

ENVIRONMENTAL ASSESSMENT FOR AL-DAHRYIA OLD CITY

By

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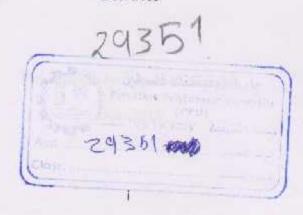
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ABSTRACT

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The architectural heritages of the region reflect the identity, culture, and the link between past and present and clear evidence of original and authenticity.

Old Cities make a connection with ancestor and give a sense and understanding of history that no other documents or evidence exist.

Old Cities should to keep them and rehabilitate of architectural heritage to protect it and to develop it to suit the circumstances of the times and cultural transformations ongoing. Preservation and reuse of historic buildings serve resource and reduce material consumption and consumes less energy than demolishing buildings and constructing new ones.

Palestine has many oldest historical cities which having an important value for national and international sector.

Al-Dahriya old city is one of the most important areas in Palestine that has a historical and religious value .it is located in the southern part of Hebron city.

This study make an environmental assessment for Al-Dahriya old city by studying the current situation of the area then making an evaluation and assessment of all environmental parameters including parts of infrastructure then making a designs for the waste water and storm water systems, this study also make the design of a suitable septic tank for the study area and it engineering solution for some environmental problems.

(कार)

الإن الذا و تحدُّر عطواتنا الأعيرة في الحياة الجامعية من وقطة ثعود إلى أعوام فضيناها في رحاب الجامعة مع أستاننا الكرام الذين قدوا تنا التثير باذلين بذلك جهودا كبيرة في بناء جيل الغد لتبعث الأمة من جديد.

وقبل أن تعضي نهدي عدلتا هذا

الى مذارة العلم والإمام المصطفى إلى الأمي الذي علم المتطمين إلى سيد الخلق إلى رسولنا الكريم سيدنا محمد صلى الله عليه وسلم.

الى الأسرى البواسل با من تقبعون خلف فضيان الحديد..في زنازين الغدر والقهر والجلادين الى وح الشهداء العظام الذين تتوشح فلسطين البوم بأثواب اجسادهم إلى الذين مهدوا تنا طريق العثم والمعرفة إلى جميع استنتنا الأفاضل ونخص بالذي مشرفة المشروع المهندة سعاح الجعبري على الجهد الذي ينتنه معنا.

وعذلك نشكر كل من ساعد على إنكام هذا البحث وقدم لنا العون ومد لنا يد المصاعدة وزودنا بالمطوسات اللازمة لإنكام هذا البحث ونفص بالذي

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ألى أبي النور الذي ينيد لي درب النجاح الذي لم يبشل على يوما يشيء ..

إلى أمي الحبيدة من بهذا أكبر وعليه أعتمد إلى شععة متفدة تثير ظلمة حباتي إلى من بوجودها أكتسب قوة ومحية لا حدود لها...

إلى الحوتي وخواتي طالبات وطلاب خندسة تكنواوجيا البينة إلى من تحلو بالإنداء ونميزوا بالوقاء والعطاء إلى ينابيع الصدقي الصافي إلى من معهم سعت ، وبرفقتهم في دروب الحيرة الحلوة والحزيئة سرت إلى من كانوا معي على طريق النجاح والخير إلى من عرفت كيف أجدهم وعلموني أن لا اضبعهم

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إلى اخي من أرى الثقاول بعينه والمساء في ضحكته إلى شعاة الذكاء والثور ...

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غين ابومبحة

سلجدة الدراويش

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Work Team

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Chapter One Introduction

1.1 General

Before the First World War, rapid industrialization and urbanization in western countries was causing rapid loss of natural resources. This continued to the period after the Second World War giving rise to concerns for pollution, quality of life and environmental stress. In early 60s, investors and people realized that the natural environment and the projects bey were under taking were affecting the environment, resources, raw materials and people must be study, evaluation and analysis. As a result of this, experience groups formed with the aim of getting a tool that can be used to safeguard the environment in any development this will be done by environmental assessment [1].

impact, of current natural environment or proposed projects or activities. An environmental assessment is, therefore, a study of the probable changes in the various expectation and biophysical characteristics of the environment which may results proposed or impending action [1].

USA decided to respond to these issues and established a National Environmental Micy Act in 1970 to consider its goal in terms of environmental protection. The USA the first country to enact legislation on Environmental Impact Assessment (EIA). Was the first time that EIA became the official tool to be used to protect the pronunct. The United Nations Conference on the Environment in Stockholm in 1972 albsequent conventions formalized EIA, So comparison between Environmental Assessment and Environmental Assessment must be considered.

any change, positive or negative-from a desirability standpoint on the biomissical environment and on man's health and well-being, to interpret and
micate information about the impact, to analyze site and process alternatives and
solutions to mitigate the negative consequences on man and the environment.

EA is: "A management tool comprising a systematic, documented, periodic and evaluation of how well environmental organization, management and are performing in the aim of helping to safeguard the environment by:

management and control of environmental practices,

 Assessing compliance with company policies, which would include meeting regulatory equirements".

requires the second encompasses varied disciplines, and consequently requires the second encompasses varied disciplines, and consequently requires the second encompasses of personal knowledgeable in various technical areas.

The second attribute consisting of both natural and human caused factor. The second is admittedly difficult to characterize because of its many attribute and applex interrelationship among them.

it's better to create a set of attribute before we began to prepare environmental comentation as shown in Table (1.1).

Table (1.1):Example of environmental attribute. [1]

	Water	Ecology	Sound	
fusion factor	Flow variation	Large animals	Physical	effects
ficulate	Suspended solid	Small game	Commun	ication
ar oxide	Acid &Alkali	Aquatic plants	Performance effects	
oxide oxide	Biological oxygen demand (BOD)	Natural and vegetation	Sound effect	behavior
monoxide	Chemical oxygen demand COD	Field crops		
8	Dissolved solid	Threatened species		_
loss toxicants	Fecal coliforms		_	

an aspects	Economic	Resources	Land
ylés	Regional economie	Fuel resources	Soil stability
	Stability		
nity needs	Public sector review	Nonfuel resources	Natural hazards
ogical needs		aesthetics	Land use patterns

lany methodologies have developed which allow the user to have more accurate formation. Depending upon the specific needs of the user and type of project being ndertaken. One particular methodology may be more useful than another.

2 Problem Definition

be old city (historic center) in any city of the world is considered as a famous site from chaeological, cultural, religious, and historical side.

Dere are many historic centers in Palestinian cities that has recently been suffering from imificant environmental problems such as water shortages, air pollution, soil pollution, and lots of other problems as a result of leaving these areas and largely neglected.

the of the most historic centers in Palestine is Al-Dahriya City.

Dubriya Old City located in the center of Al-Dahriya and represents the cultural and social side of city. It suffers from a series of environmental problem such as musiciousness of the value of heritage building, Shortage of water resources and where there is no sanitary networks and bad management of the solid waste.

13 Project Objectives

moject includes the following main objectives:

Make an environmental study for the current satiation in Al-Dahriya Old City this done madying the following points:

infrastructure.

N Water.

This is an analysis for the environmental study throughout comparison between the structure current situation and the international parameter.

while an environmental assessment for the whole area.

Stating a complete design for some parts of infrastructure or making redesign for parts are seed rehabilitation.

of primary treatment of the collected waste water.

1.4 Phases of Project

The project consists of four phases, which are designed to be completed in accordance with time schedule shown below. The description of each of the four phases of the project and tasks involved are listed below:

Table (1.2): phases of the project with their expected duration

Title	Duration "year 2015"									
	1/2	1/3	1/4	1/5	1/9	1/10	1/11	1/12		
and survey							1711	1712		
Field work										
Study and analysis										
Analysis and design parameter										
writing preparing to report										

First phase: Data collection and survey

this phase available data and information were collected from different sources.

many site visits were done. This phase includes the following activates:

needed maps for the area were collected.

secological data were collected from different source.

Callecting Infrastructure data.

14.2 Second phase: Field work

site visits to evaluate the environmental condition of Al-Dahriya Old City, visits

Studying area to assess the environmental factors and samples of soil and water were extended.

Wasting the municipality of Al-Dahriya city to get more information about the old city

Riwaq Institution to get required maps and information.

Third phase: Study and Analysis

third phase certain task were done as following:

Define the requirement activities.

the affected attribute.

solute environmental impact and summarize them.

Fourth phase: Assessment, design and/or redesign, and preparing

phase the final estimation of the last stage, the project team prepared a design for some parts of infrastructure.

prepared and submitted to the department of Environmental Technology

Palestine Polytechnic University.

Caracitation of the study

sport has been prepared in accordance with the objectives and of work.

chapters.

assessment also the comparison between environment assessment and impact assessment, then talk about environment assessment elements and

Chapter two entitled "Characteristics of the Project Area" which deals with history, socioeconomic, geographic data, and climate characterization of site.

Depter three entitled "Current Situation" which deals with the environmental condition of Al-Dahriya Old City.

Dapter four entitled "Design Parameters" which deals with quantity and volumes of the solution described in chapter four.

Dapter five entitled "Analysis and Assessment" which deals with analysis the result and solution for present environmental problems.

waste water collection system and drainage system, and containers' for solid

dusions of the study and provide recommendation for mitigation of the potential impacts and enhancement of the positive ones.

Chapter two

Characteristics of the Project Area
"Al- Dahriya Old City"

2.1. General

In this chapter, basic data of Al-Dahriya City will be discussed. Topography, meteorological data, Population data, water consumption, and wastewater production.

2.2. Project Area

Al-Dahriya City is located to the northwest of the main street connecting between the cities of Hebron and Beersaba, extending from the beginning of the valley Ghemari south to the north east area of Abu Alroazin. Figure (2.1) below show general view of Al-Dahriya Old City.

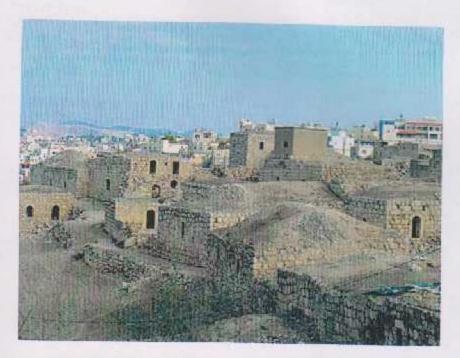
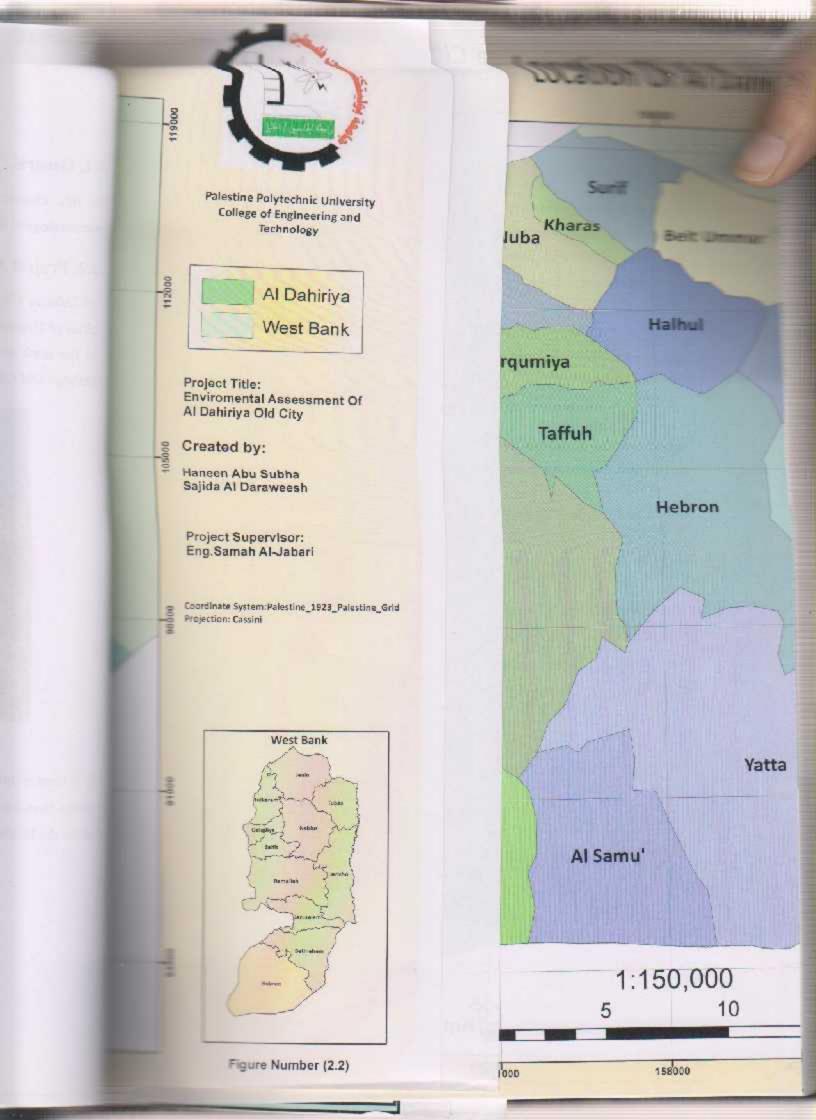
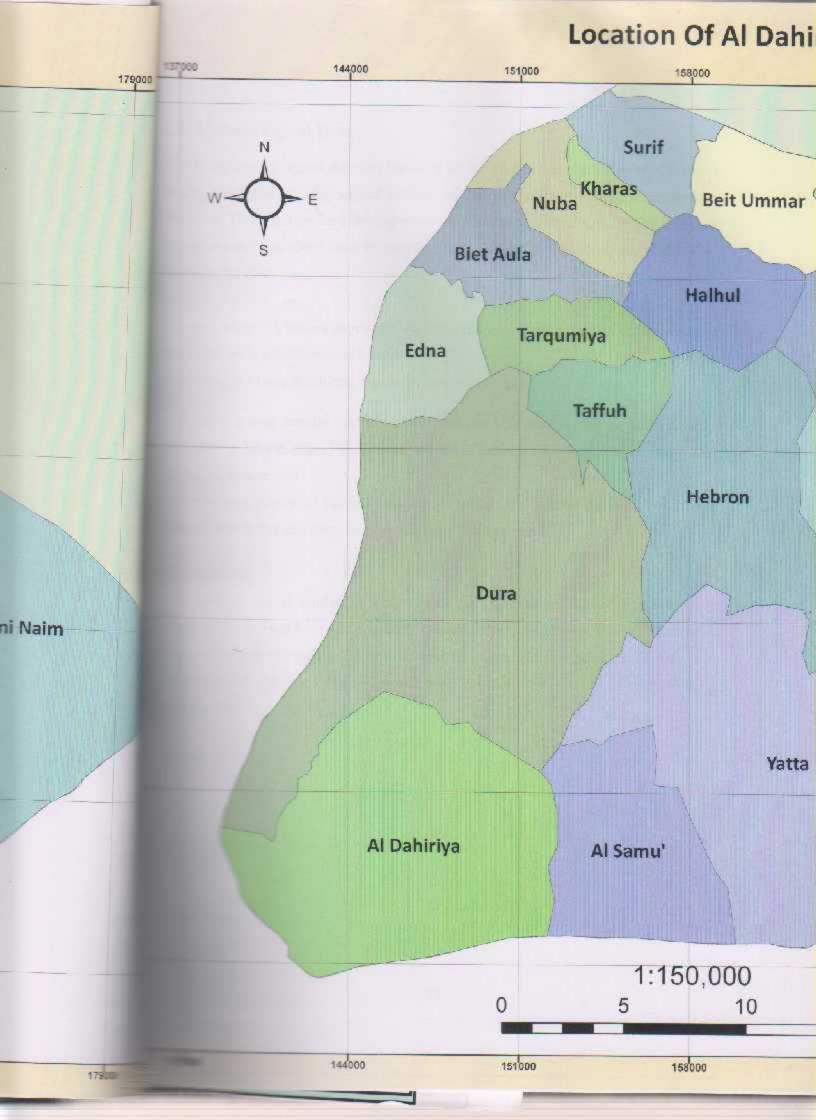


Figure (2. 1) General View of the of AL-Dahriya Old City[2].

twenty three kilometers south-west of Hebron. It surrounding from north Dura city, semu from east, Berg and Ramadeen from west, and Beersaba from south. Figure (2.2) show the location of Al-Dahriya Old City.





23. Meteorological Data

The hydrology of region depends basically on its climate, and topography. Climate is wardy dependent on geographical position of the earth surface, humidity, temperature, and wind. These factors are affecting on evaporation and transpiration. So this study will be needed data about these factors. Figure (2.3) show Digital Elevation Model of Al-

which means medium height characterized by desert to Mediterranean basin climate [3].

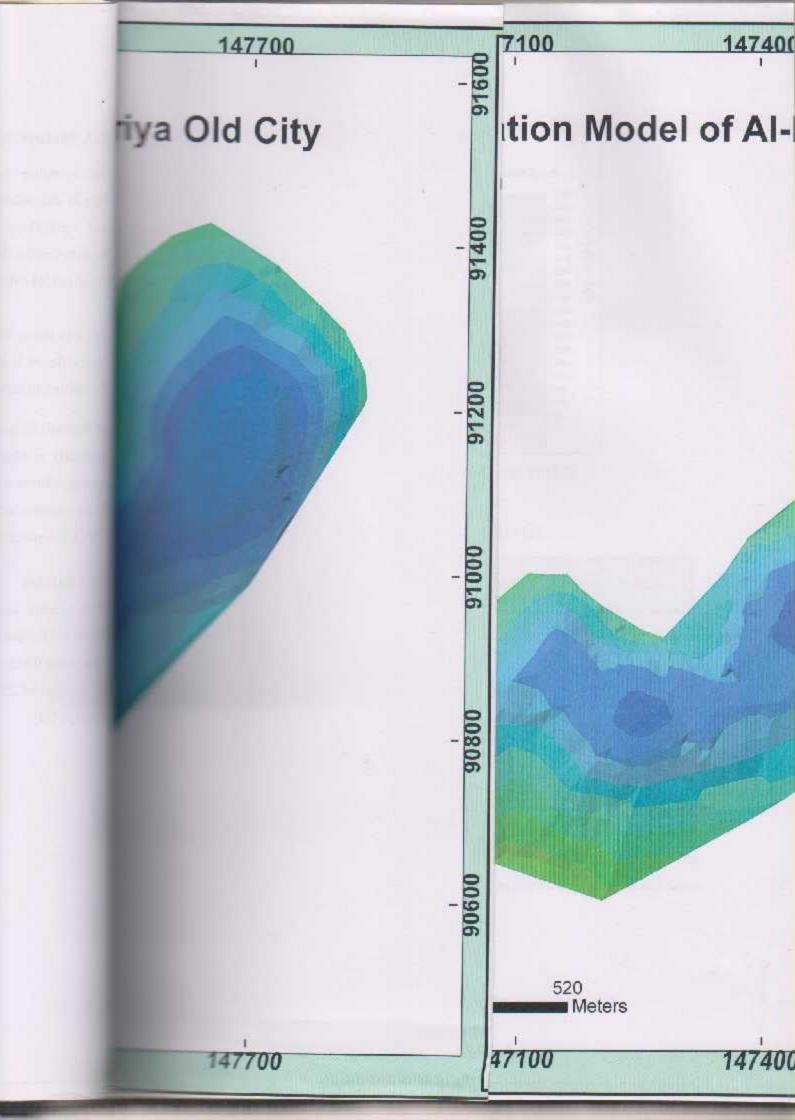
Riwaq Institution climate in general can split to two seasons:

season ,usually start in October and reach its peak in February then decrease May month. This climate consist of two seasons went season, and part of an arrann season.

September and sometimes continue to October month.

LEU Rainfall

October and May while it rarely rains in the summer season. The driest month is of 250 mm. Figure 2.4 and table 2.1 show the amount of rainfall in Al-



146800 147100 14740 Digital Elevation Model of Alnic University g &Technology ring &Technology sessment City sh ari ality. tem: stine_Grid 1:4,482 520 390 ■ Meters 147100 147400 146800



Figure (2.4): Rainfall in Al-Dahriya City till 2013 [2].

Table(2.1):Al-Dahriya Rainfall 2013 [2].

Station	Accumulative Rainfall	General rate	Percent Ratio		
Datelya	155.9	336.5	46		

- Comperature

The annual average Annual rate is (17-19 c°) .Rate of colder ranging from 6 to 14 c°, while the highest temperature (26-34 °C). The much of the year is August, with an average temperature of 26.7 °C. The lowest temperatures in the year occur in January, when it is around 12.3 °C. The temperatures throughout the year is 14.4 °C, as shown in figure 2.6 and table

Table (2.2):Al-Dahriya climate [4].

month	1	2	3	4	5	6	7	8	9	10	11	12
	114	22	6	3	2	0	0	0	0	3	8	12
10	12.3	13.1	15.8	19.0	22.9	25.6	26.6	26.7	24.7	22.6	18.7	14.2
C (min)	5.3	6.6	8.8	11.3	14.9	18.1	19.5	19.6	17.8	15.7	12.6	8.1
C (mex)	18.6	19.7	22.8	26.8	30.9	33.2	33.8	33.9	31.7	29.5	24.8	20.4
	54.2	55.6	60.4	66.2	73.2	78.1	79.9	80.1	76.5	72.7	65.7	57.6
T (min)	43.0	43.9	47.8	52.3	58.8	64.6	67.1	67.3	64.0	60.3	54.7	46.6
T (max)	65.5	67.5	73.0	80.2	87.6	91.8	92.8	93.0	89.1	85.1	76.6	68.7

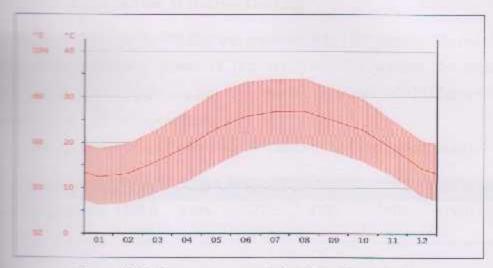


Figure (2.5): Temperature graph in Al-Dahriya City[4].

Pagulation

Population projection

- Central Bureau of Statistics (PCBS) of 28776 parsons. The annual growth rates in the west bank [1].
- acculate the population for the coming 25 year, a geometric increase is assumed,

manufaction.

a pulsation.

Mentaline growth.

Forecast for Al-Dahriya Old City

be 3693.8 in year 2036.

(2.3) Population Forecast for Al-Dahriya Old City [Project Team].

