
The Home of Competent Engineers and Researchers

# COLLEGE OF ENGINEERING AND TECHNOLOGY Electrical Engineering Department 

Industrial Automation Engineering Program

GRADUATION PROJECT REPORT

## EXOSKELETON FOR PERIPHERAL PARALYSIS CONTROLLED BY EMG SIGNALS

## Project Team

Hamza R. AL-Ajouri<br>Mohammad H. Mohsen

Tareq Z. Al-Qwasmeh

Project Supervisor
Dr. Sameer H. Khader

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Graduation Project Evaluation

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Hamza R. AL-Ajouri Mohammad H. mohsen

Tareq Z. Al-Qawasmeh

According to the orientations of the supervisor on the project and the examined committee is by the agreement of a staffers all, sending in this project to the Electrical and Computer Engineering Department are in the College of the Engineering and the Technology by the requirements of the department for the step of the bachelor's degree.

Project Supervisor Signature

Committee Signature

Department Headmaster Signature

الإهداء


إلى الذي قال تُعالى فيهما (و أخفض لهـما جناح الذل من ربياني صغيرا).

المـاس الذي لا ينكسر .
....... التي ساندتني بدعواتها و وقفت معي حتى وصلت
اللى من تعجز الكلمات عن وصفها و تسكن أمواج

الذين رفعوا رايات العلم و التعليم و أخمدوا رايات الجهل و التجهيل أهدي هذا الجهد المتواضع إلى شهلائنـا و أسرانا الأبطال و مغتربينا و كل حر فلسطيني .

سائلاً المولىى عز وجل أن يوفقتي لمـا يحب و يرضى لكم جميعا أهدي سهري و تتعبي و جهاي

## Dedication

This Project is dedicated to our parents who have been the source of inspiration and motivation all lifelong, and all people who help us. And forever we should give our thanks, obedience and gratitude to our appreciation to:

Palestine Polytechnic University<br>College of Engineering \& Technology<br>Electrical \& Engineering Department<br>Our supervisor Dr. Sameer Khader

## ABSTRACT

Spinal cordinjuries and other local injuries often lead to peripheral paralysis, while the brain stays fully functional. When this peripheral paralysis occurs in the hand, these individual are not able to execute daily activities on their own even if their arms are functional.

To remedy this problem, design an exoskeleton needs to assist paralyzed individuals. The exoskeleton's movements are controlled by the user's available electromyography(EMG) signals, a new control technique will developments to allow for a natural reaching and facilitator sequence by the natural residual muscle activation patterns.

But the signal need to purity and enlarge before entering to microcontroller, then run the motor to controlling exoskeleton.

اصـاباتالحبلالشو كيو إصـاباتمحليةأخرى عندمايحدثهذالالثلالطر فيفيلليد،فإنتلكاليدتصبحغير قادرةعلىتنفيذالأنشطة|ليو ميةمنتلقاءنفسهاحتىلو كانت

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& \text { البيتالخارجييتم التحكمبهامنخلالإشارةكهربائية (EMG signals), } \\
& \text { تقنية الجديدة يتم بناؤها ها } \\
& \text { طبيعيوتسلسلميسر الطبيعية|الفعالةةلمتبقبة. } \\
& \text { يهو تكبيرقبلالدخو لالىالمتحكمالدقيق } \\
& \text { ثمتشغيلالمحرك تيتقومبالتحكمفيالبيتالخارجيلاليد. }
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## Ab6reviation Table

| Description | Abbreviations |
| :---: | :---: |
| Electromyography | EMG |
| International Society of Electrophysiological Kinesiology | ISEK |
| Peripheral Nervous System | PNS |
| Central Nervous System | CNS |
| Biceps Muscle | BI |
| Triceps Muscle | TRI |
| Fast Oxidative Glycol tic | FOG |
| Fast Glycol tic | FG |
| Motor Unit Action Potential | MUAP |
| Chlorine lons | Cl- |
| Silver Ions | Ag+ |
| Common Mode Rejection Ratio | CMRR |
| Lower Frequency | FL |
| Higher Frequency | FH |
| Low Pass Filter | LPF |
| High Pass Filter | HPF |
| Digital to Analog Converter | DAC |
| Variable Reluctance | VR |
| Permanent Magnet | PM |
| Hybrid | HB |
| Microcontroller Family from Renesas Electronics | RX |
| Microcontroller Family from Tenesas Electronics | TX |
| Printed Circuit Board | PCB |

## Chapter One

## General Background

### 1.1 Introduction

### 1.2 Project Aim

1.3 Literature Review
1.4 Project main component
1.5 Project cost
1.6 Time diagram

### 1.1 Introduction

Not a small Percentage of people out of our Palestinian society have a weakness in one of limbs that happened by some congenital reasons or kind of accidents or was done on the hand Israeli occupation in what it does against our Palestinian nation, and out of this case it is a part of our duty in order to help them doing their daily actions normally, and now we will go to the mechanization of doing this project.

Electromyography is a technique for evaluating and recording the electrical activity produced by skeletal muscles. EMG is performed using an instrument called an electromyography, to produce a record called an electromyography.

An electromyography detects the electrical potential generated by muscle cells when these cells are electrically or neurologically activated. The signals can be analyzed to detect medical abnormalities, activation level, and recruitment order or to analyze the biomechanics of human or animal movement.

EMG signals are not easily observed as they are weak signals in range of 1100 mV ,so an EMG signal needs to be amplified by an amplifier specifically designed to measure it in order to be observed. The EMG signal is picked up by electrodes and then amplified. Generally more than one amplification stages as necessary in order to eliminate the low and high frequency noises or the other factors that can affect the output data.

EMG signal accuracy is dependent on many parameters such as electrodes number electrode placement, electrode orientation, electrode type, inter-electrode distance, skin preparation, skin and electrode gel temperature, subcutaneous fat between the electrode and muscle. The EMG signal is used for much application such as control computers and other devices.

In our project the EMG signals are tried to use for controlling of a simple hand-shaped gripper with a microcontroller interface, as shown in figure (1.1).


Figure (1.1):- The General Block Diagram.

### 1.2 Project Aim

The proposed project aims at design an artificial hand (limb) by using and processing muscle signals...

### 1.3 Literature Review

Francesco Redi (1626-1698)
First to recognize connection between muscles and generation of electric 1666-documented that electric ray fish used a highly-specialized muscle. [1] Alessandro Volta (1745-1827)

Developed a device which produced electricity,which could be used to stimulate muscles, invented the first electric battery. [1]

## Luigi Galvani

Credited as the father of neurophysiology for his similar work with frogs' legs-1791.

Showed that "electrical stimulation of muscular tissue produces contraction and force. [1]

## Carlo Matteucci (1820-1845)

In 1838, Matteucci used one to show that bioelectricity is connected with muscular contraction.

1842 - Demonstrated the existence of the action potential accompanying a frog's muscle. [2]

## Guillaume Duchenne (1806-1875)

1850 - Applied electric stimulation to intact skeletal muscles Interested in medical electricity for therapeutic purposes. Systematically mapped out functions of nearly every facial muscle Knowledge of EMG developed as fast as technology could keep up. [2]

The term electromyography comes from Etienne Marey, who modified Lippman's capillary electrometer (1876) as one of his many contributions to kinesiology. [2]

## John Bas 1962

Basmajian compiles all of the known information about EMG. Also created fine - wire electrodes that were more comfortable than needles and could be used longer. The book Muscles Alive_becomes an invaluable tool in the field and is updated through five editions, the last Carlo De Luca. Founded International Society of Electrophysiological Kinesiology, ISEK, in 1965.ISEK worked to create standards for EMG usage and reportingmajian. [2]

### 1.4 Project Main Component

1) Detecting Electrode.
2) Amplifier.
3) Microcontroller.
4) Stepper motor and driving modules.
5) Hand-shaped gripper.

### 1.5 Estimated Project Cost

Table (1.1): Component Cost:

| No. | Description | Price/ NIS |
| :--- | :--- | :--- |
| 1 | Electrodes and Fillters | 200 |
| 2 | Amplifiers | 100 |
| 3 | 4N25 opt-coupler | 5 |
| 4 | LM319D Dual-Comparator | 10 |
| 5 | AD620 Amplifier | 140 |
| 6 | Resistors + Capacitors + Rectifiers | 60 |
| 7 | 2 Arduino + shield | 400 |
| 9 | Darlington Transistors | 50 |
| 10 | 5 servo motors | 1100 |
| 11 | 5 Flex Sensors | 500 |
| 12 | 2 Xbee module S1+ shield | $500+100$ |
| 13 | DC Motor for hand + Drive Circuit | 400 |
| 14 | 2 Gears | 150 |
| 15 | design lathing (Exoskeleton) | 1500 |
| 16 | Hand - shaped Gripper (polyethylene) | 1400 |
| 17 | Other materials | 300 |
| 18 | Paint | 400 |
|  | Total | 7315 |
|  |  |  |

### 1.6 Time Diagram

Table (1. '): Time line ' of The Project:

| Weeks <br> Tasks | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Literature review and <br> problem statement |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Table (1.3): Time line 2 of The Project:

| Weeks <br> Tasks | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Starting <br> implementation of the <br> mechanical design |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Purchasing the <br> components |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Assembly the electrical <br> and mechanical part |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Testing and calibration |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Typing the final report |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Report submission and <br> preparing the project <br> presentation |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Chapter Two

## Structure Background

2.1 Anatomy of the Human Forearm
2.1.1 Neurons (Nerve Cells)
2.1.2 Reflex Arc (Nervous System in Action)
2.1.3 Antagonistic Muscles
2.2 Muscle Fibers
2.3 Optimal Electrode Placement
2.4 Skin Preparation and Electrode Placement
2.5 Normalizing the Electrodes

### 2.1 Anatomy of the Human Forearm

Initially, we talk about the Peripheral Nervous System (PNS), which is the other part of the nervous system. The main task of the PNS is to detect stimuli and send impulses to the CNS according to the stimuli. The PNS is made of receptors and nerves that carry the impulses. Receptor cells are ones whose function is to detect something about its environment.

There are many receptors in the body that are able to detect many changes like temperature, touch, light, sound and chemicals. There are some organs in the body that are there to detect just one stimulus, like the eye for example. These are called sensory organs and they can be defined as a group of receptor cells responding to specific stimuli.

Effectors are the opposite of receptors. Receptors are two detect the stimuli while effectors are two respond to it. Effectors are usually muscles and glands.

### 2.1.1 Neuroses (Nerve Cells)

Neuroses are one of the most important structures of the nervous systems. Neuroses act as a wire that transmits electrical impulses all over the body. Like a cable that consists of many wires, a bundle of neuroses is called a nerve. There are 3 types of neuroses; each type is to transmit electrical impulses from a specific place to another.

## 1) Motor Neuroses :-

This is a neurosis that transmits electrical impulses from the Central nervous system to the effectors, as shown in figure (2.1).


Figure (2.1):- Structure of Motor Neuroses. [4]

The Neuron is made up of three segments; the cell body which is the start of the motor Neuron and is in the CNS, axon which stretches out from the cell body all the way to end of the neuron, and the motor plate which is the end of the Neuron and is in the Effectors muscle.

Neurons have features that are common between most animal cells like a nucleus, cymiddlelasm and cell surface membrane, but they also have some exclusive features like the axon. The axon is an extended cymiddlelasm thread along which electrical impulses travel. Some motor neurons have axons of length 1 meter. Axons are coated by a layer of myelin called myelin sheath; this is an electrically insulating layer which is essential for the proper functioning of the nervous system.

Another exclusive feature of neurons is dendrites; these are several short threads of cymiddlelasm coming out of the cell body. Their function is to pick up electrical impulses from other cells.

The last exclusive feature of motor neurons only is motor end plate. This is just the end of the axon which is in the muscle. It passes the electrical impulses from the neuron to the muscle fibers.

## 2) Sensory Neuroses :-

Like other neurons, sensory neurons carry electrical impulses from one place to another. But sensory neurons carry electrical impulses in the direction different to that of motor neurons, from the receptors to the CNS, as shown in figure (2.2).


Figure (2.2):- Structure of Sensory Neuroses. [4]

## 3) Relay Neurons :-

Relay neurons are located in the CNS. Their job is to pass electrical impulses from the sensory neuron onto the motor neuron, so it acts like a diversion, as shown in figure (2.3).


Figure (2.3):- Structure of Relay Neuroses. [4]

### 2.1.2 Reflex Arc (Nervous System in Action)

Where neurons meet, they are not actually touching each other. Instead there is a gap called synapse or junction box. When the electrical impulses reach the end of a neuron, the neuron secretes a chemical transmitter which passes by diffusion to the other neuron causing the impulses to be carried from the first neuron to the second.

If your finger touches a hot surface, receptor cells in the skin of your finger detect a stimulus, which is a sudden rise in the temperature. The receptor uses the energy of the stimulus to generate electrical impulses. These impulses are then carried by the axons of the dendrites of the sensory neuron through cell body to axon and from the axon to the CNS. At the CNS the electrical impulses travel through the synapse to the relay neuron, which passes it onto the motor neuron. The nerve impulses are transmitted through the axon of the motor neuron to the targeted muscle which contracts when electrical impulses reach it, resulting in your finger being pulled away from the hot surface, as shown in figure (2.4).

This pathway is called the reflex arc and happens in about a fraction of a second.


Figure (2.4):- Reflex Arc: Receptor $\rightarrow$ Sensory Neuron $\rightarrow$ CNS $\rightarrow$ Motor Neuron $\rightarrow$ Effectors. [5]

### 2.1.3 Antagonistic Muscles

We have just learned that in order for the pupil to get narrower or wider, two muscles work simultaneously, when one contracts the other relaxes. Pairs of muscles like that are called antagonistic muscles.

The most known antagonistic muscle pair is the biceps and triceps of the arm. The bi and the tri for short; they are what cause the movement of the arm. They work simultaneously to bend or straighten the arm. The biceps is located in front of the humerus bone of the upper arm. The biceps is joined to the radius bone of the lower arm and the triceps is joined to the ulna bone of the lower arm. Muscles are attached to bones by strong fibers called tendons.

