Palestine Polytechnic University



College of Engineering & Technology

Mechanical Engineering Department

Design Building And Operating Of Simple Vapor Compression Refrigeration System For Laboratory Demonstration

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Hebron – Palestine

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Project Name

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نظام كلية الهندسة والتكنولوجيا وإشراف ومتابعة المشرف المباشر على المشروع وموا يم هذا المشروع إلى دائرة الهندسة الميكانيكية ، وذلك للوفاء بمتطلبات درجة البكالوريوس في الهندسة تخصص هندسة التكييف والتبريد .

توقيع المشرف

توقيع اللجنة الممتحنة

توقيع رئيس الدائرة

Dedication

To our Families For their support

To our Teachers For help us until the end

To our friends Who give us Positive sentiment

To oppressed people throughout the world and their struggle for social justice and egalitarianism

To our great Palestine

To our supervisor Dr. Ishaq Sider

To all who made this work possible

Mohammad Taha Abu Srour

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ABSTRACT

Design building and operating of simple vapor compression refrigeration system for laboratory demonstration .

In this project we will design and build an educational device which works on the principles of the simple refrigeration cycle so as simplified the understanding through learning the refrigeration subject.

This device will check refrigerant case, its temperature, pressure in each stage in the cycle, and sense the factor affecting the behavior of refrigerant, the device which we are looking to build is related the theoretical learning and experimentally on the refrigeration cycle.

يهدف هذا المشروع الى تصميم وبناء جهاز تعليمي يعمل على مبدأ دورة التبريد البسيطة التي تعتبر المكون الرئيسي للعديد من جهزة التبريد () ، كما ونهدف من خلال النموذج توضيح المكونات الرئيسية لدورة التبريد والتوصيلات الميكانيكية والكهربائية المكونة للدورة ، والعوامل المؤثرة على سلو حيث يمكننا من خلال الجهاز تتبع سلوكه في كل مرحلة من مراحل الدورة .

خذت فكرة الجهاز من نماذج تقوم العديد من الشركات العالمية بتصنيعها ويمكن تجميع الجهاز محليا

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INTRODUCTION

1.1 Introduction

1.2 Objective

1.3 Scope

1.4 Time Table

1.5 The budget of the project

CHAPTER ONE

INTRODUCTION

1.1. Introduction

This kit is specifically designed for educational aims and it includes all the components of the hydraulic of a beverage cooler . it enables students to deal with the issues concerning the assembling of the hydraulic circuit , the connection of electric components , besides the calibration of the controller for an optimum operation of the system . the kit also includes the pipes that can be used together with the standard tools for refrigerator technicians to assemble the hydraulic circuit . this kit can easily be disassembled for a repeateduse.

1.2. Objectives

The project objective are:

- 1- The building and designs of educational models help students to understand the basic of simple refrigeration cycle .
- 2- Applied the theoretical education for design and building device .
- 3- Enrich the refrigeration lab by the devices to interest education .
- 4- simplify the student's learning process by integrating concrete elements into the theory learned in the classroom and textbooks.
- 5- simplify the teacher's work by demonstrating how the theory of the topic studied is applied in practice.

1.3. Scope

- 1) Select one of the devices that are present in the catalogue.
- 2) Select and design the appropriate loading to achieve the objective of the work device .
- 3) Calculate the cooling loading .
- 4) Select the components of project.
- 5) Search for the components .

- 6) Make complete drawing design .
- 7) Buy the components and begin building thedevice.
- 8) Make tests one the device and read the measurement .
- 9) Attach instruction sheet on the device to illustrate how to use.

1.4. Time Plan

Table 1.1: Timetable for the second semester time (week)

Task\week	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
Project selection And proposal																
Information Gathering																
Writing introduction																
Cooling load Calculation																
Selection the cycle components																

Table 1.2: Timetable for the first semester time (week)

Activity	1	2	3	4	5	6	7	8	9	1 0	1 1	1 2	1 3	1 4	1 5
Drawing															
Search for the components															
Build The Project															
The Results of Project															

1.5. The Budget Of The Project

	Component name	Price (NIS)
1	Compressor	300
2	Condenser	200
3	Evaporator	250
4	Connecting pipes	250
5	2-Pressure Gauges	100
6	Frame	700
7	Refrigerant	200
8	Control Equipment's (Thermostat Filter Sight glass Capillary tube Switches Wires Valves)	800
	Total price	2800 (NIS)

Table (1.3): The budget of the project:

CHAPTER 2

Cycle components and market review

- 2.1. Name of companies
- 2.2.Simple refrigeration cycle
- 2.3.Components of assembly kit of beverage cooler

CHAPTER TWO

Cycle components and market review

In this chapter we will review the name of some companies which designs and manufactures the educational device in the field of technical refrigeration also we will review some models that we make and design, we chose one of these of these models and we will make design and implementation in practice.

2.1 Name of companies:

2.1.1Elettronica venta:

It is an Italian company recognised as a world leader in technical training equipment.

These are some of the technical equipment produced by this company[Reference11] .



Figure 2.1: Assembly kit of beverage cooler



Figure 2.2:Preassembled kit for refrigeration and air conditioning

2.1.2Edibonfor technical teaching equipment :

The American company experienced provider of design to manufacturing solutions and teaching labs to educators and students for over 25 years based in concord.[Reference10]

These are some of the technical equipment produced by this company.



Figure 2.3:Refrigeration cycle demonstration unit



Figure 2.4:Refrigeration unit with refrigeration and freezing chamber



Figure 2.5:Computer controlled absorption refrigeration unit



Figure 2.6:One condenser (water)and one evaporator



Figure 2.7:One condenser (water)and one evaporator(water)

The device will design and build like to the device in Figure 2.1(assembly kit of beverage cooler) that we will design and build .

2.2.Simple refrigeration cycle

Simple refrigeration cycle is a simple vapor compression refrigeration system, in which suitable working substance termed as refrigerant. It condenses and evaporates at a temperature and pressure close to atmospheric condition. It can be used ordinary application of refrigeration and it gives a high coefficient of performance, but the single stage refrigeration cycle is limited in the lower evaporation temperature and the lower vapor pressure in the evaporator, and the compressor sucks less refrigerant per stroke so it has a lower volumetric efficiency. This problem caused reducing capacity to the point where load and capacity are in balance [Reference1].

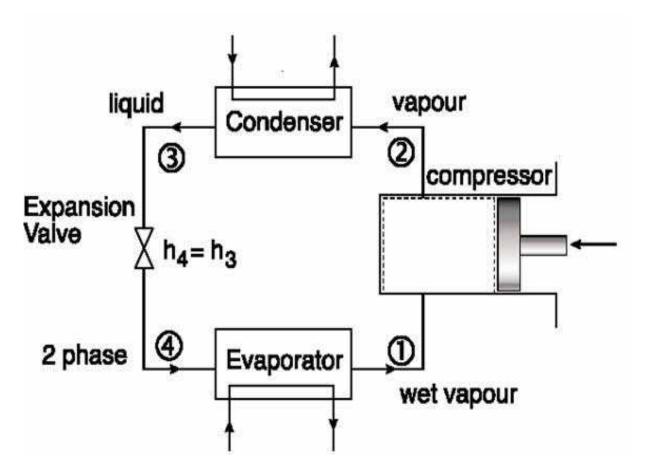


Fig.2.8:Simple vapor compression refrigeration system .

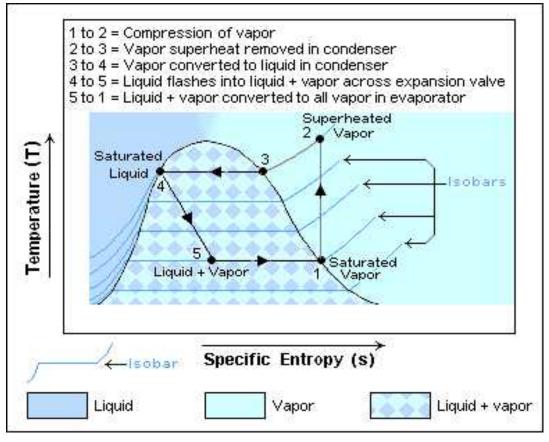


Fig.2.9: T-S diagram.

Sometimes the vapor refrigerant is required to be delivered at a very high pressure as in the case of low temperature refrigeration systems , in such cases the vapor refrigerant must be compressed by employing two or more compressors placed in series . The compression carried by this case is called multistage compression .

2.3.Components of simple refrigeration cycle

There are several mechanical components required in simple refrigeration cycle system. This part of project discuss the four major components of the system and some auxiliary equipment's working with these major components [reference 5].

The major components of the simple refrigeration cycle are as follows :

- Compressor .
- Condenser .
- Evaporator .
- Thermostatic expansion valve.

2.3.1. Compressor

In refrigeration cycle, the compressor has two main functions within the refrigeration cycle. One of this function is to pump the refrigerant vapor from the evaporator so that the desired temperature and pressure can be maintained in the evaporator . The second function is to increase the pressure of refrigerant vapor through the process of compression, and simultaneously increase the temperature of the refrigerant vapor . By this change in pressure the superheated refrigerant flows through the system. Refrigerant compressors, which are knows as the heart of the refrigeration system, can be divided into three main categories : [reference 5]

- Hermetic compressor
- Simihermetic compressor
- Open compressor

In this project we will use hermetic compressor.

Hermetic Compressor

These compressors, are available for small capacities, motor and drive are sealed in compact welded housing. The refrigerant and lubricating oil are contained in this housing. Almost all small motor-compressor pairs used in domestic refrigerator, freezers, and air conditioners are of the hermetic type. Their revolutions per minute are either 1450 or 2800 rpm. Hermetic compressors can work for a long time in small capacity refrigeration system without any maintenance requirement and without any gas leakage, but they are sensitive to electric voltage fluctuations, which may make the copper coils of the motor burn. The cost of these compressors is very low [reference 5].

