |  |                | 2570                 | 102.463                             |  |
| 0 37                  | -5.0         | 0.0149  |              |  | 01.210            | 7,782  | 0.0000         | -                    |                                     | 919  |
| 200                   |              |   | 0.0601       | 150.053                                      | 115.40            | T  |                | 2000                 | 1617                                | 4.20   |
| 1                     | **           | 0.0549  | CCCCC        |  | 1                 | 1 204  | 01000          | (000)                | 1                                   |  |
| +0.5                  |              | ١   |              | 11 905                                       | 32.779            | 2.40   | 1              | 1                    | Water Chatter                       | of president   |
|                       | , ,          | 0.0549  | 0,009        | 201.00                                       |                   | 110  | a garbering at | of the second second | Character Or                        | 1  |
| 5005                  | 69           | ١   |              | . C. Carios C.                               | alibration. Avera | ged numbers 45   | J. 10 .C. of   | cuternal or facts    | By Child Land of the Control of the | A. 1/2 To fine   |
|                       |              |   | 100          | F 120 12 12 12 12 12 12 12 12 12 12 12 12 12 |                   | The same of the sa | 1000           |                      | The same of the same of             | The same of the sa |

NI recommends a one-year calibration interval. The Absolute Accuracy at Full Scale calculations were performed for a maximum range input voltage that exam the ±10 V range) after one year, assuming 100 points of averaged data. Go to n.i. com/into and enter tuto code reaspace for example calculations.

| ### Parties Characteristics   parties Characteristics   Parties Characteristics  | Amplifier Characteristics Input impedance Normal powered on Powered off Overload Input bias current NI DAQCard-6036B NI 6034B, NI 6035B, NI PCI-6036B Input offset current Common-mode rejection ratio ( | #20 Ω #20 Ω #800 pA #200 pA #200 pA  |
|--|--|--|
| No missing codes NI DAQCard-6036E15 bits   | Runge  | Bipolar  |
| NI 6034R, NI 6035B,  | 20 V   | 85 dB  |
| NI PCI-6036B 16 bits   | 10 V   | 85 dB  |
| Offset error<br>Pregain error after calibration ±1.0 µ∨ max                      | IV   | 96 dB  |
| Pregain error after Calibration  | 100 mV   | 96 dB  |
| NI DAQCard-6036E ±3.0 mV max<br>NI 6034E, NI 6035E.<br>NI PCI-6036E ±28.8 mV max | Dynamic Characteristics<br>Bandwidth   |  |
| Postgain error after calibration   | Signal   | Bandwidth  |
| NI DAQCard-6036B ±0.20 mV max  | Small (-3 dB)  | 413 kHz  |
| NI 6034E, NI 6035E,<br>NI PCI-6036E±157 μV max                                   | Large (1% THD)   | 490 kHz  |
| Postgain error before calibration  NI DAQCard-6036E                              | Range 10 V   | ) V±4.5 LSB, 5 μs typ±2 LSB, 5 μs typ PCI-6036E±4 LSB, 5 μs typ±2 LSB, 5 μs max iding quantization)1.5 |
| NI 6034E, NI 6035E,<br>NI PCI-6036E±18,900 ppm of<br>reading max                 | Kiing  |  |

adjusted to 0 at gain = 1 ......±200 ppm of reading max

Accuracy values are valid for source impedances <1 kΩ. Refer to Multichannel Scanning Considerations of the E Series Help for more information.

| NI 6034E, NI 6035E, NI PCI-6036E       |
|--|
| Range 10 to 20 V0.8                    |
| Range 1 V1.0                           |
| Range 100 mV                           |
| CrosstalkDC to 100 kHz                 |
| Adjacent channels75 dB                 |
| Other channels90 dB                    |
| Stability<br>Recommended warm-up time  |
| NI DAQCard-6036E30 minutes             |
| NI 6034E, NI 6035E,                    |
| NI PCI-6036B15 minutes                 |
| Offset temperature coefficient         |
| Pregain±20 μV/°C                       |
| Postgain±175 μV/°C                     |
| Gain temperature coefficient±20 ppm/°C |

## Analog Output (NI 6035E/6036E Only)

#### **Output Characteristics**

transfer, demand transfer)

#### **Accuracy Information**

|            |             |   | Abso   | lute Accura                     | cy  |  |
|------------|-------------|---|--|---------------------------------|---|--|
| Nominal    | 4           | % of Readin                                     | g  |                                 |   | Absolute<br>Accuracy at  |
| Full Scale | 24<br>Hours | 90 Days   | 1 Year   | Offset<br>(μV)                  | Temp Drift<br>(%/°C)  | Full Scale<br>(mV)   |
| ±10        | 0.0091      | 0.0111  | 0.0133   | 1.22                            | 0.0005  | 2.547  |
|            | 0.18        | 0.02  | 0.022  | 5.93                            | 0.0005  | 8.127  |
|            |             | 0.011   | 0.013  | 1.1                             | 0.0005  | 2.417  |
|            | Range at    | Range at Full Scale (V)  ±10  0.0091  ±10  0.18 | Range at Full Scale (V)  24 Hours 90 Days  ±10 0.0091 0.0111 ±10 0.18 0.02 | Nominal Range at Full Scale (V) | Nominal Range at Full Scale (V)   24 Hours   90 Days   1 Year (μV)     ±10   0.0091   0.0111   0.0133   1.22     ±10   0.18   0.02   0.022   5.93 | Range at Full Scale (V)     24 Hours     90 Days     1 Year     Offset (μV)     Temp Drift (%/°C)       ±10     0.0091     0.0111     0.0133     1.22     0.0005       ±10     0.18     0.02     0.022     5.93     0.0005 |

Note: Accuracies are valid for measurements following an internal E Series calibration. Averaged numbers assume dithering and averaging of 100 single-channel readings. Measurement accuracies are listed for operational temperatures within  $\pm 1$  °C of internal calibration temperature and  $\pm 10$  °C of external or factory-calibration temperature. NI recommends a one-year calibration interval. The Absolute Accuracy at Full Scale calculations were performed for a maximum range input voltage (for example, 10 V for the  $\pm 10$  V range) after one year, assuming 100 points of averaged data. Go to ni.com/info and enter info code rdspec for example calculations.