	2007	2011	2015	2020	2025	2030	2036
mation(capita)	1300.0	1544	1772	2105	2500	2970	3651

importance of the Area(capital)

and cultural heritage. Al-Dahriya City have a particular importance because communication between the two natural environments are the Hebron and the Negev desert. The figure 2.6 show famous site in Al-Dahriya Old City sical site. Also the city have within it many of historical monuments which bandred and eighty one historical buildings as Rawq Institution Statistics like:

estria.

Mosque.

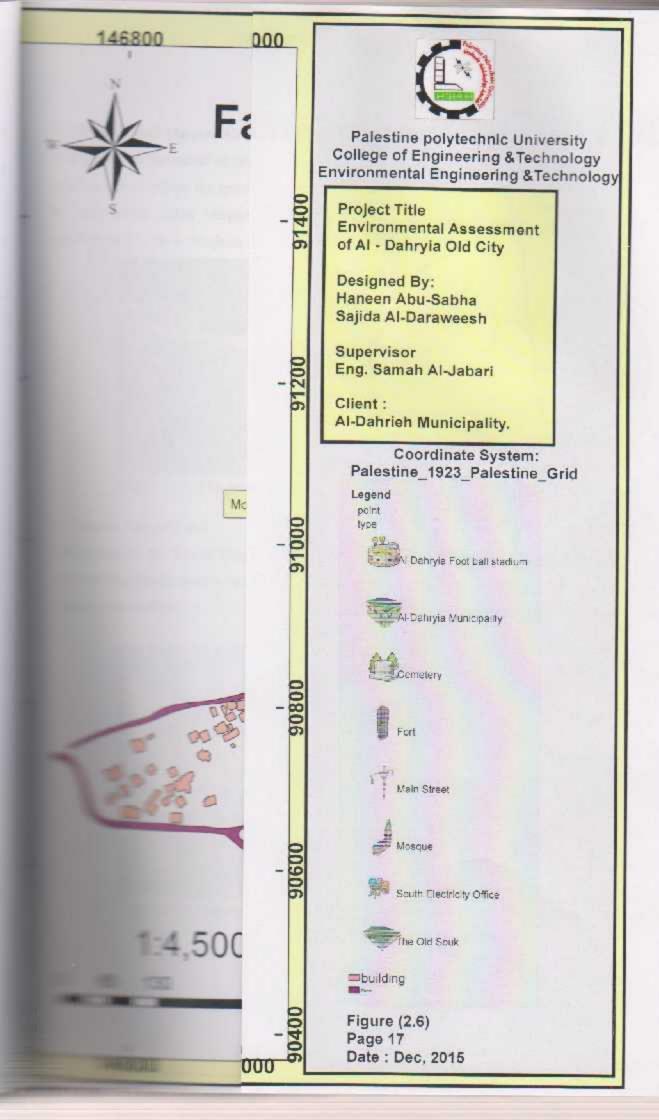
Al- Fadel.

Shohda,

- 5. Maqbara and Maqam Abu-Dabor.
- Maqam Abu-Hashim.
 - Al-Gamaree.
- the important buildings discussed below:
- Bien Qisaria
- secured in the center of the Old City, it is a huge stone wall, and seems that it is a secured old castle. Figure (2.7) show Hisen Qisaria building.



Figure (2.7): Hisen Qisaria [Project Team].



3- Maqbara and Maqam Abu-Dabor

be located in the center of the Old City, and opposite to the Hisen from the west. It is a centery where the great Tomb painted with weigh color and have a place to put was which called Maqam Abu-Dabor, and it is a shrine to the man from the Figure (2.8) show Maqbara and Maqam Abu-Dabor.



(2.8): Maqbara and Maqam Abu-Dabor [Project Team].

m Abu Al-Fasel

and the side of Maqbara Abu-Dabor, and exactly opposite to Hisen site. It is blocks have a very small square window to put the wax. Figure (2,9) show



(2.9): Maqam Abu Al-Fasel [Project Team].

- 10-Omaree Mosque

and are around with modern cement additives. It is believed that the mosque dates

the Mamluk period Baibars days, Figure (2.10) show Al-Omaree Mosque.



Figure (2.10): Al-Omaree Mosque [Project Team].

Buria Castel

The centre of the old town, and the old market area. The site features have targe rooms and Al-Ahawash contains many distinctive architectural details.

2.11) show Qisaria Castel.



Figure (2.11): Qisaria Castel [Project Team].

- Magam Abu-Karoba

The place is situated by the highway leading to Arab Al-ramadin, about 1 km west of the Old City. It consists of a large square room with a dome and a niche, and has some modern planting seedlings. Figure (2.12) show Maqam Abu-Karoba.

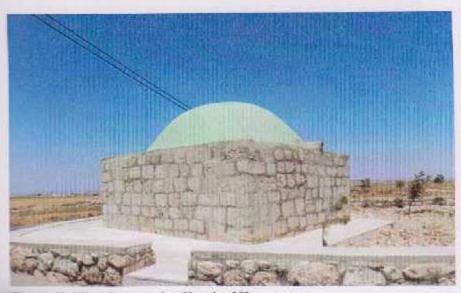


Figure (2.12): Maqam Abu-Karoba [5].

Structure of the buildings in Al-Dahriya Old City

of the old buildings in Al-Dahriya Old City is classified according to:

Ses of buildings in Al-Dahriya Old City

the doing form of the same existing buildings within the Old City by
the types of uses are divided into eight types:

me number one

use; it was found that the number of residential buildings in the area around building, and these accounted for 52 percent of total buildings. Figure (2.13) show the for residential use [6].

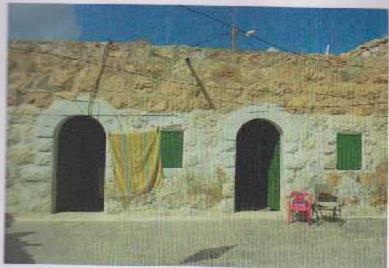


Figure (2.13): Old building for residential use [Project Team].

Type number two

member of buildings used for business purposes was found "28" building. Figure 224 show old building for commercial use [6].



Figure (2.14): Old building for commercial use [Project Team].

number three

used for industrial purposes was found "4" building and represent 1.1% of the mildings, these are light industries, such as: a factory for packing liquid soap, toilet makaging factory, as well as solar water heaters factory [6].

A Type number four

and some nearby buildings, and buildings in percentage 0.8%. Figure (2.15) show school in Al-Dahriya Old City [6].



Figure (2.15): Old building for educational use (Al-Dahriya School)[Project Team].

Type number five

which is a single building used as a dewan to Qisia.

Tope number six

buildings and mosques, its two building within study area, namely the Al-



Figure (2.16): Old religious building (Al-Omari mosque) [Project Team].

Type number seven

where it was used the buildings for housing, but are now used for storage especially for agricultural products, such as grain, hay and others, as well as part of sheds for animals, and various other uses. Figure (2.17) show old building storing food, also figure (2.18) show old building used for livestock breeding and [6].



Figure (2.17): Old building for storing [Project Team].

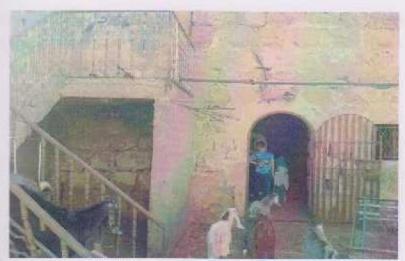


Figure (2.18): Old building for livestock breeding and animals[Project Team].

In the currently and an estimated "118" building 32.8%, and the currently are used, they are clustered in the Central old town adjacent to the consecutive. And it is Rabaa Hosh part of Al-Weradat, also part of Al-Meradat, also part of Al-Meradat, also part of the Al-Meradat, also part of the after the departure of the owners to their new homes, which have and modern kind of life. Figure (2.19) show abandoned old building [6].



Figure (2.19): Abandoned old building [Project Team].

Number of Floors

buildings, where it is found that "249" buildings, the sestimated at 69 percent, of the total buildings, this is a great majority of the total buildings the old city. Figure (2.20) show one-story buildings [6].

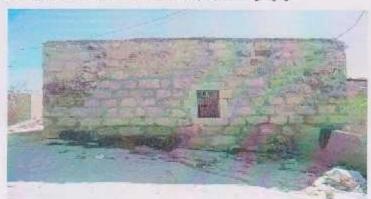


Figure (2.20): One-story buildings [Project Team].

buildings and number "98" building, with 27 percent, these buildings are reflect physical and social situation characteristic for the owners. Figure (2.21)

Mart Two



Figure (2.21): Two-story buildings [Project Team].

buildings, the "12" building; the percentage is 3.3%, and the market. Figure (2.22) show three-story buildings [6].



Figure (2.22): Three-story buildings [Project Team].

The floors, its one building in Wadi Al-Gamarce area.

The Buildings Frame

the situation existing in the old construction found that buildings are

ander construction. Figure (2.23) show building under construction.



Figure (2.23): Building under construction [Project Team].

expansion. Figure (2.24) show Building containing expansion.



Figure (2.24): Building containing expansion [Project Team].

Figure (2.25) show completed building.



Figure (2.25): Completed building [Project Team].

the buildings

see study area were found to be grouped

are in a good construction. Figure (2.26) show buildings in a good



Figure (2.26): buildings in a good construction [Project Team].

condition, as shown in figure (2.27).



Figure (2.27): Building in moderate condition [Project Team].

poor condition as shown in figure (2.28) show Buildings in poor condition.



Figure (2.28): Buildings in poor condition [Project Team].

shown in figure (2.29).

Millel Part



Figure (2.29): Destroyed buildings [Project Team].

The mature of the building and its design

characterized of cave under old building and little, small window at high the to the door, so the polluted air will transfer out of building and deceased to the building. But the ignorance of this benefits of design they cover the transfer the humidity in the buildings. Figures below shows The nature of the transfer and its design.

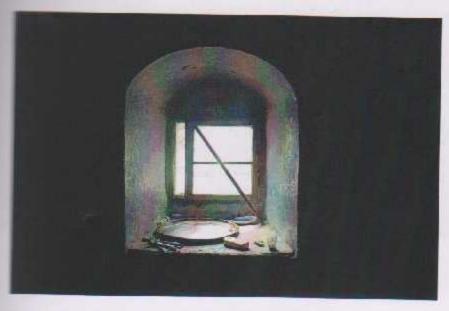
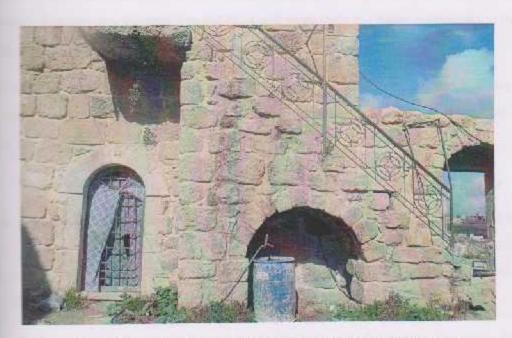


Figure (2.30): Window design in Al-Dahriya Old City buildings [Project team].



Figure(2.31):Doors and windows design in Al-Dahriya Old City [Project team].



Figure(2.32):Nature building in Al-Dahriya Old City [Project team].

Water

Water Quantity

Al-Dahriya municipality the water resources is 12% covered by Israel distributed by municipality net ,36% by collection of rainwater wells water tanks, and 19% other resources. So the city suffer from pollution and sufferent to different causes.

Water Consumption

and 81762.9 for year 2036. The result of all this is obvious, the total water ment is ever on the increase, and per capita water consumption is also on increase.

consumption is not constant, yearly, monthly, weekly, daily and hourly variations are observed, it is range from 18 to 22 liter per day. Certain dry more consumption. In hot months water is consumed in drinking, bathing, seeing lawns and gardens. On holidays and weekends the water consumption may

Maximum daily demand or maximum daily consumption usually occurs during months Forecast water consumption.

Wastewater Quantity

sewage is mostly the spent water of the community draining into the sewer lt has been observed that a small portion of spent water is lost in evaporation, in ground, leakage, etc. Usually 80% of the water supply may be expected to be sewers.

the amount of Domestic wastewater produced per capita per day is usually 80% consumption.

infortunately the city have no sewerage system, they collect the sewage from house by

Storm Water

was no storm water drainage system in the Al-Dahriya Old City; some people that the storm water and use it when there is shortage of water from municipality.

Chapter Three
Current Situation of
A "Al-Dahriya Old City"

General General

this chapter, a discussion of the environmental issues will be done. Also an arrangement of the positive and negative points in environmental evaluation of AL-

Environmental condition in Al-Dahriya Old City

and negative, direct and indirect, current and future in order to avoid adverse and enhance positive impacts in addition achieved sustainable development as with the Palestinian environmental standards.

and understand the environmental situation of the old city through the study of mellowing points:

Infrastructure in Al-Dahriya Old City

for the residents of the place of urban life so that these people can work various cavities easily and without problems. Infrastructure consist of water supply sewerage and storm water networks, electricity networks, telecommunications and networks schools, gardens, methods of solid waste disposal, and all other

and religious value, and to provide sustainable services to the residents of

services in the old city include the following:

ar network

eld city area available as the old network to a Al-Dahriya been, and mostly from the old city alleys despite its narrow and the lack of the minor roads in Alahowash region there is no water network.

Sewage system network

The serve important system to avoid ground water, soil, air pollution, they houses by cesspits and letrains then thrown it to the wadis.

the smelt, and the smelt of the

water pollution.

seemed the insects, rodents, flies in the area ,which cause a sever diseases to

see tourism because of bad smelt.

for of aesthetic view.

Environmental parameter affected by absence of sewerage system

NO.	Environmental Parameter	Description
1	Water Pollution	As the soil polluted by wastewater, if this soil is permeable and have sensitive ground water below it. And so the main source of water will be polluted.

	Soil Pollution	When the wastewater is in contact with the soil the salinity and hazardous solid material content in soil will comment the soil and loss that the impermeable to soil then send or near agricultural area, or neighbors, and may cause swamps full of wastewater, and rodent, insects exist.
	Air pollution	They dispose wastewater in wadi open to atmosphere which increases the pungent smelt from the inorganic compounds, ammonia and hydrogen sulfide which are considered to be the main causes of odor when the sewage comes from mainly households. Also the municipality use inseticed to avoid rodent insect near there but pesticides may suspended in the air as particles and carried by wind to other areas till it reach receptor and contaminating them.
•	Land Use	Use the land as a place to dispose wastewater, the land lose its value, and structure of the top soil.
8	Public Health	Whether air pollution, soil pollution, water pollution, all of that will cause a severe problem to humans and may cause death.
	Economie	When population increase ,the wastewater consumption will

morning are the ingrapes digress of waste will be rease discuses so we need more money to treat this problem.

The waste flow in wad cause

problem to neighbor or owner of agricultural area there and may cause them emigrate from their

The people will emigrate from there and also the tourism will decrease sue to pollution there. Also the aesthetic and heritage view loss their value

set work [Project team].

Beritage



Effects of sewage discharge on soil [Project team].

water accumulated in the streets during and after the incident

collection systems in old city except a small area called Faouque in cooperation with the municipality set up a network to collect

dirty, and not qualified street. The road network of the old city have show in figure (3.3), its wide range maximum from 2.5 to 3 meter.



(3.3):Roads condition in Al-Dahriya Old City [Project team].

work and telecommunication network

and telecommunication network: The electricity service in the old

was no telecommunication.

the city involve the domestic, commercial, light industries. People who leet their waste in plastic bags then disposed it throw in streets, alleys, old some of them in container which will then collect by worker cleaner and the waste in random sites. All these improper ways in collecting and waste will create severe environmental problem in area. The table 3.2

130

and a series of absence of good management of the solid waste:

of disposal the solid material by dumping it or firing in certain area will be sensitive ground water, soil, and air below if there is.

assecous dispersed in the atmosphere.

endents, insects, and diseases.

Environmental parameter affected by solid waste [Project team].

Environmental Exameter	Description
Water Pollution	The leachate of waste will penetrate to ground water and pollute it.
Seal Pollution	Firing hazards material will accumulate the hazards on soil ,and loosing there top soil
Air pollution	Whether leave the domestic waste degrade or firing it or dumping in a certain site. All these will cause air pollution.
Earnel Use	The quality and value of land will decrease, and it is hard to treat it
Health	As the soil, air, and water polluted the disease will increase too.
Committee of the last of the l	We need more money to treat this pollution.
Name of Street, or other party of the Street, or other party or ot	Neighbor of disposal site will affect, and this may cause emigration or fight.
Service .	The heritage building will abandoned.



(3.5): Burning container in Al-Dahriya Old City [Project team].



3.6):Solid waste inside Al-Dahriya Old City buildings [Project team].



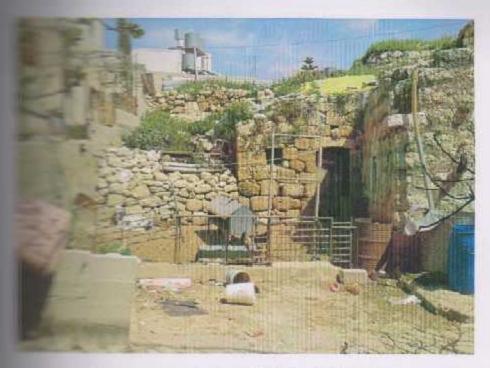
Figure (3.7): Solid waste beside Al-Dahriya Old City buildings [Project team].



Solid waste in Al-Dahriya Old City [Project team].
43

memoria and animals

All of these things are benefit point, but the negative point here is the herizage old building a place for livestock breeding, this will threat the building by increasing the strong pungent odors from animal below show the livestock breading in the city.



39:Livestock breeding in Al-Dahriya Old City [Project team].

To raison

- this city are very low because of different reason:
- the old city classified with semi arid region which receives
- potential evapotranspiration, and low vegetation index.
 - about cultivation and irrigation.
- the land use of Al-Dahriya City.

Table(3.3): Land use of Al-Dahriya city [7].

		Arable Area (Dounm)		Forest Area	Area of Open Grasslands
	Planted	Non Planted	(Dounm)	(Dounm)	(Dounm)
Table 1	22928	25572	16000	300	33200

Chapter Four

Design Parameter

Collection System Design

the water supply of community is considered to be conditional used to collect and transport wastewater to the conditional disposal are called sewers.

from residential, commercial, and industrial areas, and a manifold that may enter the system due to deteriorated manifolds. Storm sewers are exclusively designed to carry the area are designed to carry both the sanitary and the storm

The purpose of this chapter is to define the types of sewers types of wastewater collection systems that are used, the maintenance of sewers, the flow in sewers, the design of sewers, maintenance of sewers.

Sewerage System

and the location of the wastewater treatment facilities. The

mailed house connections).

THE RESERVED.

Laterals or branch sewers convey the wastewater to the main sewers.

Laterals or branch sewers convey the wastewater to the main sewers.

Laterals or branch sewers convey the wastewater to large sewers connect to the trunk sewers that convey the wastewater to large

The local sewer regulations, concerning the minimum size of the laterals.

The minimum size recommended for gravity sewer is 200 mm

Concrete and ultra polyvinyl chorides are the most common materials

Wastewater Collection Systems

starte system). In this system, the sewers are partially filled. A that the gradients of the sewers must be sufficient to create self-time transportation of sediment. These velocities are 0.6 to 0.7 m/s are flowing full or half-full. Manholes are provided at regular of sewers.

only. The system, which is entirely kept under pressure, can be distribution system. Sewage from an individual house connection

which is in manhole on the site of the premises, is pumped into the pressure system.

Tope System

The description and transportation of the wastewater. There is no special transportation of the sewers.

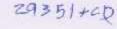
**Example systems require a comparatively high degree of management of the managemen

Lapurtenances

be of durable structure, provide easy access to the sewers for the sewer minimum interference to the sewage flow. Manholes should be and at the end of the line, at the intersections of sewers, at changes in the sewer except in curved sewers, and at intervals of 40-60 m in straight

Manholes are square, rectangular or circulation in plan, the Manholes for small sewers are generally 1.0-1.2 m in diameter. For the are provided. The maximum spacing of manholes is 40-60 m sewer and available size of sewer cleaning equipment [13].

consist of base, risers, top, frame and cover manholes benching, and materials of the manholes are usually precast concrete section,



made of cast iron and they are strength and weight.

more than about 0.6 m above the outgoing sewer. The drop pipe the enter the manholes without fear of being wetted, avoid the splashing arcsion of manhole bottom.

Parameters

The Control of the Co

flow in sanitary sewers for industrial area is made up of two

designed for peak flows from domestic, and peak infiltration

make the service area. The flow rate projection are necessary to determine

of sanitary sewers.

THE RESIDENCE

practice and experience of the designer. The following relation has

$$Pf = 1.5 + (2.5/\sqrt{q}),$$
 (4.1)

is the daily average flow rate of the network branch under consideration

mortant Numbers

- Maximum velocity-3m/s
- Minimum velocity = 0.6 m/s
- Maximum slope -15%
- Minimum slope =0.5%.
- ED=70%
- Minimum diameter 200 mm
- window cover 1.5 m
- allerimum cover 5 m

Design System Design

Sweet al

century. Today, the modern city dweller has come to think of this as

Urban drainage facilities have progressed from crude ditches and

to the present intricate coordinates systems of curbs, gutters, inlet, and

conveyance.

of the land, as well as human value considerations such as aesthetic and spects of the design. The design of storm water detention basins should possible effects of inadequate maintenance of the facility.

Shrm Water Runoff

and a short time after a storm. The dependence parameters that controlled the storm water which carried by a storm or combined sewer are the surface drainage area (A, ha), the intensity of rainfall (I, L/s.ha), and runoff coefficient C cooless(the condition of the surface). There are many methods and formulas to make the storm flow, and in all of them above parameters show up. One of the most methods is rational method which will be discussed below.

authoral method

has been applied all over the world and runoff is related to rainfall intensity by

moff rate(L/s)

coefficient, which is actually the ratio of the peak runoff rate to the average

intensity, mm/min, for period equal to the time concentration area, hectar.

catchments areas, it continues to be a reasonable method, provided that it is

warranted.

the rational method calculation procedure are summarized below:

drainage area is first subdivided into sub-areas with homogeneous land use more to the existing or planned development.