And to learn how to deliver the pulse of the muscle, we will address the case of bend and straighten muscle:


Figure (2.5):- The Effect of Bend and Straighten Arm. [6]

When you want to bend your Arm the brain send two electrical impulses, one to the bi making it contract and one to the tri telling it to relax.

To straighten your arm, the brain send electrical impulses to both muscles making the bi relax in order to leave the muscle it is attached to free. The tri contracts and becomes shorter pulling the muscle it is attached to into place and straightening the arm.

As shown in figure (2.5); the biceps can be called a flexor because it flexes (bends) the arm, the triceps can be called an extensor because it extends (straightens) the arm. It is necessary to explain the affected part of the man who will be replaced by another part mechanic to make up the shortfall effectively.

This section will be covered in detail the muscles involved with each finger movement, as shown in figure (2.6).


Figure (2.6):- Structural of Human Arm. [7]

The muscles of interest for determining grasp classification are the extensor muscles, generally located on the posterior side of the forearm. The extensor muscles extend the fingers outward as the grasp initially takes form. It is the proper capture and classification of the EMG signal during this initial movement that enables a real-time classifier to work. The specific extensor muscles involved are the extensor digitorum, extensor pollicis longus, extensor pollicis brevis, extensor indicis, and extensor digiti minimi. The extensor digitorum is responsible for the extension of the finger joints and wrist, and connects primarily to the middle and ring fingers, and secondarily to the index and little fingers. The extensor pollicis longus and extensor pollicis brevis are both responsible for the extension of the thumb as well as abduction at the wrist. The extensor indicis muscle controls both the extension and adduction of the joints of the index finger, while the extensor digiti minimi controls the extension of the joints of the little finger.

The approximate locations of these muscles are indicated, as shown in figure (2.7).


Figure (2.7):- The Approximate Locations of Muscles. [8]

The extensor indicis muscles are actually in the muscle layer below the extensor digiti minimi and extensor digitorum. Naturally, the deeper location of this muscle will have a negative impact on the energy that surface electromyography can detect.

The flexor muscles, generally located on the anterior side of the forearm, are responsible for flexion of the finger joints. For continued grasp control, following the initial classification, the flexor muscles should be monitored with additional electrodes. Ideally, the EMG collected from these muscles would indicate the closing of a grasp, the continued maintenance of a grasp, and the degree of tension used to maintain the grasp, as shown in figure (2.7).

### 2.2 Muscle Fibers

Muscle Fibers are formed during development from the fusion of several undifferentiated immature cells known as myoblasts into long, cylindrical, multinucleated cells. Differentiation into this state is primarily completed before birth with the cells continuing to grow in size thereafter. Skeletal muscle exhibits a distinctive banding pattern when viewed under the microscope due to the arrangement of cytoskeletal elements in the cytoplasm of the muscle fibers.

The principal cytoplasmic proteins are myosin and actin (also known as "thick" and "thin" filaments, respectively) which are arranged in a repeating unit called a sarcomere. The interaction of myosin and actin is responsible for muscle contraction.

## - Functional Properties of muscle fibers :-

1) Peak Force.
2) Contraction velocity.
3) Resistance to fatigue.
4) Actino-myosin ATPase activities.

Four main types are commonly identified, although further sub- group are known. For our purposes, we will focus on the four major types described here:-

1) Fast-twitch fibers - used in Anaerobic Exercise:
(Short, high energy exercise)
a) Two types of Fast - twitch fibers (A and B).
b) Fast-twitch fibers are more glycol tic than Slow-twitch fibers.
c) More explosive.
d) Exercises such as weightlifting and sprinting.

## 2) Fast- twitches fibers:

a) Fast oxidative glycolytic (FOG)- these fibers have plenty of energy and oxygen.
b) Fast and fatigue resistant (maintain force production after many contractions).

## 3) Fast-twitch B fibers:

a) Fast glycolytic (FG)- these fibers have a low oxygen capacity making it hard to complete multiple contractions without rest.
b) Fast and fatigable (high force production but fatigued after only a few contractions).
c) Low oxidative capacity.
4) Slow-twitch fibers- used in Aerobic Exercise (long, constant energy):
a) Red=slow oxidative.
b) More oxidative.
c) Mitochondria (cells power source, gets energy out of glucose in respiration) are bigger and there are more of them.
d) More capillarieo More myoglobin (a protein with oxygen bound to it so that there is an oxygenreserve for long periods of exercise) .
e) Long twitch times, low peak forces, high fatigue resistance.
f) Exercises such as long distance running and bike riding.


Figure (2.8):- Skeletal Muscles Move by Contracting. [9]
Each muscle is composed of tightly packed bundles of muscle Fibers, each containing proteins, which are responsible for muscle movement. Differentiation of muscle cells begins early in embryonic development. Myoblasts (A), the precursors of skeletal muscle cells, fuse together (B), to form multinucleated cells which eventually develop into myofibrils containing contractile fibers (C), as shown in figure(2.8).

After explain that previously, in our project will be the sensory neuron is inoperative, so we will compensated it by take the electrical signal from the motor neuron by using "Electrical stimulation of both sensory and motor nerves", it is used to record the reflex response of the muscle, however by:

1) At low stimulating levels some of sensitive sensory nerves are activated, but the motor nerves are not and hence $\mathbf{M}$ response is not seen. Also AP of the sensory nerves moves to spinal cord and generate reflex response.
2) For moderate stimuli both motor nerves and sensory nerves are stimulated and two responses are seen ( $\mathbf{M}$ and $\mathbf{H}$ ).
3) For large stimuli only $\mathbf{M}$ response is seen, as shown in figure (2.9).


Figure (2.9):- Electrical stimulation of both sensory and motor nerves in low, moderate and high levels.

### 2.3 Optimal Electrode Placement

There are several factors that must be considered and addressed in order to ensure effective EMG signal detection. To receive maximum results from your stimulation, it is important to place the electrodes correctly. Electrodes from the same pair should be placed over the same muscle (surface electrodes must be placed parallel to the muscle fibers).

The optimum placement varies slightly from person to person, so we try moving the electrodes around until you get the most comfortable and effective contractions. There are many company offers different sizes of electrodes. Small electrodes are preferably used on smaller muscles and large electrodes on larger muscles. Before placing the electrodes on your body, be sure to always wash and dry the skin in order to ensure good conductivity. be sure to only place electrodes on healthy skin. And we should never place electrodes closer than 3 cm from each other.

The figure (2.10) shown muscle stimulation, the electrodes placed over or nearby the painful area.


Figure (2.10):- Muscle Simulation. [10]

### 2.4 Skin Preparation and Electrode Placement

In order to minimize the impedance between the electrode-skin contacts, recommends that the skin surface be shaved of any hair and dead skin cells at the target location. Dry shaving works well for removing the dead skin cells. Once shaved, the skin should be cleaned with alcohol and allowed to dry before the electrodes are placed, as shown in figure (2.11).

Then, to ensure that the electrode is in the correct location, first secure the body reference electrode to the subject's wrist, on the anterior side. Then, using Siriprayoonsak's EMG Capture Program or the Establish Grasp Power procedure in the Real-Time EMG Classifier, test various positions around the target muscle area while performing a hand extension action with the corresponding muscle. The goal is to find the location that produces the greatest energy (highest amplitude) during activity and the least energy (noise) while in a rest position.


Figure (2.11):- Correct Location Test. [11]

### 2.5 Normalizing the Electrodes

The voltage potential of the EMG signal detected by the electrodes strongly depends on several factors, varying between individuals and also over time within an individual.

Thus, the amplitude of the EMG itself is not useful in group comparisons, or to follow events over a long period of time. The fact that the recorded EMG amplitude is never absolute is mainly due to the fact that the impedance varies between the active muscle fibers and electrodes and is unknown therefore, when comparing amplitude variables between measurements, normalization of some kind is required, and i.e. the EMG converted to a scale that is common to all measurement occasions.

Normalizing the signal amplitude with respect to force or torque is a commonly used technique. Typically, the EMG is related to a maximal contraction, or a sub maximal contraction at a known level of force.

## Chapter Three

## System Components

### 3.1 Hand System

### 3.1.1 EMG System

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### 3.1 Hand System

### 3.1.1 EMG System

### 3.1.1.1 The Nature of EMG Signal

Our muscles cause our body parts to move through contraction and relaxation. Each muscle consists of many muscle fibers, which range in length from a few millimeters (mm) to about 30 centimeters and have a diameter of between 10 and 100 micrometers. The muscle fibers will shorten to about $57 \%$ of their resting length during contraction. All of the muscle fibers making up a particular muscle do not contract simultaneously; rather, small groups of muscle fibers contract and relax together, as directed by their motor unit. The motor unit is the fundamental building block of an EMG signal. It consists of a motor neuron, its axon, and all of the muscle fibers that it controls. Countless motor units provide the pathway from the central nervous system to muscle fibers. However, individual motor units vary by size and by the number of muscle fibers that they innervate, from a few to over a thousand. Additionally, the innervated muscle fibers of multiple motor units are randomly intermingled (see Figure 3.1), meaning that a portion of a muscle may contain fibers belonging to between 20 and 50 different motor units.


Figure (3.1): Depiction of Two Motor Units Controlling Intermingled Muscle Fibers.[12]

Just prior to muscle contraction and the application of force, an increasing number of motor units are recruited for muscle activation. The motor units are typically recruited according to their size, beginning with the smaller motor units first. The exchange of ions across the muscle fibers innervated by the recruited motor units results in small electrical currents, which combined for a particular motor unit is referred to as the motor unit action potential (MUAP) .The aggregate electric signal generated from all of the MUAPs in a detected area is referred to as the myoelectric signal, a recording of which is called an
electromyogram (EMG). Note that this signal propagation precedes muscle.
Motion with about 10 to 100 mS . This 100 mS lead helps to minimize the length of the EMG signal is used to the hand grip, which is essential for the success of a real-time classifier and prosthetic hand control skeletal muscles contributes to the weight of the body, the skeleton classify muscle can rotating directly fastened by means of a joint, and the striated muscle to a bone or by means of tendon. Two or more groups of the skeletal muscles working against each other (s) extends . The skeletal muscle is composed of poly - nucleus cells. Action potential propagates from motor nerve to the muscle fibers controlled by the nerves, will cause and start after molecular mechanism. An immediate increase of calcium ions into the muscle cell reproduction After Identifying the nature of the EMG signal and their relationship with the motor unit, now we will talk about the EMG signal collection for Determined the amplitude and frequency of the discharge electrical muscle, and identify the factors All which depend on the quality of the EMG signal.

### 3.1.1.2 EMG Signal Collections

The basic component of skeletal muscle is the motor unit, which can be activated consciously. A number of the motor units construct a so-called muscle fiber (as explained previous in the second chapter). When a single motor unit (SMU) is activated by stimulation, a potential waveform with amplitude of $20-2000 \mu \mathrm{~V}$, a discharge frequency of $6-30 \mathrm{~Hz}$, and an interval of $3-10 \mathrm{mS}$ is observed. Thus, contraction of muscle fibers leads to a potential signal with larger amplitude and higher frequency.

It is electromyogram (EMG) as explained previous in chapter two. The motor unit regulates the fiber of skeletal muscle. Therefore, when a motor nerve is excited, the fibers controlled by this motor unit will all be activated. This process includes the production of action potential and contraction of muscle fibers. A single piece of muscle may be probably by hundreds of motor units. The nervous system makes an attempt to control different degrees of muscle activities by means of
Stimulating diverse numbers of motors units. More the motor units are excited; more the muscle fibers are activated.

The quality of an EMG signal is subject to several factors, including:

1) Timing and intensity of muscle contraction.
2) Distance of the electrode from the target muscle area.
3) Properties of the tissue overlying the muscle, skin thickness, and fatty tissue.
4) Properties of the electrodes and the amplifier.
5) Quality of the contact between the skin and electrode, including stability.

The first factors, timing and intensity of muscle contraction, encompass the data that we want to quantify and classify for each of the muscles involved in making a particular hand grasp. It is the changes in these factors that make distinguishing hand grasps using an EMG signal possible.

Naturally, the distance between the electrode and the target muscle area impact the quality of the EMG signal. Understanding the human anatomy and proper electrode placement, covered in sections 2.1 and 2.3, respectively, will help to minimize this distance.

There are several properties of the muscle and surrounding tissue that affect the EMG signal. The muscles are surrounded by extracellular fluid, fatty tissue, and skin, which cause inflections in the current field and varying levels of impedance.

Skin tissue has greater impedance than muscle tissue and therefore acts as a filter for the signal. With increasing tissue between the electrode and the target muscle, the amplitude of the EMG signals drops precipitously. Subjects with thicker skin or greater body-fat percentage will have more of the signal filtered before reaching the electrode, making proper electrode placement significantly more critical for those individuals. Muscle tissue impedance is directionally dependent, which also affects electrode placement.

Some studies have shown 7 to 10 times greater impedance levels in measurements taken perpendicular to the muscle fibers versus measurements taken in the parallel direction. The muscle tissue can also be affected by biochemical changes, which impact the conduction velocity of the muscle fibers and filtering properties of the muscle tissue. Biochemical changes occur over multiple sessions and even during the same session, to some degree. Ensuring a large training set and maintaining consistent electrode placement should mitigate some of these challenges. The properties of electrodes and amplifiers affecting the quality of the signal are addressed in detail in the next two subsections, while the quality of the electrode to skin contact is addressed in section.

After identifying that, will go to talk about electrodes, the identification of any kind of electrode kinds and the electrodes suitable location.

### 3.1.1.3 Surface Electrodes

Human body consists of numerous liquid cells which contain different electrolyte ions. The intracellular liquid includes ions of potassium, sodium and chloride. Action potential comes from the variations of ion concentration. When an electrode is used to detect action potential, the so-called interface potential will be generated. Imagine, when a metal electrode touch certain electrolyte solution, two kinds of chemical reactions will simultaneously occur. One is oxidation reaction in which metal atoms will release electrons and become metal ions.