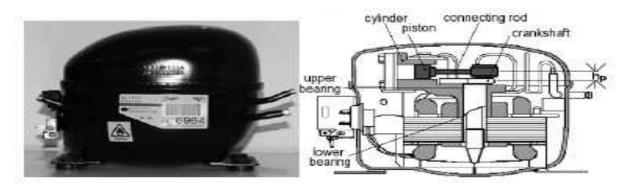


Figure 2.10: Hermetic Compressor

Expectations From The refrigerant compressors are expected to meet the following requirements high reliability, long service life, easy maintenance, quiet operation, compactness, and low cost .

2.3.2 Condensers

A condenser is a major system component of refrigeration system. It also an indirect contact heat exchanger in which the total heat rejected from the refrigerant is removed by cooling medium, usually air or water. As a result, the gaseous refrigerant is cooled and condensed to liquid at the condensing pressure [reference 2].

Air cooled condensers

The air cooled condensers find application in domestic, commercial, and industrial refrigerating, chilling, freezing, and air conditioning systems, the centrifugal fan are used in the condenser particularly for heat recovery and auxiliary ventilation applications. In fact, they employ outside air as cooling medium [reference 6].

Fans draw air past the refrigerant coil and the latent heat of the refrigerant is removed as sensible heat by the air stream[reference 6].

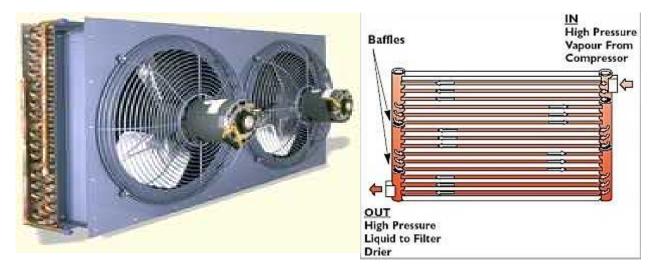


Figure 2.11: Air Cooled Condenser

2.3.3 Evaporator

Evaporator is an important device used in the low pressure side of a refrigeration system. The liquid refrigerant from the expansion valve enters into the evaporator where it boils and changes into vapor . The function of an evaporator is to absorb heat from the surrounding location or medium which is to be cooled, by means of refrigerant . The temperature of the boiling refrigerant in the evaporator must always be less than the temperature of the surrounding medium so that the heat flows to the refrigerant [reference 6].

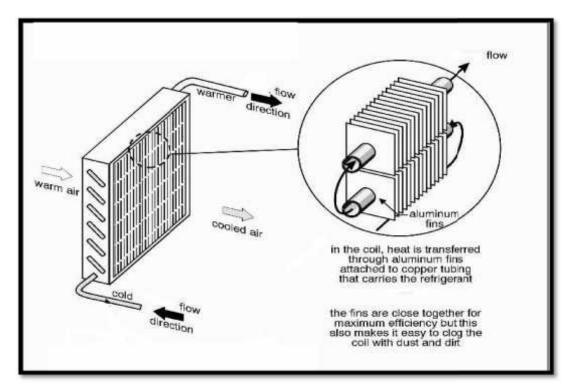


Figure 2.12: Evaporator

Bare Tube Coil Evaporator

The simplest type of evaporator is the bare tube coil evaporator, as shown in figure 3.3. The bare tube coil evaporator are also known as prime surface evaporators. Because of its simple construction, the bare tube coil is easy to clean and defrost. A little consideration will show that this type of evaporator, offers relatively little surface contact area as compared to other types of coils. The amount of surface area may be increased by simply extending the length of the tube,

but there are disadvantages of excessive tube length. The effective length of the tube is limited by the capacity of expansion valve. If the tube is too long for the valve's capacity, the liquid refrigerant will tend to completely vaporize early in its progress through the tube, thus leading to excessive superheating at the outlet. The long tubes will also cause considerably greater pressure drop between the inlet and outlet of the evaporator. This results in reduced suction line pressure.

The diameter of the tube in relation to tube length may also be critical. If the tube diameter is too large, the refrigerant velocity will be too low and the volume of refrigerant will be too great in relation to the surface area of the tube to allow complete vaporization. This, in turn, may allow liquid refrigerant to enter the suction line with possible damage to the compressor (slugging). One the other hand, if the diameter is too small, the pressure drop due to friction may be too high and will reduce the system efficiency. The bare tube coil evaporators may be used for any type refrigeration requirement [reference 6].

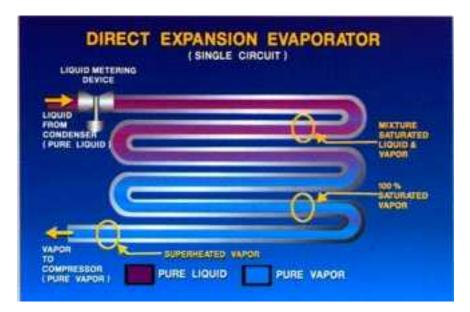


Figure 2.13: Bare Tube Coil Evaporator

2.3.4 Throttling Devices

In practice, throttling devices, called either expansion valves or throttling valves, are used to reduce the refrigerant condensing pressure (high pressure) to the evaporating pressure (low pressure) by a throttling operation and regulate the liquid refrigerant flow to the evaporator to match the equipment and load characteristics. These devices are designed to proportion the rate

at which the refrigerant enters the cooling coil to the rate of evaporation of the liquid refrigerant in the coil, the amount depends – of course – on the amount of heat being removed from the refrigerated space [reference 6].

The most common throttling devices are as follows :

- Thermostatic expansion valves .
- Constant pressure expansion valves .
- Float valves .
- Capillary tubes .

Note that a practical refrigeration system may consist of large range of mechanical and electronic expansion valves and other flow control devices for small and large scale refrigeration system, comprising thermostatic expansion valves, solenoid valves and thermostats, modulating pressure regulators, filter driers, liquid indicators, non-return valves and water valves, and furthermore, decentralized electronic systems for full regulation and control.

Capillary Tubes

The capillary tube is the simplest type of refrigerant flow control device and its shown is figure 2.14 and may be used in place of an expansion valve. The capillary tubes are small diameter tubes through which the refrigerant flows into the evaporator. These devices, reduce the condensing pressure to the evaporating pressure in a copper tube of small internal diameter (0.4 - 3 mm diameter and 1.5 - 5 m length), maintaining a constant evaporating pressure independently of the refrigeration load change. A capillary tube may also be constructed as a part of a heat exchanger, particularly in household refrigerators.

With capillary tubes, the length of the tube is adjusted to match the compressor capacity. Other consideration in determining capillary tube size include condenser efficiency and evaporator size. Capillary tubes are most effective when used in small capacity systems .



Figure 2.14:Capillary Tube

2.3.5. Auxiliary Component

The auxiliary components are very important in the refrigeration system, their working together with main components allowing system works very well, and we will discuss some auxiliaries in the following sections.

2.3.5.a FilterDrier

Filter-driers are used to protect the compressor from contamination, particularly moistureleft in the system at the time of installation and keeps the system free of impurities duringoperation, such as motor burn byproducts[reference 6].



Figure 2.15:FilterDrier

2.3.5.b Sight Glass

The Sight Glass was designed to provide an accurate method of determining the moisture content of a system's refrigerant, Unique 3% high accuracy moisture indicator, Refrigerant level indicator[reference 6].



Figure 2.16:Sight Glass

2.3.5.cThermostat

+

A thermostat is a component of a control system which senses the temperature of a system so that the system's temperature is maintained near a desired set point. The thermostat does this by switching heating or cooling devices on or off, or regulating the flow of a heat transfer fluid as needed, to maintain the correct temperature. The name is derived from the Greek words thermos "hot" and status "a standing".

Thermostat used in refrigeration system to senses the evaporating temperature. If this temperature reach the required temperature, the thermostat shut off the compressor, and when this temperature increase again it turn on the compressor [reference 1].



Figure 2.17: Thermostat

CHAPTER 3

COOLING LOAD

3.1 Introduction

3.2 load sources

3.3 Total cooling load

CHAPTER THREE

COOLING LOAD

3.1 Introduction

The total heat required to be removed from refrigerated space in order to bring it at the desired temperature and maintain it by the refrigeration equipment is known as cooling load. The purpose of a load estimation is to determine the size of the refrigeration equipment that is required to maintain inside design conditions during periods of maximum outside temperatures. The design load is based on inside and outside design conditions and its refrigeration equipment capacity to produce and satisfactory inside conditions . [reference 2].

3.2 load sources

The cooling load seldom results from any one single source of heat .Rather , it is the summation of the heat which usually evolves from several different sources . some of the more common sources of heat that impose the load on refrigerating equipment are : [Reference 3].

- 1) The wall heat gain.
- 2) Defrosts heater heat gain.
- 3) Fan motor heat gain.

Overview about the Chamber :

Storage temperature is $-5 \ ^{\circ}C$. Surrounding Temperature is $35 \ ^{\circ}C$. Chamber Dimensions (0.6, 0.5, 0.3) meter. Length = 0.6 mWidth = 0.5 mHigh = 0.3 m

Chamber size = $0.6 * 0.5 * 0.3 = 0.09 \text{m}^3 = 90 \text{ liter}$.

3.2.1 The wall heat gain

The wall heat gain load, sometimes called the leakage load, is a measure of the heat flow rate by conduction through the walls of the refrigerated space from the outside to the inside. since there is no perfect insulation, there is always a certain amount of heat passing from the outside to the inside whenever the inside temperature is below than the outside. the wall gain load is common to all refrigeration application and is ordinary a considerable part of the total cooling load, commercial storage coolers and residential air conditioning applications are both examples of applications where in the wall gain load often accounts for the greater portion of the total load. [reference 3].