For each sub-area, estimate the runoff coefficient C and the corresponding area A.

layout of the derange system is then drawn according to the topography, the sting or planned streets and roads and local deign practices.

points are then defined according to the detail of design considerations. For main so, for example, the outlets of the earlier mentioned homogeneous sub-areas should see as the inlet nodes. On the other hand in very detailed calculations all the inlet points and be defined according to local design practices.

for each inlet point A and the corresponding mean runoff coefficient C. If the subfor a given inlet has non-homogeneous land use, a weighted coefficient may be
mated.

runoff calculation are then done by means of the general rational method equations such inlet point, proceeding from the upper parts of the watershed to the final outlet.

the preliminary minor system is designed and checked for its interaction with the system, reviews are made of alternative, hydrological assumptions are verified authors are made, and final data obtained on street grades and elevations. The then should proceed with final hydraulic design of the system.

Coefficient, C

coefficient is a function of infiltration capacity, interception by vegetation, storage, and evapotranspiration. It is requires greatest exercise of judgment by and assumed constant, actually variable with time. It is desirable to develop unoff coefficient (weighted average) for each drainage area as:

$$C = \frac{\sum Ci.Ai}{\sum Ai} \tag{4.3}$$

anoff coefficient.

of coefficient with respect to general character of the area is given in the tables (Table 4.1 and Table 4.2).

**In The range of coefficient with respect to general character of the area [18].

Description of Area	Runoff coefficient
Busin	
Down town	0.7 to 0.95
Neighborhood	0.5 to 0.7
Resider	ntial
Single family	0.3 to 0.5
Multi-unit, detached	0.4 to 0.6
Multi-unit, attached	0.6 to 0.75
esidential (suburban)	0.25 to 0.4
Aparlment	0.5 to 0.7
Industri	

Light	0.5 to 0.8
Heavy	0.6 to 0.9
Parks, Cemeteries	0.1 to 0.25
Playground	0.2 to 0.35
Railroad yard	0.2 to 0.35
Unimproved	0.1 to 0.3

#2):The range of coefficient with respect to surface type of the area [18].

Character of surface	Runoff Coefficient
Pavem	ent
Asphalt and concrete	0.7 to 0.95
Brick	0.7 to 0.85
Lawns, Sar	idy soil
Flat, 2 %	0.05 to 0.1
Average, 2-7 %	0.1 to 0.15
Steep, 7%	0.15 to 0.2
Roofs	0.75 to 0.95
Lawns, heav	y soil
Flat, 2 %	0.13 to 0.17
Average, 2-7 %	0.18 to 0.22
Steep, 7%	0.25 to 0.35

intensity, i

mainfall intensity for use in rational formula it must be recognized that the function, the greater the expected average intensity will be. The critical minfall will be that which produce flow from the entire drainage area.

Shorter periods will provide lower flows since the total area is not involved and longer periods will produce lower average intensities. The storm sewer designer thus requires some relationship between duration and expected intensity. Intensities vary from place to mother and curves or equations are specified for the areas for which they were

mensity depended on many factors through which we can do our

ency of occurrence of storm (1/n) or (f).

of occurrence is the frequency with which a given event is equaled or once in a period of years. Probability of occurrence, which is the searcy, (n) is preferred by sum engineers. Thus, if the frequency of a (1/n) -5), then probability of occurrence n=0.2. Selection of storm based on cost-benefit analyses or experience. There is range of the used:

high value districts: f-10 to 50 (15 year common).

f-50 year.

and frequency characteristics of rainfall.

from gage measurement of rainfall (point rainfall) over a long period time a rainfall height diagram that show the relation between the height and time (min). The slope of the curve or rain height per unit time is

$$\frac{mm}{min} \triangle \text{ time} \left(\frac{mm}{min} \right)$$

mensity in liter per second . hectare is equal:

$$1 \left(\frac{L}{min} \right) = 166.7 \text{ i} \left[\frac{mm}{min} \right]$$

- drive intensity-duration-frequency curves long-term observation of rainfall is
 - expection.
- the most remote part (in time) of the drainage area to the point under design.

$$t_i = t_i + t_i$$
 (4.4)

me of concentration.

Town Time.

Length of pipe line (L)
$$Velocity of flow (v)$$

inlet. Inlet time is function of rainfall intensity, surface slope, surface

Senga Parameters

average, and minimum flow; storm sewer design can be completed.

The average of the sewer design can be completed.

The average of the sewer design can be completed.

The average of the sewer design can be completed.

The average of the sewer design can be completed.

The average of the sewer design can be completed.

to carry the largest storm that occurred in the

recommended is 250 to 300 mm for closed system, and the type of profile that selected.

Velocities

regularly to flush out the solids. Most countries specify

were under low flow conditions. The minimum allowable

""" m's is desirable. This way the lines will be flushed out at

""" maximum velocities for storm water system are between 4

""" wedocity is limited to prevent the erosion of sewer inverts.

slopes determined from minimum velocities, for minimum relations are shown in Table (4.3).

endation slopes of storm sewer (n=0.015) [18].

	r (D)	Slope (min)	Slope (max) = 1/D	
	ttai	anar	Cm	1
250	10	0.00735	40.0	
300	12	0.00576	0.033	
450	18	0.00336	0.0222	
600	24	0.00229	0.0167	7

For a velocity of 0.75 m/s the slope shown above should be multiplied by 1.56

Finimum slopes determined from maximum velocities, 1/D (cm) can be used as a guide.

For open channel, the slope also depended on the profile type, and generally used as the

Depth

but not less than 1 m, below the ground surface. Depth depends on the water table, sest point to be served, topography, and the freeze depth. But for the open channel it is the ground surface.

Appurtenances

sewer appurtenances include manholes, inlet, outlets and outfall, and others.

popriate storm sewer appurtenances must be selected in design of storm water sewers.

portant Numbers

- Maximum velocity=5m/s
- Minimum velocity = 1 m/s
- Maximum slope -15%
- Minimum slope =0.5%

- H/D =100%
- Minimum diameter 250-300 mm
- · Minimum cover 1 m
- Maximum cover 5 m

43 Septic Tank Design

3.1 General

which decomposes or mineralizes the waste discharged into the tank. In which wastewater flows from the waste water collection system to the septic tank through the waste pipe. The septic tank treats the wastewater naturally by holding it in the tank long much for solids and liquids to separate. The wastewater forms three layers inside the Solids lighter than water (such as greases and oils) float to the top forming a layer of seum. Solids heavier than water settle at the bottom of the tank forming a layer of badge. This leaves a middle layer of partially clarified wastewater.

so we have three distinct layers of sewage in the septic tank that will describe below.

Figure (4.1) show the layer in septic tank.

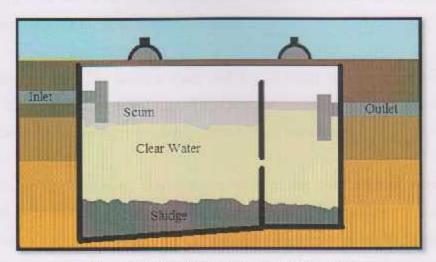


Figure (4.1): Different layers of septic tank

- Sludge Layer: All solids that are heavier than water settle at the bottom of the tank to make up the sludge layer. The anaerobic bacteria breakdown and digest the biodegradable solids in the sludge. During the process, the solids become lighter and migrate upwards to be middle of the tank or the clear zone.
- Clear Zone: The clear zone in the septic tank holds grayish or brown colored water test contains fine and microscopic biodegradable and non-biodegradable materials aspended in the liquid. It is in this liquid environment that the bacteria further break flown most of the remaining biodegradable solids. The clarified liquid then flows into the test pit.
- Scum Layer: The scum layer at the top of the septic tank contains grease, oils, soap and other materials that are lighter than water. The sludge and scum that cannot be down are retained in the tank until the tank is pumped.
- wall and outlet TEE prevent any of the seum on the top layer from exiting the walk before being treated. The inlet, outlet and the ballle wall are designed and maded to allow only the liquid from clear zone to exit into the soak pit.
- have a design parameter that classified it. Septic tank system has many but the main parameters are:
- The floating scum and sludge layers take up the top and bottom tank respectively. The effective volume is the liquid volume in the seen the scum and sludge layers in the septic tank.
- This is the time that elapses from the entry point of sewage into the betime of exit of the sewage from the clear zone of the septic tank. This is parameter for the design of septic tank, as each molecule of the incoming and exits the clear zone under the design retention time period. The

retention time is the function of the effective volume and the daily household wastewater flow.

3. Organic flow rate: One of the principal parameters used in wastewater system design as the organic flow rate which also called hydraulic loading rate. It defines as a unit solume of filter or per unit area per day of treated wastewater water.

The tank must have configuration on these points:

Base

base is usually constructed of plain concrete with the thickness of about 100-150 millimeters. This is the minimum thickness required to withstand the uplift pressure when tank is empty. The base also acts as a foundation for the side walls. A designer may reinforce the base slab in larger tanks.

Side Walls

The side walls of the septic tank are made of brick, stone masonry or concrete. The septic must be watertight.

Telet and Outlet

be correct installation of the inlet and outlet are critical in the performance of the septic

entilation

be provided in the septic tank. The simplest option is to install a vent pipe with a on the roof slab of the septic tank. The gases coming out of septic tank has a stench and so the height of the vent pipe should be higher than the normal height

Manufacture 15

care must be taken to design, construct, operate and maintain the septic system can provide years of reliable service. A poorly designed and maintained septic can be a source of pollution, which causes disease outbreaks and other problems. Therefore, it is important to understand the consequences of a segmed and maintained septic system and to take necessary precautions.

the system you must compare between the advantages and disadvantages of the

Advantages of Septic Tanks

the maintenance

system will break down solids faster so less solids will reach the draining

septic tanks, they last much longer The lifespan of a properly installed is usually between 20-40 years, but can be much longer with proper and care.

systems provide simple, effective wastewater treatment for low-density urban

systems are also simple in design, which make them generally less expensive to

storage space for the separated solids (sludge and seum).

a sedimentation tank. As the sewage enters the tank, the rate of flow is reduced ager solids in the sewage sink to the bottom of the tank.

antages of Septic Tanks

caused by poor maintenance or clogged septic systems

system

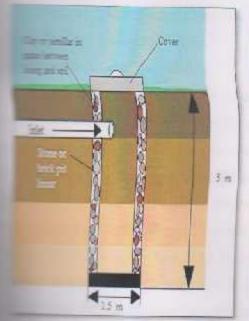
- There is a risk in rainy seasons that the septic system overflows bringing sewage to the orface.
- Clogged drains by oil, grease, fats, and other materials that may be thrown into toilets, and showers causing obstruction.
- Requires more responsibility and regular maintenance.

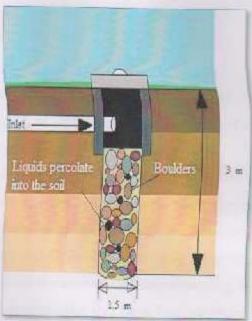




Figure (4.2): Collapse of Septic Tank due to lack of maintenance

- tank is designed to minimize pollution, but must follow with Soak for the natural process in the soil.
- walls or a hole filled with gravel or brickbats. Septic tanks should always be med to a suitable soak pit or a sewer line. The soak pit can be constructed of preservete-rings (with holes) or a dry cylindrical wall made of brick, block or stone as Figure (4.3)The minimum diameter of the pit is 1.5 meters with a minimum meters. It must be located at least 10 meters away from any waterways in soil conditions.





A lined soak pit

An unlined soak pit

the tank must be in an area where it will not experience vehicular traffic,

based from the treatment of waste water. This is inherently because a stewater treatment is removing solids from the wastewater. In addition, abstances are converted to bacterial cells, and the latter is removed from a seeding of sludge treatment is important for:

manic ingredients.

máor.

a solume and weight.

by giene by removing of pathogen organisms.

and ge for further utilization or disposal.

ways of handling the sludge treatment such as:

- 2. Aerobic/anacrobic sludge digestion.
- Mechanical drying of sludge.
- 4. Natural drying tank for sludge.

The most efficient way in our case is natural drying tank for sludge, due to high imperature of the city, also make sure the death of fly larvae and fermentation of organic material, and so increasing the efficiency of outlet sewage.

This can be done by installing a shallow basin, having area range from 100-200 m² made from Concrete resistance to sulphate and the bottom of this basin supply with tipes to collect the waste water and it cover with 30 cm of gravel.

The sludge spread along the basin less than or equal 10 cm depth to dray for seven days, ben spread another layer of sludge and so on till the total sludge depth reaching 30 cm.

There that cover the final layer of sludge with sand after five days from spread the last layer.

the sludge treated can be used in different ways such as:

- Agricultural Use as compost material, but our religion have constrain in this side so e eliminate this use.
- 2. Incineration, and use its energy for powering system.
- Land filling, but It is important consider to whether the sludge is consistent enough to be land filled.

3.2 Design Parameter of Septic Tank

- Paracteristics of manual septic tank:
- The inlet pipe shall be fixed inside the tank, with top limb rising above scum level and bottom limb extending about 300 mm below the top water level.
- The final outlet for tanks should be by 100 mm pipe diameter, the bottom limb anding to about 1/3 of the liquid depth below top water level.
- Free-Board: A minimum free board of 300 mm should be provided.
- Tentilating Pipe: Every septic tank shall be provided with ventilating pipe of at least and diameter. The ventilating pipe shall extend to a height which would cause no

nuisance to any building in the area. Generally the ventilating pipe may extend to a spit of about 2 m when the septic tank is at least 20 m away from the nearest building to a height of 2 m above the top of the building when it is located closer than 20 mess.

Floor

floor may be of cement concrete of minimum slope of 1: 10 may be provided and the sludge outlet to facilitate desludging.

Walls

walls should be of such thickness as to provide adequate strength and water

ations used in the design of septic tank are:

$$V = Q * HRT \tag{4.7}$$

Surface area = Flow rate * Organic flow rate

$$As = Q * OFR \tag{4.8}$$

$$D = \frac{V}{As} \tag{4.9}$$

$$As = W * L \tag{4.10}$$

44 Solid Waste Management

waste is the collecting, treating, and disposing of solid material that is discarded to the served its purpose or is no longer useful. While solid waste management control of generation, collection, storage, transport, source separation, treatment, recovery, and disposal of solid waste [19].

that located near grave which have large quantity of solid waste in random
way, also we make a waste collection and transportation of solid waste of the
finding the number of container needed and capacity of compactor and

malysis of solid waste management for Al- Dahriya city, required data was different source, majority from the Land, history and human heritage in book [20].

Chapter Five

Analysis and Assessment

** Estewater Collection System

Millimeral .

design of wastewater collection system for Al-Dahriya Old City is made, a future plans for construction of the collection system, corresponding to the Dahriya municipality about their future plan, in order to reduce the problem

the layout of the system established is presented, and the computation

ILL System

sewerage system is to establish an overall system layout that the mea to be sewered, showing roads, streets, buildings, other utilities, less floor elevation or all buildings to be drained.

of wastewater collection system for Al-Dahriya Old City, the

of the area to be served.

This is usually near the lowest point in the area and is often

system to serve all the contributors.

the users or future users can readily tap on. They are also seems for maintenance and thus are ordinarily placed in streets

Large trunk sewers are located in low-lying areas closely

- Revise the layout so as to optimize flow-carrying capacity at minimum cost. Pipe lengths and sizes are kept as small as possible, pipe slopes are minimized, and followed the ground surface slope to minimize the depth of excavation, and the numbers of appurtenances are kept as small as possible.
- The pumping is avoided across drainage boundaries. Pumping stations are costly and add maintenance problems.
- final layout of Al-Dahriya Old City is illustrated in Figures (5.1, 5.2).
- main trunks, five sub main lines are located on the layout.



Palestine Polytechnic University
Technology and angineering college
civil and Architecture department
Architectural Engineering

Environmental Assessment of Al-Dahrleh Old City.

Notes:-

All contour line in meter.

LEGEND

Hain Road

Sub Main Rood

Calument Area

Flow Direction

Contour Line

Drawing Title: Layout for Al-Dahrieh Old City.

Designed By: Haneen Abu-Sabba. Sajida Al-Daraweesh.

Supervisor: Eng:Samah AL-Jabary.

Client: Al-Dahrieh Municipality.

V Scale 1:50 H Scale 1:500

of Figure : 5.1

Page: 72

Date : Dec, 2015

Cumitity Of Wastewater

the selection of appropriate pipe sizes and the transport the quantity of wastewater expected from the surroundings and upstream the next pipe in series, subject to the appropriate design constrains. The design that are in the example given below.

the Isyout of the wastewater collection system the quality of wastewater collected about the area.

a gravity flow sanitary sewer

sanitary sewer for the area to outfall (line M1) shown in Figure

amption uses 18-20L/c.day.

ption uses 100L/c.day.

== 1752 capita.

using the formula $P = P_*(1+R)^n$, Where P_* is a current population

25 years as a design period.

as 80% of the water consumption.

are use 10% of the domestic sewerage flow.

conding on the formula;

25 101



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Mechanical department
Emironmental Technology and Engineering

Environmental Assessment of Al-Dubriya Old City.

Notes:1- All Pipe Diameter are
Millimeter.
2-All Pipe Depth are in
Meter.
3-Depth of Excavation up to
1.5 m.



Designed By: Hancen Abu-Sabha. Sajida Al-Daraweesh.

Supervisor: Eng:Samah AL-Jabary.

Client: Al-Dahrieh Municipality.

Drawing Title: The Profile Of Sanitry Line (Main #1) (From Manholes 1 to 7)

H.Scale 1:500

V.Scale 1:50

No.of Figure: 5.3

Page: 75

Date: Dec.2015

Point Number	7
Manhole Nui	мн7
Station	5+50
Ground Elev:	50,00
Depth of Ma	2,811
Distances	2855
Dstance of Ma	
Pipe Diamete	
Pipe Slope	

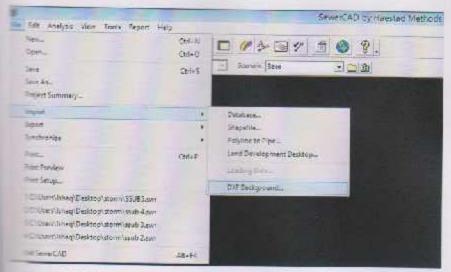
Solution

- Lay out the trunk sewer. Draw a line to represent the proposed sewer Figure (5.3).
- Locate and number the manholes. Locate manholes at (1) change in direction, (2) change in slope, (3) pipe junctions, (4) upper ends of sewers, and (5) intervals from 35 to 50 m or less. Identify each manhole with a number.
- Prepare a sewer design computation table. Based on the experience of numerous engineers, it has been found that the best approach for carrying out sewer computations is to use a computation table. The necessary computations for the sanitary sewer are presented in Table (5.1) for year 2036. The data in the tables are calculated as follow:
 - The entries in columns 1 and 2 are used to identify the line numbers and street sewer name.
 - The entries in columns 3 through 5 are used to identify the sewer manholes, their numbers and the spacing between each two manholes.
 - The entries in column 6 used to identify unit sewage. Unit sewage = 80% multiplied by the current water consumption multiplying by density.
 - 4. The entries in columns 7 and 8 are used tributary area, column 7 used incremental area, column 8 used total area in donum.
 - To calculate municipal maximum flow rates columns 9, 10 are used. Column 9 is municipal average sewage flow (unit sewage* total area), the peak factor column 10 calculated as: $PI = 1.5 + 2.5 / \sqrt{q}$ where q = Average industrial sewage flow Column 9).
 - 11 used to calculate the Qmax in year 2036, the value of it comes from 10° column 9. Column 12 calculate the infiltration which equal to (10% * column 9). Column 13 is used to show the maximum flow come from column 11+ column 12.
 - the maximum flow in each manhole separately.

											Personal Property of	11111	Polisi	C max
100	Name of	March Prop	sider year		office seatiful			Average	Presi, FRIS	Warmin		Avvenge	2	
1847	Manne			8	m³/d.dounm	dournm	dounm	m³/day		Name of the second	m³/day	m³/day	/m//day	m2/day
-	2	3	4	2	9	7	8	0	40	11	12	13	14	15
+	main 1	1	2	30.26	36.34	90.0	90.0	2.18	3.00	6.54	0.22	2.40	6.76	6.76
2 m	main 1	2	67	49.36	36.34	0.40	0.46	16.55	2.11	35.00	1,66	18.21	175.00	168.24
3	main 1	3	4	24.25	36.34	0.17	0.62	22,55	2.03	45.70	2.26	24.81	186.29	18.06
4 m	main 1	4	5	25.10	36.34	0.31	0.93	33.82	1.93	17.09	3,38	37.20	344.95	326.89
S	main 1	5	9	40.39	36.34	0.54	1.47	53.44	1.64	20.44 100 1	5.34	58.79	380.09	53.19
9 m	main 1	9	7	49.28	36.34	1.04	2.51	91.24	1.70	100.74	9.12	100.37	446.17	392.97
7 m	main 1	7	8	48.86	36.34	0.92	3.43	124.79	1.72	215.12	12.48	137.27	617.79	224.82
8	main 1	8	6	50.22	36.34	1.09	4.52	164.45	1.69	278.73	16.44	180.89	685.36	460.55
6	main 1	6	10	49.43	36.34	1.89	6.42	233.21	1.06	387.99	23.32	256.53	801.50	340,96
	main 1	10	11	49.12	36.34	1.54	7.96	289.25	1.65	476.39	28.93	318.18	895.51	554.55
11 m	main 1	11	12	50.49	36.34	1,46	9.42	342.24	1.8	559.61	34.22	376.46	984.02	429.47
12 m	main 1	12	13	46.21	36.34	0.82	10.23	371.90	1.63	909.00	37.19	409.09	1033.44	603.97
13 m	main 1	13	14	49.36	36.34	1.72	11.95	434.41	1.62	103.72	43.44	477.85	1361.36	757.39
14 m	main 1	14	15	42.90	36.34	1.72	13.67	496.92	1.61	11,110	49.69	546.61	1465.00	707.61
15 m	main 1	15	16	34.30	36.34	1.20	14.87	540.42	1.0	608.75	54.04	594.47	1537.00	829.39
	main 1	16	17	41.64	36.34	1.37	16.24	200.065	1.60	945.83	59.01	649.08	1619.04	789.65
Design Assamptions and data	Assam	ptions	and da	ta					1					
1) Water commissingtion is	musum	si uoildi		3.5	3.5 m3/d.d which		80%	return to sewer	wer	7) Minimum slope Smin =	0.5	%		
3) Infiltration is equal 4) Minimum pipe diameter= 5) Minimum velocity Vmin =	on is eq n pipe d n veloci	ual liameter ty Vmin		-0%	% of the average industrial wastewater flow min m/sec	age indus	trial was	tewater flor	, ·	9) Maximum manhole spacing = 10) Minimum depth of sewer 11) Design depth of flow h/d<	45 60 1.5 0.5	% E E		
6) Maximum velocity Vmax =	n veloc	ity Vmax	TI	(1)	m/sec					12) Manning coemicient n-	0.01			

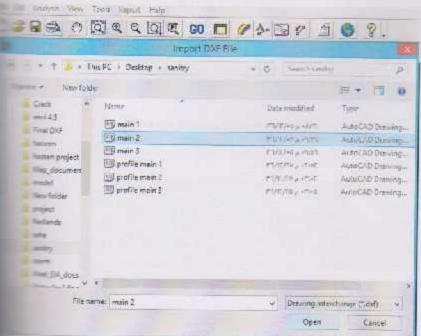
CAD program works

Open SewerCAD , select file -- import -- DXF Background to import the DXF file , (5.4) below shows this step.