The order is reduction reaction in which electrons and metal ions will be combined together and become metal atoms. In the interface between metal and electrolyte liquid, the ions with positive and negative charges will move in an opposite direction and produce two ions layers with opposite electricity. The potential difference between two ion layers is called interface potential. Immersing different between metals into electrolyte liquids will lead to different levels of interface potential.

Thus, for measuring biological signals, it is necessary to choose a metal with low interface potential as an electrode material. This can avoid the excessive interface potential during measurement. In general, the biological signal range is from $50 \mu \mathrm{~V}-1 \mathrm{mV}$ and the interface potential of metal is in the range of $0.1-1 \mathrm{~V}$. Additionally, the interface potentials of electrodes vary with time.

There are two types of electrodes used in the recording of the EMG signals; surface electrodes and needle electrodes.

While needle electrodes are inserted through the skin into the muscle tissue, surface electrodes are placed on the surface of the skin. In this project, surface electrodes $(\mathrm{Ag} / \mathrm{AgCl})$ are used as they are easy to use and can be applied without pain. Surface electrodes come in many varieties mostly characterized by number of contacts, as figure (3.2). Nowadays silver-silver chloride $(\mathrm{Ag} / \mathrm{AgCl})$ is the most used material for the production of electrodes. This kind of electrode is principally made by silver. There is a thin layer of AgCl formed by the contact between silver and electrolyte solution. And AgCl provides silver ( Ag ) and chlorine ( Cl ) ions a bi-directional exchange.

The detected amplitude normally ranges up to 5 mV for surface electrodes and up to 10 mV when using needle electrodes .The cut-off frequency of the surface electrodes vary from 10 to 1000 Hz . As the signals obtained are too low, noise is a big problem and it must be considered in the design of the system.

The motion artifact in the electrode skin interface is one of the reasons of noise caused the electrodes, which has frequencies $0-10 \mathrm{~Hz}$. The use of high-pass filtering, shielded cables, carefully taping to reduce cable movement and mounting the amplifier near the electrodes can minimize this effect.

The electrode placement and location has a big importance in the EMG recording, surface electrodes must be placed parallel to the muscle fibers. The skin must be cleaned and electrode conducting jell must be used for better results. Reference electrodes must be used near the bony parts.


Figure (3.2): Surface Electrodes. [13]

### 3.1.1.4 Noise and Artifacts

EMG recording can be interference by noise from different sources, not only by the noise from the bioelectric generator or active cell but also from the electrical fields that occur around lead cables and electrode.
Electrical fields such as power lines, computer monitors, transformers, or even EMG amplifier itself might cause noise that wills interference the signal. Because of the electronic components acting as antennas, recording devices, ambient noises, motion artifacts the design of the amplifier should have been designed considering the noise factors.

Ambient noise can be generated from any electric device that crates electromagnetic field. The ambient noise cannot be avoided, it occurs primarily between the $50-60 \mathrm{~Hz}$ band.

Two of the important parameters in bioelectric amplifiers are noise and drift. Drift is the change in output signal voltage due to changes in operating temperature and noise, in this case, is the thermal noise generated in resistances and semiconductor devices. Instrumentation amplifier is used in the pre-amplification stage of the project to perform the crucial differential signal combination and it is the solution to both high-gain and high-input impedance prop-lems. Instrumentation amplifier consists of three operational amplifiers; two non-inverting followers as input amplifiers followed by a differential amplifier. [14]

### 3.1.1.5 EMG Implementation

At the end of this section we want to get out with the implementation full of the EMG system so that it has the surface electrodes (explained previously), pre-amplifier, isolation circuit, band-reject filter, band-pass filter, gain amplifier, half-wave rectifier, integrator and buffer circuit.

### 3.1.1.5. 1 Pre-Amplifier

This pre-amplifier uses a two non-inverting amplifier and a typical differential amplifier circuit, which contains two inputs (positive input and negative input). The differential amplifier circuit subtracts two inputs and amplifiers the difference, as shown in Figure (3.3).

To get the right level of the input signal, we need a body reference circuit which works as a feedback from the inputs. Whenever the body temperature changes or signal changes due to noise introduced by the body, this body reference will help maintain the correct level of signal. In each input channel, there is one body reference feedback.


Figure (3.3):- Pre-Amplifier Circuit.
We will replace this circuit by electronic piece called AD620, because it Easy to use, low noise, high CMRR, and high $\mathrm{Z}_{\text {in }}$, and high accuracy that requires only external resistor to set the gain of circuit, as shown in Figure (3.4).


Figure (3.4):- AD620 Implementation. [15]

### 3.1.1.5.2 Optical Isolation Circuit

An isolation amplifier (also called a unity-gain amplifier) is an op-amp circuit which provides isolation of one part of a circuit from another, so that power is not used, drawn, or wasted in a part of the circuit the purpose of isolation amplifier isn't to amplify the signal. The same signal that is input into the op amp gets passed out exactly the same. This means that output voltage is the same exact as the input voltage.


Figure (3.5):- Isolation Amplifier Circuit.
Figure (5.3) illustrates a little current from the power source above. Because the op amp has such high impedance, it draws very little current. The first part of the circuit, then, is undisturbed, and, thus, is isolated from the second part of the circuit. The op amp serves as an isolation device so that practically no current gets drawn and transferred to the second part of the circuit (circuit after the op amp), because its impedance is so high. Isolation amplifiers serve as buffers. They do not amplify signals but serve to isolate parts of circuits or different circuits from each other.

In our circuit, it is Optical connection between the pre-amplifier and the band-reject filter ( $\mathrm{A} v=1$ ).
The isolation is completed by an optical method:

- Optically coupled.
- Electrically isolated.

We will use in our project opt-coupler isolation (4N35), the functional block diagram as shown in figure (3.6).


Figure (3.6):- Functional Block Diagram of The Opt-Coupler (4N35). [16]

### 3.1.1.5.3 Band-Reject Filter

Also called band-elimination, band-stop, or notch filters, this kind of filter passes all frequencies above and below a particular range set by the component values to neglect the wire noise. Not surprisingly, it can be made out of a low-pass and a high-pass filter, just like the band-pass design, except that this time we connect the two filter sections in parallel with each other instead of in series, as figure (3.7).


Figure (3.7):- System Level Block Diagram of a Band-Reject Filter.

Band rejection filters are used when relatively wide band of frequencies need to be rejected, is the opposite of a band-pass filter, as in figure (3.8).


Figure (3.8):- Band-Reject Filter Frequency Response. [17]

### 3.1.1.5.4 Band-Pass Filter

Used in electronic systems to separate a signal at one particular frequency or a range of signals that lie within a certain "band" of frequencies from signals at all other frequencies. This band or range of frequencies is set between two cut-off or corner frequency points labeled the "lower frequency" $(f \mathrm{~L})$ and the "higher frequency" ( $f \mathrm{H}$ ) while attenuating any signals outside of these two points.

### 3.1.1.5.4.1 Second-order Low Pass Active Filter circuit

- Determines the cut-off point for high frequencies.
- The voltage gain and cut-off frequency equal:

$$
A_{V}=1+\frac{R_{2}}{R_{1}} \quad F_{C}=\frac{1}{2 \pi * \sqrt{R_{3} R_{4} C_{1} C_{2}}}
$$



Figure (3.9):- Second-Order Low Pass Active Filter Circuit.
Second-order (two-pole) active filters are important because higherorder filters can be designed using them. By cascading together first and second-order filters, filters with an order value, either odd or even up to any value can be constructed. In the next tutorial about filters, we will see that Active High Pass Filters can be constructed by reversing the positions of the resistor and capacitor in the circuit.

### 3.1.1.5.4.2 Second-order High Pass Active Filter Circuit

Determines the cut-off point for high frequencies
The voltage gain equal: $A_{V}=1+\frac{R_{2}}{K_{7}}$
Cut-off frequency equal :

$$
F_{C}=\frac{1}{2 \pi * \sqrt{R_{3} R_{4} C_{1} C_{2}}}
$$



Figure (3.10):- Second-Order High Pass Active Filter Circuit.
Active Band Pass Filters can be constructed by cascading together a high pass and a low pass filter. Simple Active Band Pass Filter can be easily made by cascading together a single Low Pass Filter with a single High Pass Filter as shown in figure (3.11).


Figure (3.11):- Active Band Pass Filters Construction.

The cut-off or corner frequency of the low pass filter (LPF) is higher than the cut-off frequency of the high pass filter (HPF) and the difference between the frequencies at the -3 dB point will determine the "bandwidth" of the band pass filter while attenuating any signals outside of these points. One way of making a very simple Active Band Pass Filter is to connect the basic passive high and low pass filters we look at previously to an amplifying opamp circuit as shown in figure (3.12).


Figure (3.12):- Active Band Pass Filter Circuit.
This cascading together of the individual low and high pass passive filters produces a low "Q-factor" type filter circuit which has a wide pass band. The first stage of the filter will be the high pass stage that uses the capacitor to block any DC biasing from the source. This design has the advantage of producing a relatively flat asymmetrical pass band frequency response with one half representing the low pass response and the other half representing high pass response as shown in figure(3.13).


Figure (3.13):- Band-Pass Filter Response.

The amplifier also provides isolation between the two stages and defines the overall voltage gain of the circuit. The bandwidth of the filter is therefore the difference between these upper and lower -3dB Points. The normalized frequency response and phase shift for an active band pass filter will be as shown in Figure (3.14).

## - Active Band Pass Frequency Response:

The passive tuned filter circuit will work as a band pass filter, the pass band (bandwidth) can be quite wide and this may be a problem if we want to isolate a small band of frequencies. Active band pass filter can also be made using inverting operational amplifier. So by rearranging the positions of the resistors and capacitors within the filter we can produce a much better filter circuit as shown below. For an active band pass filter, the lower cut-off -3 dB point is given by $f \mathrm{C} 2$ while the upper cut-off -3 dB point is given by $f \mathrm{C} 1$.


Figure (3.14):- The Normalized Frequency Response and Phase Shift for an Active Band Pass Filter. [18]

### 3.1.1.5.5 Gain Amplifier

Gain amplifier is as a non-inverting amplifier, such that; the output voltage changes in the same direction as the input voltage. that the noninverting input of the operational amplifier will need a path for DC to ground; if the signal source might not give this, or if that source requires a given load impedance, the circuit will require another resistor - from input to ground. In either case, the ideal value for the feedback resistors (to give minimum offset voltage) will be such that the two resistances in parallel roughly equal the resistance to ground at the non-inverting input pin, as in figure (3.15). we will use the gain amplifier, because through change a gain of it. We get the output needed.


Figure (3.15):- Gain Amplifier Circuit. [19]

### 3.1.1.5.6 Half-Wave Rectifier

After that we need only take the positive wave of the signal, so we will use the half-wave rectifier. It is also known as a super diode, is a configuration obtained with an operational amplifier in order to have a circuit behave like an ideal diode and rectifier, it is useful for high-precision signal processing.

When the input is positive, it is amplified by the operational amplifier which switches the diode on. Current flows through the load and, because of the feedback, the output voltage is equal to the input voltage.

When the input is greater than zero, D1 is OFF and D2 is ON, so the output is zero because one side of $R_{2}$ is connected to the virtual ground, and there is no current through it. When the input is less than zero, D1 is ON and D 2 is OFF , and the output is like the input with an amplification of $-R_{2} / R_{1}$. This circuit has the benefit that the op-amp never goes into saturation, as shown in figure (3.16).


Figure (3.16):- Half-Wave Rectifier Circuit. [20]

### 3.1.1.5.7 Dual-Comparator

After that we will have two signals, one coming from a biceps muscle and other from a triceps muscle, enter each one to the different comparator by using dual-comparator, such that, When reach the signal from the biceps muscle, go out signal from the first comparator to move the motor, but when reach a signal from the triceps muscle, go out signal from the second comparator to reverse the motor rotation. In other word (how move the hand, moves the motor). We will use in our project (LM319D) dual comparator, The LM319 is a dual high speed voltage comparator designed to operate from a single +5 V supply up to $\pm 15 \mathrm{~V}$ dual supplies, as shown in figure (3.17).


Figure (3.17):- LM319D (Dual-Comparator) Implementation. [21]

### 3.1.1.6 Block Diagram of completed EMG System

After identified all previously, now we will be show the block diagram of completed EMG system, as in Figure (3.18).


Figure (3.18):- Block Diagram of The Completed EMG System.

### 3.1.2 Motor Drive

After getting the electrical signal from the hand muscle for either contraction or diastole by an EMG device, as explained previously, introduced this signal to the microcontroller (Arduino) for control movement motor is installed on the side arm hand. So, that if the signal is outside of the bi muscle; motor rotates counter clock wise to contraction of hand, else if the signal is outside of the tri muscle, motor rotates clock wise to diastole of hand.

We used DC motor type of power window LH as shown in figure (3.1 ), Where we will design it in order to get moves 90 degrees and this movement is very suitable for the movement of the hand, it also has high torque approximately $30 \mathrm{~kg} . \mathrm{cm}$, speed of about 85 RPM , size of acceptable and needs to be fed by a 12 V .


Figure (3.19):- Power Window Motor LH.[22]

### 3.2 Fingers System

In previous chapters, we have able to move the infected hand using the EMG signal that taken from the bi and tri muscles by a surface electrodes, But in order to take fingers signals from the muscles is so difficult and need to use a needle electrodes, and that need to surgery under the supervision of a doctor, and this is not available, to avoid this problem, we find a solution, which is take the fingers signals from the other right hand.