 $Q_{wall} = \mathbf{U} * \mathbf{A} * \Delta T \qquad (3.1)$

Where :-

- A : Outside Surface Area of The Wall $[m^2]$.
- U: the overall heat transfer coefficient [$W_{\circ C * m^2}$].
- *T*: the temperature differences across the walls [$^{\circ}$ C].

$$T = T_{out} - T_{in}$$

Where :

T_{in}: -5 °C T_{out}: 35 °C

Overall heat transfer coefficient is computed by the following :

$$U = \frac{1}{\frac{1}{h_{i}} + \frac{x_{1}}{k_{1}} + \frac{x_{2}}{k_{2}} + \dots + \frac{1}{h_{0}}}....(3.2)$$

Where :

 \mathbf{x} : the thickness of the layer of the wall [m].

k : the thermal conductivity of the material [W $_{m. \circ C}$].

 h_i : the convection heat transfer coefficient of inside air [$W_{\text{°C}, m^2}$].

Forced convection by using fan (30 - 100), taken $50[W_{\circ C. m^2}]$. h_o : the convection heat transfer coefficient of outside air $[W_{\circ C. m^2}]$. Free convection inside the room (5 - 20), taken $10[W_{\circ C. m^2}]$. All walls are constructed of three layers as shown in Figure 3.1.

Figure 3.1: Chamber wall layer

- 1) Galvanized steel 0.1 [cm] , k = 15.60 [$W_{m, \circ C}$] . From Table A-1.
- 2) polyethylene 5 [cm] , k = 0.036 [$\frac{W}{m}$ $\frac{C}{C}$]. From Table A-1.
- 3) Galvanized steel 0.1 [cm], k = 15.60 [$W_{m, \circ C}$]. From Table A-1.

$$U_{wall} = \frac{1}{\frac{1}{50} + \frac{0.002}{156} + \frac{0.05}{0.036} + \frac{1}{10}} = 0.662 \ [W_{\circ C} \ m^2].$$

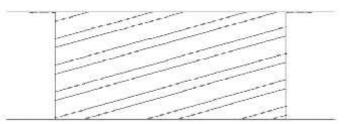


Figure 3.2: Chamber door layer

1) Glass single layer 1 [cm] , $k = 6.42 [\frac{W}{m} \circ C]$. From Table A-1.

$$U_{door} = \frac{1}{\frac{1}{50+642}+10} = 8.226 \ [W_{\circ C. m^2}].$$

3.2.2 Defrosts heater heat gain

The process of removing frost from the evaporator and around the door is called defrosting .

3.2.2.a Defrosts heater heat gain of the evaporator

If the surface temperature of the evaporator coil is ($0 \ ^{\circ}C$) and lower, frost accumulates on the coil surface. Because frost impedes air passage and reduces the rate of heat transfer of the coil, it must be removed periodically. An electric heating element is used as a simple and effective way to defrost the coil. [reference 1].

 $Q_{defrosts} = \varphi * P$ (3.3) Where :

P : Power of heater, taken 500 [W]

 φ : heater usage factor (0.1 – 0.5), taken 0.2

 $Q_{detrosts} = P * \varphi = 0.2 * 500 = 100$ [W]

3.2.3 Fan motor heat gain

The evaporator fan motor release a heat, this heat relatively equal the power of the motor :

 Q_{motor} = power of motor = 25 [W]

3.3 Total cooling load

The total cooling load is the summation of the heat gains:

 $Q_T = Q_{wall} + Q_{defrost} + Q_{motor}....(3.4)$ $Q_T = 87.825 + 100 + 25$ $Q_T = 212.825$ [W]

Add 20 % as safety of factor.

Total cooling load = $Q_T * 1.2$ (3.5) Total cooling load = 212.825 * 1.2 = 255.39 [W]

CHAPTER 4

CYCLE ANALYSIS

- 4.1 Refrigerant Selection
- 4.2 Cycle Analysis
- 4.4 Calculation for cycle using R-134a
- 4.5 Calculation of the coefficient of performance (COP)

CHAPTER FOUR

CYCLE ANALYSIS

4.1 Refrigerant selection

In the selection of an appropriate refrigerant for use in a refrigeration or heat pump system, there are many criteria to be considered. Briefly, the refrigerant are expected to meet the following condition.

- Low boiling point .
- High critical temperature .
- High latent heat of vaporization .
- Low specific volume of vapor .
- Non corrosive to metal .
- Nonflammable and non-explosive .
- Nontoxic.
- Low cost.
- Easy to liquefy at moderate pressure and temperature .
- Easy of locating leaks by suitable indicator .
- Mixes well with oil .

To select refrigerants successfully we must consider the above properties . We made a comparison between various refrigerants and found that , the best refrigerants could be used is R-134a. In addition to above properties in selection process of R-134a we have to determine the compressor type that works perfectly with R-134a, and it has to be cheap and available . The pressure inside cycle must be a little greater than atmospheric pressure . If the atmospheric pressure became greater than inside cycle pressure will destroy the cycle, so we select R-134a . Refrigerant 134a has low temperature at 0.5 atm., so R134a is suitable for our system[reference 1].

4.2 Cycle Analysis

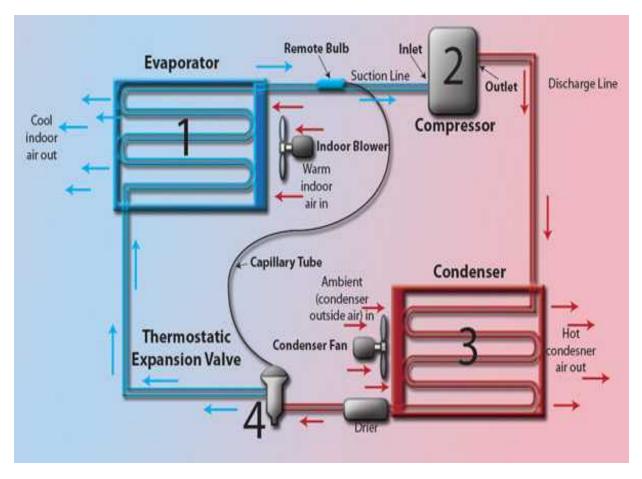


Figure 4.1: Simple Refrigeration Cycle

4.3Calculation For cycle Using R-134a

Figure 4.2 Shows P-h chart for R-134a [reference 7].

$Q_e = \vec{m} \times q_e \dots \dots$	
----------------------------------------------------------------------------------------------------------------------------------------------	--

$$Q_e = \vec{m} \times (h_1 - h_4)$$
(4.2)

$$\dot{m} = \frac{Qe}{(h1 - h4)}.$$
(4.3)

where :

 \vec{m} : mass flow rate [kg/s]

- Q_e : Heat transfer rate in evaporator (cooling effect) [W]
- q_e : Refrigeration effect [kJ/kg]
- h1: Enthalpy at point before compressor [kJ/kg]
- h₄ : Enthalpy at point before evaporator [kJ/kg]

 $\dot{m} = \frac{0.255}{394.284 - 256.160} = 0.00184 \text{ [kg/s]}$

 $Q_c = \vec{m} \times (h_2 - h_3)$ (4.4)

- $h_2: Enthalpy \ at \ point \ after \ compressor \ [kJ/kg]$
- $h_3: Enthalpy \ at \ point \ after \ condenser \ [kJ/kg]$
- Q_c : Heat transfer rate in condenser (condenser load) [W]

 $Q_c = 0.00184 \times (\; 423.835 - 256.160 \;)$

- $Q_c = 0.3085 \; [KW] = 308.82 [W]$
- $W_c = \dot{m} \times (h_2 h_1)$ (4.5)
- W_c : Compressor Work [W]
- $W_c = 0.00184 \times (423.835 394.284)$
- $W_c = 0.05437[KW] = 54.37[W]$

In horse Power = 142.7/746 = 0.0728 HP

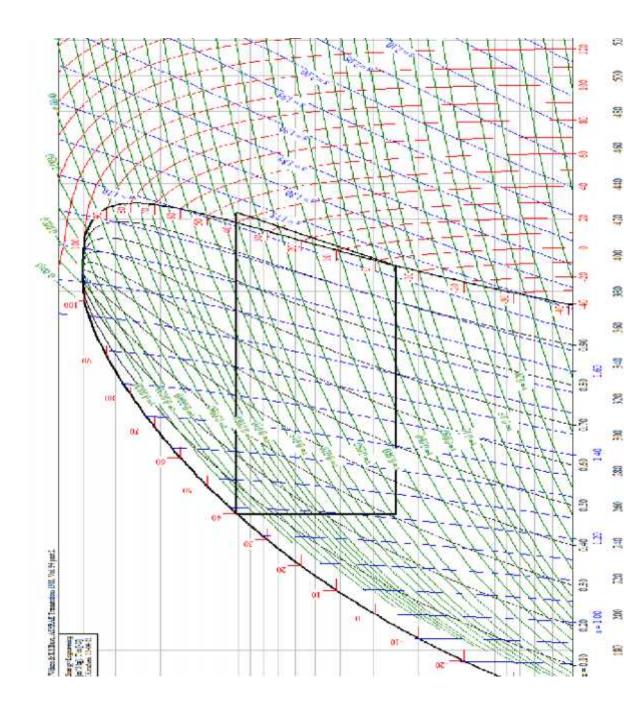


Figure 4.2: P-h chart for R-134a

Point	T	P	V	h	s
	[*C]	[bar]	[m^3/kg]	[kJ/kg]	[kJ/(kg K)]
1	-5.000	2.434	0.082302	394.284	1.7249
2	44.802	10.164	0.020555	423.835	1.7249
3	44.802	10.164	0.020555	423.835	1.7249
4	40.000	10.164	N/A	256.160	N/A
5	N/A	2.434	N/A	256.160	N/A
6	-5.000	2.434	0.082299	394.284	1.7249
15	N/A	10.164	N/A	256.160	N/A

Figure 4.3:properties of cycle

4.4 Calculation Of Coefficient Of Performance (COP)

 $W_c = 54.37 \ [W]$

 $COP = \frac{Qe}{Wc}....(4.6)$ $COP = \frac{255.39}{54.37} = 4.69$

4.5 Compressor Calculation And Selection

To determine the volumetric efficiency for the compressor can be used the equation (4.7).