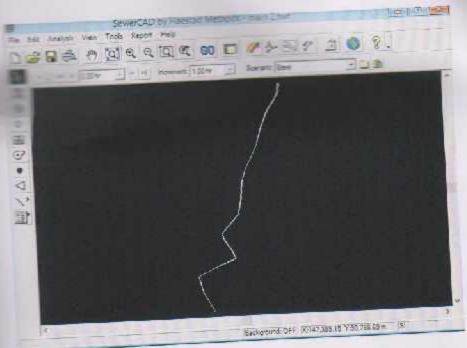


gure(5.4): Importing DXF file

file location is then press open ,figure(5.5) below shows this step. And figure line(main 2).



Figure(5.5):Opening the DXF file



Figure(5.6):main2 line

Press pipe icon, a massage will appear tell you to create a project see figure (5.7).

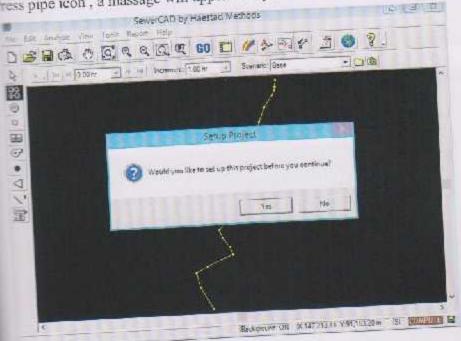


Figure (5.7): Creating Project

These yes and define the project then press next twice, then select finish, the figure (5.8) who will step.

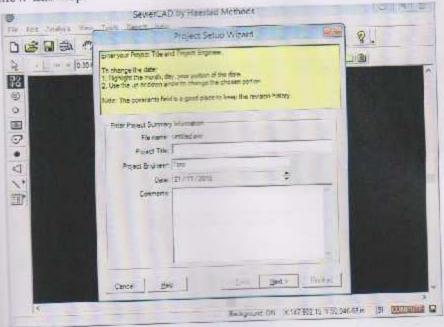
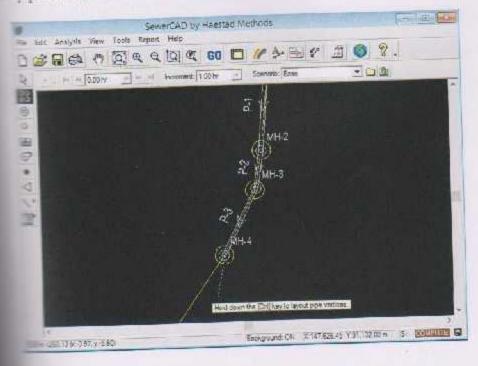


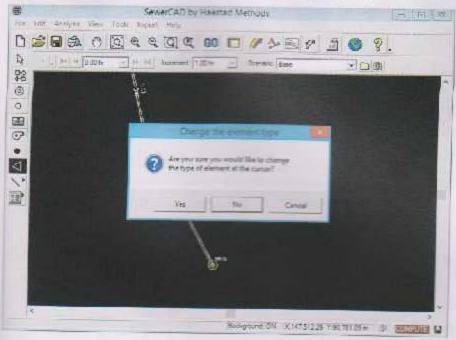
Figure (5.8): Defining the project

pipe icon and connect between manholes, figure(5.9) below show this step.



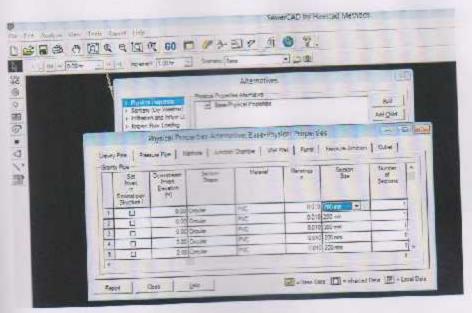
Figure(5.9): Creating a pipe network

After you connect all manholes, press on the out let icon and click on the last manhole, then press yes to replace the manhole with outlet, the figure (5.10) below shows the step.



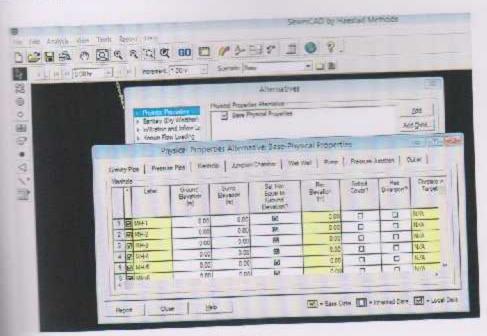
Figure(5.10): Creating outlet

your project, then select analysis — alternatives — physical properties — edit, eart editing gravity pipe, see figure (5.11).



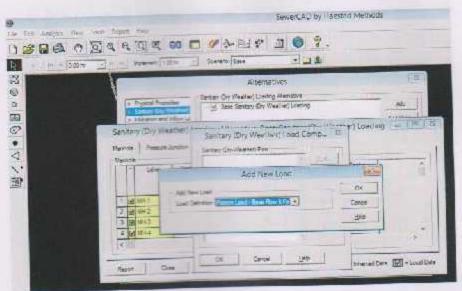
Figure(5.11): Editing design parameter

Select manhole to enter the ground elevations of manholes, then select out let to enter its manhole. Then press close, Figure (5.12) below shows the step.



Feure(5.12); Editing design parameter

Select sanitary (dry weather) -- edit -- manhole to select the type of load and to mer the load for each manhole, figure (5.13) below shows the step.



Figure(5.13): Editing design parameter

After doing this for each manhole press close, then select design constrains — edit to the design specifications, figure (5.14) below shows the step.

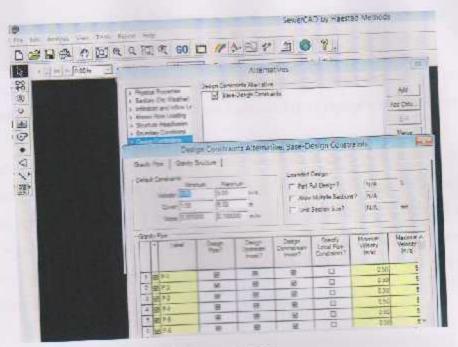
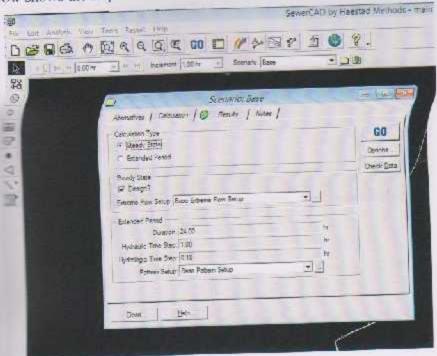


Figure (5.14): Editing design parameter

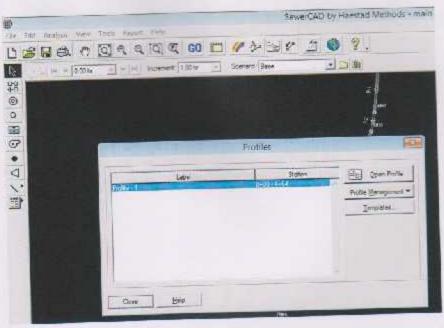
step press save, press GO button to start design then press on GO,

15)below shows the step.

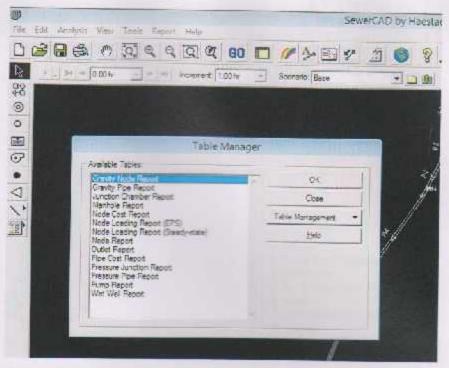


Figure(5.15): Checking the design

- If you have green light that mean there is no problems in the design work, but if you have yellow or red light that's mean there is problem, read the massages and fix these moblems.
- After finishing design work we need to show the pipe line profile, gravity pipe report and gravity node report. Press profile button to make the profile see figure (5.16), have we would put the scale of the profile. The profile for this project are attached in appendix. We get the required tables by pressing tabular report button see figure (5.17), and then mose gravity pipe report and gravity node report. The required reports for this project are maked in appendix.



Figure(5.16): Creating Profile



Figure(5.17): Creating Tables

(5.18) shows the profile of sanitary main 1, and gravity pipe report and gravity node for the same profile presented in tables (5.2, 5.3).





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Notes:1- All Pipe Diameter are
Millimeter.
2-All Pipe Depth are in
Meter.
3-Depth of Excavation up to
1.5 m.

Designed By: Haneen Abu-Sabha. Sajida Al-Daraweesh.

Supervisor: Eng:Samah AL-Jabary.

Client: Al-Dahrieh Municipality.

Drawing Title : The Profile Of Sanitry Line (Main #1)

H.Scale 1:500

V.Scale 1:50

No. of Figure: 5.18

Page: 87

P-16

Date: Dec.2015

Upstream Node	Downstream Node	Section Size Description	Section Shape	Average Velocity (m/s)	Slope (m/m)		
MH-1	MH-2	200 mm	Circular	0.40	0.035		
MH-2	MH-3	200 mm	Circular	1.08	0.035		
MH-3	MH-4	200 mm	Circular	0.60	0.006054		
MH-4	MH-5	200 mm	Circular	0.75	0.005		
MH-5	MH-6	200 mm	Circular	1.53	0.034572		
MH-6	MH-7	200 mm	Circular	1.79	0.035		
MH-7	MH-8	200 mm	Circular	1.90	0.035		
MH-8	MH-9	200 mm	Circular	2.08	0.035		
WH-9	MH-10	200 mm	Circular	2.19	0.035		
MH-10	MH-11	200 mm	Circular	2.35	0.035		
MH-11	MH-12	200 mm	Circular	2.19	0.026119		
MH-12	MH-13	200 mm	Circular	2.56	0.035		
VEH-13	MH-14	200 mm	Circular	2.69	0.035		
WH-14	MH-15	250 mm	Circular	2.77	0.034449		
ME-15	MH-16	250 mm	Circular	2.90	0.035		
E-16	O-1	300 mm	Circular	1.42	0.005		

Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)			
MH-1	6+83	644.94	1.2	6.76	0.22			
MH-2	6+52	642.86	1.2	175	0.50			
MH-3	6+03	639.9	1.2	193.06	0.51			
MH-4	5+78	639.79	1.2	519.95	0.68			
MH-5	5+53	639.71	1.2	573.14	0.70			
MH-6	5+13	639.53	1.2	966.11	0.82			
MH-7	4+63	636.25	1.2	1190.93	0.87			
MH-8	4-14	633.36	1.2	1651.48	0.98			
MH-9	3-64	630.98	1.2	1992.44	1,05			
MH-10	3-14	628,61	1.2	2546.99	1.17			
MH-11	2+65	626.37	1.2	2976.46	1.26			
MH-12	2+15	624.99	1.2	3580.43	1.41			
MH-13	1+69	622.32	1.2	4337,82	1.62			
MH-14	1+19	620.1	1.2	5045.43	1.39			
MH-15	0+76	619.07	1.2	5874.82	1.52			
MH-16	0+42	617.34	1.2	6664.47	1.40			
0-1		617.34		6664.47	0.00			

5.2 Storm Water

5.2.1 General

in this project, design of storm water drainage system for Al-Dahriya Old City, in order to solve problem causes by the commutative flooded storm water in the streets will be prepared.

in this section, the computation procedures and tables are given along the drawings of avout.

52.2 Quantity of Storm Water

After preparing the layout of storm water drainage system the quality of storm water that the system must carry it will be calculated using the date collected about the area.

Example:

besign a gravity flow storm water drainage pipe for the area of Al-Dahriya Old City use sub-main 1 as example this is line down in figure (5.19). Assume that the following esign criteria have been developed and adopted based on an analysis of local conditions end codes.

weighted runoff coefficient (C) uses 0.65.

The inlet time (t;)use 10 minutes.

by concentration time (t_c) use equations:

$$t_c = t_i + t_f \tag{4.4}$$

runoff rate depending on the formula:

runoff intensity use Figure (5.20).

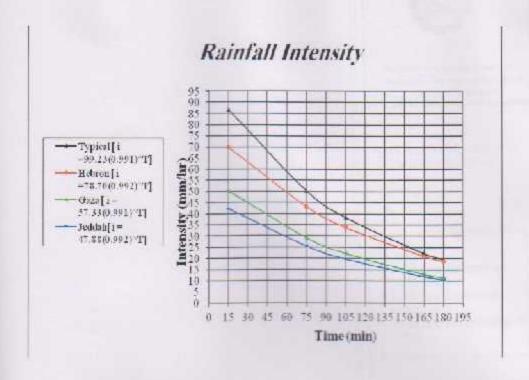


Figure (5.20) The rainfall intensity-duration curve for several areas.



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Environmental Assessment of Al-Dahriya Old City.

Notes:1- All Pipe Diameter are
Millimeter.
2-All Pipe Depth are in
Meter.
3-Depth of Excavation up to
1.5 m.

General Elevation
Sever Une
Manholes

Designed By: Hancen Ahu-Sabha. Sajida Al-Daraweesh.

Supervisor: Eng:Samah AL-Jabary.

Client: Al-Dahrieh Municipality.

Drawing Title: The Profile Of Storm Line (Sub main #1) (From Manholes 1 to 9)

H.Scale 1:500

V.Scale 1:50

No.of Figure: 5.19

Page: 92

Date : Dec. 2015

Manhe Station Groun Depth Distar

Point

Dstand Pipe I

Pipe S

Solution:

- L Lay out the storm water sewer. Draw a line to represent the proposed sewer Figure (5.19).
- 2. Locate and number the upper and lower points of the line(sum-main1).
- 3. The necessary computations for the storm water sewer are presented in Table (5.4) for year 2036. The data in the tables are calculated as follow:
 - a. The entries in columns 1 through 6 are used to identify the point location, their numbers and the length between them.
 - b. The entries in column 7 used to identify the sewer area, column 7 shows the partial sewered area in hectare.
 - c. The entries in columns 8 through 14are used to calculate the design flow .Runoff coefficient (C) is entered in column 8. The partial sewer area in hectare is multiplied by runoff coefficient (C) and the result is given in column 9. The cumulative multiplication of the sewered area in hectare is multiplied by runoff coefficient are given in column 10. The concentration time is shown in column 11 and rainfall intensity (L/s.ha) is shown in column 12. Column 14 shows the quantity of storm water separately between two inlets

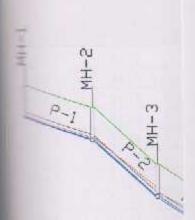
-	metric .
	A.
	M
- 1	٠,

	Hy.	ÖI	(1/s)	48	0 TOE	607.7	9.480	11,270	19.369	14.000	22.448	12,386	27 256	003.13	7.626	58,580	040 000	91.350	12.521	
		ď	(8/1)	47	1010	5.7.65	12.266	23.536	25 005	20.200	58,353	70.739	000000	96.380	105.622	164 202	1	255.552	268.073	
-		(1)	(I/s.ha)	44	1	201.191	200.539	199,943	400 000	188,343	198.614	198 232	200000000000000000000000000000000000000	197.488	197.012	105 404	190,401	191.990	190,117	
-		э1	(min)	11.7	-	10.438	10.842	41 213		11.586	12.043	42 283	14.200	12.751	13,051	CTAAA	14.01.4	16,266	17.487	
	∃∧	SUM(AC)	(ha)		9	0.014	0.061	0.448	0.110	0.180	0.294	0.983	0.337	0.496	0.536	0000	0.840	1.331	1.410	
	20	A.C FEEFF	(ha)	/ /		0.014	0.047	0.067	0.00	0.062	0.114	0000	0.063	0.139	0.040		0.304	0.491	0.079	
		FACTOR set and industry	anta	ш	6	0.65	0.85	20.0	0.65	0.65	0.65	0.00	0.65	0.65	0.65	0,00	0.65	0.65	0.65	20.00
	pu	AREA of Street at Industri	/hal		7	0.00	20.00	0.07	60.0	0.10	440	0.1	0.10	0.24	200	0,00	0.47	0.76	0 40	0.12
а		LENGTH	-	(H)	9	76 96	20.21	29.92	72.78	95 19	2000	122,59	136.96	405.05	20,001	183.08	244.31	375 06	373.30	449.19
	ŀ	LENGTH	100	(m)	15	0000	77.97	24.26	22.26	22 A4	14.77	27.40	14.36	00 00	28.03	18.04	64.23	20000	131.56	73.23
OCATION		NO.	MC	רכ	P		2	3	4		0	9	7		90	6	40	TO	11	12
	IN MH. NO.		Bdd	ın	4	2	-	2	~	,	4	22	e	0	7	80		n	10	11
		E NAME	INI	1		M	sub1	sub1	Pales	ans	sub1	Subi	1	Lans	1dus	this		sub1	2np1	Pales
		язами	N			-	-	2		2	4	4	,	9	7	8	0	6	10	4.4

SormCAD program works

this program works at the same steps in the SewerCAD program, figure (5.21) shows the same of storm sub main 1, and gravity pipe report and gravity node report for the same presented in tables (5.5, 5.6).

required reports and profiles for this project are attached in appendix.





Polastine Polytechnic University
Technology and engineering college
Mechanical department
Environmental Technology and Engineering

Environmental Assessment of Al-Dahriya Old City.

Notes:

I- All Pipe Diameter are Millimeter.

2-All Pipe Depth are in Meter.

3-Depth of Excavation up to 1.5 m.

Designed By: Hancen Abu-Sabha. Sajida Al-Daraweesh.

Supervisor: Eng:Samah AL-Jabary.

Client: Al-Dahrieh Municipality.

Drawing Title: The Profile Of Storm Line (Sub main #1)

H.Scale 1:500

V.Scale 1:50

P-11

No.of Figure: 5.21

Page: 96

Date : Dec. 2015

Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)
MH-1	4+42	659.8	1.2	240.67	0.55
MH-2	4+16	659	1.2	1.059.78	0.84
MH-3	3+92	656.88	1.2	2,033.53	1.06
MH-4	3+70	655.47	1.2	3,102.17	1.29
MH-5	3+48	651.65	1.2	5,041.67	1.84
MH-6	3+21	649.81	1.2	6,111.86	2.2
MH-7	3-07	646.95	1.2	8,466.81	1.99
MH-8	2+79	645.81	1.2	9,125.73	1.41
MH-9	2+61	645.81	1.2	14,187.01	1.72
MH-10	2+00	643.99	1.2	22,079.68	1.87
MH-11	0+68	643.1	1.2	23,161,54	1.9
0-1		643.1		23,161.54	0

Label	Calculated Station (m)	ode Report for Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)
MH-1	4-42	659.8	1.2	240.67	0.55
MH-2	4+16	659	1.2	1,059.78	0.84
MH-3	3192	656.88	1.2	2,033.53	1.06
MH-4	3+70	655.47	1.2	3,102,17	1.29
MH-5	3+48	651.65	1.2	5,041.67	1.84
MH-6	3+21	649.81	1.2	6,111.86	2.2
MH-7	3+07	646.95	1.2	8,466.81	1.99
MH-8	2+79	645.81	1.2	9,125.73	1.41
MH-9	2+61	645.81	1.2	14,187.01	1.72
MH-10	2+00	643.99	1.2	22,079.68	1.87
	0+68	643.1	1.2	23,161.54	1.9
MH-11 O-1	0100	643.1		23,161.54	0

5.3 Septic Tank Design

5.3.1 Septic tank

Assume that:

- HRT=2 hr
- Organic flow rate=35 m3/m2/d
- Depth =3 Width (D 3W)
- 2 tank (L₁=2L₂), Slope of tank nearly 1:10
- The suspended solid concentration and BOD concentration of the influent discharge
- == 450 ppm, 300 ppm respectively.
 - Removal ratio of BOD and suspended solid is 33 %, 60 % respectively.

$$T = 6664.47 * \frac{2}{24}$$

$$= W * L$$

$$A_S - W*D = W*3W$$

W-7.9m=8, and L-24 m

Suppose that we have two septic tanks.

 $\mathbb{L} = L_1 + L_2$

 $\mathbb{L}=\mathbb{L}_1 + 2\mathbb{L}_1$

Then $L_1 = 16$ m, and $L_2 = 8$ m

- The SS concentration in effluent=200 ppm
- The BOD concentration in effluent =180 ppm

Figure (5.22) show the dimension of the septic tank.





Palestine Paytechnic University Technology and engineering college Mechanical department Environmental Technology and Engineering

Environmental Assessment of Al-Dahrich Old City.

Notes:-

All Diamention are meter.

Designed By: Hancen Abu-Sabha. Sajida Al-Daraweesh.

Supervisor: Eng:Samah AL-Jabary.

Client: Al-Dahrieh Municipality.