And we did it by installed a five flex sensors on the all fingers of the other right hand, when move this fingers will result from this sensors five signals, enter to the microcontroller to processing this signals as character and through serial pin in arduino. And to avoid contact wires in the hands of the patient and provide freedom of movement for him, we will use a wireless transfer data xbee module using a zigbee's technique . then uploading a code from first arduino to sending Xbee module, Which will be sending this code to receiving Xbee module installed on the infected hand through wireless characteristic, connect this Xbee module with other arduino to enter this code to it. And therefore, this code will move the servo motor as required. Now will recall all the pieces used full characteristics and principles operation each and explain why we used in detail.

### 3.2.1 Flex Sensor

Flex sensor are sensors that change in resistance depending on the amount of bend on the sensor, they convert the change in bend to electrical resistance - the more the bend , the more the resistance value .

The working principle as follows : the flex sensor are analog resistors they work as variable analog voltage dividers, inside the flex sensor are carbon resistive elements within a thin flexible substrate. More carbon means less resistance when the substrate is bent the sensor produces a resistance output relative to the bend radius . as shown in figure (3.20)


Figure (3.20):- Flex Sensors.[23]

The impedance buffer in the Basic Flex Sensor Circuit is a single sided Operational Amplifier, used with these sensors because the low bias current of the Op-Amp reduces error due to source impedance of the flex sensor as voltage divider, as shown in figure (3.21).


Figure (3.21) :- Basic Flex Sensor Circuit.

After fixed this flex sensors on the other right hand finger, we have become a five analog signals from the five fingers, and we connect after each flex sensor resistance of 1 K for protection, then we will use are as an analog inputs to the first microcontroller, as shown in figure (3.22).


Figure (3.22):- How to Connect The Flex Sensor With a Microcontroller.

### 3.2.2 Arduino Uno

The Arduino Uno is a microcontroller board based on the ATmega328. It has 14 digital input/output pins (of which 6 can be used as PWM outputs), 6 analog inputs, a 16 MHz ceramic resonator, a USB connection, a power jack, an ICSP header, and a reset button. It contains everything needed to support the microcontroller; simply connect it to a computer with a USB cable or power it with an AC-to-DC adapter or battery to get started, as shown in figure (3.23)


Figure (3.23):- Arduino Uno. [24]

Each of the 14 digital pins on the Uno can be used as an input or output, using pin Mode(), digital Write(), and digital Read() functions. They operate at 5 volts. Each pin can provide or receive a maximum of 40 mA and has an internal pull-up resistor (disconnected by default) of $20-50 \mathrm{~K}$. In addition, some pins have specialized functions:

Serial: 0 (RX) and 1 (TX). Used to receive (RX) and transmit (TX) TTL serial data. These pins are connected to the corresponding pins of the ATmega8U2 USB-to-TTL Serial chip.
External Interrupts: 2 and 3. These pins can be configured to trigger an interrupt on a low value, a rising or falling edge, or a change in value. See the attach Interrupt() function for details.

- PWM: 3, 5, 6, 9, 10, and 11. Provide 8-bit PWM output with the analog Write() function.

SPI: 10 (SS), 11 (MOSI), 12 (MISO), 13 (SCK). These pins support SPI communication using the SPI library.

The arduino is used as the core of the system, it captures analog signals from flex sensors, converts them to digital through the integrated ADC module and do the recognition process by using a lookup table; when the letter is recognized, a corresponding digital value will be sent via the TX pin (integrated serial module) to the XBee transmitter serial module board, by write asuitable code, we will explain it in the next chapters.

### 3.2.3 XBee Module

XBee is a wireless RF module using the wireless communication standard 802.15.4; it has longer range than Bluetooth but lower power consumption than WiFi (802.11). It has a 250 kbps RF data rate. It operates at 2.4 GHz . The XBee modules have sleep modes for extended battery life.

We will use two pieces of the XBee module, one as a transmitter and the last one as a receiver, and now we will explain how to connect are with each other based on the figure (3.24).


Figure (3.24):- System Data Flow Diagram in a UART-Interfaced Environment.

### 3.2.3.1 XBee transmitter

We will connect the first microcontroller with the XBee transmitter, such that; Devices that have a UART interface can connect directly to the pins of the RF module, data enters the module UART through the DI pin (pin 3) as an asynchronous serial signal. The signal should idle high when no data is being transmitted.

Each data byte consists of a start bit (low), 8 data bits (least significant bit first) and a stop bit (high), the serial bit pattern of data passing through the module, as shown in figure(3.25).


Figure (3.25) :- UART Data Packet 0x1F (Decimal Number 31 ) as
Transmitted Through The RF Module. [25]

Serial communications depend on the two UARTs (the microcontroller's and the RF) to be configured with compatible settings (baud rate, parity, start bits, stop bits, data bits). The UART baud rate and parity settings on the XBee module can be configured with the BD and SB commands, respectively.

When serial data enters the RF module through the DI pin (pin 3), the data is stored in the DI Buffer until it can be processed, When the DI buffer is 17 bytes away from being full; by default, the module de-asserts CTS (high) to signal to the host device to stop sending data [refer to D7 (DIO7 Configuration) parameter, CTS is re-asserted after the DI Buffer has 34 bytes of memory available.

Case in which the DI buffer may become full and possibly over flow; if the module is receiving a continuous stream of RF data, any serial data that arrives on the DI pin is placed in the DI Buffer, the data in the DI buffer will be transmitted over-the-air when the module is no longer receiving RF data in the network.

### 3.2.3.2 Xbee Reciever

When RF data is received, the data enters the DO buffer and is sent out the serial port to a second microcontroller, once the DO Buffer reaches capacity, any additional incoming RF data is lost, as shown in the figure (3.26).


Figure (3.26):- Internal Data Flow Diagram. [25]
The second microcontroller will enter it two different inputs, the first one come from EMG device to control the motor movement to move the hand, and the last one come from the XBee receiver module to control a five servo motors to move the fingers.

### 3.2.4 Servo Motors

We have to control the servo motors using the microcontroller, so that when we move the fingers of the other hand right, servo motors moves are allowed to move the fingers of the infected hand also moved a similar right Other Hand.

Where they put the servo motors on the soles of the hand inside the plastic box, and connects with shaft every one of them copper wire is strong and taut dramatically transmission as Hey, connecting joints ferrous mounted on the fingers of the hand infected and in this way we were able to move the fingers of the hand are easy to smooth close to reality, as shown in figure (3.27).


Figure (3.27):- Servo Motor Place in The Design.

We will use servo motor type of high torque - standard size (FS5105B), is a powerful, low-cost, reliable servo for all your mechatronic needs. This servo is able to take in 6 volts and deliver 83.47 oz-in of maximum torque at $0.16 \mathrm{sec} / 60^{\circ}$ and Rotation $180^{\circ}$, this is a tough little servo with a standard 3 pin powers and control cable, as shown in figure (3.28).

$1+$
Figure (3.28):- Servo Motor High Torque - Standard Size (FS5105B). [26]

We used servo motors because it contains many advantages such as; a clear torque advantage for servo motors at the high speeds gained by electric actuators, When high speed and high torque is required, a significant edge goes to these type of motors, and A servo motor continuously reads in current position data vs. the commanded position data and provides current to the motor proportional to the degree of error. In summary, the inherent use of an encoder aids the servo motor in its ability to have a position fault error limit, ther clear advantage of using a servo motor is the capability of achieving high speed at relatively high torque values over a much larger amount of time.

The motor can better handle dynamic loading applications. Due to this extended time, a servo motor is capable of providing short bursts of additional torque over the entire speed spectrum of cylinder length. In situations where the load is dynamic, the reserve of torque allows more changing and flexible motion control, a major weakness of servo motors is its cost due to having the complex encoder feedback device in the hardware. All of the performance capability comes at a premium cost.

### 3.2.5 Power Circuit

### 3.2.5.1 Battaries (Power Supplies)

Any project in the electric field of industrial or other, where electronic or electrical pieces need a feed source for the work, these pieces differ in the amount of effort they need.

In our project there are several electric or electronic pieces need to source feed and vary the amount of effort they need, for example to the servo motors need to 5 V and 12 V need amplifiers, microcontrollers also require 5 V and XBee needs 3.3 V , so we choose the battery gives a larger effort our piece and we distribute the voltage on the other pieces by using the voltage dividers to reach the effort required for each piece.

Our project is a exoskeleton of hand for the paralyzed, the paralyzed person can't always stay close to the source of nutrition, so we will use 12 V portable battery, we fix it on the side of the person to facilitate the unimpeded movement, comes with this battery charger for shipment when it will be discharges, as shown in figure (3.29).


Figure (3.29):- Portable Battery 12v DC. [27]

### 3.2.5.2 Voltage Regulators

Regulators provide a power source which remains very close to a fixed value, independent of the load placed on it, provided that the current drawn doesn't exceed the rating of the device, the minimum and maximum output voltage specification for fixed voltage regulators indicated the values which can be expected with variations in load on the device, the same specification for adjustable regulators indicated the range of voltage output which can be achieved through external component.

We used two types of voltage regulators, the first LD1117-3.3 V for the XBee module, and the other is LM1084 5 V for the microcontrollers and the servo motors, as shown in figure (3.30).


Figure (3.30):- Voltage Regulators. [28]

## Chapter Four

## Calculations and Measurements

### 4.1 EMG Device

### 4.1.1 Pre-Amplifier

4.1.2 Optical Isolation Circuit
4.1.3 Band-Reject Filter
4.1.4 Band-Pass Filter
4.1.5 Gain Amplifier
4.1.6 Precise Half - Wave Rectifier Circuit
4.1.7 Dual-Comparator
4.2 Selection the Appropriate Motor and Actuators
4.2.1 Static Analysis
4.2.2 Dynamic Analysis
4.3 Gear Calculation
4.4 Servo Motor Calculation

In this chapter we will calculate every input and output value of the devices to go out with the wanted results, for EMG device and DC motor practically.

### 4.1 EMG Device

### 4.1.1 Pre-Amplifier

The pre-amplifier circuit (Instrumentation amplifier usually with $\mathrm{A} v=10$ ) is used for picking up the unipolar EMG signals.

And we used IC represent this circuit called AD 620, as shown in figure (4.1a+b)


Figure (4.1a):- Pre-Amplifier Circuit
Figure (4.1b):- AD620
 Implementation.

Where $\mathrm{R}_{\mathrm{g}}$ the gain resistance is is used to determine the gain of the amplifier.
$\mathrm{A}_{\mathrm{v}}=\frac{49.4 \mathrm{k} \Omega}{\mathrm{R}_{\mathrm{g}}}+1$
We used gain $\left(A_{v}\right)$ equal 10 , then
$10=\frac{44.4 \mathrm{~K} \Omega}{\mathrm{Rg}_{\mathrm{g}}}+1$

$R_{g}=5.48 \mathrm{k} \Omega$
$\mathrm{R}_{\mathrm{g}}=5.48 \mathrm{k} \Omega$, is used to control in the gain.
So, as tacked previous a potential waveform with an amplitude of $20-2000 \mu \mathrm{~V}$ Then $V_{\text {in }}=20-2000 \mu \mathrm{~V}$, and $\mathrm{Av}=10$.

Then $V_{\text {OUT }}$ of the pre-amplifier $=20-2000 \mu \mathrm{~V} * 10=0.2-20 \mathrm{mV}$. [31]

### 4.1.2 Optical Isolation Circuit

Optical connection between the preamplifier and the band-reject filter ( $\mathrm{A} v=1$ ), as shown in figure (4.2).


Figure (4.2):- Isolation Circuit.
$\mathrm{Av}=1$, then $V_{\text {in }}=V_{\text {ouT }}$
So, $V_{\text {oUI }}=0.2-20 \mathrm{mV}$.

### 4.1.3 Band-Reject Filter

The band-reject filter is used to remove the noise from power line (50 or 60 Hz ).

- If ( $C_{1}=C_{2}, R_{1}=R_{2}, R_{1}=2 R_{3}$ and $\left.C_{3}=2 C_{1}\right)$, as shown in figure(4.3) then :

The center frequency can be calculated by:

$$
\begin{aligned}
& f_{c}=\frac{1}{2 \pi C 1 R 1}=50 \mathrm{~Hz} \\
& \text { Let } \mathrm{C}_{1}=1 \mu \mathrm{~F}=\mathrm{C}_{2} \\
& 50=1 /\left[\left(6.28^{*} 1 \mu \mathrm{~F}\right)^{*} \mathrm{R}_{1}\right] \\
&
\end{aligned}
$$



Figure (4.3):- Band-Reject Filter Circuit. [31]

### 4.1.4 Band-Pass Filter

The op-amp is used to construct an active $2^{\text {nd }}$ order low-pass and high-pass filters. As shown in figure (4.4).


Figure (4.4):- Active Band-Pass Filter Circuit.
In Band-Pass Filter must a $\mathrm{Av}=1.56$, to keep not increasing the noise of the signal.

$$
\begin{aligned}
& A_{v}=\left(\frac{R_{8}}{R_{7}}\right)+1 \\
& 1.56=\left(\frac{R_{8}}{R_{7}}\right)+1 \rightleftharpoons\left(\frac{R_{8}}{R_{7}}\right)=1.56
\end{aligned}
$$

Let $R_{8}=100 \mathrm{k} \Omega$ and $R_{7}=180 \mathrm{k} \Omega$

- The range of the frequency for band pass filter between ( $6-30 \mathrm{~Hz}$ ) so ,

Such that, $F_{C H}=6 \mathrm{~Hz}$ and $F_{C l}=30 \mathrm{~Hz}$.

- Suppose, $\mathrm{C}_{4}=1 \mu \mathrm{~F}$ and $\mathrm{C}_{5}=1 \mu \mathrm{~F}$.

Such that, $F_{C H}=\frac{1}{2 \pi R_{5} C_{4}}$, then :
$6=\frac{1}{2 * 3.14 * 1 \mu F * R_{5}} \longrightarrow \quad R_{5}=26.5 \mathrm{k} \Omega$.