 $v = c^* h......(4.7)$

where :

 $_{v}$: volumetric efficiency .

 $_{\rm c}$: volumetric efficiency due to clearance volume in compressor .

 $_{\rm h}$: volumetric efficiency due to heating occurs in compressor .

The volumetric efficiency due the clearance volume in compressor calculated by equation (4.8), [reference 8]

$$_{c} = 1 - c \left[\left(\frac{PH}{PL} \right)^{1/n} - 1 \right] \dots (4.8)$$

where :

- c : clearance volume (ratio between volumetric clearance and volume of cylinder of the compressor, c = 0.04 for low pressure, c = 0.02 for high pressure, [reference 9]
- n : exponential coefficient of expansion for refrigerant , n = 1 , [reference 4]
- PH : High pressure of the cycle .

PL: Low pressure of the cycle.

$$_{\rm c} = 1 - 0.02 \left[\left(\frac{10.164}{2.434} \right)^{1/1} - 1 \right] = 93\%$$

The volumetric efficiency due to the heating in compressor is get from equation (4.9), [reference 3]

 $h = \frac{Tevap}{Tcond}.$ (4.9)

where :

T_{evap.} : evaporator temperature [°K]

T_{cond.} : condenser temperature [°K]

$$_{h} = \frac{268}{313} = 85.6\%$$

 $_{v} = 93\% * 85.6\% = 79.6\%$

The theoretical volume flow rate (V) of the compressor can be calculated in equation(4.10), [reference 8]

 $\dot{V}_{theo} = \dot{m}^*$ (4.10)

Where :

 \dot{V}_{theo} : theoretical volume flow rate of the compressor [m³/s]

m : mass flow rate of refrigerant [Kg/s]

: specific volume at the inlet of compressor $[m^3/s]$.

$$\dot{V}_{theo} = 0.00184 * 0.082302 = 1.514 * 10^{-4} [m^3/s]$$

To determine the actual volume flow rate, using equation (4.),[reference 3]

 $\dot{V}_{act} = \frac{\dot{V}_{the}}{v} \tag{4.11}$

Where :

 \dot{V}_{act} : actual volumetric flow rate [m³/s]

$$\dot{V}_{act} = \frac{0.0001514}{0.795} = 1.9 * 10^{-4} [\text{m}^3/\text{s}]$$

The main consider to select the compressor is the actual volumetric flow rate, so we will chose a compressor that satisfy it in the next semester.

CHAPTER 5

Drawing

References

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Appendix A

- TABLE A-1Thermal Conductivity Of Materials
- TABLE A-2Maximum And Minimum Temperature For Hebron City

faterial	Description	Thermal Conductivity (k) W/m K	Thermal Conductance (C) <u>W/m² K</u>
Aasonry	Brick, common	0.72	
		1.30	
	Brick, face	0.72	
	Concrete, mortar or plaster	1.73	
	Concrete, sand aggregate Concrete block	1.75	
	Sand aggregate 100 mm		7.95
	Sand aggregate 200 mm		5.11
	Sand aggregate 200 mm		4.43
/oods	Manta ante cimitar burdunoda	0.16	
	Maple, oak, similar hardwoods Fir, pine, similar softwoods	0.12	
	Plywood 13 mm	V. 14	9.09
	Plywood 1.9mm		6.08
Roofing	Asphalt roll roofing		36.9
	Built-up roofing 9 mm		17.03
sulating	Blanket or batt, mineral or Polythane	0.039	
naterials	Board or slab		
	Cellular glass	0.058	
	Corkboard	0.043	
	Glass fiber	0.036	
	Expanded polystyrene (smooth)	0.029	
	Expanded polystyrene (cut cell)	0.036	
	Expanded polyurethane	0.025	
oose fill			
	Milled paper or wood pulp	0.039	
	Sawdust or shavings	0.065	
	Mineral wool (rock, glass, slag)	0.039	
	Redwood bark	0.037 0.043	
	Wood fiber (soft woods)	0.045	
	5° 4		6.42
Glass	Single pane		2.61
	Two pane		1.65
	Three pane		1.19
	Four pane		
Metal	Galvanized steel	15.6	
0.0000000	Aluminum	202	
	cooper	386	

TABLE A-1 Thermal Conductivity Of Materials

Month	Max. Temp.	Min. Temp.
	C°	C°
Jan	10.3	3
Fep	11.5	4.7
Mar	14.6	6.5
Apri	19.6	9.9
May	25.6	13.2
Jun	26	15.8
Jul	28	17
Aug	38	18
Sep	29	15
Oct	28	14
Nov	22	9,9
Dec	12	5.6

TABLE A-2 Maximum And Minimum Temperature For Hebron City

Appendix B

Catalogues

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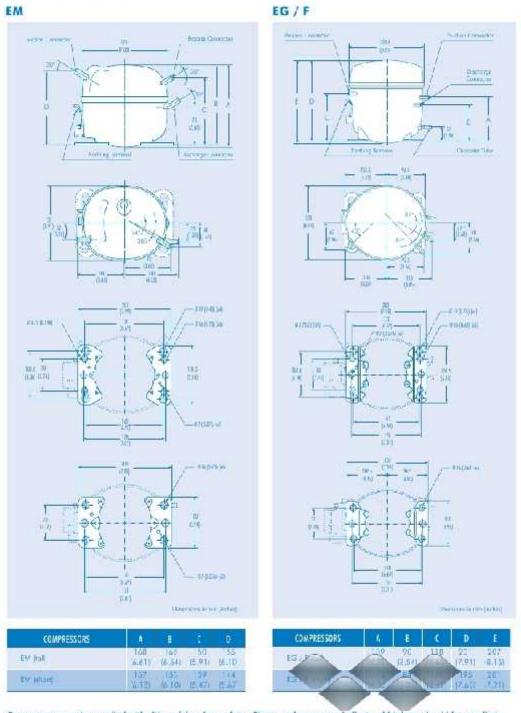
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1251	310	1225	174	1477	177	2975	246	ш,	752	312	1.94	24	2.14	202	317	21	103	LUT/RS # COR	213516159	(TARHEN) E		36. 33(
1544	112	1772	51.9	171	433	237	758	180	10	31	1.1	王將	215	3065	Ni	3149	1819	LSF/RSTR CSIR	293516678	MSP57AHK (1590		52.64
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R-600a - R-134a - Blends - R-290

10) - COMPRESSOR HOUSING

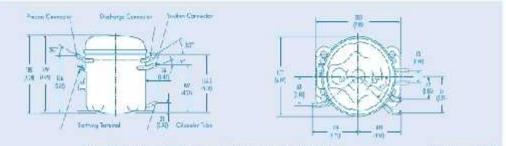


Compressors may be supplied with either of the above plotes. Please make sure you indicate which base should be supplied.

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PW



New Antonio piller with a flat FW transmitter the transmit houses we in the FM transport

Itispachens + mon bulled

				CONNEC	TORS INT	FNAL DU	MET SES -	nur (inc	ms)					
COMPLEXES				а	M						1	W		
MATERIAL			COOPE	1		COOF	IR ANTE	STER.		COOPE	1	COOP	ER PLATE	ATTE .
SUCTION	6.50 (0.256)	6.50 0.256	8.20 (0.023)	8.20	A#0 10.23et	the second second	6.50 (0.256)	A.40 (0.256)	100000000	8.90 (0.023)	A 20 (0.323)	.8.80 E.256)	A 20 (0.023)	6.10
DISCHARGE	4.54	3.50	4.54	6.50 (1006)	5.10	5.00	5.00 (n. 27)	8,50	Contraction of the	8.53	656 (* 254)	5.00	6.50 (7.254)	5.00
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OIL COOLER TUBE			×			-		12	1		-	4,77	1.0	~

				1	ONNECTO	JRS N	RNALDI	WETERS	- me di	nence]						
COMPRESSOR COMPRESSOR		F/E6														
AKATERIAL			000	5878						00	OF BRID	ATED ST	titi.			
SUCTION	3.50 £ (0.256) (0	100000000000000000000000000000000000000		COLUMN DOCUMENT	10000						6.50 (0.266)		8.20 (0.353)	8.20 (0.3.23)	CONTRACTOR OF	6.50
DISCHARGE	6.96 d (0.124) (3										(57) [] 25日					
PROCESS	5.50 E	100 T 100 T			6.50 (0.256)						6.53				6.50	
OIL COOLER TUBE	6. VD (0.12-) (0				(3.256)	-	-				±.51 (0.256)				4.77 (0.188)	

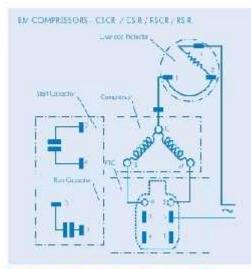
For other connectors configurations, please contact consules division.