Drawing Title:

Septic Tank Plan and Section

Page : 101

No.of Figure: 5.22

Date : Dec. 2015

sassilid waste management

- 38864 capita in Al-Dahriya city
- 8000 student in school and kindergartens
- III public service office
- 5 Emertainment centers
- commercial markets
- patient beds (Health care centers)
- member of container assuming that:
- 1 time /day
- of type 240 I.
- mer of type 1100 L.
- of type 4 m³
- succent is 1 household
- ment beds is 1 household
- in compaction truck = 0.7 ton / m3
- = 86%
- end in container = 0.25 ton / m3
- per container = 6 min
- 6.5 hr
- for household, student, public service office, Entertainment centers, and are 1.5, 1.5, 1.5, 3, 3, and 1.5 respectively.
- *Safety of Waste Generated Daily =Number of Unit * Waste Generation *Safety
- Density of Compactor = Volume Of Truck * Density Of Solid In Compaction
- Rate* Loading Rate

Effective Capacity of Compactor = Volume Of Container * Density Of Solid In Container Operating Rate

For each unit apply below equation:

The Total Volume of Waste Generated Daily =Number of Unit * Waste Generation

-The Total Volume of Waste Generated Daily of household - 38864 Cap*4L/Cap.Day* Safety Factor 1.5

= 233184 L /day

We have 8000 student and every 50 student is 1 household so we have 160 hh The Total Volume of Waste Generated Daily of student in school and kindergariens = 160hh*24L/Cap.Day* 1.5

= 5760 L/day

The Total Volume of Waste Generated Daily of student in public service office

= 11 *24L/Cap.Day* 1.5 = 396 L /day

The Total Volume of Waste Generated Daily of student Entertainment centers

= 5 *24L/Cap.Day* 3 = 360 L /day

The Total Volume of Waste Generated Daily of commercial markets

= 700 *24L/Cap,Day* 3 = 50400 L/day

We have 600 patent bed and every 2 bed is 1 household so we have 300 hh The Total Volume of Waste Generated Daily of Health care centers

= 300hh*24L/Cap.Day* 1.5 = 10800 L /day

The Total Volume of Waste Generated Daily

=233184+5760+396+360+50400+10800

- 300900 L/day

- 10% container of type 240 L = 10%*(300900/240) = 125 container of type 240 L
- 60% container of type 1100 L =60%*(300900/1100) = 164 container of type 1100 L
- 30% container of type 4 m³ =30%*(300900/4000) = 23 container of type 4 m³

Table(5.7): Capacity per trip

Number		l capacity outsiner	Loading Rate	Operating Rate	Effective Capacity
1	m3	ton/m3	(%)	(%)	ton
	5	0.7	90	86	2.7
2	8	0.7	90	86	4.33
3	12	0.7	90	86	6.5
4	21	0.7	90	86	11,4

 Effective Capacity of Compactor – Volume of Truck * Density Of Solid In Compaction Truck *Operating Rate* Loading Rate

Table(5.8): number of container

Type of compactor		l capacity utainer	Operating Rate	Effective Capacity	number of container per trip
m2	m3	ton/m3	(%)	Ton	7
5	1.1	0.25	80	0.22	12
8	1.1	0.25	80	0.22	20
12	1.1	0.25	80	0.22	30
21	4.3	0.25	80	0.86	13

Effective Capacity of Compactor = Volume Of Container * Density Of Solid In
 Container *Operating Rate

= 1.1 m3 *.25 ton /m3 *.8 *.22 ton

Transportation

	Type of compact or	number of container	hauling time per	1 trip in minute			average trip per shift	average capacity per shift	
		per trip			total time	total time		in ton	
	m2		Min	min	min	Min	hr	1	I
	5	12	6	73.9	40	113.9	1.9	3.4	9,3
2	8	20	6	118.2	40	158.2	2.6	2.5	10.7
10	12	30	6	177.3	40	217.3	3.6	1.8	11.7
	21	13	6	79.4	40	119.4	2.0	3.3	37.2

- Total time(min) = time for collection + time for transportation

$$=40 \pm 73.9$$

$$= 113.9 \, \text{min}$$

Total time(hr) = 113.9 min *(1 min / 60 hr)

$$= 1.9 \text{ hr}$$

- Average trip per shift = Shift working / total time

$$= 6.5 / 1.9$$

- Average capacity per shift - Average trip per shift * effective capacity of compactor

$$-2.7*3.4$$

5.5Park design

the idea of park was by cooperation between us as an environmental engineering and student from architectural student working at the same project, but in architectural view.

and scapes are more than just pretty views. They can provide economic benefits and create more appealing places to live

The are looking for ways to make our landscape design more sustainable, we must take in assideration these points:

we look to the sustainable sites; the site oversees a unique view of historical place, in milition to place which has a large quantity of solid waste by converting it to a place miller for children to play in it, figure (5.23) show the bad condition for the site, and miller (5.24) show the landscape of small park.



Figure (5.23): Parking site prior implementation and the bad condition there

water of container for landscape distributed to limit solid waste on ground.

water quality and quantity, by making storm water collection system and gradient in each part of park.

park benches, and lots of thing can be built by these wheel.



Figure (5.25): Reuse cans, wheel for agricultural use

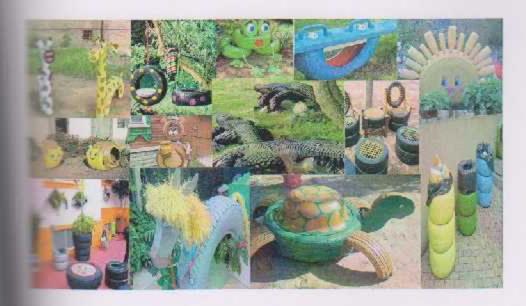


Figure (5.25): Use wheel for different uses.

Create direct, comfortable and safe pedestrian routes. Generally; main footpaths should be wide enough to allow two wheelchairs to pass comfortably.

Provide shade and high-quality landscaping and enhancing Wildlife Habitat

Provide children's play areas that should be safe for them.

Landscapes need to be maintained and managed to conserve investment.



Salestine Polytechnic University
Technology and angineering college
civil and Architecture department
Architectural Engineering

Environmental Assessment of Al-Dahrieh Old City.

Drawing Title: Landscape of Small Park in Al-Daheryia Old City.

Designed By: Deema Alamllah. Hancon Abu-Sabha. Leena Abu- Reesh. Sajida Al-Daraweesh.

Supervisor: Eng:Samah AL-Jabary.

Client: Al-Dahrieh Municipality.

V Scale 1:50 H Scale 1:500

of Figure: 5.24

Page: 109

Date: Dec, 2015

Chapter Six Bill of Quantity

Chapter Six Bill of Quantity

1. For the Proposed Wastewater Collection System

No	EXCAVATION	UNI	QTY		NIT ICE	TOT	CE
*		Т		S	C	S	C
AI	Excavation of pipes trench in all kind of soil for one pipe diameter 200 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	2685				
A2	Excavation of pipes trench in all kind of soil for one pipe diameter 250 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	128				
43	Excavation of pipes trench in all kind of soil for one pipe diameter 300 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	92				
	Sub-Total						-
3	PIPE WORK				-	-	-
	Supplying, storing and installing of uPVC	LM	2905				
	Sub-Total						

BACKFILLING	UNI	QT	UNIT	TOTAL
	T	Y	PRICE	PRICE
PIPE BEDDING AND BACKFILLING Dimension and material				

C1 Supplying and embedment of sand for one pipe diameter 8 inch, depth up to 1.5 meter and disposing of the debris and the top soil unsuitable for backfill outside the site.	LM	2685	
Supplying and embedment of sand for one pipe diameter 10 inch, depth up to 1.5 meter and disposing of the debris and the top soil unsuitable for backfill outside the site.	LM	128	
Supplying and embedment of sand for one pipe diameter 12 inch, depth up to 1.5 meter and disposing of the debris and the top soil unsuitable for backfill outside the site.	LM	92	
Sub-Total			
MANHOLES, Details according to the drawing			
Supplying and installing of precasted manhole including excavation pipe connection, epoxytar coating, 25-aon cast iron cover and backfill, size 1200mm, depth up to 1.5m.	NR	85	
Supplying and installing of precasted manhole including excavation pipe connection, epoxytar coating, 25 ton cast iron cover and backfill, size 1200mm, depth up to 2.5m.	NR	26	
Sub-Total			
Concrete Surround			
Supplying and east iron (B200) surround for sewer.	M ³	109	
Sub-Total			

EXCAVATION	UNI	QT Y	UNIT PRICE	TOTAL PRICE
Air And Water Leakage Test				
Air leakage test for sewer pipe lines 8,10,12,and 14inch according to specifications, including for all t emporary works.	LM	2905		

F2	Water leakage tests for manholes, depth up to 1.5 meter according to specifications.	NR	85	
F3	Water leakage test for manholes, depth up to 2.5 meter according to specification	NR	26	
	Sub-Tota	ıl		
G	Rode reinstatment			
GI.	Removing and dispose of the asphalt and repassing and re-Asphalting after BACKFILL, road structure layers compacted basecoarse 125+125 mm, MCO layer 11/m2, asphalt layer 50mm(3/4").	LM	2905	
	Sub-Tota	1		
王	Survey work			
1	Topographical survey required for shop drawings and as built DWGS using absoluct Elev. And coordinate system	LM	2905	
	Sub-Total			-

2.For The Proposed Storm water Collection System

No	EXCAVATION	UNI	QTY		NIT ICE		TAL
-		1		S	C	S	C
Al	Excavation of pipes trench in all kind of soil for one pipe diameter 200 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	561				
A2	Excavation of pipes trench in all kind of soil for one pipe diameter 250 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	212				
A3	Excavation of pipes trench in all kind of soil for one pipe diameter 300 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	236				
84	Excavation of pipes trench in all kind of soil for one pipe diameter 375 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	281				
15	Excavation of pipes trench in all kind of soil for one pipe diameter 450 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	507				
10	Excavation of pipes trench in all kind of soil for one pipe diameter 600 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	406				

A7	Excavation of pipes trench in all kind of soil for one pipe diameter 750 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	96	
A8	Excavation of pipes trench in all kind of soil for one pipe diameter 900 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	94	
A9	Excavation of pipes trench in all kind of soil for one pipe diameter 1050 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	24	
A1 0	Excavation of pipes trench in all kind of soil for one pipe diameter 375 mm depth and disposing of the debris and the top soil unsuitable for backfill outside the site	LM	28	
	Sub-Total			
B	PIPE WORK			
	Supplying, storing and installing of uPVC	LM	2445	
	Sub-Total			

No.	BACKFILLING	UNI T	QT Y	UNIT PRICE	TOTAL PRICE
Ĭ	PIPE BEDDING AND BACKFILLING Dimension and material				
	Supplying and embedment of sand for one pipe diameter 200 mm, depth up to 1.5 meter and disposing of the debris and the top soil unsuitable for backfill outside the site.	LM	561		

-						
C2	Supplying and embedment sand for one pipe diameter 2 mm, depth up to 1.5 meter a disposing of the debris and t top soil unsuitable for backtoutside the site.	nd I	М	212		
C3	Supplying and embedment sand for one pipe diameter 3 mm, depth up to 1.5 meter as disposing of the debris and top soil unsuitable for backfoutside the site.	nd he I	.M	236		
C4	Supplying and embedment sand for one pipe diameter 3' mm, depth up to 1.5 meter ar disposing of the debris and the top soil unsuitable for backtioutside the site.	75 nd L	М	281		
2 m 50 m	Supplying and embedment of and for one pipe diameter 450 m, depth up to 1.5 meter and sposing of the debris and the soil unsuitable for backfill taide the site.	LM	5	07		1
10 10 10	pplying and embedment of od for one pipe diameter 600 to depth up to 1.5 meter and posing of the debris and the soil unsuitable for backfill side the site.	LM	40	06		
A STATE	for one pipe diameter 750 depth up to 1.5 meter and posing of the debris and the soil unsuitable for backfill ade the site.	LM	90	5		
THE REAL PROPERTY.	for one pipe diameter 900 depth up to 1.5 meter and unsuitable for backfill de the site.	LM	94			

				_	 _	
C9	Supplying and embedment of sand for one pipe diameter 1050 mm, depth up to 1.5 meter and disposing of the debris and the top soil unsuitable for backfill outside the site.	LM	24			
C1 0	Supplying and embedment of sand for one pipe diameter 1200 mm, depth up to 1.5 meter and disposing of the debris and the top soil unsuitable for backfill outside the site.	LM	28			
	Sub-Total					
D	MANHOLES, Details according to the drawing					
D1	Supplying and installing of precasted manhole including excavation pipe connection, epoxytar coating, 25-ton cast iron cover and backfill, size 1200mm, depth up to 1.5m.	NR	35			
02	Supplying and installing of precasted manhole including excavation pape connection, epoxytar coating, 25-ton cast iron cover and backfill, size 1200mm, depth up to 2.5m.	NR	45			
	Sub-Total					
E	Concrete Surround					
EL	Supplying and cast iron (B200) surround for sewer.	M ³	221			
	Sub-Total					-

EXCAVATION	UNI T	QT Y	UNIT PRICE	TOTAL PRICE
Air And Water Leakage Test				
Air leakage test for sewer pipe lines 8,10,12,and 14inch according to specifications, including for all temporary works.	LM	2445		
Water leakage tests for manholes, depth up to 1.5 meter according to specifications.	NR	35		
Water leakage test for manholes, depth up to 2.5 meter according to specification	NR	45		
Sub-Tet	al			
Rode reinstatment				

Beauting and dispose of the asphalt and re-Asphalting after BACKFILL, road structure layers expected basecoarse 125+125 mm, MCO layer 11/m2, asphalt layer 55mm(3.47).	LM	2445	
Sub-Tota	il		
Survey work			
and as built DWGS using	LM	2445	
Sub-Total			

3. For the Proposed Septic tank:

No		UNI	QTY		ICE		ICE
		T		S	C	5	C
A	Septic Tank						-
A1	Volume of septic tank	M ³	555.4				-

4. For the Proposed Solid Waste management:

No		UNI	QTY		NIT ICE		TAL ICE
		T	~	S	C	S	C
	Container						-
11	Type 240 L	NR	125				-
10	Type 1100 L	NR	164				-
13	Type 4 m ³	NR	23				

Chapter Seven

"Conclusions and Recommendations"

CONCLUSIONS

in this project, the trial is done make an environmental assessment for Al-Dahriya Old City in addition to make a design for wastewater and storm water collection systems for the coming 25 years. The main conclusions drown from the present study are summarized below:

- The environmental condition in Al-Dahriya Old City is assessed in bad condition, as absence of sanitary systems, and an absence of solid waste management.
- 2 Al-Dahriya Old City like other city in Palestine has no sewage facilities. The people are using latrines, and cesspits. The wastewater has been seeping into the people through the over flow of the deteriorated cesspits and latrines, causing series are proposed and health problems.
- The proposed wastewater and storm water systems covered all of the areas of Al-Debriya Old City and the two systems are done by gravity.
- The septic tank for whole area is with volume equal 555.4 m³ and it design in order save environment.
- Making a solid waste management to avoid random landfilling, and design small at the old damping site in order to save environment, heritage and vegetation

RECOMMENDATIONS

- This study was done for Al-Dahriya Old City and we recommend to make a complete study for all old cities in Palestine.
- A cooperation with architectural and civil engineers is in high need and very use fall to make a good assessment.

APPENDIX

(A)

- WASTE WATER QUANTITY TABLES
- STORM WATER QUANTITY TABLE

First: Waste water quantity calculation

Example on calculation of waste water quantity for manhole number 1 to manhole number 2:

- Unit scwage = waste water * Pop density
- Waste water = 0.8* water consumption

- * Waste water = $0.08 \frac{m^3}{c.day}$
- Pop density = $\frac{population}{Area}$
- Population growth= 3, 5 %

$$P_f = P_p \left(1 + \frac{r}{100} \right)^n$$

Pop 2040 = 1772
$$\left(1 + \frac{3.5}{100}\right)^{25}$$

- Area of Old City = 44.82 dounum.
- Pop Present density = No of floor*Na of House*arg individual

 Total Area

 22719-6

Pop density =
$$\frac{2*718*6}{44.82}$$

· Pop Future density

$$D_f = D_p \left(1 + \frac{r}{100}\right)^n$$

Pop Future density -

$$D_f = 192.24 \left(1 + \frac{3.5}{100}\right)^{25}$$

$$Df = 454.31 \, Cap / dounm$$

- remental area is the expected area for each manhole.
- area is the sum of all previous manholes area.
 - Q Average = Unit sewage * Total Area

- Q Average = 2.18m³/day
- Peak factor = $1.5 + \frac{2.5}{\sqrt{Qavg}}$

Peak factor =
$$1.5 + \frac{2.5}{\sqrt{2.18}}$$

- factor should be less than 3
- Q= Peak factor * Qavg

$$=6.54 \text{ m}^3/day$$

$$0.22 m^3/day$$

$$=0.22 + 2.18$$

The erage =
$$2.4 m^3/day$$

$$=0.22+6.54$$

$$= 6.76 \, m^3/day$$

Second: Storm water quantity calculation;

Example on calculation of storm water quantity for manhole number 1 to manhole number 2:

- Pipe length =103.67 m.
- Tributary area = 0.64 m².
- Runoff coefficient = 0.65.
- C.A= 0.416 ha.
- ∑C.A= 0.416 ha.
- Concentration time (Tc) = ti +tf
- ti = 10 min.
- If = $\frac{\text{Distance}}{\text{Velocity}}$.

$$tf = \frac{103.67}{1*60} = 1.728 \text{ min.}$$

- Te = 10+1.73-11.728 min.
- Rain Fall intensity = $71.62 \frac{mm}{hr}$.

Rain Fall intensity $= 199.117 \frac{l}{s.h}$.