<sup>&</sup>lt;sup>1</sup> DMA is not available on the NI DAQCard-6036E.

| Transfer Characteristics   NL after calibration   NI DACCard-Go36E   | Characteristics                       |                         |   |
|--|---------------------------------------|-------------------------|---|
| NIL   Age            | Transfer Characteristics              |                         | Initial power-up attack                 |
| N   DAQCard-6036E  | offer calibration                     |                         | Magnitude                               |
| A0.3 LSB typ,   a0.5 LSB max   by   av.   by   by   by   by   by   by   by   b   |                                       | ±2100                   |   |
| DNL   ±1.0 LSB max   N   PCI-6036E   ±2.2 V  | NI PCI-6030E                          |                         | NI 6036B±1.6 V                          |
| DNL  | NI 6035E                              | ±0.3 LSB typ,           | NI DCI (024)                            |
| DNL  |                                       |                         | Duration #2.2 V                         |
| Monotonicity   NI 6035E   2.0 ms   NI FCI-6036E   42 μs  | pNL                                   | ±1.0 LSB max            |   |
| N   DAQCard-6036E  |                                       |                         | NI 60250                                |
| NI PCI-6036E   | Monotonicity                          |                         | NI 0035E2.0 ms                          |
| NI 6035E   12 bits, guaranteed after calibration   12 bits, guaranteed after calibration   NI DAQCard-6036E   22.2 V   | NI DAQCard-00502,                     | 16 bits, guaranteed     |   |
| Magnitude   NI DAQCard-6036E   ±1.6 V   NI 6035E   ±1.6 V   NI 6035E   ±2.2 V   Duration   NI DAQCard-6036E   ±2.2 V   Duration   NI DAQCard-6036E   ±2.2 V   Duration   NI DAQCard-6036E   ±4.2 μs   NI 6035E   ±4.2 μs   NI 6035E   ±4.2 μs   NI 6035E   ±2.2 v   Duration   NI DAQCard-6036E   ±4.2 μs   NI 6035E   ±2.2 μs               | NI PCI-00302                          | after calibration       | Power reset glitch                      |
| Offset error   After calibration   NI DAQCard-6036E   ±2.2 V   |                                       |                         | Magnitude                               |
| Offset error   | NI 6033E                              | after calibration       | NI DAQCard-6036E±1.6 V                  |
| Offset error   After calibration   NI DAQCard-6036E,   NI PCI-6036E   ±305 μV max   NI 6035E   42 μs   NI FCI-6036E   42 μs   NI FCI-6036E   42 μs   NI PCI-6036E   44 μs   NI PCI-6036E   5 μs to ±4.5 LSB   accuracy   NI PCI-6036E   10 μs to ±0.5 LSB   accuracy   NI PCI-6036E   10 μs to ±0.5 LSB   accuracy   NI PCI-6036E   5 μs to ±1 LSB   accuracy   NI PCI-6036E   15 ν/μs   NI PCI-6036E   15 ν/μs   NI PCI-6036E   15 ν/μs   NI PCI-6036E   10 μν <sub>max</sub>   DC to 400 kHz   DC  |                                       |                         | NI 6035E, NI PCI-6036E ±2.2 V           |
| NI DAQCard-6036E   545 ms     NI DAQCard-6036E   ±305 μV max     NI PCI-6036E   ±200 mV max     NI DAQCard-6036E   ±40 mV max     NI PCI-6036E   ±44 mV max     NI DAQCard-6036E   ±44 mV max     Output coupling   DC     Output impedance   ±10 V     Output coupling   DC     Output impedance   ±5 mA max     Output impedance   ±60 mV     NI DAQCard-6036E   ±60 mV     NI DAQCard-6036E   ±10 mV     NI DAQCard-6036E   ±10 mX     NI DAQCard-            | Offset error                          |                         |   |
| NI DAQCard-6036E,   ±305 μV max   NI 6035E   | After calibration                     |                         | NI DAOCard-6036E545 ms                  |
| NI PCI-6036E   | NI DAOCard-6036E,                     |                         |   |
| NI 6035E   | NI PCI-6036E                          | ±305 μV max             |   |
| Dynamic Characteristics   Ni DAQCard-6036E   ±60 mV max   Ni 6035E   ±200 mV max   Ni FOI-6036E   ±44 mV max   Ni FOI-6036E   ±44 mV max   Ni FOI-6036E   ±0.50 kB   ±0.75 kB            | NI 6035E                              | ±1.0 mV max             | 111 C1 00302                            |
| NI DAQCard-6036E   ±60 mV max   NI 6035E   ±200 mV max   NI 6035E   ±44 mV max   NI DAQCard-6036E   ±44 mV max   NI DAQCard-6036E   10 μs to ±0.5 LSB accuracy   After calibration   NI DAQCard-6036E   ±30.5 ppm   NI 6035E   ±100 ppm   NI DAQCard-6036E   ±100 ppm   NI DAQCard-6036E   ±0.50%   NI PCI-6036E   ±0.50%   NI PCI-6036E   ±0.75%   NI PCI-6036E   ±0.75%   NI DAQCard-6036E   110 μV/μs   NI 6035E   100 μV/μs   NI 6035E   NI DAQCard-6036E   110 μV/μs   NI 6035E   110 μV/μs   NI 6035E   ±10 mV   NI PCI-6036E   ±            |                                       |                         | Dynamic Characteristics                 |
| NI 6035E   | NI DAOCard-6036E                      | ±60 mV max              |   |
| NI PCI-6036E   | NI DAQCAIG GODGE                      | +200 mV max             | NI DAOCard-6036E5 μs to ±4.5 LSB        |
| After calibration  | NI 6035E                              | +44 mV max              | accuracy                                |
| After calibration  | -00000                                |                         | NI 6035E10 μs to ±0.5 LSB               |
| After calibration  | Gain error (relative to internal re   | eference)               | accuracy                                |
| NI DAQCard-6036E,   ±30.5 ppm   Slew rate   NI DAQCard-6036E   ±100 ppm   NI DAQCard-6036E   10 V/μs   NI DAQCard-6036E,   15 V/μs   NI PCI-6036E   ±0.50%   NI PCI-6036E   ±0.75%   Noise   NI DAQCard-6036E   160 μV <sub>rms</sub> ,   DC to 400 kHz   DC to 400 kHz   DC to 1 MHz   DC to 1 MHz   DC to 400 kHz    |                                       |                         | NI PCI-6036E5 $\mu$ s to $\pm 1$ LSB    |
| NI PCI-6036E   | NI DAOCard-6036E,                     |                         | accuracy                                |
| NI 6035E   | NI PCI-6036E                          | ±30.5 ppm               | Slaw rate                               |
| NI DAQCard-6036E,   10 V/μs   NI PCI-6036E   15 V/μs   NI PCI-6036E   15 V/μs   Noise   NI DAQCard-6036E   160 μV <sub>rms</sub> .   DC to 400 kHz   DC to 1 MHz   DC to 1 MHz   DC to 400 kHz   DC to 1 MHz   DC to 1 MHz   DC to 400 kHz   DC to 400 | NI 6035F                              | ±100 ppm                | NLDA OCard-6036Ε5 V/μs                  |
| NI DAQCard-6036E,         NI PCI-6036E       ±0.50%         NI 6035E       ±0.75%         Noise       NI DAQCard-6036E         NI DAQCard-6036E       160 μV <sub>rms</sub> DC to 400 kHz         NI 6035E       200 μV <sub>rms</sub> DC to 1 MHz         Output coupling       DC         Output impedance       0.1 Ω max         Current drive       ±5 mA max         Protection       Short-circuit to ground         Power-on state (steady state)       ±60 mV         NI DAQCard-6036E       ±60 mV         NI DAQCard-6036E       ±200 mV  |                                       |                         | NI 6035Ε 10 V/μs                        |
| NI PCI-6036E       ±0.50%         NI 6035E       ±0.75%         Noise       NI DAQCard-6036E         NI DAQCard-6036E       160 μV <sub>rms</sub> , DC to 400 kHz         DC to 400 kHz       DC to 1 MHz         NI PCI-6036E       110 μV <sub>rms</sub> , DC to 400 kHz         Output impedance       0.1 Ω max         Current drive       ±5 mA max         Protection       Short-circuit to ground         Power-on state (steady state)       Mid-scale transition glitch (NI 6035E and NI PCI-6036E only)         NI PCI-6036E       ±12 mV         NI PCI-6036E       ±10 mV         NI PCI-6036E       ±10 mV         NI 6035E       ±10 mV         NI 6035E       1.0 μs  |                                       |                         | NI 0035Ε15 V/μs                         |
| NI 6035E   | NI DAQCard-6036E,                     | ±0.50%                  | NI PCI-0030E                            |
| Voltage Output         Range       ±10 V       NI 6035E       200 μV <sub>rms</sub> .         Output coupling       DC       NI PCI-6036E       110 μV <sub>rms</sub> .         Output impedance       0.1 Ω max       Mid-scale transition glitch (NI 6035E and NI PCI-6036E only)         Current drive       Short-circuit to ground       Magnitude         Protection       \$hi 6035E       ±12 mV         NI PCI-6036E       ±10 mV         Duration       \$1.0 μs   | NI PCI-6036E                          | +0.75%                  | Noise                                   |
| Voltage Output         Range   | NI 6035E                              | 10.75 %                 | NI DAQCard-6036E160 µV <sub>rms</sub> , |
| Range  |                                       |                         | DC 10 400 1215                          |
| Range  | Voltage Output                        | +10 V                   | NI 6035E200 µV <sub>ms</sub> ,          |
| Output coupling       DC       NI PCI-6036E       TIO μ V mms         Output impedance       0.1 Ω max       DC to 400 kHz         Current drive       ±5 mA max       Mid-scale transition glitch (NI 6035E and NI PCI-6036E only)         Protection       Short-circuit to ground       NI 6035E       ±12 mV         NI PCI-6036E       ±10 mV         NI PCI-6036E       ±0 mV         NI DAQCard-6036E       ±60 mV       Duration         NI 6035E       2.0 μs         +200 mV       NI 6035E       1.0 μs   | Range                                 | , ±10 ¥                 | De le 1                                 |
| Output impedance   | · · · · · · · · · · · · · · · · · · · | DC                      | NI PCI-6036E110 µV <sub>ms</sub> ,      |
| Current drive       ±5 mA max       Magnitude         Protection       Short-circuit to ground       Magnitude         NI 6035E       ±10 mV         NI PCI-6036E       ±10 mV         Duration       2.0 μs         NI 6035E       1.0 μs   | Output coupling                       | o I O may               | -                                       |
| Current drive       ±5 mA max       Magnitude         Protection       Short-circuit to ground       Magnitude         NI 6035E       ±10 mV         NI PCI-6036E       ±10 mV         Duration       2.0 μs         NI 6035E       1.0 μs   | Output impedance                      | 0.1 \$2 max             | and NI PCI-6036E only)                  |
| Protection   |                                       | ±5 mA max               | Mid-scale transition gitter (           |
| Power-on state (steady state)  NI PCI-6036E  | Current drive                         | :it to ground           | Magnitude +12 mV                        |
| Power-on state (steady state)  NI DAQCard-6036E±60 mV  Duration  NI 6035E2.0 μs  NI 6035E1.0 μs  | Protection                            | Short-circuit to ground | NI 6035E                                |
| Power-on state (steady state)  NI DAQCard-6036E±60 mV  NI 6035E2.0 μs  NI 6035E1.0 μs  |                                       |                         | NI PCI-6036E                            |
| NI DAQCard-6036E±200 mV NI 6035E   | Power-on state (steady state)         | 460 mV                  |   |
| NI (025E   | W D 4 O G 4 6036F                     | ±00 m v                 | 2.5Ε                                    |
| NI PCI-6036E±44 mV   | NII COSEC                             | 1200                    | NI PCI-6036E1.0 μs                      |
| NI PCI-0030E   | NI DCI 6036F                          | ±44 mV                  | Mileran                                 |
|  | MI PCI-0030E                          |                         |   |