	IU LEKA)	KE				
WATERIAL	CCORE		0	DOPERTI	ATED TTR	1) — (
CONNECTORS	$ \begin{array}{cccc} 1 & 1 & 2 & 0 & 0 & 0 & 0 \\ + 0 & 10 & 0 & 10 & 10 & 10 & 10 \\ - 2 & 10 & -3 & 0 & 0 & 0 \\ - 2 & 10 & -3 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 \\ & -3 & 0 & 0 & 0 & 0 \\ & -3 & $	4 A 		* 0 -C.12 -0.00 (0.201 (0.000) (0.000)	$\begin{pmatrix} 8.4 \\ -2.12 \\ 0.01 \\ (1255 \\ 0.205 \\ 2102 \end{pmatrix}$	100 400 400 400 400 400 400 400 400 400
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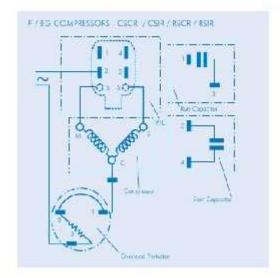
R-600a - R-134a - Blends - R-290

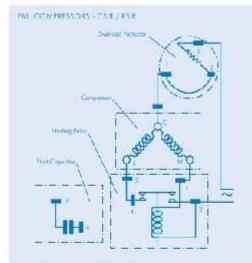
11) - ELECTRICAL DIAGRAMS



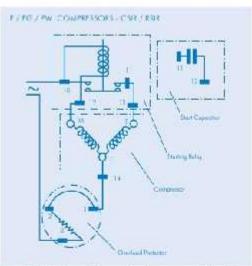
Compressors with a run capacitor must use PTC with 3 terminals.

Compressors without run capacitor use PIC with 1 terminal.





If application of a start capacitar is necessary, then it must be connected between terminals 3 and 4. To achieve this, just rupture this bridge.

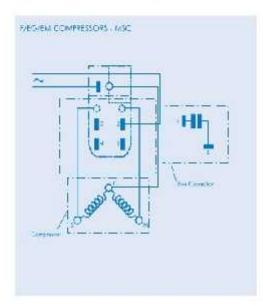


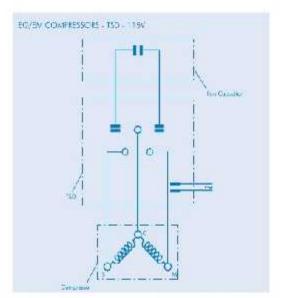
If application of a start capacitor is necessary, then it must be connected between terminals 11 and 13. This requires a specific relay, with fast on terminals for better start capacitor installation, which can be supplified over request

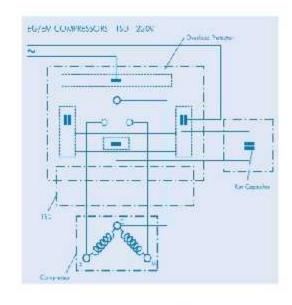


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11) - ELECTRICAL DIAGRAMS



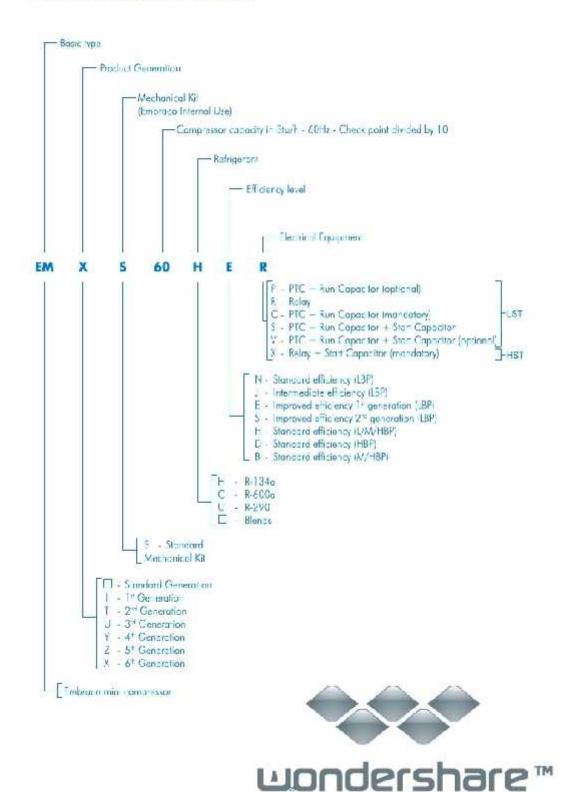






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13) - EM COMPRESSOR DENOMINATION