And, $F_{C l}=\frac{1}{2 * \mu * R_{6} * C_{5}}$
Then, $30=\frac{1}{2 * 3.14 * 1 \mu \mathrm{~F} * R_{6}} \leadsto R_{1}=5.3 \mathrm{k} \Omega$.
So, $V_{\text {OUI }}=1.56 *(0.2-20) \mathrm{mV}=(0.312-31.2) \mathrm{mV} .[29]$

### 4.1.5 Gain Amplifier

In this stage we can amplify the signal to any wanted value without any noise, that by use the gain amplifier, as shown in figure (4.5).


Figure (4.5):- Gain Amplifier Circuit.

As shown in figure (5.5), Suppose $R_{1}=100 \mathrm{~K} \Omega, R_{2}=700 \Omega$, then :

$$
A_{v}=\frac{R_{9}}{K_{10}}+1=\frac{100 K \Omega 2}{700 \Omega 2}+1=145
$$

Then, $V_{\text {OUT }}=145 *(0.312-31.2)=(0.045-4.5) \mathrm{V} .[31]$

### 4.1.6 Precise Half-Wave Rectifier Circuit

In this stage, we aim to take the positive part of the signal, so we will use the precise half-wave rectifier, as shown in figure (4.6)


Figure (4.6):- Precise Half-Wave Rectifier Circuit.


Figure (4.7):- Input-output Relationship of Half-Wave Rectifier Circuit.

Assume $R_{11}=R_{12}=1 \mathrm{~K} \Omega$

We used $R_{11}=R_{12}$ until the output voltage is have the same of amplitude for input voltage, then $V_{\text {our }}=(0.045-4.5) \mathrm{V}$. [31]

### 4.1.7 Dual-Comparator

In this stage we want to get 5 v exactly, so we will use a comparator, such that, the value at pin number 4 equal 5 V , and the value at pin number 5 it is the output of the Precise half-wave rectifier circuit, the same thing for the second comparator, as shown in figure (4.8).


Figure (4.8):- LM319D Dual-Comparator Implementation.

Finally, because the output of the precise half-wave rectifier circuit is less than 5 V always, then the output of the EMG System equal 5 V .

### 4.2 Selection the Appropriate Motor and Actuators

For precise calculations of the appropriate motor that being used for moving exoskeleton hand, an analyzes of the forces acting on the arm being conducted in order to choose the motor can able to move this structure. Therefore there is a need to understand the concept of static and dynamics equilibrium and solving related tasks.

While statics is the study of structures at a fixed point in time, dynamics is the study of structures over a period of time. Basically statics describes things that don't move, while dynamics describes things that do some movements. Statics is concerned with moments, forces, stresses, torque, pressure, etc. Dynamics is concerned with displacement, velocity, acceleration, momentum, etc. If we want to calculate and optimize forces generated or required for a moving Exo-skeleton for arm, this chapter has the basics that we will need to understand. It is highly recommended you read the statics tutorial first as this tutorial will build off of it.

When one undertakes an analysis of any human movement, one must take into account a number of forces acting on the system, to simplify the problem for better understanding, a free body diagram is often used. A free body diagram is a stick figure drawing of the system showing the vector representations of the external forces acting on the system. In biomechanics, the system refers to the total human body or parts of the human body and any other objects that may be important in the analysis [32].

### 4.2.1 Static Analysis

The free body diagram as in figure (4.9), showing the vector representations of the external forces acting on the system.


Figure (4.9):- Analysis Forces for The Free Body Figure Diagram of The Arm.

The static case is devoted to systems at rest or moving at a constant velocity. In both of these situations, the acceleration of the system is zero. When the acceleration of a system is zero, the system is said to be in equilibrium. A system is in equilibrium when, as stated in Newton's first law, it remains at rest or it is in motion at a constant velocity. [33]

In translational motion, when a system is in equilibrium, all forces that are acting on the system cancel each other out, and the effect is zero. That is, the sum of all forces acting on the system must total zero. This is expressed algebraically as:
$\sum F_{\text {system }}=0$
$F_{B}-F_{E}-W_{A}-W_{B}=0$
Where:
$F_{B}$ : force resulting of biceps muscles.
$F_{E}$ : force resulting of triceps muscles.
$W_{A}$ : The outcome of the weight of the arm and hand and Exo-skeleton.
$W_{B}$ : An external body weight.

We will design a motor to compensate for the force resulting from the muscles. The force/torque resulting from the motor must be equal the force/torque from the muscles.

- To calculate the force :

The force equals the weight of objects.

## - Weight of the parts:

Table (4.1) Mean Segment Weights Expressed as Percentages \% of Total Body Weight.

| Segment | Males (sample =35) | Females (sample = 73) |
| :--- | :---: | :---: |
| Head | 8.26 | 8.20 |
| Whole trunk | 55.10 | 53.20 |
| Thorax | 20.10 | 17.02 |
| Abdomen | 13.06 | 12.24 |
| Pelvis | 13.66 | 15.96 |
| Total arm | 5.77 | 4.97 |
| Upper arm | 3.25 | 2.90 |
| Forearm | 1.87 | 1.57 |
| Hand | 0.65 | 2.50 |
| Forearm and hand | 2.52 | 2.07 |
| Total leg | 16.68 | 18.43 |
| Thigh | 10.50 | 11.75 |
| Leg | 4.75 | 5.35 |
| Foot | 1.43 | 1.33 |
| Leg and Foot | 6.18 | 6.68 |

## 1) Arm:

Arm mass varies from person to person and depends on the total mass of the human body. We will calculate the weight of the arm based on previous studies by Plagenhoef in 1983 accomplishing that applied on a sample of 37 men and 100 women [34], as table (4.9).

Weight $=$ mass * acceleration of gravity.
We will be assumed the patient is male
And can be calculate as:

## a) forearm :

Let body mass $=76.5 \mathrm{~N}$, then the body weight equal:

$$
\text { Body weight }=76.5 * 9.81=750 \mathrm{~kg} . \quad \mathrm{N} / \mathrm{s}^{2}=750 \mathrm{~N}
$$

The Forearm and Hand weights can be calculate as:
Forearm weight $=1.87 \%$ * total body weight

$$
=0.0187 * 750 \mathrm{~N}=14.025 \mathrm{~N}(\sqrt{2})
$$

## b) Hand :

Hand weight $=0.65 \%$ * total body weight.

$$
=0.0065 * 750=4.875 \mathrm{~N}(\sqrt{ })
$$

## 2) Exo-skeleton and other objects:

Assume; weight $=80 \mathrm{~N}$ ( 』 )

Total force $=$ total weight $=$ forearm weight + hand weight + Exo-skeleton and other objects weight.

Total force $=14.025+4.875+80=98.9 \mathrm{~N} . \quad$ Total mass $=10 \mathrm{Kg}$.
Therefore, you must be the force resulting from the motor greater or equal to the sum of the forces acting on the arm to achieve equilibrium.

$$
F_{M}>=98.9 \mathrm{~N} .
$$

- To calculate the torque :

Torque equals applied force multiplied by the perpendicular distance (R) from the line of action of the force to the pivot point.

To measure the perpendicular distance between the line of action of the force and the pivot point we must identify the length of arm, then we identify the center of mass for arm.

Depending on previous studies by Plagenhoef in 1983 accomplishing that applied on a sample of 37 men and 100 women [25], as tables (4.2+4.3).

## - Length of arm:

## 1) Forearm:

Length of forearm $=0.157 *$ total human length.
Let, total human length $=170 \mathrm{~cm}$.
Then, length of forearm $=0.157 * 170=26.7 \mathrm{~cm}$.

## 2) Hand:

Length of hand $=0.0575 *$ total human length.
Then, length of hand $=0.0575 * 170=9.775 \mathrm{~cm}$.

Table (4.2) Mean Segment Lengths Expressed as Percentages (\%) of Total Body Height.

| Segment | Males (sample =35) | Females (sample = 73) |
| :--- | :---: | :---: |
| Head | 10.75 | 10.75 |
| Trunk (hip to shoulder) | 30.00 | 29.00 |
| Thorax | 12.70 | 12.70 |
| Abdomen | 8.10 | 8.10 |
| Pelvis | 9.30 | 9.30 |
| Upperarm | 17.20 | 17.30 |
| Forearm | 15.70 | 18.00 |
| Hand | 5.75 | 5.75 |
| Thigh | 23.20 | 24.90 |
| Leg | 24.70 | 25.70 |
| Foot | 4.25 | 4.25 |
| Biacromial | 24.50 | 20.00 |
| Bi-iliac | 11.30 | 12.00 |

After identify the length of the forearm and the hand, now we can identify the center mass of each.

## - Center of mass :

Forearm center of mass $=43 \% *$ long of forearm

$$
=0.43 * 26.7=11.481 \mathrm{~cm}
$$

Hand center of mass $=46.8 \% *$ long of hand

$$
=0.468 * 9.775=4.5747 \mathrm{~cm}
$$

Let: - Exoskeleton Length $=36.5 \mathrm{~cm}$.

- Exoskeleton Center of Mass $=18.25 \mathrm{~cm}$.

Table (4.3) Segmental Center of Gravity Locations Expressed as Percentages (\%) of Segment Lengths Measured From The Proximal Ends.

| Segment | Males (sample=7) | Females (sample $=9$ ) |
| :--- | :---: | :---: |
| Head and neck | 55.0 | 55.0 |
| Trunk | 63.0 | 56.9 |
| Upper arm | 43.6 | 45.8 |
| Forearm | 43.0 | 43.4 |
| Hand | -46.8 | -46.8 |
| Pekis | 5.0 | 5.0 |
| Abdomen | 46.0 | 46.0 |
| Thorax | 56.7 | 56.3 |
| Thigh | 43.3 | 42.8 |
| Leg | 43.4 | 41.9 |
| Foot | 50.0 | 50.0 |
| Abdomen and pehis | 44.5 | 39.0 |

Then, total torque $=\Sigma(F * R)=[($ forearm weight $*$ Center of mass for forearm weight $)+($ Hand weight $*$ Center of mass for hand $)+($ Exo-skeleton and other objects * Center of mass for Exo-skeleton and other objects)].

Total torque $=\left[(14.025 \mathrm{~N} * 0.11481)+\left(4.875 \mathrm{~N}^{*} 0.045747\right)+(80 \mathrm{~N} *\right.$ 0.1825)]

$$
\begin{aligned}
& =1.61021+0.2230167+14.6 \\
& =16.43 \mathrm{~N} . \mathrm{m}
\end{aligned}
$$

### 4.2.2 Dynamic Analysis

The above equations only deal with the case where the Exo-skeleton is being held horizontally (not in motion). For the arm to move from a rest position, acceleration is required. To solve for this added torque, it is known that the sum of torques acting at a pivot point is equal to the moment of inertia (I) multiplied by the angular acceleration (alpha). [35]

- To calculate the force acting on the axis:

$$
F_{T}=m_{t} * \alpha * r_{G} \ldots . . . . . . . . . . . . e q u .(1)
$$

To calculate $u$ :

$$
\begin{align*}
& \alpha=\frac{u}{r_{G}} \ldots \ldots . . . . \text { equ.(1.1); but } ; \\
& a=\frac{v}{\tau} . . . . . . . . . . . e q u \cdot(1.2) \tag{1.2}
\end{align*}
$$

We must assume that the values of the time be suitable for moving the hand properly. Then;

Assume:
$\mathrm{t}=5$ second.

To find v :

$$
\mathrm{v}=\frac{l}{t} \text {........... ..equ (1.3); but: }
$$

We will calculate the maximum circular distance traveled round hand.
Then be angle $=90$, so it becomes the length of the circular Arc, as shown in figure (4.10).
$\mathrm{I}=\frac{\pi}{4} r_{G}=\frac{\pi}{4} * 0.182$.

$$
=0.14326 \mathrm{~m} \quad \text {... ... ... sub.in equ(1.3) }
$$



Figure (4.10):- Path Movement of The Arm.

$$
\begin{aligned}
& \mathrm{v}=\frac{1}{\mathrm{t}}=\frac{0.14326}{5}=0.02865 \mathrm{~m} / \mathrm{s} \quad \ldots . . . . . \text { sub.in equ }(1.2) \\
& \mathrm{a}=\frac{\mathrm{v}}{\boldsymbol{t}}=\frac{0.02865}{5}=0.00573 \mathrm{~m} / \mathrm{s}^{2} \quad \ldots \ldots . . \text { sub.in equ(1.1) } \\
& \alpha=\frac{u}{r_{G}}=\frac{0.00573}{0.1825}=0.01341 / \mathrm{s}^{2} \ldots \ldots . . . . . . . \text { sub.in e } q u(1) \\
& F_{T}=m_{t} * u * r_{G}=10 * 0.0314 * 0.1825=0.0573 \frac{\mathrm{~kg} * \mathrm{~m}}{\mathrm{~s}^{2}}
\end{aligned}
$$

Icon Symbols used in equations:
$m_{t}$ : Total mass (hand and forearm and Exo-skeleton).
$\alpha$ angular acceleration.
$r_{G}$ Distance between shaft of motor to force acting on center of mass.
a: Acceleration.
v : velocity .
t : time .
1: The length of a quarter circular arc.

- To calculate the moment caused by the force:

Moment is equal to the output torque of static and dynamic

$$
\begin{aligned}
& \left.\sum M_{G}=I_{G} * \alpha+T_{S} \ldots \ldots \ldots \ldots . . \text { equ( } 2\right) \\
& I_{G}=\frac{m_{t} * l^{2}}{12}=\frac{10 *(0.365)^{2}}{12}=0.111 \mathrm{~kg} . \mathrm{m}^{2} \ldots \ldots \ldots . \text { sub.ï equ(2) } \\
& \sum M_{G}=I_{G} * \alpha+T_{S}=0.111 * 0.0314+16.43=16.4335 \mathrm{~N} . \mathrm{m} \mathrm{~m}
\end{aligned}
$$

Where;
$T_{S}:$ output torque of static analysis.
$I_{G}:$ moment of inertia.