### Offset temperature coefficient NI DAQCard-6036B .....±150 μV/°C NI 6035B.....±50 μV/°C

NI PCI-6036Ε .....±35 μV/°C Gain temperature coefficient NI DAQCard-6036E .....±8 ppm/°C

NI 6035E.....±25 ppm/°C NI PCI-6036E .....±6.5 ppm/°C

Digital I/O

Number of channels......8 input/output Compatibility......5 V TTL/CMOS

Digital logic levels on P0.<0..7>

| Digital logic level                            | Min    | Max     |
|--|--------|---------|
| Input low voltage                              | 0 V    | 0.8 V   |
| Input high voltage                             | 2.0 V  | 5.0 V   |
| Input low current $(V_{in} = 0 \text{ V})$     | _      | -320 μA |
| Input high current ( $V_{in} = 5 \text{ V}$ )  | _      | 10 μΑ   |
| Output low voltage (I <sub>OL</sub> = 24 mA)   | _      | 0.4 V   |
| Output high voltage (I <sub>OH</sub> = -13 mA) | 4.35 V | _       |

| Power-on state                                      | Input (high-impedance), $50~\mathrm{k}\Omega$ pull-up to +5 VDC |
|---|---|
| Data transfers                                      | Programmed I/O  |
| Transfer rate $(1 \text{ word} = 8 \text{ bits})^1$ | 50 kwords/s, typ  |
| Constant sustainable rate <sup>1</sup>              | 1 to 10 kwords/s, typ   |