Quick Select Guide	Co	ndensing Units, Type	• Optyma [™]					
Introduction and Ow	anuleu Co	tyma ^{re} is the widest rang	e of hermetic					
	Cor Cop Cor Cor Cos Al effi Cor	idensing units on the ma tyma ¹⁴ condensing unit i seaty models of reaproc appressors so to cover a la mmercial refrigeration ap tts and complexity of the Optyma ¹⁴ condensing un icient and reliable. That n rsumption and less runni s, for service and mainter	ake, s available with high ating and scroll rige range of plications, reoucing systems, iits are extremely nears less energy ing costs, less				Ţ	
Nomenclature / Mod	el No.				V		•	
		-		-				
Application Design	1							
Refrigerant								
Condensersize		11060003	3UWA000B					
hp rating			SUWAUUUB					
				1111				
6 Certification								
5 Certification 7 Version 8 Electrica code		1234 5	6.7 8					
7 Version	1	1234 5 L H	6 7 8 C: Air cooled condenser, G: Air cooled condenser,	110 			2	
7 Version 8 Electrical code Luw	n	L		110 			2	
7 Version 8 Electrical code Low Medium/High	n 1	L H U		dual fan, nem			2	
7 Versian 8 Electrica code Luw MediumvHich Universe Low/Mec/Hig	(in	L H	G : A rootled condenset	dualfan, rem	netic compres		2	
Version Electrical code Luw MediumvHigh Universal Low/Med/Hig E-12 replacement	d G	L H U	G: A rootled condense;	dualfan, rem	nètic compres: I Recognized		2	
Version Electrical code Medium/Hich Universal Low/Med/Hig E-12 replacement E-134c R-404A/7-537	З G H	L H U Condenset size-	G : A reacted condenses hp rating in hundraths of 16,0033 = 1/5 hc	dualfan, rem	nètic compres: I Recognized		2	
Version Electrical code Luw Medium/High Universal Low/Med/Hig E-12 replacement E-134a	З G H M	L H U Condenset size-	G : A reacted condenses hp rating in hundraths of 16,0033 = 1/5 hc	9 0: 01	netic compres: I Renngn zerf L Listed	sc/	2	
Version Electrical code Low Medium/High Universal Low/Med/Hig E-12/replacement E-134s R-4044/1-537 R-22 P-4044/1-134s/R-90/7/R	3 G H M R-407(* 7	L H U U Condenset size fra 11/PF ambre 1	G : A reacted condenses hp rating in hundraths of 16,0033 = 1/5 hc	decifan, -em -p 5 2: UL 0: UL 0: UL 0: UL	netic compless I Rectignized L'Listed	ser 115V, 1 ph		8
Version Electrical code Universal Low/Mec/Hig E-12 replacement E-134a E-4044/13-537 E-22 E-4044/13-537 E-22 E-4044/13-134a/R-90/7/R	З G H M	L H U U Condenset size fra 11/PF ambre 1	G : A reacted condenses hp rating in hundraths of 16,0033 = 1/5 hc	decifan, -em p 5 U: Ui N: Compn N: Compn	netic compress I Rectognized L Listed recons & fan(s) I resson & fan(s) I	ser 115V, 1 pr., 259V, 1 pr.,	GC 11z	000
Version Electrical code Luw MediumvHich Universal Low/Med/High F-12 replacement F-12 replacement F-12 replacement F-22 F-4044/1-537 F-22 F-4044/1-537 Universal Low/R-90/1/R M a s	G H H R-ANYC 7 Wholesale mode	L H U Condenser size-4 sizer fra 11%F ambre 1	G : A reacted condenses hp rating in hundraths of 16,0033 = 1/5 hc	a ili a i i a i i i i	netic compress I Rectognized Litisted recons & fan(s) I resson & fan(s) I resson 205-2304	ser 115V, 1 թղ, 250V, 1 թղ,	60 Hz Hz: Far (6) 230V, 1 p	
Version Electrical code Luw Medium/High Universal Low/Med/High R-12/replacement R-4044/15-537 R-4044/15-537 R-22 P-4044/15-134-a/R-907/R M = B = B =	3 G H M R-ANYC 7 Wholesale mode Power rand Power rand	L H U U Goudenset size-4 sizer fra 119F ambie 1	G : A reacted condenses hp rating in hundraths of 16,0033 = 1/5 hc	A Compr P A III U: UI A Compr N: Compr Q: Compr R: Compr	netic compress I Rennigni zed L Listed resson & fan(s) I resson 205-2304 resson 205-2304	ster 115V, 1 p.n. 250V, 1 p.n. 250V, 1 p.n. 3 ph, 60 Hz, F	60 Hz Hz Har (5) 230V, 1 p an(c) 460V, 1 ph, 6	l Hz
Version Electrical code Luw MediumvHich Universal Low/Med/High E-12 replacement E-12 replacement E-12 replacement E-12 replacement E-12 replacement P-4044/1-537 P-22 P-4044/1-134-x/R-9077/R W = B = B = C =	3 G H M N.ANY 7 Wholesale mode Power cord, rece Clectrical box, pr	L H U U Condenset size - 4 sizer fra 110F ambie 1	G : A reacted condenset hp rating in hundraths of LE: 0033 = 1/5 hg 1030 = 10 hp	A Compr P A III U: UI A Compr N: Compr Q: Compr R: Compr	netic compress I Rennigni zed L Listed resson & fan(s) I resson 205-2304 resson 205-2304	ster 115V, 1 p.n. 250V, 1 p.n. 250V, 1 p.n. 3 ph, 60 Hz, F	60 Hz Hz: Far (6) 230V, 1 p	l Hz
 Version Electrical code Luw MediumvHigh Universal Low/Med/High R-12 replacement R-4044/12-537 R-22 R-4044/12-537 R-23 R-4044/12-537 R-24 R-4044/12-537 R-24 R-4044/12-537 R-25 R-26 R-4044/12-537 R-26 R-4044/12-537 R-27 R-27 R-27 R-27 R-34 R-34	3 G H M NANY 7 Wholesale mode Power rand Power rand Power rord, rece Clectrical box, pr Electrical box, re	L H U U Gondenset size-4 sizer Fri 119F ambre 1 el el Tover over cord, receiver receiver, fuel pressure conto	G: A reacted condenses hp rating in hundraths of 16:0033 = 1/5 hg 10:00 = 10 hp ol, cantridge fan cycling rol, cantridge fan cycling	A Compr P A III U: UI A Compr N: Compr Q: Compr R: Compr	netic compress I Rennigni zed L Listed resson & fan(s) I resson 205-2304 resson 205-2304	ster 115V, 1 p.n. 250V, 1 p.n. 250V, 1 p.n. 3 ph, 60 Hz, F	60 Hz Hz Har (5) 230V, 1 p an(c) 460V, 1 ph, 6	l Hz
7 Version Electrical code Luw MediumvHich Universal Low/Med/High R-12 replacement R-4044/15-537 R-22 P-4044/15-537 R-22 P-4044/15-134-3/R-907/R N = B = C = D = E = E =	3 G H M A.any 7 Wholesale mode Power rand Power rand Power rord, reco Clectrical box, pr Electrical box, re Electrical box, re	L H U U U U U U U U U U U U U U U U U U	G: A reacted condenses hp rating in hundraths of 16:0033 = 1/5 hp 10:00 = 10 hp 00, cartridge fan cycling rol, cartridge fan cycling KPU fan cycling control	A Compr A Compr A Compr A Compr A Compr A Compr A Compr	netic compress I Rennigni zed L Listed resson & fan(s) I resson 205-2304 resson 205-2304 resson 205-2304 resson 205-2304	scr 115V, 1 p.n. 250V, 1 p.n. 250V, 1 p.n. 3 p.h. 50 Hz, 5 3 h, 50 Hz, 5	60 Hz Hz Har (5) 230V, 1 p an(c) 460V, 1 ph, 6	l Hz
Version Electrical code Luw MediumvHich Universal Low/Med/High R-12 replacement R-4044/15-537 R-22 P-4044/15-537 R-22 P-4044/15-134-3/R-907/R N = B = C = D = E = C = D =	3 G H M N-ANY 7 Wholesale mode Power cord, rece Clectrical box, pr Electrical box, re Electrical box, re Clectrical box, re Electrical box, re Control, larger fil WE + filter driar,	L H U U Condenses size - 4 disec for 110F amble 1 amble 1 el over ord, receiver steines, low pressure contre celver, dual pressure contre celver, dual pressure contre celver, dual pressure contre inter 3 hp dual fan units use	G: A reacted condenses hp rating in hundraths of 16:0033 = 1/5 hp 10:00 = 10 hp 00, cartridge fan cycling rol, cartridge fan cycling KPU fan cycling control	A UII P A UII U: UI A Compo N: Compo R: Compo R: Compo R: Compo R: Compo R: Compo R: Compo R: Compo	netic compress I Bertrign zed L Listed resson & fan(c) I resson 205-2304 resson 205-2304 resso	scr 115V, 1 p.n. 250V, 1 p.n. 250V, 1 p.n. 35, 50 H.z. F 35, 50 H.z. F 35, 50 H.z. F 36, 50 H.z. F 3	60 Hz Hz: Fanks) 232V, 1 p an(s) 460V, 1 ph, 6 Fan(s) 372V, 1 ph, 6 MBP/HBP	l Hz
Version Electrical code Luw MediumvHigh Universal Low/Med/High K-12 replacement R-404A/7-537 R-22 P-404A/7-134 x/R-9077R W I B - B - C - D - E - P -	3 G H M A.40% 7 Wholeszie mode Power cord, recs Cleatrical bax, pr Electrical bax, pr Electrical bax, re ronthol, larger til WE 4 filter driar, F	L H U U U U U U U U U U U U U U U U U U	G: A reacted condenses hp rating in hundraths of 16:0033 = 1/5 hp 10:00 = 10 hp 00, cartridge fan cycling rol, cartridge fan cycling KPU fan cycling control	A Compo A Compo	netic compress I Rectignized Litited recent & fan(s) I resson & fan(s) I resson & fan(s) I resson 205-2309 resson 205-2309 resson 275Y 0 p resson 575Y 0 p resson 575Y 0 p	stor 115V, 1 p. n. 250V, 1 p. n. 250V, 1 p. n. 350 h, 60 Hz; F 35h, 6, 0 Hz; F 35h, 6, 0 Hz; F 35h, 6, 0 Hz; F	60 Hz Hz Han (s) 232V, 1 p an (s) 460V, 1 ph, 6 Fan (s) 372V, 1 ph, 6 MBP, HBP 90°F	l Hz
Version Electrical code Luw MediumvHigh Universal Low/Med/High K-12 replacement R-124 P-4044/1-537 R-22 P-4044/1-537 R-22 P-4044/1-1344/R-00/7/R W = B = D = E = D = S = S = QU = D =	3 G H M A. ANY 7 Wholesale mode Power cord, rece Clectrical box, pr Electrical box, pr Electrical box, re Electrical box, re Electrical box, re Electrical box, re Electrical box, re Electrical box, re Stancard unit.	L H U U Condenses size - 4 disec for 110F amble 1 amble 1 el over ord, receiver steines, low pressure contre celver, dual pressure contre celver, dual pressure contre celver, dual pressure contre inter 3 hp dual fan units use	G: A reacted condenses hp rating in hundraths of 16:0033 = 1/5 hp 10:00 = 10 hp 00, cartridge fan cycling rol, cartridge fan cycling KPU fan cycling control	A Compo A Compo	netic compress I Bertrign zed L Listed resson & fan(c) I resson 205-2304 resson 205-2304 resso	scr 115V, 1 p.n. 250V, 1 p.n. 250V, 1 p.n. 35, 50 H.z. F 35, 50 H.z. F 35, 50 H.z. F 36, 50 H.z. F 3	60 Hz Hz: Fanks) 232V, 1 p an(s) 460V, 1 ph, 6 Fan(s) 372V, 1 ph, 6 MBP/HBP	l Hz



USCO.PS.CO3.33.22 / 53' J0229



Quick Select Guide

Condensing Units, Type Optyma"

Produ	ct Se	lection	n .

*Ambient temperature = 90°F Return gas = 65°F Subcooling = 5°F

	R-194a MEP		Ambient temperature ("F)				atevap	Capacit ASHI erating (A:"	tira (°F)			
Competitor Nodel Nos.	Damfess Model No.	Code Nc.		Ó	5	10	15	28	25	36	35	40	45
			sc	1052	1106	1330	1505	1671	'8SD	2546	3260	2472	2530
#FA347* M2PH002D	005000000000000000000000000000000000000	11412017	25	000	1148	1237	34/7	1607	1723	1972	2176	2383	260
M2FH3024		114112212	:00:	566	1100	1254	1386	1543	1518	1655	A.92	2239	253
CALIFORNIA P.			HO	EBO	1004	1129	1271	:43	1577:	1740	1923	2.02	230
			50	11930	1955	1514	9900	1884	2095	38%	7541	2775	302
PEA443U	UCGC0025EWB000D	114N2019	<u>55</u>	1151	1306	1451	1629	1818	2022	2225	2452	2680	292
M2EH0026	0000002281100000	11402015	100	1109	1256	1407	1580	1752	:945	2144	2164	2583	251
			110	1024	1Hz	13.11	1901	1020	NCB1	Ester	2366	2389	
			SC		1709	1927	2179	2431	2717	30%4	3324	3644	399
AEA4440	HEGCODSEUWCODDB	116N2022	C5		1£48	1858	2101	23.45	2622	2916	3108	3517	394
M2FHA283	neacouse of reason	Henzezz	100		1560	1739	2024	2259	2325	2753	3091	3395	370
			114		Mc.2	licol	186.9	108°	2135	258.2	2859	3 30	343
			¢¢	2330	2682	1025	3420	38'5	4254	4013	6212	5713	521
4K 65464 6 6 6 7 19 7	UCGC005CUWC0008	116N2024	55	2295	2529	2913	ses:	3678	41:29	4541	5020	5499	508
M2FH0049	a sacasse offensive	119/12/02/4	100	2150	2476	2301	3171	3540	3954	4368	4627	5285	577
		1	110	1951	3270	1578	3952	3265	3645	4054	4241	4857	522
A.IA4484			90		4596	7:379	3774	6470	7325	BIEC	9129	10077	136
A1A7555		8	55		4270	\$171	5457	0:55	5/52	1/65	0005	9551	104
FTA-A075	HCGC0075UWC000B HCGC0075UWC0008	114N2027 114N2028	00/		3956	4463	1131	5800	6573	7357	8190	9026	985
1 AMA3/4 1 AMA3/4 1 TAMA3/5			110				4582	5234	5985	66/3	7383	8119	
			sc		C529	7098	7754	8491	9273	0055	10385	11715	125
A/A4512	Nor call an in party		55		66.03	0000	1242	79.8	Bo/J	9421	EXT	1126.1	112
FTAFA 03	RC3C0103UWD003N	114N2029	100		ĺ	6034	5690	7346	8067	8765	\$538	10288	110
			110		ĺ		5566	6102	6361	7520	1		



USCIDES 300 AT 22 / 521U0204

33

CAP TUBING/DRIERS





Our Soft Copper Capillary Tubing is precision blug drawn with the internal clameter held to a tolerance of +/-.001. It has been thoroughly dehydrated sealed and individually packaged.