Qmax =C.I.A

$$Qmax = 0.416 * 199.117 *$$
$$= 82.83 \frac{l}{s}$$

Name	N	Bower	Chrown felt bes fatte Pas	CANTO PAID	5	onti newage			Average	Peak Pactor	Sandanian S			-	St max
4 5 6 7 8 9 10 2 30.26 36.34 0.06 0.06 2.18 3.00 3 49.36 36.34 0.06 0.06 1.65 2.18 3.00 4 24.25 36.34 0.17 0.62 22.55 2.03 5 25.10 36.34 0.17 0.62 22.55 2.03 6 40.39 36.34 0.54 1.47 53.44 1.84 7 49.26 36.34 1.04 2.51 91.24 1.84 8 48.86 36.34 1.04 2.51 91.24 1.75 9 50.22 36.34 1.09 4.52 164.45 1.75 10 49.43 36.34 1.54 7.96 289.25 1.64 11 49.43 36.34 1.72 11.95 434.41 1.64 12 50.49 36.34 1.72 11.87 540	euiJ	Name			E	mand, d. dounm	dounm	фипор	wayday		m ³ dav	m ³ /day	m) stav	1	
2 30.26 36.34 0.06 0.06 2.18 3.00 3 49.36 36.34 0.40 0.46 16.55 2.15 5 25.10 36.34 0.17 0.62 22.55 2.03 5 25.10 36.34 0.54 1.47 53.44 1.84 7 49.26 36.34 0.54 1.47 53.44 1.84 7 49.43 36.34 1.09 4.52 16.45 1.65 11 49.12 36.34 1.64 2.51 91.24 1.72 12 50.49 36.34 1.54 2.33.21 1.65 14 49.36 36.34 1.72 10.23 371.90 1.63 15 42.90 36.34 1.72 10.23 371.90 1.63 16 34.30 36.34 1.20 14.87 540.42 1.61 17 41.64 36.34 1.37 16.24 590.07 1.60 18 36.34 1.37 16.24 590.07 1.60 200 mm	-	2	3	4	5	9	7	80	8	10		97		Mr. /day	m7day
3 49.36 36.34 0.40 0.46 16.55 2.11 4 24.25 36.34 0.17 0.62 22.55 2.03 5 25.10 36.34 0.17 0.62 22.55 2.03 6 40.39 36.34 0.54 1.47 53.44 1.84 7 49.26 36.34 1.04 2.51 91.24 1.75 9 50.22 36.34 1.09 4.52 16.45 1.89 10 49.43 36.34 1.54 2.33.21 1.65 11 49.12 36.34 1.54 2.33.21 1.65 12 50.49 36.34 1.54 7.86 288.25 1.65 14 49.36 36.34 1.72 11.95 434.41 1.62 15 42.90 36.34 1.20 14.87 540.42 1.61 16 34.30 36.34 1.37 16.24 590.07 1.60 10 data 3.5 m3/d d which 80% return to sewer 10 % of the average industrial wantewater flow 200 mm	-	main 1	-	2	30.26	36.34	0.08	A GR	2 12	200		12	13	14	15
4 24.25 36.34 0.17 0.62 22.55 2.03 5.25 2.503 5.24 1.84 0.31 0.93 33.82 1.93 6.34 0.31 0.93 33.82 1.93 6.34 0.54 1.47 63.44 1.84 1.84 0.54 1.47 63.44 1.84 1.75 0.62 36.34 1.09 4.52 164.45 1.75 0.62 36.34 1.09 4.52 164.45 1.69 1.72 0.49 36.34 1.54 7.86 288.25 1.65 1.65 1.83 6.24 1.89 6.42 233.21 1.65 1.65 1.83 6.34 1.72 11.95 434.41 1.62 1.64 1.72 11.95 434.41 1.62 1.61 1.72 11.95 434.41 1.62 1.61 1.72 11.95 434.41 1.62 1.61 1.72 11.95 434.41 1.62 1.61 1.72 11.95 434.41 1.62 1.61 1.72 11.95 434.41 1.62 1.61 1.72 11.95 434.41 1.62 1.61 1.72 11.95 434.41 1.62 1.61 1.72 11.95 1.96.92 1.61 1.61 1.72 11.95 1.96.92 1.61 1.61 1.72 11.95 1.96.92 1.61 1.61 1.90 1.90 1.90 1.90 1.90 1.90 1.90 1.9	2	main 1			49.36	36,34	0.40	0.48	18 88	2 44	6.54	0.22	2.40	6.76	6.76
5 25.10 36.34 0.31 0.93 33.82 1.93 6.40.39 36.34 0.54 1.47 53.44 1.84 7 49.26 36.34 0.54 1.47 53.44 1.84 1.84 8.86 36.34 0.92 3.43 124.79 1.72 1.69 1.65 1.69 1.72 1.86 1.89 6.42 233.21 1.65 1.69 1.72 1.89 6.42 233.21 1.65 1.69 1.89 6.42 233.21 1.65 1.69 1.89 6.42 233.21 1.65 1.69 1.89 6.42 233.21 1.65 1.69 1.89 6.42 233.21 1.65 1.65 1.89 1.89 6.42 233.21 1.65 1.65 1.89 1.89 1.89 1.89 1.89 1.89 1.89 1.89	co	main 1			24.25	36.34	0.17	0.62	22.55	2.03	35.00	1.66	18.21	175.00	168.24
6 40.39 36.34 0.54 1.47 53.44 1.84 7 49.26 36.34 1.04 2.51 91.24 1.76 8 48.86 36.34 1.04 2.51 91.24 1.75 9 50.22 36.34 1.09 4.52 164.45 1.69 10 49.43 36.34 1.89 6.42 233.21 1.65 12 50.49 36.34 1.54 7.96 289.25 1.65 13 46.21 36.34 1.72 11.95 434.41 1.62 14 49.36 36.34 1.72 11.95 434.41 1.62 17 41.64 36.34 1.37 16.24 590.07 1.60 10 % of the average industrial vantawater flow. 200 mm	4	main 1			25.10	36.34	0.31	0.93	33.82	1 93	43.10	27.70	24.81	186.29	18.06
7 49.26 36.34 1.04 2.51 91.24 1.76 8 48.86 36.34 1.04 2.51 91.24 1.76 9 50.22 36.34 1.09 4.52 164.45 1.89 10 49.43 36.34 1.89 6.42 233.21 1.65 11 49.12 36.34 1.54 7.96 289.25 1.65 12 50.49 36.34 1.54 7.96 289.25 1.65 13 46.21 36.34 1.72 11.95 434.41 1.62 14 49.36 36.34 1.72 11.95 434.41 1.62 17 41.64 36.34 1.37 16.24 590.07 1.60 10 % of the average industrial vantewater flow. 200 mm	ın	main 1			40.39	36.34	0.54	1 47	62.44	1 84	17.00	3.38	37.20	344.85	326.89
8 48.86 36.34 0.92 3.43 124.79 1.72 9 50.22 36.34 1.09 4.52 164.45 1.69 10 49.43 36.34 1.54 7.96 288.25 1.65 12 50.49 36.34 1.54 7.96 288.25 1.65 13 46.21 36.34 1.72 10.23 377.90 1.63 14 49.36 36.34 1.72 11.95 434.41 1.62 15 42.90 36.34 1.72 13.67 496.92 1.61 17 41.64 36.34 1.37 16.24 590.07 1.60 10 % of the average industrial vantewater flow. 200 mm	9	main 1			49.26	36.34	1.04	2 54	D4 24	176	98.44	5.34	58.79	380.09	53,19
9 50.22 36.34 1.09 4.52 164.45 1.69 10 49.43 36.34 1.89 6.42 233.21 1.65 12 50.49 36.34 1.54 7.96 288.25 1.65 13 46.21 36.34 1.46 9.42 342.24 1.64 13 46.21 36.34 1.72 11.95 434.41 1.62 15 42.90 36.34 1.72 11.95 434.41 1.62 17 41.64 36.34 1.20 14.87 540.42 1.61 17 41.64 36.34 1.37 16.24 590.07 1.60 10 % of the average industrial vantewater flow. 200 mm	7	main 1			48.86	36.34	0.92	3.43	124 79	172	760.74	21.5	100.37	446.17	392.97
10 49.43 36.34 1.89 6.42 233.21 1.65 12 50.49 36.34 1.54 7.96 288.25 1.65 1.65 1.40 36.34 1.72 10.23 371.90 1.63 1.40 34.30 36.34 1.72 11.95 434.41 1.62 1.63 1.72 11.95 434.41 1.62 1.63 1.72 11.95 434.41 1.62 1.63 1.72 11.95 434.41 1.65 1.60 1.72 11.95 434.41 1.65 1.60 1.72 1.72 1.72 1.72 1.72 1.60 1.61 1.60 1.72 1.72 1.60 1.61 1.60 1.72 1.60 1.61 1.60 1.61 1.60 1.61 1.60 1.61 1.61	8	main 1			50.22	36.34	1 00	4 52	184.45	1 80	215.12	12.48	137.27	617.79	224.82
11 49.12 36.34 1.54 7.96 288.25 1.65 1.2 50.49 36.34 1.46 9.42 342.24 1.64 1.46 9.42 342.24 1.64 1.46 9.42 342.24 1.64 1.46 9.42 342.24 1.64 1.46 34.30 36.34 1.72 11.95 434.41 1.62 1.6 1.4 1.2 1.2 1.2 1.3 1.6 1.6 1.6 1.2 1.2 1.2 1.3 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	6	main 1	Ų	Т	49.43	36.34	1.89	679	233.24	1 86	2/8//3	16,44	180.89	685.36	460.55
12 50.49 36.34 1.46 9.42 342.24 1.64 13 46.21 36.34 0.82 10.23 371.90 1.63 14 49.36 36.34 1.72 11.95 434.41 1.62 16 34.30 36.34 1.72 13.67 496.92 1.61 17 41.64 36.34 1.37 16.24 590.07 1.60 10 % of the average industrial wantewater flow. 200 mm	10	main 1	10		49.12	36.34	1 54	7 06	30 000	18.5	387.99	23.32	256.53	801.50	340,96
13 46.21 36.34 0.82 10.23 377.90 1.63 14 49.36 36.34 1.72 11.95 434.41 1.62 15 34.30 36.34 1.20 14.87 540.42 1.61 17 41.64 36.34 1.37 16.24 590.07 1.60 and data 10 % of the average industrial wantewater flow. 200 mm	11	main 1	11		50.49	36 34	1 48	0 40	AC CAC	20.	476.39	28.93	318,18	895,51	554.55
14 49.36 36.34 1.72 11.95 434.41 1.62 16 34.30 36.34 1.72 13.67 496.92 1.61 17 41.64 36.34 1.37 16.24 590.07 1.60 11 data 3.5 m3/d.d which 80% return to sewer 10 % of the average industrial wantewater flow.	12	main 1	12		46.21	36.34	0.80	40.22	274 00	40.4	559.61	34.22	376.46	984.02	429.47
15 42.90 36.34 1.72 13.67 496.92 1.61 16 34.30 36.34 1.20 14.87 540.42 1.61 17 41.64 36.34 1.37 16.24 590.07 1.60 1nd data 3.5 m3/d.d which 80% return to sewer 10 % of the average industrial wantewater flow. 200 mm	13	main 1	13		49.36	36.34	472	44 05	424 44	4 43	90.909	37.19	409.09	1033.44	603.97
16 34.30 36.34 1.20 14.87 540.42 1.61 and data 3.5 m3/d.d which 80% return to sewer 10 % of the average industrial wantewater flow.	14	main 1	14		42.90	36.34	479	42.67	400 00	4 64	(03.72	43.44		1361.36	757.39
17 41.64 36.34 1.37 16.24 590.07 1.60 3.5 m3/d.d which 80% return to sewer 10 % of the average industrial wantewater flow.	15	main 1	15		34.30	36 34	4 20	44.07	E40.34	0.0	801.11	49.68	_	1465.00	707.61
3.5 m3/d.d which 80% return to sewer 10 % of the average industrial wantewater flow.	16	main 1	16	t	11 64	20.34	4 44	19.07	340.44	1.0.1	868.75	54.04	584.47	1537.00	829.39
3.5 m3/d/d which 80% return to sewer 10 % of the average industrial wantewater flow.	Desig	in Assan	nptions a	and data		30.34	1.31	10.24	290.07	1.60	945.83	59.01	649.08	1619.04	789.65
10 % of the average industrial wantewater flow. 200 mm	Vator	commsur	mption is		10.	n3/d.d which		1	turn to sev) Minimum slope Smin=	20	ò ³		
0,0 m/86c	offiltes Tinim Tinim	ation is equal to the control of the	qual diameter= ity Vmin =			6 of the average mm	pe indont	rial wante		w G = 3	8) Maximum slope Smax = 9) Maximum manhole spacing = 10) Minimum depth of sewer	60 45	S R E E		
	Aaxin	num veloc	ity Vmax		3	n/sec					2) Malning coefficient	0.00			

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	June.	THIN!		STATE OF THE PERSON	STATE STREET, SQUARE	Tutal		No. of Street, or other Persons and Street, o		Infiltration	Total	Total	O max
Sewer	MINNO	MH NO	7	obuwas juo			Average	Peak Factor	Maximum		Average	Maximum	
Name			ā	m/d.dounm	downm	dounm	m ³ /day		m³/day	wabi ^e m	m³/day	m ³ /day	m*/day
2	3	4	5	9	7	8	6	10	11	12	13	1.4	45
main2	-	2	12.34	36.34	0.10	0.10	3.63	2.81	10.22	0.38	400	40 52	40.00
main2	2	3	5.40	36.34	0.03	0.13	4.68	2.66	12.44	0.47	£ 1E	42.04	10.36
main2	3	4	9.65	36.34	0.05	0.18	6.50	2.48	18.13	0.65	7.45	16.70	2.53
main2	4	9	24.49	36.34	0.13	0.31	11.15	2.25	25.08	1.12	12.27	26.20	14.45
main2	2	9	26.05	36.34	0.16	0.46	16.90	2.11	35.62	1.69	18 50	37.34	35.67
main2	9	7	35.69	36.34	0.17	0.64	23.11	2.02	46.69	2.31	25.49	40 00	25.43
main2	1	00	45.07	36.34	0.11	0.75	27.17	1.98	53.79	272	20.80	20.57	25.43
main2	8	6	22.27	36,34	0.03	0.77	28.12	1.97	55,44	2.81	30.03	56 95	33.08
main2	6	10	25.40	36.34	80.0	0.85	30.85	1.95	60.15	3.08	22.02	E2 24	11.63
main2	10	=	28.03	36.34	0.19	1.04	37.86	1.91	72.17	3.70	ALGE	75.00	38.06
main2	11	12	43.11	36,34	0.23	1.27	46.11	1.87	86.14	4.61	60.73	00.00	20.00
main2	12	13	14.65	36.34	60.0	1.36	49.44	1.86	91.74	4 94	54.30	06.60	22,35
main2	13	14	19.97	36,34	0.14	1.50	54.80	1.84	100.37	5.46	60.06	405 82	45.05
main2	14	15	13.62	36.34	0.08	1.58	57.57	1.83	105.32	5.76	63 33	111 08	40.00
main2	15	16	47.89	36.34	0.17	1.76	63.85	1.81	115.75	6.38	70.23	122.13	73.05
main2	16	17	21.49	36,34	60'0	1,85	67.07	1.81	121.07	6.71	73.77	127.78	EA 77
main2	17	18	26,69	36.34	0.10	1,95	70.74	1.80	127,14	7.07	77.81	134.24	70.40
main2	18	19	41.35	36,34	90.0	2.01	72.88	1.79	130.67	7.20	80.17	437.06	60 49
Assan	phions	Design Assamptions and data								1	200.16	101.30	28.47
musum	1) Water comnsumption is		3.5	m3/d.d which		25.00	return to sewer	war	7) Minimum slope Smin =	0.5	*		
No. of the last	100			The Contract of Contract of	SOUTH STATE OF STATE	SWINDS. AND	The Control of		8) Maximum slope Smax =	15	%		
3) Infiltration is equal	lan			7s of the average industrial wastewater flow	the fretund	rial was	ewater flor	1,4	9) Maximum manhole spacing =	9	Ε		
velocity	5) Minimum velocity Votin =		0.6	cultan					10) Minimum depth of sewer	1.5	E		
1000				TO BOOK					11) Design deptin of flow hids	0.5			
veloc	6) Maximum velocity Vmax =	#	2	rr/sec					12) Maining coefficient n=	0.01			

						-					CONTRACTOR STATES	and the second second		-
		New No.	No No	-	Sewage .	THE SHALL BELLEVIA	1000	Average	Average Peak Factor	Maximum		Average	Maximum	
i di	Name	MIL PRO		E	ma,da.dounm	dounm	dounm	m³/day		m³/day	m3/day	Wab/m	m³/day	m³/day
	2			7	4	-	a	σ	10	11	12	13	14	12
	2	3	4	0	0	Г	2 4 4	000	284	13.27	0.51	5.60	13.78	13.78
n	main3	Y	2	8.92	36.34		0.14	40.00	0 40	20 43	1.35	14.84	30.77	16.99
0	main3	2	3	18.28	36.34		0.37	13.43	2.10	A7 67	2 27	26.04	50 04	33.04
2 00	main3	3	P	23.57	36.34	0.28	0.65	23.67	2.01	10.14	700	36.20	67.04	24 97
	main3	4	10	21.9	36.34	0.26	0.91	33.08	1.93	64.01	0.01	20.00	CA 80	64.45
	main3	5	9	33.18	36.34		1.39	50.42		93.38	0,04	74 53	234 42	186 97
	rnain3	5	9	48.95	36.34		1.86	67.76		1277	7.35	80.85	241 18	74 19
	main3	7	8	47.67	36.34	, 1	2.02	73.50		131,00	10.77	118 43	300 33	226.14
	main3	8	6	49.91	36.34		2.96	107.66		100,00	12.29	135 22	326.53	100.39
100	main3	6	10	47.55	36.34	0.42	3.38	122.93		254.66	14.75	162 28	368.55	268.15
	main3	10	11	49.82	36.34	0.68	4.06	147.53		200 84	17.18	189.03	409.85	141.70
П	main3	11	12	47.82	36.34	0.67	4.73	171.85		200.36	19 18	100	443.69	301.99
Г	main3	12	13	43.68	36.34	0.55	5.28	191.83		302 84	23.67	100	825.02	523.03
	main3	13	14	50.34	36.34	1.24	6.51	236.72		A02.60	30.02	1 1000	931.52	408.49
	main3		15	55.88	36.34	1.75	8.26	8.26 300.25		EB 7.0	35.83			
	main3	15	16	50.44	36,34	1.60	986	358.25		000000	40.54			486.99
	main3	-16	17	50.03	36,34	1.30	11.16	405.43		206.00	48 72		1242 50	_
1.	main3	17	18	50.21	36,34	2.25	13.41	487.20	1.61	105.30	1			
esign	Assar	Design Assamptions and data	and da	ntan										
		and land		2	m3/d, d which	-	%08	return to sewer	O SOWER	7) Minimum slope Smin =	0.5	* >		
Vater	comnst	1) Water commsumption is	9	44/40	The same of the sa					8) Maximum slope Smax =	2	2		
-	-	- Inches		40	% of the average industrial wastewater flow	rings Indus	strial wa	atowater	r flow.	9) Maximum manhole spacing =	09	E		
Ainim	Minimum pipe dian	Innitration is equal Minimum pipe diameter=	E	200	mm					10) Minimum depth of Sewer	0.5			
Minim	olav mu	5) Minimum velocity Vmin =	11 22	9.0	rrysec					12) Maining coefficient n=	0.01			

0.02 0.02 0.73	NAME.	1,74,400	m m/m/mmm			
0.73	7 8	1	2 9	2 9	2 9	2 9
7		0.02	0.02	36.34 0.02	20.26 36.34 0.02	20.26 36.34 0.02
1 00 +	T	0.03	36.34 0.03	36.34 0.03	13.4 36.34 0.03	3 13.4 36.34 0.03
70.1	0.09	60.0	36.34 0.09	36.34 0.09	24.25 36.34 0.09	24.25 36.34 0.09
	0.05	0.05	36.34 0.05	11.39 36.34 0.05	5 11.39 36.34 0.05	4 5 11.39 36.34 0.05
27 0.10	80.0	80.0	36.34 0.08	20.55 36.34 0.08	20.55 36.34 0.08	6 20.55 36.34 0.08
43 15 40		0.16	36.34 0.16	26.06 36.34 0.16	26.06 36.34 0.16	6 7 26.06 36.34 0.16
53 19 4-	0.11	0.11	36.34 0.11	14.78 36.34 0.11	8 14.78 36.34 0.11	7 8 14.78 36.34 0.11
74 26 7		0.20	30.34 0.20	25.03 30.34 0.20	9 25.03 30.34 0.20	8 9 25.03 30.34 0.20
79 28 62	0.05	0.05	30.34 0.05	18.75 30.34 0.05	10 18.75 30.34 0.05	9 10 18.75 30.34 0.05
03 27 2	0.24	0.24	50.34 0.24	39.25 30.34 0.24	11 39.25 30.34 0.24	10 11 39.25 36.34 0.24
2K AR 2		0.22	36.34 0.22	24.77 36.34 0.22	12 24.77 36.34 0.22	12 24.77 36.34 0.22
50 50 50	0.35	0.35	36.34 0.35	48.51 36.34 0.35	13 48.51 36.34 0.35	12 13 48.51 36.34 0.35
74 65 VY	1/32	35.34 0.14	35.34 0.14	37.4 35.34 0.14	37.4 35.34 0.14	14 37.4 35.34 0.14
00 00.23	0.16	36.34 0.16	36.34 0.16	49.53 36.34 0.16	15 49.53 36.34 0.16	15 49.53 36.34 0.16
00 70	1 -	36.34 0.09	36.34 0.09	39.34 36.34 0.09	39.34 36.34 0.09	16 39.34 36.34 0.09
00 16.38	0.02	36.34 0.02	0.81 36.34 0.02	0.81 36.34 0.02	0.81 36.34 0.02	0.81 36.34 0.02
	1	0.00				Design Assamptions and data
		m3/d.d which		3.5 m3/d.d whiteh	3.5 m3/d.d whiteh	m3/d.d which
al wastewater flow.	Verage Industrial w	% of the average industrial wired mysec	10 % of the average industrial wi 200 mm 0.6 m/sec 3 m/sec	= 200 mm average industries = 0.6 m/sec x = 3 m/sec	= 200 mm verage industry = 0.6 m/sec x x = 3 m/sec	= 200 mm average industries = 0.6 m/sec x = 3 m/sec

Name Min No	N WIN NO	No No	unitsewage			Average P	Average Peak Factor	Maximum	Infiltration	Total	
Malling		E	munop.p/, m	dounm	munop	m³/day		HIPTONIA .		Average Maximum	
2 3	4	r.	9	7	a		1	m²/day	th ³ /day	m Jetan	1
sub 2 1	2	37.47	36.34	0.19	0 40	000	10	7			m rday
sub2 2	3	12.17			2 5	0.91	2.45	16.93	12	13	14
sub 2 3	4				-	9.09	2.33	21.16	0.69	7.60	17.62
sub 2 8	6			0.03		10.18	2.28	23.24	0.91	9.99	22.07
sub 2 8	10		L	270	0.41	14.80	2.15	32.00	1.02	- 10	10200
sub 2 10	11			0.04		27.26	1.98	53.94		16,39 33,49	1553
sub 2 11	12			0.27	1 20	33.80	1.93	65.23		29.98 56.67	6
sub 2 12	13			0.34		43.61	1.88	81.93		37.18 68.61	601
sub 2 13	14	35.40		0.00	80 -	39.66	1.83	102.48			0
Design Assamptions and data	s and o	lata		2000	9	29.16	1.83	107.98	6.59		얼마
1) Water commsumption is	स	3.5	m3/d.d which		80% re	refurn to sewer				65.08 113.89	63
3) Infiltration is equal 4) Minimum pipe diameter= 5) Minimum velocity Vmin = 6) Maximum velocity Vmax =	n = u	10 200 0.6 3	% of the average industrial wastewater flow min m/sec m/sec	ge industri	al waste	water flox		9) Maximum stope Smin = 8) Maximum stope Smax = 9) Maximum manhole spacing = 10) Minimum depth of sewer 11) Design depth of flow h/d<	0.5 60 1.5	**EE	

0.01

					The same of the same				FIOW Hattis				
HYBRIT.	Oppus	P. Owner		11111	Internation and	Total				Infiltration	Total	Total	Total O may
Sewer	Min No	MIN No	FT	sewage			Average I	Average Peak Factor	Maximum		105	2	A III III
Name			8	m"/d.dounm	dounm	doumm	doumm m³/day		m²/day	m³/day	m³/day		m"/day
2	3	4	S.	9	7	8	6	10	11	42	5	4.4	-
sub 3		2	42.25	36.34	0.32	0.32	11.63	2.23	25.97	118	12.70	27 43	10
sub 3	2	3	27.61	36.34	0.31	0.63	22.90	2.02	46.31	9.30	25.10	40.60	21.73
sub 3	3	4	16.02	36.34	0.03	99.0	24.00	2.01	48.24	2.40	38.40	40.00 F0.64	27.46
sub 3	4	5	34.82	36.34	0.22	0.88	32.02	1.94	62.17	3.20	25.22	86.30	20.78
sub 3	5	9	25.63	36.34	0.26	114	41.29	1.89	77.99	4 12	45 A3	00.00	30.20
sub 3	9	7	35.2	36.34	0.53	1.67	60.55	1.82	110.28	6.05	86.60	446 99	40.83
sub 3	7	8	39.5	36.34	20.0	1.74	63.09	1.81	114.50	6.31	80.40	420.03	70.47
sub 3	8	6	24.82	36.34	0.04	1.78	64.55	1.81	116.91	E AR	74 00	400.001	20.40
sub 3	6	10	39.21	36.34	1.60	3.38	122.70	1.73	21174	49.97	434 07		12.90
SSal	Design Assamptions and data	and da	ıta							14.41	134.81	224.01	151.05
nusn	1) Water comnsumption is	¥	3.5	m3/d.d which	1	%08	return to sewer	Sewer	7) Minimum slape Smin =	0.5	8		
SECTION S	No.		The state of	The state of the s		1000			8) Maximum slope Smax =	15	%		
3) Infiltration is equal	dnal			% of the average industrial	age indus	trial was	wastewater flow	low.	9) Maximum manhole spacing =	3	E		
pipe	4) Minimum pipe diameter		002	mm					10) Minimum depth of sewer	1.5	E		
Acid.	cut vimin		0.0	mand					11) Design depth of flow h/d<	0.5			
velo	6) Maximum velocity Vmax =	3 3	3	miling					12) Maining coefficient n=	0.04			

Infiltration Total	A	m ³ /day m ³ /day m ³ /day	13	4.40	9.43	24.30	2.97 32.01 54.09		48.98	4.78 52.56 05.90				60 m		1.5
Infi		E		0	0	2	2	8	*	4	50					30
	Macimum	m ³ /day	11	11,00	20.19	44,88	57.14	74.07	83,44	88.95	96,87		7) Minimum slope Smin =	9) Maximum manhole spacing =	10) Minimum depth of sewer	TT) Design depth of flow hide
	Poul Factor		10	2.75	2.35	2.03	1.96	1.90	1.87	1.86	1.85		ewer			
	Average	m³/day	6	4.00	8.58	22.09	29.10	38.98	44.51	47.78	52.51		80% return to sewer	ter flow.		
Tutat		dottom	8	0.11	0.24	0.61	0.80	1.07	1,22	1.31	1.44		80% n	wastewa		
		nunop	7	0.11	0.13	0.37	0.19	0.27	0.15	60.0	0.13			ge industria		
	odewes im	m³/d,dounm dounm	9	36.34	36.34	36.34	36.34	36.34	36.34	36.34	36.34		3.5 m3/d.d which	% of the average industrial wastewater flow.	mm	m/sec
H	an,	u.	2	39.28	12.52	47.2	17.42	37.8	13.54	13.56	20.82	63	3.5	10		0.0
	All No		4	2	m	4	5	9	7	8	6	and da			2	8
			63	1	2	3	4	5	9	7	8	nptions	mption is	qual	diameter	ony Vrnin
	Burrent	Namo	2	sub 4	sub 4	sub 4	sub 4	sub 4	sub 4	sub 4	sub 4	Design Assamptions and data	1) Water commsumption is	3) Infiltration is equal	4) Minimum pipe diameter=	5) Minimum velocity Vrnin =
	34	PUIT	+	-	2	es	4	2	9	7	8	Desig) Water) Infiltra	Minim (Minim (