Safety factor: we must add additional torque to the total output torque for safety as equals:

Safety factor $=1.5 *$ total output torque.

$$
=1.5 * 16.4335=24.65 \mathrm{~N} . \mathrm{m}
$$

And to supplement the process of selecting the appropriate DC motor, speed must be determined:

- To find speed:
$n=\frac{w^{*} * 0}{2 \pi} \quad \ldots \ldots \ldots$ equ(3).
$\mathrm{w}=\frac{v}{\tau_{G}}=\frac{0.02865}{0.1825}=0.157 \mathrm{rad} /$ seconde
............. sub. in equ(3).
$\mathrm{n}=\frac{0.15 / * 60}{2 \pi}=90 \mathrm{rps}$
Where:
n : speed of motor in rpm.
w : angular speed .
$\longrightarrow$ The appropriate DC motor speed and torque equal:
Speed $=90 \mathrm{rps}$.
Torque $=24.65 \mathrm{~N} . \mathrm{m}$


### 4.3 Gear Calculation

Motor driven systems usually have optimal motor speeds at which the motor operates with the greatest power and efficiency. These motor speeds are expressed in rotations per minute (RPM) of the motor shaft. In many applications, this optimal motor speed is not the optimal speed (RPM) at which the load should be driven. Gearing is used in the form of differently sized gears. These gears are attached to the motor shaft and load shaft, and are coupled together by intermeshed teeth. This produces a gear ratio, which is a direct measure of the ratio of motor shaft rotational speed to load shaft rotational speed. The gear divided into two parts, a drive gear and driven gear.

A drive gear attached to the motor shaft and a driven gear attached to the load shaft.

## 1) Gear ratio:

- Number of teeth on each gear used in the system:

Gear ratio is determined starting with the drive gear, so it should be noted which gear in the gear load, counting from the drive gear to the driven gear, has what number of teeth, figure(4.11).


Figure (4.11):- Structure of Gear. [36]

And can be calculate as:
Gear Ratio $=\frac{\text { number of teeth for driven }}{\text { number of teeth for drive }}=\frac{12}{8}=1.5$

That means when motor turns 1 time the gear load turns 1.5 time.

## 2) Gear efficiency ( $\boldsymbol{\eta}$ ):

$\eta=\frac{\text { input power }}{\text { output power }}=\frac{\text { input speed*input torque }}{\text { output speed*output torque }}=\frac{w_{1} * p_{1}}{w_{2} * p_{2}}$

Output power $=\eta$ * input power
Assume $\eta=0.8$
Output power $=0.8 * T_{1} * w_{1}$
Output from the previous equations $T_{1}=24.65$ and $w_{1}=0.157$

Output power $=0.8 * T_{1} * w_{1}=0.8 * 24.65 * 0.157=3.1$ watt
After selecting the appropriate DC motor and gear we will link this gear with Exo-skeleton.

### 4.4 Servo Motor Calculation

To calculate the torque load of the finger to select the suitable motor is capable of pulling the finger, was chosen motor is capable of pulling times a pregnancy resulting from the withdrawal of the largest and longest finger, a middle finger in the hand, and thus the rest of the motor is able to pull the finger because the other fingers smaller and shorter than the middle finger, therefore calculations were only for the middle finger of the hand.

For adults, the weight of the middle finger of the hand almost $=150 \mathrm{gm}$, and the distance from the center of mass of the finger to the end of the finger almost $=8 \mathrm{~cm}$.

So, $\mathrm{M}=150 \mathrm{~g}$ and $\mathrm{D}=8 \mathrm{~cm}$, where:-
M :-the weight of the middle finger of the hand. ( Kg )
D:-the distance $b=$ from the center of mass of the finger to the end of it. (m)
T:-torque load of the finger. (N.m)
Then, $\mathrm{T}=\mathrm{M} . \mathrm{D}$

$$
=150 \mathrm{gm} * 8 \mathrm{~cm}=1200 \mathrm{gm} \cdot \mathrm{~cm}=0.012 \text { N.m. }
$$

To a motor can carry a hand when it carry a light load, was double the torque load, then the total load torque $=5 * 0.012=0.06 \mathrm{~N} . \mathrm{m}$.

So were selected servo motors torque is equal 0.34 N.m according to datasheet for it.

## Chapter Five

## Designand Results

5.1 Mechanical Design
5.1.1 Hand Exoskeleton Design
5.1.2 Fingers Exoskeleton Design

### 5.2 Electrical Design

5.2.1 EMG Circuit
5.2.2 Transmitter Circuit
5.2.3 Receiver Circuit
5.3 Codes
5.4 Block Diagram of the Project

Will detailed explanation the work process that has been done as the form of steps.

### 5.1 Mechanical Design

### 5.1.1 Hand Exoskeleton Design

Step 1:- Polyethylene is used for forming artificial arm that resembles natural hand, as shown in figure (5.1).


Figure (5.1):- Forming Artificial Arm Using Polyethylene.
Polyethylene (PE) resins are a general class of thermoplastics produced from ethylene gas. Ethylene gas is derived from the cracking of natural gas feed stocks or petroleum byproducts. Under broad ranges of pressures, temperatures and catalysts (depending PE type), ethylene generally polymerizes to form very long polymer chains, this article is too harsh, when placed in hot water becomes very soft take it out, and shape in any way and after a while takes the desired shape, as shown in figure (5.2).


Figure (5.2):- Polyethylene Plate.

It was also a box of polyethylene, which is a five of servo motors with a specific shape as shown in the figure (5.3), where not inconsistent shafts of this motors with each other.


Figure (5.3):- FixedThe Five Servo Motor in Box That Made of Polyethylene.

After that, dish of sponge on the parties to the pieces to ensure the protection of the patient from scratch, coverage pieces of leather plate to give a form is nice and comfortable to the patient, as shown in figure (5.4).


Figure (5.4):-Pieces of PolyethyleneLeather Covered.
Then we installed a DC motor on the first piece of figure (5.4), and connect the shaft of motor with gear, and connect a gear with another gear installed on the elbow by belt, then connect the second gear with the second piece, as shown in figure (5.5).


Figure (5.5):- Mechanical Design of Hand.

### 5.1.2 Fingers Exoskeleton Design

Was installed the Flex sensors on glove over the fingers of the right hand, as shown in figure (5.6).


Figure (5.6):- Installed The Flex Sensors on The Fingers

Was formed 3 pieces of polyethylene for each finger of the hand, as shown in figure (5.7).


Figure (5.7):- Formed Fingers of Hand Using Polyethylene.

And was installed each piece using the stud to get stretched and removed when needed, and the connection between these pieces by a small spring replace the hinge, as shown in figure (5.8).


Figure (5.8):- InstalledEach Pieces Using Stud.

And each finger has been linked with a servo motorcustom for him using a very strong plastic cord, as shown in figure (5.9).


Figure (5.9) :- Connected The Servo Motors With The Fingers.
Finally, to come up with a complete mechanical design of the project, as shown in figure (5.10).


Figure (5.10):- Complete Mechanical Design of Exoskeleton.

### 5.2 Electrical Design

The electrical design of the project was built in 3 circuits, and these circuits have been designed using proteus 8 professional program, these circuits are:-

### 5.2.1 EMG Circuit

This circuit is designed to extract electrical muscle signal, then amplified and filtered this signal to introduced to microcontrollers to control the movement of the DC motor, where havepre-amplifier, optical isolation circuit, band-reject filter, band-pass filter,gain amplifier,half-wave rectifier and dual-comparator, where is drawn using proteus 8 professional program as schematic, as shown in figure (5.11).


Figure (5.11):- Schematic of EMG Circuit.

And converted to PCB layout to enter it to the electronic board printed machine, as shown in figure (5.12).


Figure (5.12):- EMG Circuit on PCB Board.

### 5.2.2 Transmitter Circuit

This circuit is designed to take a signal of right fingers and enter it to the microcontroller (ATMEGA 328P) and transfer it to transmitter Xbee through serial bins to send it to the receiver Xbee wirelessly, where is drawn usingproteus 8 professional program as schematic, as shown in figure (5.13).


Figure (5.13):- Schematic of Transmitter Circuit.
And converted to PCB layout to enter it to the electronic board printed machine, as shown in figure (5.14).


Figure (5.14):- Transmitter Circuit on PCB Board.

### 5.2.3 Receiver Circuit

This circuit designed to receive the text from the transmitter Xbee through the receiver Xbee and enter it to the microcontroller (ATMEGA 328P), to control the 5 servo motors movements, where is drawn using proteus 8 professional program as schematic, as shown in figure (5.15).


Figure (5.15):- Schematic of ReceiverCircuit.

And converted to PCB layout to enter it to the electronic board printed machine, as shown in figure (5.16).


Figure (5.16):- ReceiverCircuit on PCB Board.

### 5.3 Codes

In this section will give the codes, that downloaded on the microcontroller (ATMEGA 328P) using Arduino shield, such that; there are two microcontroller (ATMEGA 328P), the first to read the signals from the flex sensors and send that by the transmitter Xbee, and the second to read the serial text from the receiver Xbee and send orders to the servo motors.

- The code for the first ATMEGA328P :
const int analogInPin $1=\mathrm{A} 0$;
sensors are attached to
const int analogInPin2 $=\mathrm{A} 1$;
const int analogInPin3 $=\mathrm{A} 2$;
const int analogInPin4 $=\mathrm{A} 3$;
const int analogInPin5 = A4;
int sensorValue $1=0 ; \quad / /$ value read from the flex sensors
int sensorValue $2=0$;
int sensorValue $3=0$;
int sensorValue4 $=0$;
int sensorValue $5=0$;
void setup() \{
Serial.begin(9600); // initialize serial communications at 9600 bps:
\}
void loop() \{
// read the analog in value:
sensorValue1 = analogRead(analogInPin1);
sensorValue2 $=\operatorname{analogRead}(\operatorname{analogInPin} 2) ;$
sensorValue3 $=$ analogRead( analogInPin3);
sensorValue4 $=$ analogRead(analogInPin4);
sensorValue $5=$ analogRead(analogInPin5);
// map it to the range of the analog out:
sensorValue $1=\operatorname{map}($ sensorValue1, 150,340, 180, 30); //for small sensor
sensorValue2 $=$ map (sensorValue $2,150,340,180,30$ );
sensorValue3 $=$ map(sensorValue3, 512,614, 0, 180); // for the large sensors
sensorValue4 $=\operatorname{map}($ sensorValue $4,512,614,0,180)$;
sensorValue5 $=\operatorname{map}($ sensorValue5, $512,614,0,180)$;
// change the analog out value:
// print the results to the serial monitor:
Serial.print(sensorValue1);
Serial.print("a");
Serial.print(sensorValue2);
Serial.print("b");
Serial.print(sensorValue3);
Serial.print("c");
Serial.print(sensorValue4);
Serial.print("d");
Serial.print(sensorValue5);
Serial.print("e");
delay(10); // wait 10 ms
\}
- The code for the second ATMEGA328P:-
\#include <Servo.h>
Servo servo1;
Servo servo2;
Servo servo3;
Servo servo4;
Servo servo5;
int motorPin=8;
int analogPin=A0;
int sensorvalue $=0$;
void setup() \{
pinMode(8,OUTPUT);
servo1.attach(2);
servo2.attach(3);
servo3.attach(4);
servo4.attach(5);
servo5.attach(6);
Serial.begin(9600);
Serial.println("Ready");
\}

```
void loop() {
sensorvalue=analogRead(analogPin);
if(sensorvalue>=70 & sensorvalue<=140)
{ digitalWrite(motorPin, HIGH);
}
else
{
digitalWrite(motorPin, LOW);
}
static int v = 0;
    if ( Serial.available()) {
    char ch = Serial.read();
switch(ch) {
case '0'...'9':
    v = v * 10 + ch - '0';
    break;
case 'a':
    servo1.write(v);
    v = 0;
break;
```

case 'b':
servo2.write(v);
$\mathrm{v}=0 ;$
break;
case 'c':
servo3.write(v);

$$
\mathrm{v}=0
$$

break;
case 'd':
servo4.write(v);

$$
\mathrm{v}=0
$$

break;
case 'e': servo5.write(v); $\mathrm{v}=0 ;$
break;
\}
\}
\}

### 5.4 Block Diagram of the Project

The figure (5.17) illustrates the general block diagram for our project.


Figure (5.17):- The General Block Diagram of Project.

## Chapter Six

## Conclusions, Challenges and Recommendation

6.1 Conclusions
6.2 Challenges
6.3 Recommendation

### 6.1 Conclusions

1- The team extracted the muscle electrical signal through building a device that sensing the difference voltage resulting from muscle and then amplified and filtered it to aim of the ability to deal with the resultant signal.

2- The team has implemented mechanism congruence between the movement of non-infected fingers and movement of infected fingers through use a flex sensors to responds with fingers movement.

3- The microcontroller was the human mind in this project,where the team has done a program to control the movement of motors based on the extracted signals.

4- The team used the ZIG-BEE technology through piece called XBEE and that to send signals wirelessly to avoid block the movement of paralyzed.

5-The team used two types of motors, the first is DC motor of adequate capacity to do the hand-carry, and the second is servo motors to do the fingers movement.

6- The team designed the exoskeleton using Chemical material called polyethylene for easy formed and solidity after restructuring.

### 6.2 Challenges

The challenge was to extract a signals of fingers, Where that this moderation require a surgery to transplant the electrodes, that because the responsible nerve that transfer the signals to fingers non surface and could be reached only through the conduct of such operations. The solution was,the team has done to take these responsible signals to moving the fingers of the infected hand in the non-infected hand using flex sensors and send the signals antenna to provide freedom of movement of the paralyzed.

### 6.3 Recommendation

1- An alternative to taking finger's signals from the hand self using needle electrodes recompense taking it from the fingers of the other hand.

2- An alternative to using plastic cord that tension the fingers.

3- Improving electrical muscle for people who suffer from weakness in the nervous system of gonorrhea in a certain way instead of going into the enlarged and purified and control of the weak signals.

4- Work on moving the hand in three directions instead of just moving it in two directions.