BC SERIES BULLET® RESTRICTO CAPTUBING

Fits ANY domestic and commercial refrigerator or room air conditioner from 1/B H.P. to 5 H.P.

FEATURES

- Precision Bore, Plus or Minus .001
- The Bullet Restricto Cap is consolidated into a five-pak replacement kir. Ifs. guaranteed to provide you with uniformity on all applications. • The five "Restricto Cap" sizes cover hundreds of applications (see chart below).

PART NO.	SIZE	LENGTH
BCI	.061 O.D x .031 I.C.	IO FT. COL
BCE	.093 C.D x .040 I.D.	12 FT. CCIL
BC3	.093 O.D x .052 LD.	12 FT. CCIL
BC4	.125 O.D. x .064 LD	12 FT. COIL
BC5	.071 O D. x .028 .D.	10 FT. CCIL
BC1-103-	.081 O D. x .C31 I.D.	100 FT. COIL
BC2-103	.093 O D. x .040 I.D.	100 FT, COIL
BC3-100	.093 O.D. x .352 I.D.	100 FT. COIL
BC4 103	125 O D. x .064 .D.	100 FT. COIL
HC5-107-	071 D D x C28 D	100 FL COIL
5 PAK	Five pack replacement kit.	

REFERENCE CHART FOR BULLET® "RESTRICTO" CAPILLARY TUBING FOR ALL REFRIGERANTS IN LOW, MEDIUM AND HIGH APPLICATIONS

NOTE: This chart is average measurements for average conditions, and may have to be "fine tuned" for exact replacement. These charts are for Ean Cooled units only. Add 10% to the length of the cap tubing for Static Cooled Units.

REF	HP	LDW	MED	HIGH	FIEF	HP	LOW	MED	HIGH
B12/R416A	1/8-IP	110* # 5	84" # 5	48' # 5	E402E/E403E	1/8 HP	144" # 5	111*#5	63' # 5
	1/6 HP	71' # 5	96" # 1	72' # 1	B404A/B407C	1/6 HP	35" # 5	78' # 5	95" # 1
	1,5 -IP	51' #1	36' # 1	24' # 1	R408A/R502	1/E HP	70" # 1	16" # "	31" # 1
	1/4 #P	43' #1	90" # 2	60' # 2	20202007002055	1/4 HF	36° #1	31' # 1	79' # 2
	1/3 IP	33° # 2	72*# 2	36" # 2		1)\$ HP	30" # 1	90" # 2	47. # 2
	1/2 -12	95° # 3	/8* # 3	90* # 4		1,2 HP	29" # 2	63' # 1	32" # 3
	3/4 HP	50° # 8	92*#4	72*#4		3.4 HF	79" # 3	32" # 3	96" # 4
	1 HP	38' # 3	84' # 4	54' # 4		1.HP	46" # 3	1111#4	72* # 4
	1.1/2 平	34° ≠ 4	60' # 4	43' # 4		1-1/2 HP	111* ≠ 4	79° ≠4	56" # 2
	2 HP	55° ≠4	40'#4	26' # 4		2 HP	74' # 4	52" ≠4	34° # ≤
R134A / R401A	1/8 🐨	121"#5	92" #5	53' # 5	R4024/R407A	138.HP	V/4	19≿≠5	69' #
R401B/R405A	1/G -IP	79° # 3	105" # 1	79-41	R407E/R507	1/6 HP	104" # 5	133 # 1	105'#1
H409A/H500	15-12	59' #1	39' #1	26' # 1	200052852004500	1/E HP	77" #1	50' ≠ 1	34' ≠
	1/4 HP	¥7° ≠1	99° #2	66 # 2		1/4 HP	52" #1	34' # 1	86° ≠1
	1/3 世	132* # 2	70* #2	39" # 2		15° HP	33" #1	103*#2	52" # 1
	1/2-12	105*#1	52" # 3	99° # 4		1,2 HP	31" # 2	69° ≠ 3	35' # 3
	3/4 HP	33' # 3	101*#4	79 # 4		3/4 HP	37" # 3	34. 22	100' # 4
	1 HP	331 + 3	92' #1	59" # 4		1 HP	52" # 8	20" # 2	79° 🖈
	1-1/2 🐨	92° #4	66' #4	47 # 4		1-1/2 HP	32" # 3	86' # 4	62" #
	2 HP	ð1° ≠4	44' #4	29' # 4		2 HP	32" # 4	58' #4	37" +
HZ2	1/8 HP	1327#5	101'#5	58' # 5	E410A	1/8 HP	VA	144*#5	81' # :
	1,6 册	351 + 5	1'5'#1	86' 📌 1		1/6 HP	123" # 5	100 # 5	78* # 1
	1/5 -IP	34° ≠1	42" #1	28" # 1		15 HP	30, 41	60° ≠ 1	41" #
	1/4 🐨	51' #1	109"#2	72* # 2		1)4 HP	73" #1	40' #	101' # 2
	1/3 🕀	112" + 2	871 # 2	431 # 2		1/2 HP	38" # 1	30" + 1	62* # 1
	1/2 -₽	115" # 3	57" #3	109'#4		1.2 HP	37" # 2	84' # 3	42" # 3
	3/4 - P	72* # 3	1117#4	87' # 4		3/4 HP	104" # 3	44" # 3	34* + :
	1 HP	42' # 3	101' # 4	65° # 4	0	1HP	52" # 3	36' # 3	94° ≠
	1-1/2 HP	131"#4	72* # 4	511 # 4		1-1/2 HP	31 # 3	ALL PAR	74" # 4
	2 HP	67° ≠ 4	48° # 4	321 🖸 4		2-HP	30 94 4	(011 + 4 >	45" # .

⊔ondershare™

20 - 1



Drain fitting at 45° angle so drain can be run through the back or bottom of refrigerator. Room for expansion valve inside so that it is out of sight, Model TA is available with optional coated coll for consistent protection rose model designation TAKL A so features repair inlet connection to reduce leaks.

Model TA reach-in evaporators are thin units that mount in the top of a feltigerator, making the entite top shelf area usable. The attractive low silhouette makes this unit particularly desirable for display-type refrigerators. If can also be

Motor (Total FLA) Fair Dimensions (in.) Connections (in) (BTUH) Арргох TA K Shaded Pole Net Wt. Liquid Mede 10"F TD Suction Drain CEM ŧ. Ð (ibs.) Qty. î. 208 +25 SST 115/1/60 00 ID 00 230,1/60 TA10 1,000 0.0 16-1/2 4-1/2 13-:/2 3/8 1/B 1/2 10 120 1 0.4 TATE 1300 170 16 08 26-1.5 4.1/7 12:0 3.8 北京 1/2 13 TA17 1.700 2 219 1.6 0.8 23 4-1/2 14.12 3/8 3/8 1/2 17 2,300 33) 41/2 111/2 TA23 3 21 1.7 31.5.8 3/8 3/B 1/2 23 3,000 **TA30** 360 24 1.2 40 4-1/2 14:72 3/8 1/226 TA451 4,300 540 32 1.0 4-1/2 14-1/2 1/2 4 53-3/8 1/2 5/6 36 TASSI 5,500 n'il 40 2.6 53-3/8 6-3/4 14-72 1/2 245

* These models use external equalized expansion value

Reach-In Unit Coolers

Thin Profile Air Defrost Unit Coolers

used in back bais, under counter cabinets or wherever space is at a premium.

Thin Profile Electric Defrost Unit Coolers

Model TL low temperature reach-in evaporators have an automatic defrost system. Mounted in the top of a refrigerator, its extremely compact cable of a refrigerator, its extremely compact cable of a refrigerator. Its extremely compact cable of a refrigerator allow in the entire top shelf area for storage. With a normal operating range of 13°F to -20°F. This unit is ideally suited for such applications as commercial freezers, ice clearn boxes, bakery treezers and dual-temp reach-in boxes. Mechanical contact is provided between the heater elements and the drain pan ensuring a warm pan during the defrost cycle. Sufficient space is provided to mount the expansion valve within the cablest. Systems for both 1° 5 volt and 208-230 volt operation are available. A so features sweat inlet connection to reduce leaks, Some mode a available. With Comotors, contact your sets representative for availability.