#### Timing I/O

Number of channels

Up/down counter/timers .....2 Frequency scaler .....1

Resolution

Up/down counter/timers ......24 bits Frequency scaler ......4 bits

Compatibility......5 V TTL/CMOS

## Digital logic levels

| Level  | Min   | Max    |
|--|-------|--------|
| Input low voltage                                | 0.0 V | 0.8 V  |
| Input high voltage                               | 2.0 V | 5.0 V  |
| Output low voltage (lout = 5 mA)                 |       | 4.35 V |
| Output high voltage (I <sub>out</sub> = -3.5 mA) | 0.4 V | _      |

#### Base clocks available

| Up/down counter/timers | 20 MHz, | 100 kHz |
|------------------------|---------|---------|
| Frequency scaler       | 10 MHz, | 100 kHz |

Base clock accuracy ...... ±0.01%

Max external source frequency

up/down counter/timers ...... 20 MHz

External source selections......PFI <0..9>, RTSI <0..6> (except DAQCard), analog trigger, software-selectable

External gate selections ......PFI <0..9>, RTSI <0..6> (except DAQCard), analog trigger, software-selectable

Min source pulse duration...... 10 ns in edge-detect mode

Min gate pulse duration ...... 10 ns in edge-detect mode

Data transfers

PCI up/down counter/timer ...... DMA2 (scatter-gather), interrupts, programmed I/O

DAQCard up/down

counter/timer ...... Interrupts, programmed I/O

Frequency scaler ...... Programmed I/O

<sup>&</sup>lt;sup>1</sup> Not guaranteed on the NI DAQCard-6036E.

<sup>&</sup>lt;sup>2</sup> DMA is not available on the NI DAQCard-6036E.

#### triggers

| Triggers                      |   |
|-------------------------------|---|
| Digital Trigger               |   |
| Digital                       |   |
| Purpose Analog input          | Start, reference,<br>and pause trigger,<br>sample clock |
| Analog output                 | Start and pause trigger,<br>sample clock                |
| Counter/timers                | ., Source, gate   |
| External sources              | PFI <09>, RTSI <06><br>(except DAQCard)                 |
| Compatibility                 | 5 V TTL   |
| Response                      |   |
| Pulse width                   | 10 ns min   |
| RTSI (PCI Only) Trigger lines | 7   |
| Calibration                   |   |

| Recommended warm-up time       |   |
|--------------------------------|---|
| PCI                            | 15 minutes                                      |
| DAQCard                        |   |
| Interval                       |   |
| External calibration reference | . Between 6 and 10 V                            |
| Onboard calibration reference  |   |
| Level                          | . 5.000 V (±3.5 mV)                             |
|                                | (over full operating                            |
|                                | temperature, actual value stored in EEPROM)     |
| Temperature coefficient        | . ±5.0 ppm/°C max                               |
| Long-term stability            | $\pm 15.0 \text{ ppm} / \sqrt{1,000 \text{ h}}$ |
| Long-term stability            |   |

#### **Power Requirement**

| Tonor Hodan Small | - 11DC (150%) at 0.9 A |
|-------------------|------------------------|
| PCI               | +5 VDC (±5%) at 0.9 A  |
| DAOCard           | +5 VDC (±5%) at 0.3 A  |



Note Excludes power consumed through +5 V available at the I/O connector.

#### Power available at I/O connector

| PCI     | +4.65 to +5.25 VDC   |
|---------|----------------------|
|         |                      |
| DAQCard | . +4.65 to +5.25 VDC |
| DAQCard | at 0.75 A            |

#### Physical

| Dimensions             |  |
|------------------------|--|
| PCI                    |  |
| (not including connect | ors) 17.5 cm × 10.6 cm                     |
| DADCont                | $(6.9 \text{ in.} \times 4.2 \text{ in.})$ |
| Weight                 | (6.9 in. × 4.2 in.)<br>Type II PC Card     |
| NI DAQCard-6036E.      | 32 g (1.1 oz)                              |
| ст-6034Е               |  |
| NI PCI-6036E           | 165 g (5.8 oz)                             |
| I/O connector          | g (114 02)                                 |
| PCI                    | 68-pin male SCSI-II typ                    |
| DAQCard                | 68-position female                         |

#### Maximum Working Voltage

Maximum working voltage refers to the signal voltage plus the common-mode voltage,

| Channel-to-earth   | ±11 V,                            |
|--------------------|-----------------------------------|
|                    | Installation Category I           |
| Channel-to-channel | ±11 V,<br>Installation Category I |

#### **Environmental**

| Environmental Operating temperature0 to 55 °C              |  |
|--|--|
| Storage temperature20 to 70 °C                             |  |
| Relative humidity NI DAQCard-6036E10 to 90%, noncondensing |  |
| NI 6035E, NI PCI-6036E10 to 90%, noncondensing             |  |

#### Safety

#### NI PCI-6034E/6035E/6036E

The device meets the requirements of the following standards of safety for electrical equipment for measurement, control, and laboratory use:

- IEC 61010-1, EN 61010-1
- UL 61010-1
- CAN/CSA-C22.2 No. 61010-1



Note For UL and other safety certifications, refer to the product label or visit ni.com/ certification, search by model number or product line, and click the appropriate link in the Certification column.

NI DAQCard-6036E NI pagearu-uses the requirements of the following standards The device and electrical equipment for measurement, control, for safety and electrical equipment for measurement, control, and laboratory use:

- IEC 60950, EN 60950
- UL 1950, UL 60950
- CAN/CSA-C22.2 No. 60950



Note For UL and other safety certifications. refer to the product label, or visit ni.com/ certification, search by model number or product line, and click the appropriate link in the Certification column.

## **Electromagnetic Compatibility**

Emissions......EN 55011 Class A at 10 m FCC Part 15A above

1 GHz

Immunity ..... EN 61326:1997 A2:2001, Table 1

CE, C-Tick, and FCC Part 15 (Class A) Compliant



Note For EMC compliance, you must operate this device with shielded cabling.