												The state of the s	
			-	STATE SANGEROOM	THE REAL PROPERTY.	-	Average	Poak Factor	Maximum		Average	Average Maximum	
E I	Special Ann Miles	1991.740		_	dounm	фини	rm3/day		m ² /day	m ² /day	m3/day	m ³ /day	m ³ /day
ž	Name			m.va.domin		-		-	**	12	13	14	15
	3	4	2	9	7	00	6	01	N. Cr	2.14	23.59	45.89	45.89
10	enh 5	2	49.99	36.34	0.59	0.59	21.44	2.04	40.04	67 6	27.35	52.24	6.35
1 6	sub 5 2	9	9.25	36.34	60.0	99.0	24.86	2.00	40.10	5.78	63.57	111.46	105.11
	sub 5 3	4	49.48	36.34	0.68	1.59	57.79	1.83	447.47	8.29	91.23	155.47	50.36
120	sub 5 4	ın	40.94	36.34	69.0	2.28	82.94	1.77	14/11	9.41	103.54	174.86	124.51
	sub 5 5	9	34.00	36.34	0.31	2.59	94.13		404 40	11.01	121.13	202.43	77.92
	sub 5 6	-	21.41	36.34	0.44	3.03	110.12	1.74	20,101	13.05	143.52	237.32	159.39
	Sub 5 7	80	28.12	36.34	0.07	3.59	130.47		930.70	13.45	147.92	244.15	84.75
	Sub 5	6	36.24	36.34	0.11	3.70	134.47		202.00	16.68	183.50	299.20	214.45
T	Sub 5	10	33.69	36.34	80.0	4.59	166.82		20.202	17.06	187.70	305.67	91.23
	sub 5 10	11	44.52	36.34	0.11	4.70	170,64	1.69	1000				
esign /	Design Assamptions and data	s and da	to								18.0%		
Vater co	1) Water commsumption is	16	3.5	m3/d.d which		80%	80% return to sewer	o sewer	7) Minimum slope Smin = 8) Maximum slope Smax =	15.5	* * 1		
Minimun	Infiltration is equal Minimum pipe diameter= Minimum velocity Vmin = Minimum velocity Vmin =	1 1 1 1 1	200 200 2	% of the average industrial wastewater flow. mm m/sec	rage Indus	trial was	tewater fi	low.	9) Maximum manhole spacing = 10) Minimum depth of sewer 11) Design depth of flow h/d 12) Maining coefficient n=	0.01	E		

					90	98	6	000	74	-	75	55
		ID	(1/8)	18	350,906	315.308	155,119	672.530	360.074	84.331	851.061	317.655
		Ö	(1/s)	17	350,906	666.214	821.333	1493.863	1853.937	1938.268	2789.329	3106.984
		(1)	(l/s.ha)	16	199.117	197.591	195.946	192.123	189.336	188.501	186.551	184.314
		ĐΪ	(min)	16	11.728	12.686	13.726	16.180	17.999	18,549	19.844	21.346
		COMULATIVE SUM(AC)	(ha)	**	0.416	0.936	1.736	4.160	6.123	6.598	9.029	10.862
The second second		C.A STREET	(ha)	111	0.416	0.520	0.800	2.425	1.963	0.475	2.431	1.833
		FACTOR and industry	as C	6	0.65	0.65	0.65	0.65	0.65	99.0	0.65	0.65
Mail	1	Street and Industry	(ha)	1	0.64	0.80	1.23	3.73	3.02	0.73	3.74	2.82
	3/	геметн СОМULATIV	(m)	9	103.67	161.14	223.58	370.79	479.94	512.95	590.63	680.73
		ГЕИВІН	(m)	10	103.67	57.47	62.45	147.21	109.14	33.01	77.68	90.10
		WER MH.	го	4	2	3	4	2	9	7	00	6
	LOCATION	NO.	dП	173	-	2	23	4	2	9	7	00
		BMAN BNI.	1	2	main 1	main 1	main 1	main 1	main 1	main 1	main 1	main 1
		илмвек		-	-	2	63	4	22	9	7	89

	10		(8/1)	18	15.711	11.735	15,556	34.649	22,450	11.042	23.752	29.460	29.047	1.884
	D		(8/1)	44	15.711	05 000 CV	700.00	17.651	100.101	424 000	34.895	104.355	193.402	195.286
	(1)		(I/s.ha)	304 404	201.068	200.475	100 104	107 427	106 540	195 784	194 502	+	193.209	
	əī		(min)	10.296	10.514	10.882	11.736	12.783	13.350	13.830	14.647	15.478	16.673	17.832
1	(AA)MU	191		0.078	0.137	0.215	0.390	0.507	0.566	0.689	0.845	1.001	1.021	1.125
	A.: TEERTE	(ha)	111	0.078	0.059	0.078	0.176	0.117	0.059	0.124	0.156	0.156	0.020	0.104
	Street and industry FACTOR set and and return	(ha) C	6		0.09 0.65	+	+	+	+	1	-	+	+	0.00
THE STATE OF THE S	COMULATIVE OF AREA of	(m)	+		52.90	1	-	1						-
	LENGTH	(m)	47 74	13.10	22.07	51.26	62.79	34.05	28.76	49.05	49.88	7171	69.49	
	OWER MH,	ר	0	6	4	2	9	7	20	6	10	11	12	
NO INCOME	IPPER MH.	0 00	-	2	3	4	2	9	7	8	6	10	11	
	LINE NAME	2	main 2	main 2	main 2	main 2	main 2	main 2	main 2	main 2	main 2	main 2	main 2	
	MUMBER				+	+	1	1	-	1	-	-		

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		ÖI	(I/s)	18	57.480	28.545	52.870	42.242	36.008	162.895	91.108	37.110	36.829	400 224	189.224	398.957	383.996	
		ď	(8/1)	-41	57.480	86.025	138.896	181.138	217.146	380.040	471.149	508.259	5.45.08R	0000000	734.312	1133.269	1517.265	
Ī		(1)	(l/s.ha)	416	200.980	200.525	199,706	199.053	196.512	194.245	192.778	192 358	404 000	191.033	189.549	186.869	184.380	
-		οT	(min)	29	10.569	10.851	11.360	11,768	13.367	14 812	45.756	46.037	10.021	16,525	17,859	19.632	21.301	
	IVE	(DA)MUE	hal	114	0.286	0.420	0.696	0 910	4 105	4 057	1.001	C. state	2.042	2.841	3.874	6,065	8.229	-
	1	A.C	(ha)	(110)	2000	0.449	0.145	0.245	0.405	0.180	70970	0.488	0.198	0.198	1.034	2 191	2.165	-
		et and	ent	S	2	0.00	0.65	0.00	0.00	0.65	0.65	0.65	0.65	0.65	0.65	0.00	0.00	00'0
	pu	Street a indust		(ha)		0.44	0.22	0.41	0.33	0.30	1.31	0.75	0.31	0.34	200	1,03	3.37	3.00
3		CENGTI		(m)	9	34.13	51.05	81.62	106.10	202.05	288.73	345.37	361.64	270 64	3/3.01	471.55	677.90	0.7 M O.7
	H	ГЕИӨЦ		(m)	10	34.13	16.92	30.57	24.48	95.95	89.68	56.64	16.27	40.00	17.87	92.04	106.35	2000
		ER MH.		07	*	2	67	4	5	9	7	8	o		10	11	12	40.7
	LOCATION	9 MH.		dn	200	-	2	3	4	2	8	1		8	6	10	11	
	7	BMAN	AN	רו	C	main 3	main 3	main 3	main 3	o month	mann 2	C HIGH	mains	main 3	main 3	main 3	main 3	-
		язамі	nn		-		- 0	3 6	3 4	3 1	0	9	7	83	0	40	44	

							_	-	_	_	-	-	-	_	_			
		۵۱		(1/s)	18	2.785	0.400	9.400	11.270	12,369	22.448	12.386	27.256	1000	070.7	58.580	91.350	12.521
		Ö		(1/18)	17	2.785	12 266	2000	23.536	35,905	58.353	70.739	97.996	105 600	404 000	164.202	255.552	268.073
		(1)		(l/s.ha)	48	201.191	200.539	400000	199,943	199.343	198.614	198.232	197,488	197 012	405 404	195.404	191.990	190.117
		οT		(min)	16	10,438	10,842	44 549	11.213	11.586	12.043	12,283	12.751	13.051	44.079	40.000	10.200	17.487
		(DA)MU		(na)	-	0.014	0.061	0110	0.110	0.180	0.294	0.357	0.496	0.536	0840	4 204	1000	1.410
		A.: TBBRT8	0	(na)		0.014	0.047	0.057	1000	790.0	0.114	0.063	0.139	0.040	0 304	0.404	0.401	0.079
age of		PACTOR ef and visubn	ente	2	20 6	0.65	0.65	0.65	0.66	0.00	0.65	0.65	0.65	0.65	0.65	0.65	200	0.65
	pu	Street as taubri	(ha)	(mil)	000	0.02	0.07	60.0	010	200	0.17	0.10	0.21	90.0	0.47	0.76	07.0	21.0
		COMNTY.	Ē	1	28.27	50.80	200	8/3/6	95.19	122.50	138 00	168.00	183.05	24.08	4.31	36.86	449.10	
	*10	NET (E	M.	26.37	24.00	24.20	22.26	22.41	27.40	44.00	14.30	58.09	18.04	61.23	131.66	73.23		
	HW	NO"	4	2	3		1	4O	9	1		0	0	10	4	12		
THILLETINE	ж	UPPER I	3	-	2	3	2	4	2	9	1		0	T.	10	11		
	3WI	LINE NA	04	1qns	sub1	cuh1	- Cano	Sub1	Sub1	Sub-1	emb4	out of	- Cano	lans	sub1	sub1		
	858	MUN	-	-	2	3	,	4	5	9	7		0	'n	10	11		

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17.487 190.117 268.073

	(lis) 18 18.322 23.301 3.723 49.869 29.211 78.395
	(Vs) 18.322 41.622 45.345 95.214 124.425 202.821 213.364
	(Vs.ha) 16 201.337 200.108 199.320 197.344 196.246 196.246
	(min) 18 10.348 11.110 12.459 12.459 13.536 14.082
	SVITAJUMOD
	(ha) (ha) 0.228 0.481 1.034 1.092
	(ha) STREET 0.020 0.150 0.150 0.059
1b 2	0.65 0.065 0.65 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.
Sub	0.09 0.23 Street and 0.09 0.03 0.03 0.03 0.03 0.03 0.03 0.03
-	20.87 COMULATIVE 66.61 (m) COMULATIVE 147.55 12.16 244.91
	(m) (т) 20.87 45.74 45.74 29.45 51.49 22.95 41.66 32.75
2	.ou + ™ LOWER MH.
LOCATION	ON THE WH.
	Sub2 Sub2 Sub2 Sub2 Sub2 Sub2 Sub2 Sub2
	язамии — + м м 4 го ю г

	Ö	(1/2)	18	30.072	28,539	27.030	27.990	22 640	33,040	86.402	20.421	5.521	454 398	100000000000000000000000000000000000000
	Ö	(1/8)	11	30.072	58.611	85,640	443,630	100000	146.679	233.080	253.501	259 022	440 494	410.451
	(1)	(l/s.ha)	94	201.149	200.379	199.628	100 054	180.03*	197.947	197.025	195,981	405 244	193,541	194.282
	эТ	(min)	15	10.464	10.942	11 400	00000	12.018	12.462	13.043	43.705	0000	14.112	14.788
HVE	COMULA)	(ha)	1	0.150	0.903	0.400	0.429	0.572	0.741	1 183	1 204	1.434	1.326	2.113
1	A.c	(hal)	(lia)	0.450	0.100	0.143	0.137	0.143	0.160	0.449	O. open	0.111	0.033	0.787
Æ	Street a industry et and etry	l tre	0	-	1				+	0.26 0.05		0.17 0.65	0.05 0.65	+
ΞVΙΤ	CMULA	0	(m)	9	27.85	56.50	84.53	20,000	121.00	147.72	182.58	222 28	016.70	2002 24
H	LENGTI		(m)	10	27.85	28.65	20 00	70.07	36.53	26.66	34.87	20.60	33.03	24.42
	.OV.		רסו	**	2		,	4	0	9	1		20	6
LOCATION	HM. 9		Har		-	- (7	3	4	u		0	7	8
	BMAN	1E	רוע	-	4	Sub 3	sub 3	sub 3	- P 4	Sans	sons o	sub 3	sub 3	sub 3
	мвек	nN				-	2	2	,	4	2	9	7	00

		Ø!	100	(SII)	18	16 945	20 444	20.045	03.010	00.040	44 040	14.870
		Ö	107-1	(1/5)	11	16.945	40 257	80.474	149 847	180 184	174 276	186.244
		(1)	(He ha)	(no-rig)	16	200.535	199.824	198.821	197 520	197 125	196 756	196.253
		эТ	(mim)	1	0.00	10.844	11,287	11.913	12.725	12.980	13.213	13.532
		SUM(AC)	hal		-	0.085	0.247	0.449	0.722	0.813	0.871	0.949
		A.D TAERT	(ha)	-		0.085	0.163	0.202	0.273	0.091	0.059	0.078
Sub 4		FACTOR 66t and industry		O		0.65	0.65	0.65	0.65	0.65	0.65	0.65
Su		Street and industry	(ha)	1	47.4	0.13	0.25	0.31	0.42	0.14	0.09	0.12
	3/	LENGTH	(m)	9	40.00	99.00	77.19	114.79	163.51	178.77	192.77	211.89
		ГЕИОТН	(m)	in	20.00	20.00	26.53	37.60	48.72	15.26	14.00	19.12
		WER MH.	го	4	c	7	n	4	2	9	7	00
	LOCATION	NO.	чn	80	,	-	2	P*7	4	5	9	7
		BMAN BNI.	1	2	Cuth A	t ans	sub 4					
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			ď	(8/1)	48	89.822	200,545	24.792	63.980	7.070	20.963
			Ö	(1/8)	17	89.822	290.367	315,159	379.139	386.209	407.172
		(1)			116	200.271	197.663	197.098	195,735	194.809	192.744
		SUM(AC)		(min)	111	11,008	12.641	12.997	13,861	14,451	15,778
				(ha)	9.6	0.449	1.469	1.599	1.937	1.983	2.113
			с. Втреет	(ha)	-	0.449	1.021	0.130	0.338	0.046	0.130
00	FACTOR seet and variety			er C	6	99.0	99.0	0.65	99.0	99'0	0.65
Sub		pu	Street a	(ha)	1	69.0	1.57	0.20	0.52	0.07	0.20
i	3/	COMULATIVE			9	60.50	158.44	179.83	231.65	267.07	346.67
		Н	LENGT	(m)	10	60.50	97.94	21.39	51.82	35.42	79.60
			NEK MH.	רסו	-	2		4	LC.	9	7
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Sanitary main 1

Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In
MH-1	6+83	644.94	1.2	6,76	0.22
MH-2	6+52	642.86	1.2	175	
MH-3	6+03	639.9	1.2	193.06	0.50
MH-4	5+78	639.79	1.2	519.95	0.000
MH-5	5+53	639,71	1.2	573.14	0.68
MH-6	5+13	639.53	1.2	966.11	0.70
MH-7	4+63	636.25	1.2	1190.93	0.82
MH-8	4+14	633,36	1.2	1651.48	0.87
MH-9	3+64	630.98	1.2	1992.44	0.98
MH-10	3+14	628.61	1.2	2546.99	1.05
ИН-11	2+65	626.37	1.2	2976.46	1.17
MH-12	2+15	624.99	1.2		1.26
/IH-13	1+69	622.32	1.2	3580.43	1.41
MH-14	1+19	620.1		4337.82	1.62
IH-15	0+76	619.07	1.2	5045,43	1.39
fH-16	0+42	617.34	1.2	5874.82	1.52
0-1	12		1.2	6664.47	1.40
		617.34		6664.47	0.00

abel	Upstream Node	Downstream Node	Section Size Description	Section Shape	Average Velocity (m/s)	Slope (m/m)
P-I	MH-I	MH-2	200 mm	Circular	0.40	0.035
2-2	MH-2	MH-3	200 mm	Circular	1.08	0.035
2-3	MH-3	MH-4	200 mm	Circular	0.60	0.006054
14	MH-4	MH-5	200 mm	Circular	0.75	0.005
1-5	MH-5	MH-6	200 mm	Circular	1.53	0.034572
P-6	MII-6	MH-7	200 mm	Circular	1.79	0.035
7-7	MH-7	MH-8	200 mm	Circular	1.90	0.035
2-8	MH-8	MH-9	200 mm	Circular	2.08	0.035
2-9	MH-9	MH-10	200 mm	Circular	2.19	0.035
-10	MH-10	MH-11	200 mm	Circular	2.35	0.035
111	MH-11	MH-12	200 mm	Circular	2,19	0.026119
-12	MH-12	MH-13	200 mm	Circular	2.56	0.035
13	MH-13	MH-14	200 mm	Circular	2.69	0.035
14	MH-14	MH-15	250 mm	Circular	2.77	0.034449
-15	MH-15	MH-16	250 mm	Circular	2.90	0.035
-16	MH-16	O-1	300 mm	Circular	1.42	0.005

Sanitary main 2

Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)
MH-1	4+64	656.14	1.2	10.58	0.25
MH-2	4+52	656.09	1.2	12.91	0.26
MH-3	4+46	656.03	1.2	27.36	0.31
MH-4	4+36	655.65	1.2	39.10	0.34
MH-5	4+12	654.46	1.2	64.67	0.39
МН-6	3+86	653.52	1.2	88.10	0.42
MH-7	3+50	652.07	1.2	121.18	0.45
MH-8	3+05	650.13	1.2	146.35	0.48
MH-9	2+83	650	1.2	184.41	0.51
H-10	2+57	647.58	1.2	222.30	0.54
VH-11	2+29	645.7	1.2	275.16	0.57
CH-12	1+86	645.66	1.2	318.99	0.59
GH-13	1+71	644.98	1.2	380.99	0.62
MH-14	1+51	644.8	1.2	430.07	0.64
GH-15	1438	644.29	1.2	503.12	0.67
CH-16	0.90	643.45	1.2	557.85	0.69
IH-17	0.68	643.33	1.2	637.34	0.72
/H-18	0.42	640.21	1.2	695.81	0.74
0-1		640.21		695.81	0.00

avity	pipe Report				Average	Constructed
abel	Upstream Node	Downstream Node	Section Size Description	Section Shape	Velocity (m/s)	Slope (m/m)
P-I	MH-1	MH-2	200 mm	Circular	0.6	0.075587
2-2	MH-2	MH-3	200 mm	Circular	0.6	0.063411
2-3	MH-3	MH-4	200 mm	Circular	0.6	0.0359
24	MH-4	MH-5	200 mm	Circular	0.69	0.0359
2.5	MH-5	MH-6	200 mm	Circular	0.79	0.0359
3-6	MH-6	MH-7	200 mm	Circular	0.88	0.0359
2-7	MH-7	MH-8	200 mm	Circular	0.97	0.0359
2.8	MH-8	MH-9	200 mm	Circular	1.03	0.0359
2.9	MH-9	MH-10	200 mm	Circular	1.1	0.0359
110	MH-10	MH-11	200 mm	Circular	1.39	0.064725
111	MH-11	MH-12	200 mm	Circular	1.25	0.0359
112	MH-12	MH-13	200 mm	Circular	1.3	0.0359
13	MH-13	MH-14	200 mm	Circular	1.37	0.0359
114	MH-14	MH-15	200 mm	Circular	1.43	0.0359
43	MH-15	MII-16	200 mm	Circular	1.49	0.0359
46	MII-16	MH-17	200mm	Circular	1.54	0.0359
117	MH-17	MH-18	200mm	Circular	1.6	0.0359
13.	MH-18	0-1	200 mm	Circular	1.65	0.0359

Sanitary main 3

Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter	Total Flow	Velocity In
MH-1	6+99	633.68	(m)	(m³/day)	(m/s)
MH-2	6+90	633.27	1.2	13.78	0.26
MH-3	6+71	632.4	1,2	30.77	0.32
MH-4	6+48	632.27	1.2	63.81	0.38
MH-5	6+26	631.72	1.2	98.08	0.43
MH-6	5+93	630.96	1.2	162.23	0.49
MH-7	5+44	630.46	1.2	329.2	0.60
MH-8	4+96	630.39	1.2	403,39	0.63
MH-9	4+46	630	1.2	629.53	0.72
MH-10	3+99	625	1.2	729,92	0.75
MH-11	3-49	620	1.2	998.07	0.82
MH-12	3+01		1.2	1139.77	0.86
MH-13	2+57	615	1.2	1441.76	0.93
MH-14	2+07	612.3	1,2	1964.79	1.05
MH-15	1+51	605	1.2	2373.28	1.13
MH-16	1+00	604	1.2	2993.12	1.27
MH-17	0+50	603.5	1.2	3480.11	1.17
0-1	0100	603.2	1.2	4235.63	1.17
-		603.2		4235.63	0.00

ibel	Upstream Node	Downstream Node	Section Size Description	Section Shape	Average Velocity (m/s)	Slope (m/m)
2-1	MII-I	MH-2	200 mm	Circular	0.60	0.059866
2-2	MH-2	MH-3	200 mm	Circular	0.65	0.036768
-3	MH-3	MH-4	200 mm	Circular	0.60	0.015626
4	MH-4	MH-5	200 mm	Circular	0.60	0.010775
-5	MH-5	MH-6	200 mm	Circular	0.86	0.019779
-6	MH-6	MH-7	200 mm	Circular	0.81	0.008959
-7	MH-7	MH-8	200 mm	Circular	0.70	.005
-8	MH-8	MH-9	200 mm	Circular	1.40	0.02479
19	MH-9	MH-10	200 mm	Circular	2.21	0.08
10	MH-10	MH-11	200 mm	Circular	2.42	0.08
21	MH-11	MH-12	200 mm	Circular	2.52	0.08
12	MH-12	MH-13	200 mm	Circular	2.44	0.060667
13	MH-13	MH-14	200 mm	Circular	2.94	0.08
14	MH-14	MH-15	200 mm	Circular	1.76	0.016768
15	MH-15	MH-16	200mm	Circular	1,43	0.008693
16	MH-16	MH-17	250mm	Circular	1.29	0.005796
17.	MH-17	0-1	300mm	Circular	1.29	0.005