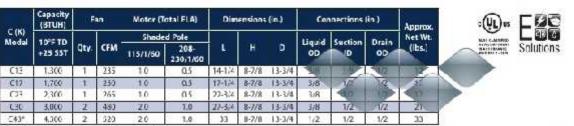
			Motor (T	otal FLA)	,	Defrost He	ater	Dim	ensions	(in.)	Cor	ncctions	(ind)	Approx.	
TL Medel	10°F TD -10°F 55T	Qty.	(TFN)		d Pole 208- 230/1/60	Watts		230/1/00 Amps	L	H	D	Liquid CD	Suction ID	Drain OD	Ne: Wi. (Ihi.)
TL09	000	- 835	110	0,3	0,4	475	4.1	2.*	16-1/2	412	13-1/2	3/8	3/8	1/2	10
IL12	1,200	1	210	1.5	0.8	500	5.2	2.6	20-1/2	4-12	13-1/2	3/8	1/2	1/2	15
TL16	1,600	2	210	1.5	0,0	730	6.1	3.0	24	4-12	14-1/2	3/8	1/2	1/2	19
TL21	2.100	*3	240	1.3	05	1,100	9.6	4.8	24	6-3/4	16-1/2	3/8	1/2	1/2	19
TL28	2,300	3	335	<u> </u>	12	1,430	12421	5,7	31-5/8	5-3/4	141/2	3/8	1/2	1/2	22
TL35*	3,300	1	430		1.0	1,600		7.0	38-3/B	5-3,4	16-1/2	1/2	5/8	1/2	11
11.53*	5,300	3	595	. S.	15	1,950	124-11	8.5	49-1/8	5-3/4	16-1/2	1/2	7/8	1/2	45

* These models use external equalized expansion valve

High Profile Air Defrost Unit Coolers

Model C unit cobies are ideal for refrigerated reach-ins, it mounts to the top of the refrigerator and discharges cold air against the back wail. With this air flow pattern, the air is not blasted on the product, but is diffused along the back wall and then gently drawn across the product as it returns to the unit thus, uniform temperatures are maintained throughout the refrigerator in addition, door sweating and refrigeration loss due to door opening it greatly induced because the air is not discharged against the doors. Mounting is easy with aluminum hangers that automatically space the unit the correct distance from the back wall. The expansion valve fits inside, out of sight. Model C is available with an optional coared coil (designated as more LCK) for company protection. Also features sweat inlet connection to reduce leaks. Some models available with EC motors, context your sales representative for eval ability.

	3	1	-	100	
15	1		8.4	A.	
12		W	14	₩.	
23	- 04	0	1	2	
100		10.0		6626	88



522.43 uses external equalized expansion value



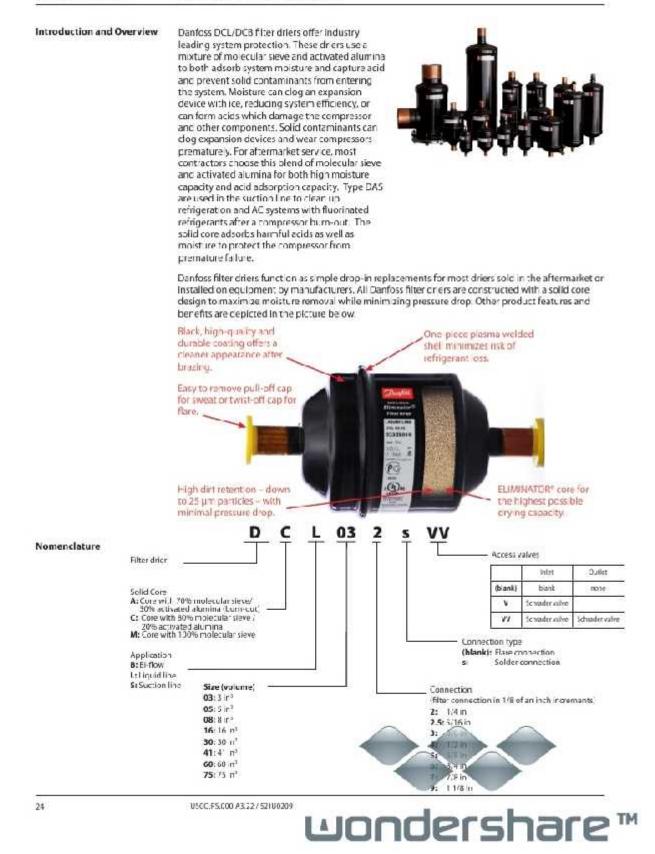






Quick Select Guide

Fliter Driers, Types DCL/DCB/DAS





Quick Select Guide

Filter Driers, Types DCL/DCB/DAS

Type	Connection solder (in.)		Code No.	
DCL 0321	1/4	0.19	02325013	
JULUSS	3,18	U.42	02325015	
DCL 0524	1/4	061	02325018	
DCL 0534	3,В	DE4	02325015	
CL 0621	1,4	D.64	02325033	
201 0334	1.8	0.66	02375023	
OCL 084:	1/2	0.68	023Z5026	
DCL 1624	1/4	1.69	023Z5028	
DCL 1645	کارک	172	02525025	
JCL 1645	1/Z	1.14	02525032	
DCL 165:	5/8	176	02325033	
DOL 167:	7/B	1.85	02325034	
301.303	3.8	264	02320030	
101 101	1,2	256	02370011	
DCL 3055	5/8	2.68	02320032	
DCL 3075	7,B	257	02320034	
OCL 309s	1-1/8	259	02320035	
DCL 4145	1/2	4.47	02320104	
DCL-4151	S/B	4.49	02320105	
ECL 417:	7,8	4 5B	02320106	
DCL-4194	1 1/8	4 60	023Z0107	
DCI -6074	7,A	526	02370016	
DCL 6095	1 1/8	528	02320037	
DCL 757s	7,8	7.44	02320115	
DC8 (82)	1/4	1.1	023Z1434	
JCB (2855	5,8	1J	02321433	
DC3 084s	1/2	1.3	02321432	
DCB 1635	3.B	1.8	023Z1437	
DCB 1641	1/2	1.4	023Z1436	
DCB 1655	5,8	2.0	02321435	
DCB 304s	1/2	2.2	023Z1440	
DCB 305s	5/8	2.4	023Z1439	
X.B.30/3	1/B	2.4	02521458	
DAS 063:WV	3/8	1.0	02321093	
DAS 084:VV	t/Z	tá	023Z1004	
DAS 0853VV	5/8	1.1	02321005	
DAS OBS(\V	1,4	t.i	023Z1006	
DAS 154632	1.7	2/3	02371009	
DAS 165sWV	5/B	1.9	02321010	
DAS 155sVV	3/4	1.9	02321011	
DA5 167:00	7,8	1.9	02321012	
DAS 3055VV	5/8	2.9	02321013	
DAG 30G/VY	3/4	2.9	02321014	
DAS 307 WV	7,8	2.0	02321015	
TAS REALY	1.1/8	20	02371016	
DAS 417:VV	7,8	4,5	02321017	
DAS 4195W	1.1/8	4,5	02321018	
DAS 607sVV	7,8	5.3	02321019	
DAS PORT	1 1/8	 5.3	02321019	

Type	Connection flare (in.)	Weight (bsi	Code Nc.	
DCL 032	1/4	0.44	02325000	
JCL 062	1)4	0.44	02345075	
CL 033	3/8	0.51	02325001	
CL 033	3/8	0.51	02325085	
OCL 052	1,4	0.96	02325002	
001.051	1/8	0.97	02325003	
DCL 082	LA\$	0.88	023Z5CO4	
DCL 083	3/8	0.97	02325005	
UCL 084	1/2	.00	02325006	
JCL 152	1/4	1,04	92325007	
OCL 153	3/6	1.80	923Z5C08	
DCL 154	1/2	1.91	02325009	
OCL 155	5/8	2.00	62325010	
EUE LOG	3/8	7 93	02370012	
DCL 304	1/2	3.04	02320013	
DCL 305	5/8	3.62	023Z0014	
DCL 306	3,4	3.28	02320156	
DCL-413	11/8	4.09	023Z0101	
DCL 414	1/2	4.20 02320		
DCL 415	S/8	4,29	02320103	
DCB C60	LM	្រារ	02321402	
DC30R3	3.6	011	02371403	
DC306\$	1/2	1.3	023Z1400	
DCB162	1/4	1.8	023Z1406	
DCB 163	3/8	1.8	023Z1405	
UCB 164	1/2	2.0	02321404	
QC3 165	5/8	2.0	023Z1403	
VV680 2/C	3./8	1,12	023Z1001	
DAS OB4VV	1/2	'.37	.37 0232100	
DAS 154VV	1/2	2.01 023210		
DAS 155VV	5/8	2.09	02321008	

* Wire mesh in filter drier outlet

Type	Material	Code No.	
ECF core insert, type 48-0° solid mie	B0% moleculer sieve & 20% activated alumna	023U4383	
DCR core assert. type 48 DA solid core	30% molecularis eve & 70% act valed alumina	02305381	



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uondershare™



Quick Select Guide

Sight Glasses, Types SGN/SGRN

Introduction and Overview Danfoss sight glasses are designed to accurately indicate the presence of moisture in refrigeration and air-conditioning systems. When system moisture content rises above permissible levels, the "dry/green" indicator will change to yellow indicating a "wet" system. The indication of dangerous moisture levels is essential in helping prevent the formation of harmful acids which are detrimental to the system.

Danfoss offers two types of sight glasses, inline and vessel mount. In line sight glass, type SGN is used in the system's liquid line to indicate both the condition and molsture content of the refrigerant. They incorporate an indicator which changes color dependent on the moisture content. Type SGN is recommended for all HCFC and HFC refrigerants. Vessel sight glasses, type SGRN are specially designed to be mounted directly on either a receiver or the compressor crankcase to ind cate liquid level. Type SGRN are available with a refrigerant moisture indicator which can be used with all fluorinated refrigerants.



Product Selection

Гуре	Version	Connection (In.)	Ambient Temperature (°F)	Mazimum working pressure (psig)	Weight (Ibs)	Code No.
SGN S	Flare int.x.ext.1	1/4 x 1/4		500	0.22	014-0137
SGN 10		3/8 x 3/8		500	0.44	014-0138
5GN 12		1/2 x 1/2	1	500	0.66	014-0139
5GN 6:	ODF X OD - Solder	1/4 × 1/4		500	0 22	014 0142
3GN 105		3/3 x 3/8	-50 to 175	509	0.22	014-0143
5GN 12s		1/2 x 1/2		500	0.44	014-0144
SGN 16k		F/R ¥ 5/3		508	0.44	014-0145
\$GN 225		7/3 x 7/8		400	D.44	014 0147
SURN		3/2		900	0.22	D14-COCC

' can be screwed directly on to Danfoss filter drier.



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