#### **CE Compliance**

This product meets the essential requirements of applicable European Directives, as amended for CE marking, as follows:

Low-Voltage Directive (safety)......73/23/EEC

Electromagnetic Compatibility

Directive (EMC)......89/336/EEC



Note Refer to the Declaration of Conformity (DoC) for this product for any additional regulatory compliance information. To obtain the DoC for this product, visit ni.com/certification, search by model number or product line, and click the appropriate link in the Certification column.

| (  | $\overline{}$ |    |                   |
|--|---------------|----|-------------------|
| Al 8   | 34            | 68 | Al O              |
| Al 1   | 33            | 67 | AI GND            |
| AI GND   | 32            | 66 | Al 9              |
| AI 10  | 31            | 65 | Al 2              |
| AI 3   | 30            | 64 | AI GND            |
| AI GND   | 29            | 63 | Al 11             |
| Al 4   | 28            | 62 | AI SENSE          |
| AI GND   | 27            | 61 | Al 12             |
| AI 13  | 26            | 60 | Al 5              |
| Al 6   | 25            | 59 | AI GND            |
| AI GND   | 24            | 58 | Al 14             |
| Al 15  | 23            | 57 | Al 7              |
| NC   | 22            | 56 | AI GND            |
| NC   | 21            | 55 | AO GND            |
| NC   | 20            | 54 | AO GND            |
| P0.4   | 19            | 53 | D GND             |
| D GND  | 18            | 52 | P0.0              |
| P0.1   | 17            | 51 | P0.5              |
| P0.6   | 16            | 50 | D GND             |
| D GND  | 15            | 49 | P0.2              |
| +5 V   | 14            | 48 | P0.7              |
| D GND  | 13            | 47 | P0.3              |
| D GND  | 12            | 46 | AI HOLD COMP      |
| PFI 0/AI START TRIG  | 11            | 45 | EXT STROBE        |
| PFI 1/AI REF TRIG  | 10            | 44 | D GND             |
| The state of the s | 9             | 43 | PFI 2/AI CONV CLK |
| D GND  | 8             | 42 | PFI 3/CTR 1 SRC   |
| +5 V   | 7 41          |    | PFI 4/CTR 1 GATE  |
| D GND  | 6 40          |    | CTR 1 OUT         |
| PFI 5/AO SAMP CLK  | 5             | 39 | D GND             |
| PFI 6/AO START TRIG  | 113           | 38 | PFI 7/AI SAMP CLK |
| D GND  | 11—           | -  | TRANSPORTE        |
| PFI 9/CTR 0 GATE   | 3             | +  | 1 - 010           |
| CTR 0 OUT  | 2             | _  | CND               |
| FREQ OUT   | 11            | 35 | ٦) ال             |
| -HEW OU.   |               | _  |                   |

Figure 1. NI 6034E Pinout

AI B 34 AI O AI 1 33 67 AI GND AI GND 32 66 AI 9 AI 10 31 65 Al 2 AI3 30 AI GND AI GND 29 63 AI 11 **AI 4** 28 62 AI SENSE AI GND 27 61 AI 12 AI 13 26 60 AI 5 AI 6 25 59 AI GND AI GND 24 58 AI 14 AI 15 23 57 **AI7** 22 AO 0 56 AI GND AO 1 21 55 **AO GND** 20 NC 54 AO GND P0.4 19 53 D GND D GND 18 52 P0.0 17 51 P0.1 P0.5 16 50 P0.6 D GND 15 49 D GND P0.2 14 48 P0.7 +5 V 13 47 P0.3 D GND AI HOLD COMP 12 46 D GND EXT STROBE 11 45 PFI 0/AI START TRIG D GND 10 44 PFI 1/AI REF TRIG PFI 2/AI CONV CLK 9 43 D GND PFI 3/CTR 1 SRC 8 42 +5 V PFI 4/CTR 1 GATE 41 7 D GND 40 CTR 1 OUT 6 PFI 5/AO SAMP CLK D GND PFI 6/AO START TRIG 5 39 PFI 7/AI SAMP CLK 4 38 D GND PFI 8/CTR 0 SRC 37 3 PFI 9/CTR 0 GATE D GND 2 36 CTR 0 OUT D GND 35 FREQ OUT NC = No Connect

Figure 2. NI 6035E/6036E Pinout

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# <sub>General</sub> Description

temally frequency compensated operational amplifiers which consists of two independent, high gain, injemally frequency specifically to operate from a single power were designed specifically to operate from a single power law over a wide range of voltages. Operation for were designed wide range of voltages. Operation from split supply supplies is also possible and the low notice. gupply over a visual and possible and the low power supply power supplies in also possible and the low power supply power supply and drain is independent of the magnitude of the power supplies in the power supply guildent drain is independent of the magnitude of the power supplies yourself and yours

supply voltage. Application areas include transducer amplifiers, do gain Application electron and all the conventional op amp circuits which now have again implemented in single power contents. blocks and all the solutions of amp circuits which now out he more easily implemented in single power supply system for example, the

tems. For example, the tens. For the standard +6V power supply voltage which is aled bit of digital systems and will easily provide the required used in digital systems and will easily provide the required used in digital vision without requiring the additional ±15V power supplies.

## Unique Characteristics

- In the linear mode the Input common-mode voltage range includes ground and the output voltage can also swing to ground, even though operated from only a single power supply voltage.
- The unity gain cross frequency is temperature compensated.
- The input blas current is also temperature compensated.