		Gravity No	de Report		
Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)
MH-1	1+35	659.78	1.22	2.25	0.16
MH-2	1+29	659.26	1.22	5.63	0.2
MH-3	1+25	657.94	1.22	15.72	0.27
MH-4	1+17	558.04	1.22	22.95	0.3
MH-5	1+14	655.26	1.22	38.96	0.34
MH-6	1+08	651.75	1.22	57.56	0.37
MH-7	1+00	649.82	1.22	81.03	0.41
MH-8	0+95	647.08	1.22	113.22	0.45
MH-9	0+87	645.99	1.22	140.03	0.47
MH-10	0+82	645.92	1.22	188.08	0.51
MH-11	0+70	645	1.22	229.24	0.5
MH-12	0+62	644.24	1.22	299.86	0.58
MH-13	0+48	644	1.22	350,28	0.6
MH-14	0+36	643.9	1.22	430.91	0.6
MH-15	0+21	643.1	1.22	487.35	0.6
MH-16	0+09	642.9	1.22	569.25	0.
0-1		642.9		569.25	

		Gravity	pipe Re	port		
Label	Upstream Node	Downstream Node	Section Shape	Section Size	Average Velocity (m/s)	Hydraulic Slope (m/m)
P-1	MH-1	MH-2	Circular	200 mm	1.58	0.08583
P-2	MH-2	MH-3	Circular	200 mm	0.64	0.150889
P-3	MH-3	MH-4	Circular	200 mm	0.86	0.150822
P-4	MH-4	MH-5	Circular	200 mm	0.97	0.152144
P-5	MH-5	MH-6	Circular	200 mm	1.13	0,151493
P-6	MH-6	MH-7	Circular	200 mm	1.28	0.151504
P-7	MH-7	MH-8	Circular	200 mm	1.42	0.153103
P-8	MH-8	MH-9	Circular	200 mm	1.54	0.143165
P-9	MH-9	MH-10	Circular	200 mm	0.63	0.010375
P-10	MH-10	MH-11	Circular	200 mm	1.44	0.077696
P-11	MH-11	MH-12	Circular	200 mm	1.67	0.100658
P-12	MH-12	MH-13	Circular	200 mm	0.95	0.016275
P-13	MH-13	MH-14	Circular	200 mm	0.77	0.00817
P-14	MH-14	MH-15	Circular	200 mm	1.63	0.054374
P-15	MH-15	MH-16	Circular	200 mm	1.1	0.017052
P-16	MH-16	0-1	Circular	200 mm	0.77	0.005489

		Gravity N	ode Repor	t	
Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)
ИH-1	2+31	649.66	1.2	17.62	0.28
ин-2	1+93	648.25	1.2	22.08	0.29
ИН-3	1+81	648.25	1.2	41.88	0.34
ИH-4	1+52	645.46	1.2	55.57	0.37
/IH-5	1+31	644.00	1.2	98.54	0.43
4H-6	0-98	642.00	1.2	124.18	0.46
4H-7	0+75	641.00	1.2	184.83	0.51
4H-8	0+57	639.59	1.2	232.24	0.54
411-9	0+36	637.72	1.2	298.72	0.58
0-1		637,72		298.72	0

		Gravity	pipe Re	port		
Label	Upstream Node	Downstream Node	Section Shape	Section Size	Average Velocity (m/s)	Hydraulic Slope (m/m)
-1	MH-1	MH-2	Circular	200 mm	0.64	0.059962
-2	MH-2	MH-3	Circular	200 mm	0.69	0.059605
-3	MH-3	MH-4	Circular	200 mm	0.84	0.059907
-4	MH-4	MH-5	Circular	200 mm	0.92	0.059664
-5	MH-5	MH-6	Circular	200 mm	1.09	0.059893
-6	MH-6	MH-7	Circular	200 mm	1.17	0.059699
-7	MII-7	MH-8	Circular	200 mm	1.32	0.059736
-8	MH-8	MH-9	Circular	200 mm	1.51	0.071152
-9	MH-9	0-1	Circular	200 mm	1.53	0.06067

	Gravity Node Report									
Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)					
MH-1	2+85	644.97	1.2	27.13	0.31					
MH-2	2+42	644.97	1.2	48.59	0.36					
MH-3	2+15	642.99	1.2	77.77	0.41					
MH-4	1+99	639.49	1.2	113.97	0.45					
MH-5	1+64	634,56	1.20	159.9	0.49					
MH-6	1+39	634.04	1.20	230.31	0.54					
MH-7	1+04	630	1.20	280.71	0.57					
MH-8	0+64	625	1.20	353.67	0.61					
MH-9	0+39	623.8	1.20	504.72	0.67					
0-1		623.8		504.72	0					

	Gravity pipe Report							
Label	Upstream Node	Downstream Node	Section Shape	Section Size	Average Velocity (m/s)	Hydraulic Slope (m/m)		
P-1	MH-1	MH-2	Circular	200 mm	0.6	0.033105		
P-2	MH-2	MH-3	Circular	200 mm	1	0.086032		
P-3	MH-3	MH-4	Circular	200 mm	1.22	0.100803		
P-4	MH-4	MH-5	Circular	200 mm	1.37	0.100461		
P-5	MH-5	MH-6	Circular	200 mm	1.07	0.037359		
P-6	MH-6	MH-7	Circular	200 mm	1.69	0.100661		
P-7	MH-7	MH-8	Circular	200 mm	1.79	0.100651		
P-8	MH-8	MH-9	Circular	200 mm	1.46	0.046529		
P-9	MH-9	0-1	Circular	200 mm	0.74	0.005111		

Gravity Node Report								
Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m²/day)	Velocity In (m/s)			
MH-1	0+62	649.99	1.22	11.4	0.25			
MH-2	0+50	646.74	1,22	21.05	0.29			
МН-3	0+46	645.4	1.22	58,49	0.38			
MH-4	0+31	641.17	1.22	81.09	0.41			
MH-5	0+26	640.47	1.22	138.45	0.47			
MH-6	0+15	637.98	1.22	168.98	0.5			
MH-7	0+11	636.04	1.22	230.18	0.54			
MH-8	0+06	634.23	1.22	271.11	0.57			
0-1	WWW.	634.23		271.11	0.07			

Gravity pipe Report							
Label	Upstream Node	Downstream Node	Section Shape	Section Size	Average Velocity (m/s)	Hydraulic Slope (m/m)	
P-1	MH-1	MH-2	Circular	200 mm	0.78	0.150416	
P-2	MH-2	MH-3	Circular	200 mm	0.94	0.151743	
P-3	MH-3	MH-4	Circular	200 mm	1.28	0.150831	
P-4	MH-4	MH-5	Circular	200 mm	1.33	0.127173	
P-5	MH-5	MH-6	Circular	200 mm	1.66	0.151673	
P-6	MH-6	MH-7	Circular	200 mm	1.77	0.155331	
P-7	MH-7	MH-8	Circular	200 mm	1.95	0.155839	
P-8	MH-8	0-1	Circular	200 mm	0.62	0.005443	

	Gravity Node Report								
Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)				
MH-1	3+47	637.59	1.20	45.89	0.35				
MH-2	2+97	636.09	1.20	52.24	0.37				
MH-3	2+88	636.04	1.20	157.35	0.49				
MH-4	2+38	635	1.20	207.71	0.53				
MH-5	1+97	634.98	1.20	332.22	0.6				
MH-6	1+63	634.47	1.20	410.14	0.63				
MH-7	1+42	630	1.20	569.53	0.7				
MH-8	1+15	625	1.2	654.28	0.73				
MH-9	0-78	620	1.2	868.73	0.79				
MH-10	0+45	615	1.2	959.96	0.81				
0-1		615		959.96	0				

Gravity pipe Report								
Label	Upstream Node	Downstream Node	Section Shape	Section Size	Average Velocity (m/s)	Hydraulic Slope (m/m)		
P-1	MH-1	MH-2	Circular	200 mm	0.68	0.03		
P-2	MH-2	MH-3	Circular	200 mm	0.6	0.018596		
P-3	MH-3	MH-4	Circular	200 mm	0.83	0.018451		
P-4	MH-4	MH-5	Circular	200 mm	0.6	0.005693		
P-5	MH-5	MH-6	Circular	200 mm	1.73	0.078429		
P-6	MH-6	MH-7	Circular	200 mm	2.01	0.1		
P-7	MH-7	MH-8	Circular	200 mm	2.22	0.1		
P-8	MH-8	MH-9	Circular	200 mm	2.31	0.1		
2-9	MH-9	MH-10	Circular	200 mm	2.51	0.1		
-10	MH-10	O-1	Circular	200 mm	0.89	0.005		

storm main 1

	Gravity Node Report							
Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)			
MH-1	2+08	644.94	1.22	30,318.26	2.28			
MH-2	1+76	639.79	1.22	57,560.85	2,49			
MH-3	1+58	639.58	1.22	70,963.17	2.92			
MH-4	1+39	635.81	1.22	129,069.74	3.37			
MH-5	0+94	628.45	1.22	160,180.13	3.07			
MH-6	0+61	624.99	1.22	167,466.37	3.17			
MH-7	0+51	622.32	1.22	240,998.03	3.37			
MH-8	0+27	620.01	1.22	268,443.45	3.13			
0-1		620.01		268,443.45	0			

Gravity pipe Report							
Label	Upstream Node	Downstrea m Node	Section Shape	Section Size	Averag e Velocit y (m/s)	Constructe d Slope (m/m)	
P-1	MH-1	MH-2	Circular	450 mm	2.67	0.01	
P-2	MH-2	MH-3	Circular	600 mm	3.17	0.01	
P-3	MH-3	MH-4	Circular	600 mm	3.25	0.01	
P-4	MH-4	MH-5	Circular	750 mm	3.77	0.01	
P-5	MH-5	MH-6	Circular	900 mm	4.11	0.01	
P-6	MH-6	MH-7	Circular	900 mm	4.14	0.01	
P-7	MH-7	MH-8	Circular	1050 mm	4.55	0.01	
P-8	MH-8	0-1	Circular	1200 mm	3.58	0.005	

storm main 2

Gravity Node Report								
Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In (m/s)			
МН-1	1+43	656.14	1.22	1,357.42	0.91			
MH-2	1+38	656.03	1.22	2,371.32	1.13			
МН-3	1+35	655.48	1.22	3,715.37	1,45			
MH-4	1+27	654.50	1.22	6,709.01	2.4			
MH-5	1+12	652.88	1.22	8,648.71	3.09			
MH-6	0+92	650.08	1.22	9,602.77	3.43			
MH-7	0+82	648.44	1.22	11,654.96	2.67			
MH-8	0-73	645.90	1.22	14,200.27	1.72			
MH-9	0+58	645.78	1.22	16,709.92	1.89			
MH-10	0+43	644.33	1.22	16,872.69	1.9			
MH-11	0+21	643.44	1.22	18,420.04	1.71			
0-1		643.44		18,420.04	0			

		Gravi	ity pipe I	Report		
Label	Upstream Node	Downstrea m Node	Section Shape		Average Velocity (m/s)	Constructe d Slope (m/m)
P-1	MH-1	MH-2	Circula	200 mm	1.61	0.02005
P-2	MH-2	MH-3	Circula	r 200 mm	3	0.073
P-3	MH-3	MH-4	Circula	r 200 mm	3.4	0.073
P-4	MH-4	MH-5	Circula	r 200 mm	3.94	0.073
P-5	MH-5	MH-6	Circular	200 mm	4.15	0.073
P-6	MH-6	MH-7	Circular	200 mm /	4.21	0.073
P-7	MH-7	MH-8	Circular	250 mm	4.53	0.073
P-8	MH-8	MH-9	Circular	375 mm	3.39	0.02956
P-9	MII-9	MH-10	Circular	375 mm	4.93	0.073
P-10	MII-10	MH-11	Circular	375 mm	4.06	0.042569
P-11	MH-11	0-1	Circular	450 mm	1.84	0.005

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		Gravity N	ode Repo	rt	
Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m²/day)	Velocity In (m/s)
MH-1	6+03	633.68	1.2	45.89	0.35
MH-2	5+85	632.22	1.2	5,012.17	1.24
MH-3	5+62	632.22	1.2	7,478,46	1.48
MH-4	5+40	631.32	1.2	12,046,46	1.59
MH-5	5+07	630.83	1.2	15,696.20	1.6
MH-6	4+45	630.83	1.2	18,807.30	1.73
MH-7	3+85	625	1.2	32,881.39	2.43
MH-8	2+85	620	1.2	40,753.16	2.05
MII-9	2+69	615	1.2	43,959.44	2.13
MH-10	2+51	612.5	1.2	47,141.51	2.21
MH-11	1+57	610	1.2	63,490.43	2.67
MH-12	1-01	605	1.2	97,960.29	2.74
MH-13	0+50	604	1.2	131,137,55	2.72
O-1		604		131,137.55	0

		Grav	ity pipe R	teport		
Label	Upstream Node	Downstream Node	Section Shape	Section Size	Average Velocity (m/s)	Constructed Slope (m/m)
P-1	MH-1	MH-2	Circular	200 mm	0.47	0.01
P-2	MH-2	MH-3	Circular	300 mm	1.34	0.005
P-3	MH-3	MH-4	Circular	300 mm	1.92	0.01
P-4	MH-4	MH-5	Circular	375 mm	2.17	0.01
P-5	MH-5	MH-6	Circular	450 mm	1.78	0.005
P-6	MH-6	MH-7	Circular	450 mm	2.42	0.01
P-7	MH-7	MH-8	Circular	450 mm	2.68	0.01
P-8	MH-8	MH-9	Circular	600 mm	2.94	
P-9	MH-9	MH-10	Circular	600 mm	2.99	
	MH-10	MH-11	Circular	600 mm	3.04	COLUMN TO SERVICE STATE OF THE PERSON STATE OF
P-10	MH-11	MH-12	Circular	600 mm	3.22	A CONTRACTOR OF THE PARTY OF TH
P-11		MH-13	Circular	750 mm	3.63	0.01
P-12 P-13	MH-12 MH-13	0-1	Circular	900 mm	2.98	0.005

Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity in (m/s)
MH-1	4+42	659.8	1.2	240.67	0.55
MH-2	4+16	659	1.2	1,059.78	0.84
MH-3	3+92	656.88	1.2	2,033.53	1.06
MH-4	3+70	655.47	1.2	3,102.17	1.29
MH-5	3+48	651.65	1.2	5,041.67	1.84
MH-6	3+21	649.81	1.2	6,111.86	2.2
MH-7	3+07	646.95	1.2	8,466.81	1.99
MH-8	2+79	645,81	1.2	9,125.73	1.41
МН-9	2+61	645.81	1.2	14,187.01	1.72
CH-10	2+00	643.99	1.2	22,079.68	1.87
CH-11	0+68	643.1	1.2	23,161.54	1.9
0-1		643.1		23,161.54	0

Gravity	Upstream Node	Downstream Node	Section Size Description	Section Shape	Average Velocity (m/s)	Constructed Slope (m/m)
P-1	MH-1	MH-2	200 mm	Circular	1.13	0.030769
P-2	MH-2	MH-3	200 mm	Circular	2.52	0.085792
P-3	MH-3	MH-4	200 mm	Circular	2.7	0.061318
P-4	MH-4	MH-5	200 mm	Circular	3.63	0.1
P-5	MH-5	MH-6	200 mm	Circular	3.52	0.064691
P-6	MH-6	MH-7	200 mm	Circular	4.34	0.1
P-7	MH-7	MH-8	250mm	Circular	3.42	0.042707
P-8	MH-8	MH-9	375mm	Circular	1.56	0.005
P-9	MH-9	MH-10	375mm	Circular	3.31	0.02761
P-10	MH-10	MH-11	450mm	Circular	2.17	0.006884
P-11	MH-11	0-1	450mm	Circular	1.9	0.005

Label	Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity Ir
MH-1	2+45	649.68	1,2	1,582.99	0.96
MH-2	2+24	649.35	1,2	3,596.18	1.41
MH-3	1+79	648.26	1.2	3,917.85	1.5
MH-4	1+49	645.4	1.2	8,226.55	2.94
MH-5	0+98	642	1.2	10,750.37	1.83
MH-6	0)+75	641.6	1.2	17,523.73	2.8
MH-7	0+33	637.53	1.2	18,434.64	1.71
0-1		637.53		18,434.64	0

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abel	Upstream Node	Downstream Node	Section Size Description	Section Shape	Average Velocity (m/s)	Constructed Slope (m/m)			
P-1	MH-1	MH-2	200 mm	Circular	1.54	0.015714			
P-2	MH-2	MH-3	200 mm	Circular	2.17	0.022615			
P-3	MH-3	MH-4	200 mm	Circular	3	0.05			
P-4	MH-4	MH-5	200 mm	Circular	3.49	0.05			
P-5	MH-5	MH-6	300 mm	Circular	2.68	0.019157			
P-6	MH-6	MH-7	300 mm	Circular	4.34	0.05			
P-7	MH-7	0-1	450mm	Circular	1.84	0.005			

Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In
MH-1	2+86	645.9	1.2	2,598.26	1.18
MH-2	2+59	645.73	1.2	5,064.03	1.85
MH-3	2+30	644.8	1.2	7,399.40	2.65
MH-4	2+02	639.88	1.2	9,817.72	2.27
MH-5	1+66	634.67	1.2	12,673.08	2.08
MH-6	1+40	633.92	1.2	20,138.20	3.2
MH-7	1+05	630	1.2	21,902.54	3.48
MH-8	0+65	625	1.2	22,379.57	3.55
MH-9	0+41	623.8	1.2	35,460.39	1.92
O-1		623.8		35,460.39	0

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Label	Upstream Node	Downstream Node	Section Size Description	Section Shape	Average Velocity (m/s)	Constructed Slope (m/m)				
P-1	MH-1	MH-2	200 mm	Circular	1.21	0.006182				
P-2	MH-2	MH-3	200 mm	Circular	2.61	0.029966				
P-3	MH-3	MH-4	200 mm	Circular	3.45	0.05				
P-4	MH-4	MH-5	250mm	Circular	3.76	0.05				
P-5	MH-5	MH-6	300 mm	Circular	3.22	0.027917				
P-6	MH-6	MH-7	300 mm	Circular	4.46	0.05				
P-7	MH-7	MH-8	300mm	Circular	4.52	0.05				
p-8	MH-8	MH-9	300mm	Circular	4.39	0.04649				
p.9	MH-9	0-1	600mm	Circular	2.34	0.00602				

Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In
МН-1	2+11	649.99	1.2	1,464.07	(m/s) 0.94
MH-2	1+60	646.48	1.2	4,264.41	1.6
МН-3	1+34	643,79	1.2	7,704.40	2.76
MII-4	0+96	640.74	1.2	12,313,46	2.82
MH-5	0+47	637.6	1.2	13,838.21	3,17
МН-6	0+32	635.71	1.2	14,806.78	3.39
MH-7	0÷18	633.82	1.2	16,091.52	1.85
0-1		633,82	114	16,091.52	0

label	Upstream Node	Downstream Node	Section Size Description	Section Shape	Average Velocity (m/s)	Constructed Slope (m/m)
P-1	MH-1	MH-2	200 mm	Circular	2.29	0.05
P-2	MH-2	MH-3	200 mm	Circular	3.06	
P-3	MH-3	MH-4	200 mm			0.05
P-4	MH-4	MH-5		Circular	3.47	0.05
P-5			250 mm	Circular	3.95	0.05
	MH-5	MH-6	250 mm	Circular	4.02	0.05
P-6	MH-6	MH-7	250 mm	Circular	4.05	3000000
P-7	MH-7	0-1	375mm	Circular	1.99	0.05

Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity Ir
MH-1	2+11	649.99	1.2	1,464.07	0.94
MH-2	1+60	646.48	1.2	4,264.41	1.6
MH-3	1+34	643.79	1.2	7,704.40	2.76
MH-4	0+96	640.74	1.2	12,313.46	2.82
MH-5	0+47	637.6	1.2	13,838.21	3.17
MH-6	0+32	635.71	1.2	14,806.78	3.39
MH-7	0-18	633.82	1.2	16,091.52	1.85
0-1		633.82		16,091.52	0

ravity	ravity pipe Report									
label	Upstream Node	Downstream Node	Section Size Description	Section Shape	Average Velocity (m/s)	Slope (m/m)				
P-1	MH-1	MH-2	200 mm	Circular	2.29	0.05				
P-2	MH-2	MH-3	200 mm	Circular	3.06	0.05				
P-3	MH-3	MH-4	200 mm	Circular	3,47	0.05				
P-4	MH-4	MH-5	250 mm	Circular	3.95	0.05				
P-5	MH-5	MH-6	250 mm	Circular	4.02	0.05				
P-6	MH-6	MH-7	250 mm	Circular	4.05	0.05				
P-7	MH-7	0-1	375mm	Circular	1.99	0.007056				

Gravity Node Report									
Label	Calculated Station (m)	Ground Elevation (m)	Structure Diameter (m)	Total Flow (m³/day)	Velocity In				
MH-1	3+47	637.59	1.2	7,760.60	1.85				
MH-2	2+87	636.22	1.2	25,087.67	2.59				
МН-3	1+89	634.43	1.2	27,229.73	1.73				
MH-4	1+67	634.43	1.2	32,757.57	1.86				
MH-5	1+15	625	1.2	33,368.40	1.87				
MH-6	0+80	620	1.2	35,179.59	1.92				
0-1		620		35,179.59	0				

ravity pipe Report									
abel	Upstream Node	Downstream Node	Section Size Description	Section Shape	Average Velocity (m/s)	Constructed Slope (m/m)			
1-1	MH-1	MH-2	250 mm	Circular	2.67	0.023736			
P-2	MH-2	MH-3	375 mm	Circular	3.32	0.019976			
P-3	MH-3	MH-4	600 mm	Circular	2.05	0.0050			
P-4	MH-4	MH-5	600 mm	Circular	4.97	0.049			
P-5	MH-5	MH-6	600 mm	Circular	5	0.049			
P-6	MH-6	0-1	600 mm	Circular	2.18	0.005			

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