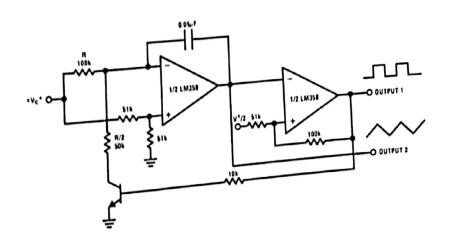
#### Advantages

- Two internally compensated op amps
- Eliminates need for dual supplies
- Allows direct sensing near GND and Vout also goes to
- Compatible with all forms of logic
- Power drain suitable for battery operation
- Pin-out same as LM1558/LM1458 dual op amp

#### Features

- Internally frequency compensated for unity gain
- Large do voltage gain: 100 dB
- Wide bandwidth (unity gain): 1 MHz (temperature compensated)
- Wide power supply range:
  - Single supply: 3V to 32V
  - or dual supplies: ±1.5V to ±16V
- Very low supply current drain (500 µA) essentially independent of supply voltage
- Low Input offset voltage: 2 mV
- Input common-mode voltage range includes ground
- Differential input voltage range equal to the power supply voltage
- Large output voltage swing: 0V to V\*- 1.5V

# Voltage Controlled Oscillator (VCO)



Wing Shing Computer Components Co., (H.K.)Ltd. Homepage: http://www.wingshing.com

Tel:(852)2341 9276 Fax:(852)2797 8153 E-mail: wsccltd@hkstar.com



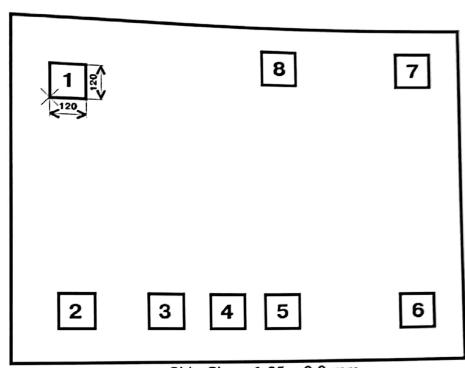
electrical characteristics at specified free-air temper

| PARAMETER  | pecified free-air temperature, Vo  |              | THE RESIDENCE OF THE PERSON NAMED IN COLUMN 2 IN COLUM | UNIT                                   |      |          |        |
|--|--|--------------|--|--|------|----------|--------|
|  |  | -            | LM   | AND DESCRIPTION OF THE PERSON NAMED IN | MAX  | O.V.     | 1      |
|  | Vcc = 5 V to MAX.  | 25 ° C       | MIN  | TYP                                    | 7    | mV       | -      |
| νο<br><sub>input offset</sub> voltage                              | V V  | ull range    |  | -                                      | 9    | ,,,,,    |        |
| aVio<br>Average temperature coefficient<br>of input offset voltage |  | Full range   |  | 7                                      |      | μV/°C    |        |
|  | Vo=1.4 V   | 25 ° C       |  | 2                                      | 50   | nA       |        |
| offset current   |  | Full range   |  |  | 150  |          |        |
| xilO<br>Average temperature coefficient<br>of input offset current |  | Full range   |  | 10                                     |      | pA/°     | c<br>  |
|  | Vo=1.4 V   | 25 ° C       |  | -20                                    | -250 | O nA     |        |
| Input bias current   |  | Full range   |  |  | -500 |          |        |
|  | Vcc = 5 V to MAX   | 25° C        | 0 to Vcc-1.  | 5                                      |      | V        |        |
| V <sub>ICR</sub><br>Common-mode input voltage                      |  | Full range   | 0 to Vcc - 2   | 2                                      |      |          |        |
| range  | RL≥2 KΩ  | 25 ° C       | Vcc-1.5  |  |      | V        |        |
| <i>l</i> он<br><sub>High-</sub> level output voltage               | $Vcc = MAX, R_L=2 k\Omega$   | Full range   | 26   |  |      | $\Box$   |        |
|  | Vcc = MAX,   | Full range   | 27   | 28                                     |      | - 1      |        |
|  | $R_L \ge 10 \text{ k}\Omega$   |              |  |  |      | - m      | ,      |
| V <sub>OL</sub>  | R <sub>L</sub> ≥ 10 kΩ   | Full range   |  | 5                                      | 20   |          |        |
| Low-level output voltage   | Vcc = 15 V,<br>Vo=1V to 11 V,  | 25 ° C       | 25   | 10                                     | 0    | V        | /mV    |
| Large-signal differential  | The same of the sa | Full range   | 15   |  |      |          |        |
| voltage amplification  | $R_L \ge 2 \text{ k}\Omega$<br>Vcc = 5 V to MAX,   | 25 °C        | 65   | 80                                     | 5    |          | В      |
| CMRR   | 1-1-100  | 25 0         |  |  |      |          |        |
| Common-mode rejection ratio  | $V_{IC} = V_{ICR} min$ $V_{CC} = 5 V to MAX$   | 25 ° C       | 65   | 1                                      | 00   | 1        | dB.    |
| ratio (ΔVcc/ΔV <sub>IO</sub> )                                     | f=1 kHz to 20 kHz  | 25 ° C       |  | 1                                      | 20   |          | dB     |
| Vo1 /Vo2<br>Crosstalk attenuation                                  | 1-1 KHZ to 20 11.13  |              | 20   | -                                      | 30   |          | mA     |
| o attenuation  | Vcc = 15 V,  | 25 ° C       | -20  | <del></del>                            | +    | -        |        |
|  | $V_{ID}=1 V_{I}V_{O}=0$  | Full range   |  |  | 20   |          |        |
| Output current   | Vcc = 15 V.  | 25 ° C       | 10   |  | -    |          |        |
|  | $V_{ID} = -1 \text{ V, Vo} = 15$   | V Full range | 5  |  | 30   |          | μА     |
|  | $V_{ID} = -1 V$  | 25 ° C       | 12   |  | 30   |          | ,,,    |
|  | Vo =200 mV   |              |  |  | ±40  | ±60      | mA     |
|  | Vcc at 5 V   | 25 ° C       |  |  |      |          |        |
| os<br>Short-circuit output current                                 | GND at -5 V,Vo=0   |              | 9  |  | 0.7  | 1.2      | mA     |
| cc   | Vo - 2.5 V, No load  | Full rang    |  |  | 1    | 2        | $\neg$ |
| Supply current (two amplifiers)                                    | Vcc = MAX,<br>Vo = 0.5Vcc, No lo   | ad           | ommon-mode   |  |      | <u> </u> |        |

<sup>\*</sup> All characteristics are measured under open-loop conditions with zero common-mode input voltage unless otherwise specified. «MAX» Vcc for testing purposes is 30 V. Full range is 0 ° C to 70 ° C.



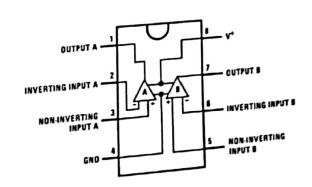
## ad Location



Chip Size: 1.65 x 0.9 mm

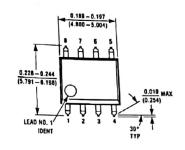
| Pad N   | Pad             | Coordinates, mkm |     |  |
|---------|-----------------|------------------|-----|--|
| 1 44 11 | Name            | Х                | Υ   |  |
| 1       | #1 OUT          | 85               | 625 |  |
| 2       | #1 IN-          | 182              | 88  |  |
|         | #1 IN+          | 518              | 88  |  |
| 3       | GND             | 845              | 88  |  |
| 4       |                 | 1045             | 88  |  |
| 5       | #2 IN+          | 1381             | 88  |  |
| 6       | #2 IN-          | 1478             | 625 |  |
| 7       | #2 OUT          | 909              | 720 |  |
| 8       | V <sub>CC</sub> | 300              |     |  |

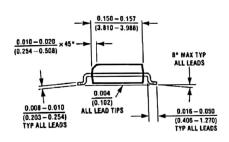
# **Connection Diagrams**

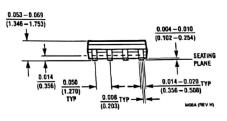




# physical Dimensions inches (millimeters) unless otherwise noted (Continued)

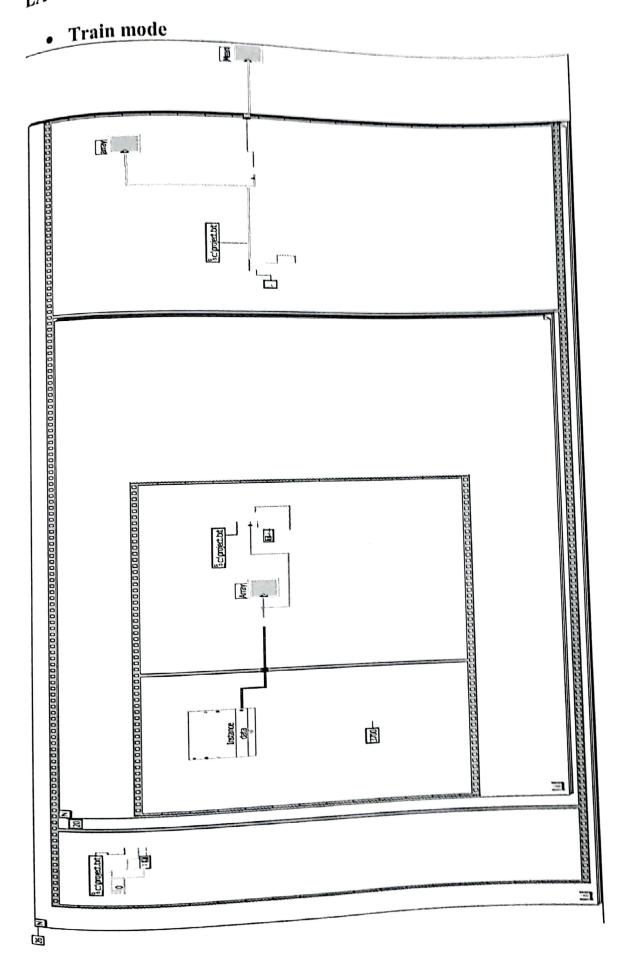




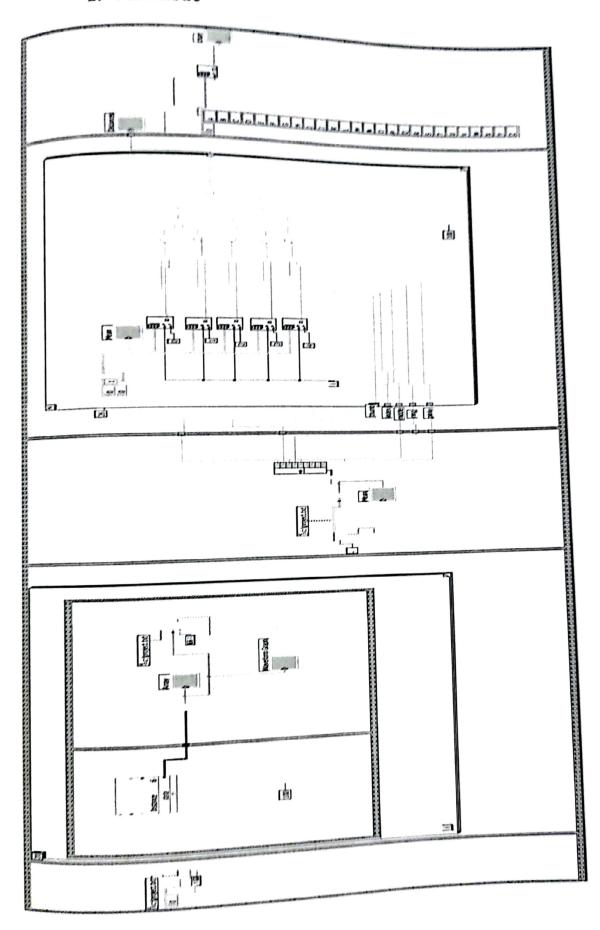


# APPENDIX B SOURCE CODE

# LAVBIEW software



## 2. Test mode



```
<sub>Train</sub> mode of PIC
```

```
#include<p18f4550.h>
#include < adc. h>
#include < delays.h>
#include<math.h>
#include"gamelcd_v3.h"
//#include<timers.h>
#pragma config WDT=OFF
#pragma config LVP=OFF
#pragma config DEBUG=OFF
#pragma config PWRT=OFF
int thumb, index, middle, Ring, Pinky;
int sumT,sumI,sumM,sumR,sumP;
int T,I,M,R,P;
int i;
int Array[5];
char chararray[5]={'T','I','M','R','P'};
void main(void)
 TRISA=1; //input
 TRISD=0; // output
 //TRISC=0; //output
 ADCON1=0x00; // all channels works as analoge
        sumT=0.0;
                      sumI=0.0;
               sumM=0.0;
                      sumR=0.0;
                      sumP=0.0;
```

// A/D converter
// read the value of the first finger

OpenADC(ADC\_FOSC\_64 & ADC\_RIGHT\_JUST & ADC\_2\_TAD, ADC\_CH0 & ADC\_INT\_OFF & ADC\_REF\_VDD\_VSS,00);

```
for(i=0;i<20;i++)
 {
// read the value of the second finger
SetChanADC(ADC_CH0);
ConvertADC();
while(BusyADC());
thumb=ReadADC();
// read the value of the second finger
 SetChanADC(ADC_CH1);
ConvertADC();
while(BusyADC());
index=ReadADC();
 // read the value of the third finger
 SetChanADC(ADC_CH2);
 ConvertADC();
 while(BusyADC());
 middle=ReadADC();
 // read the value of the fourth finger
                   SetChanADC(ADC_CH3);
 ConvertADC();
 while(BusyADC());
 Ring=ReadADC();
  // read the value of the fifth finger
  SetChanADC(ADC_CH4);
```

```
ConvertADC();
      while(BusyADC());
      Pinky=ReadADC();
      CloseADC();
   sumT+=thumb;
                sumI+=index;
         sumM+=middle;
                sumR+=Ring;
                sumP+=Pinky;
     } // for
  T=sumT/20;
  I=sumI/20;
  M=sumM/20;
  R=sumR/20;
  P=sumP/20;
  Array[0]=T;
  Aπay[1]=I;
  Array[2]=M;
  Array[3]=R;
  Array[4]=P;
// LCD
lcd_init();
 for(i=0; i<5; i++)
 {
  lcd_gotoyx(1,1);
  lcd_putc(chararray[i]);
  lcd_putc(' ');
  lcd_puti(Array[i]);
  Delay10KTCYx(500);
} // for
```

Delay10KTCYx(500);

```
} // main
PIC Test mode
#include<p18f4550.h>
#include<adc.h>
#include<delays.h>
#include<math.h>
#include"gamelcd_v3.h"
//#include<timers.h>
#pragma config WDT=OFF
#pragma config LVP=OFF
#pragma config DEBUG=OFF
#pragma config PWRT=OFF
 int thumb, index, middle, Ring, Pinky;
   float x ,D;
              int i ,j;
    int T,I,M,R,P;
 int sumT,sumI,sumM,sumR,sumP;
 sign\_values[26][5] = \{ \{45,14,58,51,81\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,47,77\}, \{48,18,24\}, \{43,12,46,46,66\}, \{44,13,47,47,47,47\}, \{48,18,24\}, \{44,13,47,47,47\}, \{48,18,24\}, \{44,13,47,47,47\}, \{48,18,24\}, \{44,13,47,47,47\}, \{48,18,24\}, \{44,13,47,47,47\}, \{48,18,24\}, \{44,13,47,47,47\}, \{48,18,24\}, \{44,13,47,47,47\}, \{48,18,24\}, \{44,13,47,47\}, \{48,18,24\}, \{44,13,47,47\}, \{48,18,24\}, \{44,13,47,47\}, \{48,18,24\}, \{44,13,47,47\}, \{48,18,24\}, \{44,13,47,47\}, \{48,18,24\}, \{44,13,47,47\}, \{48,18,24\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,47\}, \{44,13,4
  {43,12,46,46,66},{49,20,26,53,13},{45,14,48,48,88},{44,13,47,47,77},
  \{49, 20, 26, 53, 13\}, \{44, 14, 47, 47, 77\}, \{43, 13, 46, 46, 66\},
  {43,12,46,46,66},{47,18,25,51,11},{43,13,46,46,66},{43,12,46,46,66},
  {45,14,48,48,88},{43,13,46,46,66},{45,14,48,48,88},{49,20,26,53,13},
  {47,18,24,51,11},{48,19,25,52,12},{46,15,49,49,99},{44,13,47,47,77},
  {45,14,48,48,88},{43,14,46,47,77},{44,14,47,47,77}};
 characters[26]={'A','B','C','D','E','F','G','H','I','J','k','L','M','N','O','P','Q','R','S','T','U','V','
   W','X','Y','Z'};
    float distance[26];
  void calculate_N(float thumb,float index,float middle,float Ring,float Pinky);
   void nearest_N(float distance[]);
   void match(int count);
```

```
void LCD_display(char letter);
void main(void)
TRISA=1; //input
TRISD=0; // output
//TRISC=0; //output
ADCON1=0x00; // all channels works as analoge
  for(j=0;j<2;){
                   sumT=0.0;
                   sumI=0.0;
            sumM=0.0;
                   sumR=0.0;
                   sumP=0.0;
        for(i=0;i<10;i++)
         { // for
        // A/D converter
            // read the value of the first finger
         OpenADC(ADC_FOSC_64 & ADC_RIGHT_JUST & ADC_2_TAD,
ADC_CH0 & ADC_INT_OFF & ADC_REF_VDD_VSS,00);
         ConvertADC();
         while(BusyADC());
         thumb=ReadADC();
         // read the value of the second finger
          SetChanADC(ADC_CH1);
         ConvertADC();
         while(BusyADC());
         index=ReadADC();
```

```
// read the value of the third finger
  SetChanADC(ADC_CH2);
  ConvertADC();
  while(BusyADC());
  middle=ReadADC();
  // read the value of the fourth finger
                   SetChanADC(ADC_CH3);
  ConvertADC();
  while(BusyADC());
  Ring=ReadADC();
   // read the value of the fifth finger
   SetChanADC(ADC_CH4);
  ConvertADC();
  while(BusyADC());
   Pinky=ReadADC();
   CloseADC();
sumT+=thumb;
             sumI+=index;
      sumM+=middle;
             sumR+=Ring;
             sumP+=Pinky;
    } // for
```

```
I=sumI/10;
       M=sumM/10;
       R=sumR/10;
       P=sumP/10:
                             if (j=0)j++;
                                    else {
           // calculate the nearest neighor
           calculate_N(T,I, M, R,P);
           nearest_N(distance);
            }
 }// outer for
} // main
 // calculate of distance b/w points
 void calculate_N(float thumb, float index, float middle,float Ring,float Pinky)
   {
      for(i=0;i<26;i++) //row
              x=pow((thumb-sign_values[i][0]),2);
              x += pow((index-sign_values[i][1]),2);
                                       x+=pow((middle-sign\_values[i][2]),2);
              x + = pow( (Ring-sign_values[i][3]),2 );
              x+=pow((Pinky-sign_values[i][4]),2);
              D=sqrt(x);
      distance[i]=D;
     } // outer for
   }// method
```

```
// to find the nearest neighbors
//.....
 void nearest_N(float distance[])
   {
     float min;
   int i, count=0;
   min=distance[0];
     for(i=0;i<26;i++)
       if(distance[i]< min)
            min=distance[i];
            count=i;
          } // if
       } // for
      match(count);
    }// function
// .....
   void match(int count)
     char letter;
         letter=characters[count];
     LCD display(letter);
    } //function
    void LCD_display(char letter)
        lcd init();
        lcd_gotoyx(1,1);
        lcd_putc(letter);
        while(1);
       } // function
```