## References

[1] Engyglopedia of the scientific revolution from Copernicus to newton, Wilbur Applebanm, Gapland publishing, Newyork and London, 2000, P-P 12-13.
[2] Electricaly and Life, GiulianoPanclad, P-P 9-80, university di bologna, 2011.
[3] Flex Sensor Based Servo Motor Controller using Microcontroller, Abidhusain Syed, Journal of software engineering and application, India, 2012.
[4]Neuroanatomy, "An Illustrated Colour Text", A. R. Crossman, Dneary, $4^{\text {th }}$ edition. Elsevier published, China, 2010.
[5] Reflex Physiology, Dr. Ali Ebneslahidi, Sciencie Paper, Ebneslahidi, calibornia state, 2009.
[6] Agonistand and Antagonist Muscle, Daniel Baker and Robert U. Newton, Journal of Strength and Conditioning Research, AQustaralia, 2005, PP 202-205.
[7] Atlas of Human Anatomy, Frank H. Netter MD, $5^{\text {th }}$ edition,
Saunders published, Newyork, 2010, PP 313-320.
[8] MuscularSystem, Gross Anatomy, Anatomy and
Physiology,SeeleyStephens6thedition,Part 2Support and
Movement, The McGraw-Hill Companies published, 2004, PP 342-350.
[9] Muscle Fiber Types, Bryancollins,
http://www.factstaff.unca.edu/cnicolary/BIO108/HO-Fiber
Types.p.d.f.
[10] Optimal Electrode Palcements, Dr. Robert D. Sidman, et al, Journal, Brain Toporaphy USA Spring 1994, vol 6, issue 3, PP 277-230.
[11] Computational Intelligence in Electromygraphy Analysis, Ganesh R. Naik, Published CCBY 3.0 License, Sydney, 2012, Ch18.
[12] Effective Acquisition of EMG Signals,
http://www.medusa.sdsu.edu/Robotic/Neuromuscular/Theses/Miller/

## Miller.chapter2.p.d.f.

[13] Important Factors in Surface EMG Measurement, Dr. Scott Day,Brotec Biomedical Journal, 225,604-1 st STSW, Calgary, AB.
[14] Surface Electromyography Signal Processing and Classification Techniques, Rubana H. Chowdhury, Hd, Sensors Journal, Malaysia, 17 sep 2013, PP 2-5.
[15] A Designer's Guide to Instrumentation Amplifiers, Charles Kitchin and Lew counts, 3rd edition, analog Devices Journal, G02678-159106(B) USA, 2006, PP1.1-3.5.
[16] Phototransistor Opt-coupler General Purpose type4N35. Avago Technologies Published,http://www.avagotech.com/docs/AV02-0773EN.
[17] Design Active Band Reject Filter using Op-Amp, Farouq M. AlTaweel, World Applied Sciences Journal 23(3), IDOSI Publications, 2013, Jordan, PP 305-308.
[18] Active Filter Design Techniques, Thomas Kugelstandt, Texas Instruments Journal, Texas, 2008, 2008, Chl6.
[19] Gain amplifier
circuit,http://webpages.ussinus.edu/riley/ref/circuits/node5.htm|
[20] Precision Half-Wave Rectifier (Superdiode), NTUEE Electronics, Dr. Robert D. Sidman, 4 ${ }^{\text {th }}$ edition, L. H. Lu Published, California, 2005. PP 884-889.
[21]Dual Comparator,
http://cds.linear.com/docs/en/datasheet/119a319afc.pdf.
[22] Power Window Motor, Global Market, China.
http://www.globalmarket.com/hotproducts/car+window+parts.html ? gclid=CLW.
[23] Flex Sensor, KhwajaHaris Jan, journal of electrical engineering publishe, Newyork, 2010, PP all pages.
[24] Arduino Uno, http://arduino.cc/en/Main/arduinoBoardUno.
[25] Xbee / Xbee - Pro RF Modules, product manual V1.xEx.-802.15.4 protocol, Digi international.
[26] Servo Motor, Baldor, BaldorElactric Company, BR 1202-F , 32,000 PROG, USA, 2005.
[27] Batteries for portable devices,Esmeralda Florez and Martin Adolph, TU-T TechWatch Alert,February 2010.
[28] Voltage Regulators, ON Semiconductor published, Japan, 2002, PP 8-55.
[29] Darlington's Contributions toTransistor Circuit Design, David A. Hodges, Fellow, Invited Paper,VOL. 46, NO. 1, JANUARY 1999.
[30] Stepper Motor, ShinanKenshi Journal, 6065 BRISTOL PARKWAY, CULVER CITY, CA 90230, PHONE (310) 693-7600,TOLL FREE (800) 7550752.
[31] Op-Amps, Design, Application and Troubleshooting, David L. Trrell.2nd edition.Terrell Technologies.Inc Published. USA. 1996. PP 212245.
[32] Biomechanical Basis of human movement, Joseph Hamill and Kathleen M.kutzen , $3^{\text {rd }}$ edition, wolters klumer published, naurth american , 2008, PP 340-370.
[33] Engineering Mechanics Statics, R. C. Hibbeler, 12 ${ }^{\text {th }}$, the evolution of electrical insulation technology published, japan, 2009, PP 217255.
[34] Weight, Volume, and CenterofMss of SegmentsoftheHman Body, C'VIIRLFS E. CLAUSEII, et al, Natioua" Tacknicallnftort ServiceU. S. DEPARTMENT OF COMMERCE Published, USA, AUGUST 1969, PP 245.
[35] Engineering Mechanics Dynamics, R. C. Hibbeler, $11^{\text {th }}$, Pearson Prentice Hall Published, New Jersey, 2007, PP 414-428.
[36] Gears, Educational Systems, LLC, Hanvor, 2000.
http://pdf.datasheetarchive.com/indexerfiles/Datasheet-
$017 / D S A 00296384$.

## FEATURES <br> EASY TO USE

Gain Set with One External Resistor
(Gain Range 1 to 1000)
Wide Power Supply Range ( $\pm 2.3 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$ )
Higher Performance than Three Op Amp IA Designs
Available in 8-Lead DIP and SOIC Packaging
Low Power, 1.3 mA max Supply Current
EXCELLENT DC PERFORMANCE ("B GRADE")
$50 \mu \mathrm{~V}$ max, Input Offset Voltage
$0.6 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ max, Input Offset Drift
1.0 nA max, Input Bias Current

100 dB min Common-Mode Rejection Ratio ( $G=10$ )
LOW NOISE
$9 \mathrm{nV} / \sqrt{\mathrm{Hz}}$, @ 1 kHz , Input Voltage Noise
$0.28 \mu \mathrm{~V}$ p-p Noise ( 0.1 Hz to 10 Hz )

## EXCELLENT AC SPECIFICATIONS

120 kHz Bandwidth (G = 100)
$15 \mu \mathrm{~s}$ Settling Time to 0.01\%

## APPLICATIONS

Weigh Scales
ECG and Medical Instrumentation
Transducer Interface
Data Acquisition Systems
Industrial Process Controls
Battery Powered and Portable Equipment

## PRODUCT DESCRIPTION

The AD620 is a low cost, high accuracy instrumentation amplifier that requires only one external resistor to set gains of 1 to


Figure 1. Three Op Amp IA Designs vs. AD620
REV. E

[^0]CONNECTION DIAGRAM
8-Lead Plastic Mini-DIP (N), Cerdip (Q) and SOIC (R) Packages

1000. Furthermore, the AD620 features 8-lead SOIC and DIP packaging that is smaller than discrete designs, and offers lower power (only 1.3 mA max supply current), making it a good fit for battery powered, portable (or remote) applications.

The AD620, with its high accuracy of 40 ppm maximum nonlinearity, low offset voltage of $50 \mu \mathrm{~V}$ max and offset drift of $0.6 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ max, is ideal for use in precision data acquisition systems, such as weigh scales and transducer interfaces. Furthermore, the low noise, low input bias current, and low power of the AD620 make it well suited for medical applications such as ECG and noninvasive blood pressure monitors.
The low input bias current of 1.0 nA max is made possible with the use of Super $\beta$ eta processing in the input stage. The AD620 works well as a preamplifier due to its low input voltage noise of $9 \mathrm{nV} / \sqrt{\mathrm{Hz}}$ at $1 \mathrm{kHz}, 0.28 \mu \mathrm{~V}$ p-p in the 0.1 Hz to 10 Hz band, $0.1 \mathrm{pA} / \sqrt{\mathrm{Hz}}$ input current noise. Also, the AD620 is well suited for multiplexed applications with its settling time of $15 \mu \mathrm{~s}$ to $0.01 \%$ and its cost is low enough to enable designs with one inamp per channel.


Figure 2. Total Voltage Noise vs. Source Resistance

[^1]
## AD620-SPECIFICATIONS

(Typical @ $+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$, and $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega$, unless otherwise noted)



NOTES
${ }^{1}$ See Analog Devices military data sheet for 883B tested specifications.
${ }^{2}$ Does not include effects of external resistor $\mathrm{R}_{\mathrm{G}}$.
${ }^{3}$ One input grounded. $\mathrm{G}=1$.
${ }^{4}$ This is defined as the same supply range which is used to specify PSR.
Specifications subject to change without notice.

## AD620

## ABSOLUTE MAXIMUM RATINGS ${ }^{1}$

Supply Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $\pm 18$ V Internal Power Dissipation ${ }^{2}$. . . . . . . . . . . . . . . . . . . . . . 650 mW
Input Voltage (Common Mode) . . . . . . . . . . . . . . . . . . . . $\pm$ V $_{S}$
Differential Input Voltage . . . . . . . . . . . . . . . . . . . . . . . . $\pm 25$ V
Output Short Circuit Duration . . . . . . . . . . . . . . . . . Indefinite
Storage Temperature Range (Q) . . . . . . . . . $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Storage Temperature Range (N, R) . . . . . . . $-65^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Operating Temperature Range
AD620 (A, B) . . . . . . . . . . . . . . . . . . . . . . $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
AD620 (S) . . . . . . . . . . . . . . . . . . . . . . . . $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Lead Temperature Range
(Soldering 10 seconds)
$+300^{\circ} \mathrm{C}$

## NOTES

${ }^{1}$ Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.
${ }^{2}$ Specification is for device in free air:
8 -Lead Plastic Package: $\theta_{\mathrm{JA}}=95^{\circ} \mathrm{C} / \mathrm{W}$
8-Lead Cerdip Package: $\theta_{\mathrm{JA}}=110^{\circ} \mathrm{C} / \mathrm{W}$
8 -Lead SOIC Package: $\theta_{\mathrm{JA}}=155^{\circ} \mathrm{C} / \mathrm{W}$

ORDERING GUIDE

| Model | Temperature Ranges | Package Options |
| :--- | :--- | :--- |
| AD620AN | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $\mathrm{N}-8$ |
| AD620BN | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $\mathrm{N}-8$ |
| AD620AR | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | SO-8 |
| AD620AR-REEL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $13{ }^{\prime \prime}$ REEL |
| AD620AR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 7 " REEL |
| AD620BR | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | SO-8 |
| AD620BR-REEL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $13 " \mathrm{REEL}$ |
| AD620BR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $7{ }^{\prime \prime}$ REEL |
| AD620ACHIPS | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | Die Form |
| AD620SQ/883B | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | Q-8 |

* $\mathrm{N}=$ Plastic DIP; $\mathrm{Q}=$ Cerdip; SO = Small Outline.


## METALIZATION PHOTOGRAPH

Dimensions shown in inches and (mm).
Contact factory for latest dimensions.

*FOR CHIP APPLICATIONS: THE PADS $1 \mathrm{R}_{\mathrm{G}}$ AND $8 \mathrm{R}_{\mathrm{G}}$ MUST BE CONNECTED IN PARALLEL TO THE EXTERNAL GAIN REGISTER $R_{G}$. DO NOT CONNECT THEM IN SERIES TO $R_{G}$. FOR UNITY GAIN APPLICATIONS WHERE $R_{G}$ IS NOT REQUIRED, THE PADS $1 \mathrm{R}_{\mathrm{G}}$ MAY SIMPLY BE BONDED TOGETHER, AS WELL AS THE PADS $8 \mathrm{R}_{\mathrm{G}}$.

## CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the AD620 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD

## Typical Characteristics (@ $+25^{\circ}, V_{s}= \pm 15 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega$, unless otherwise noted)



Figure 3. Typical Distribution of Input Offset Voltage


Figure 4. Typical Distribution of Input Bias Current


Figure 5. Typical Distribution of Input Offset Current


Figure 6. Input Bias Current vs. Temperature


Figure 7. Change in Input Offset Voltage vs. Warm-Up Time


Figure 8. Voltage Noise Spectral Density vs. Frequency, ( $G=1-1000$ )

## AD620-Typical Characteristics



Figure 9. Current Noise Spectral Density vs. Frequency


Figure 10a. 0.1 Hz to 10 Hz RTI Voltage Noise ( $G=1$ )


Figure 10b. 0.1 Hz to 10 Hz RTI Voltage Noise ( $G=1000$ )


Figure 11. 0.1 Hz to 10 Hz Current Noise, $5 \mathrm{pA} / \mathrm{Div}$


Figure 12. Total Drift vs. Source Resistance


Figure 13. CMR vs. Frequency, RTI, Zero to $1 \mathrm{k} \Omega$ Source Imbalance


Figure 14. Positive PSR vs. Frequency, RTI ( $G=1-1000$ )


Figure 15. Negative PSR vs. Frequency, RTI ( $G=1-1000$ )

Figure 16. Gain vs. Frequency


Figure 17. Large Signal Frequency Response


Figure 18. Input Voltage Range vs. Supply Voltage, $G=1$


Figure 19. Output Voltage Swing vs. Supply Voltage, $G=10$

## AD620



Figure 20. Output Voltage Swing vs. Load Resistance


Figure 21. Large Signal Pulse Response and Settling Time $G=1(0.5 \mathrm{mV}=0.01 \%)$


Figure 22. Small Signal Response, $G=1, R_{L}=2 k \Omega$, $C_{L}=100 \mathrm{pF}$


Figure 23. Large Signal Response and Settling Time, $G=10$ ( $0.5 \mathrm{mV}=001 \%$ )


Figure 24. Small Signal Response, $G=10, R_{L}=2 k \Omega$, $C_{L}=100 \mathrm{pF}$


Figure 25. Large Signal Response and Settling Time, $G=100(0.5 \mathrm{mV}=0.01 \%)$


Figure 26. Small Signal Pulse Response, $G=100$, $R_{L}=2 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$


Figure 27. Large Signal Response and Settling Time, $G=1000$ ( $0.5 \mathrm{mV}=0.01 \%$ )


Figure 28. Small Signal Pulse Response, $G=1000$, $R_{L}=2 k \Omega, C_{L}=100 \mathrm{pF}$


Figure 29. Settling Time vs. Step Size ( $G=1$ )


Figure 30. Settling Time to $0.01 \%$ vs. Gain, for a 10 V Step


Figure 31a. Gain Nonlinearity, $G=1, R_{L}=10 \mathrm{k} \Omega$ (10 $\mu \mathrm{V}=1 \mathrm{ppm}$ )


Figure 31b. Gain Nonlinearity, $G=100, R_{L}=10 \mathrm{k} \Omega$ ( $100 \mu \mathrm{~V}=10 \mathrm{ppm}$ )


Figure 31c. Gain Nonlinearity, $G=1000, R_{L}=10 \mathrm{k} \Omega$ (1 mV = 100 ppm )

*ALL RESISTORS 1\% TOLERANCE
Figure 32. Settling Time Test Circuit


Figure 33. Simplified Schematic of AD620

## THEORY OF OPERATION

The AD620 is a monolithic instrumentation amplifier based on a modification of the classic three op amp approach. Absolute value trimming allows the user to program gain accurately (to $0.15 \%$ at $G=100$ ) with only one resistor. Monolithic construction and laser wafer trimming allow the tight matching and tracking of circuit components, thus ensuring the high level of performance inherent in this circuit.
The input transistors Q1 and Q2 provide a single differentialpair bipolar input for high precision (Figure 33), yet offer 10x lower Input Bias Current thanks to Super $\beta$ eta processing. Feedback through the Q1-A1-R1 loop and the Q2-A2-R2 loop maintains constant collector current of the input devices Q1, Q2 thereby impressing the input voltage across the external gain setting resistor $\mathrm{R}_{\mathrm{G}}$. This creates a differential gain from the inputs to the $\mathrm{A} 1 / \mathrm{A} 2$ outputs given by $\mathrm{G}=(\mathrm{R} 1+\mathrm{R} 2) / \mathrm{R}_{\mathrm{G}}+1$. The unity-gain subtracter A3 removes any common-mode signal, yielding a single-ended output referred to the REF pin potential.
The value of $R_{G}$ also determines the transconductance of the preamp stage. As $R_{G}$ is reduced for larger gains, the transconductance increases asymptotically to that of the input transistors. This has three important advantages: (a) Open-loop gain is boosted for increasing programmed gain, thus reducing gainrelated errors. (b) The gain-bandwidth product (determined by $\mathrm{C} 1, \mathrm{C} 2$ and the preamp transconductance) increases with programmed gain, thus optimizing frequency response. (c) The input voltage noise is reduced to a value of $9 \mathrm{nV} / \sqrt{\mathrm{Hz}}$, determined mainly by the collector current and base resistance of the input devices.
The internal gain resistors, R1 and R2, are trimmed to an absolute value of $24.7 \mathrm{k} \Omega$, allowing the gain to be programmed accurately with a single external resistor.

The gain equation is then

$$
G=\frac{49.4 k \Omega}{R_{G}}+1
$$

so that

$$
R_{G}=\frac{49.4 k \Omega}{G-1}
$$

Make vs. Buy: A Typical Bridge Application Error Budget The AD620 offers improved performance over "homebrew" three op amp IA designs, along with smaller size, fewer components and $10 \times$ lower supply current. In the typical application, shown in Figure 34, a gain of 100 is required to amplify a bridge output of 20 mV full scale over the industrial temperature range of $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. The error budget table below shows how to calculate the effect various error sources have on circuit accuracy.
Regardless of the system in which it is being used, the AD620 provides greater accuracy, and at low power and price. In simple
systems, absolute accuracy and drift errors are by far the most significant contributors to error. In more complex systems with an intelligent processor, an autogain/autozero cycle will remove all absolute accuracy and drift errors leaving only the resolution errors of gain nonlinearity and noise, thus allowing full 14-bit accuracy.
Note that for the homebrew circuit, the OP07 specifications for input voltage offset and noise have been multiplied by $\sqrt{2}$. This is because a three op amp type in-amp has two op amps at its inputs, both contributing to the overall input error.


PRECISION BRIDGE TRANSDUCER


AD620A MONOLITHIC INSTRUMENTATION AMPLIFIER, $\mathrm{G}=100$

SUPPLY CURRENT $=1.3 \mathrm{~mA}$ MAX

"HOMEBREW" IN-AMP, G = 100
${ }^{*} 0.02 \%$ RESISTOR MATCH, 3 PPM $/{ }^{\circ} \mathrm{C}$ TRACKING **DISCRETE $1 \%$ RESISTOR, 100 PPM $/{ }^{\circ} \mathrm{C}$ TRACKING SUPPLY CURRENT $=15 \mathrm{~mA}$ MAX

Figure 34. Make vs. Buy

Table I. Make vs. Buy Error Budget

| Error Source | AD620 Circuit Calculation | "Homebrew" Circuit Calculation | Error, ppm of Full Scale |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AD620 | Homebrew |
| ABSOLUTE ACCURACY at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ <br> Input Offset Voltage, $\mu \mathrm{V}$ <br> Output Offset Voltage, $\mu \mathrm{V}$ <br> Input Offset Current, nA <br> CMR, dB | $\begin{aligned} & 125 \mu \mathrm{~V} / 20 \mathrm{mV} \\ & 1000 \mu \mathrm{~V} / 100 / 20 \mathrm{mV} \\ & 2 \mathrm{nA} \times 350 \Omega / 20 \mathrm{mV} \\ & 110 \mathrm{~dB} \rightarrow 3.16 \mathrm{ppm}, \times 5 \mathrm{~V} / 20 \mathrm{mV} \end{aligned}$ | $\begin{aligned} & (150 \mu \mathrm{~V} \times \sqrt{2}) / 20 \mathrm{mV} \\ & ((150 \mu \mathrm{~V} \times 2) / 100) / 20 \mathrm{mV} \\ & (6 \mathrm{nA} \times 350 \Omega) / 20 \mathrm{mV} \\ & (0.02 \% \text { Match } \times 5 \mathrm{~V}) / 20 \mathrm{mV} / 100 \end{aligned}$ | $\begin{array}{r} 6,250 \\ 500 \\ 18 \\ 791 \end{array}$ | $\begin{array}{r} 10,607 \\ 150 \\ 53 \\ 500 \end{array}$ |
| DRIFT TO $+85^{\circ} \mathrm{C}$ <br> Gain Drift, ppm $/{ }^{\circ} \mathrm{C}$ <br> Input Offset Voltage Drift, $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ <br> Output Offset Voltage Drift, $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ | $\begin{aligned} & (50 \mathrm{ppm}+10 \mathrm{ppm}) \times 60^{\circ} \mathrm{C} \\ & 1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \times 60^{\circ} \mathrm{C} / 20 \mathrm{mV} \\ & 15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \times 60^{\circ} \mathrm{C} / 100 / 20 \mathrm{mV} \end{aligned}$ | $\begin{aligned} & \text { Total Absolute Error } \\ & 100 \mathrm{ppm} /{ }^{\circ} \mathrm{C} \text { Track } \times 60^{\circ} \mathrm{C} \\ & \left(2.5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \times \sqrt{2} \times 60^{\circ} \mathrm{C}\right) / 20 \mathrm{mV} \\ & \left(2.5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \times 2 \times 60^{\circ} \mathrm{C}\right) / 100 / 20 \mathrm{mV} \end{aligned}$ | $\begin{array}{r} 7,558 \\ 3,600 \\ 3,000 \\ 450 \end{array}$ | $\begin{array}{r} 11,310 \\ \\ 6,000 \\ 10,607 \\ 150 \end{array}$ |
| RESOLUTION <br> Gain Nonlinearity, ppm of Full Scale Typ $0.1 \mathrm{~Hz}-10 \mathrm{~Hz}$ Voltage Noise, $\mu \mathrm{V}$ p-p | $\begin{aligned} & 40 \mathrm{ppm} \\ & 0.28 \mu \mathrm{~V}-\mathrm{p} / 20 \mathrm{mV} \end{aligned}$ | Total Drift Error $\begin{aligned} & 40 \mathrm{ppm} \\ & (0.38 \mu \mathrm{~V} \text { p-p } \times \sqrt{2}) / 20 \mathrm{mV} \end{aligned}$ | $\begin{array}{r} 7,050 \\ 40 \\ 14 \end{array}$ | $16,757$ <br> 40 $27$ |
|  |  | Total Resolution Error | 54 | 67 |
|  |  | Grand Total Error | 14,662 | 28,134 |

$\mathrm{G}=100, \mathrm{~V}_{\mathrm{S}}= \pm 15 \mathrm{~V}$.
(All errors are $\min / \mathrm{max}$ and referred to input.)


Figure 35. A Pressure Monitor Circuit which Operates on a +5 V Single Supply

## Pressure Measurement

Although useful in many bridge applications such as weigh scales, the AD620 is especially suitable for higher resistance pressure sensors powered at lower voltages where small size and low power become more significant.
Figure 35 shows a $3 \mathrm{k} \Omega$ pressure transducer bridge powered from +5 V . In such a circuit, the bridge consumes only 1.7 mA . Adding the AD620 and a buffered voltage divider allows the signal to be conditioned for only 3.8 mA of total supply current.
Small size and low cost make the AD620 especially attractive for voltage output pressure transducers. Since it delivers low noise and drift, it will also serve applications such as diagnostic noninvasive blood pressure measurement.

## Medical ECG

The low current noise of the AD620 allows its use in ECG monitors (Figure 36) where high source resistances of $1 \mathrm{M} \Omega$ or higher are not uncommon. The AD620's low power, low supply voltage requirements, and space-saving 8-lead mini-DIP and SOIC package offerings make it an excellent choice for battery powered data recorders.
Furthermore, the low bias currents and low current noise coupled with the low voltage noise of the AD620 improve the dynamic range for better performance.
The value of capacitor C 1 is chosen to maintain stability of the right leg drive loop. Proper safeguards, such as isolation, must be added to this circuit to protect the patient from possible harm.


Figure 36. A Medical ECG Monitor Circuit

## Precision V-I Converter

The AD620, along with another op amp and two resistors, makes a precision current source (Figure 37). The op amp buffers the reference terminal to maintain good CMR. The output voltage $\mathrm{V}_{\mathrm{X}}$ of the AD620 appears across R1, which converts it to a current. This current less only, the input bias current of the op amp , then flows out to the load.


Figure 37. Precision Voltage-to-Current Converter (Operates on $1.8 \mathrm{~mA}, \pm 3 \mathrm{~V}$ )

## GAIN SELECTION

The AD620's gain is resistor programmed by $\mathrm{R}_{\mathrm{G}}$, or more precisely, by whatever impedance appears between Pins 1 and 8 . The AD620 is designed to offer accurate gains using $0.1 \%-1 \%$ resistors. Table II shows required values of $\mathrm{R}_{\mathrm{G}}$ for various gains. Note that for $G=1$, the $R_{G}$ pins are unconnected $\left(R_{G}=\infty\right)$. For any arbitrary gain $\mathrm{R}_{\mathrm{G}}$ can be calculated by using the formula:

$$
R_{G}=\frac{49.4 k \Omega}{G-1}
$$

To minimize gain error, avoid high parasitic resistance in series with $\mathrm{R}_{\mathrm{G}}$; to minimize gain drift, $\mathrm{R}_{\mathrm{G}}$ should have a low TC -less than $10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$-for the best performance.

Table II. Required Values of Gain Resistors

| $\mathbf{1 \%}$ Std Table <br> Value of $\mathbf{R}_{\mathbf{G}}, \boldsymbol{\Omega}$ | Calculated <br> Gain | $\mathbf{0 . 1 \% \text { Std Table }}$ <br> Value of $\mathbf{R}_{\mathbf{G}}, \boldsymbol{\Omega}$ | Calculated <br> Gain |
| :---: | :--- | :--- | :--- |
| 49.9 k | 1.990 | 49.3 k | 2.002 |
| 12.4 k | 4.984 | 12.4 k | 4.984 |
| 5.49 k | 9.998 | 5.49 k | 9.998 |
| 2.61 k | 19.93 | 2.61 k | 19.93 |
| 1.00 k | 50.40 | 1.01 k | 49.91 |
| 499 | 100.0 | 499 | 100.0 |
| 249 | 199.4 | 249 | 199.4 |
| 100 | 495.0 | 98.8 | 501.0 |
| 49.9 | 991.0 | 49.3 | 1,003 |

## INPUT AND OUTPUT OFFSET VOLTAGE

The low errors of the AD620 are attributed to two sources, input and output errors. The output error is divided by G when referred to the input. In practice, the input errors dominate at high gains and the output errors dominate at low gains. The total $\mathrm{V}_{\mathrm{OS}}$ for a given gain is calculated as:

> Total Error RTI $=$ input error $+($ output error $/ \mathrm{G})$
> Total Error RTO $=$ (input error $\times \mathrm{G})+$ output error

## REFERENCE TERMINAL

The reference terminal potential defines the zero output voltage, and is especially useful when the load does not share a precise ground with the rest of the system. It provides a direct means of injecting a precise offset to the output, with an allowable range of 2 V within the supply voltages. Parasitic resistance should be kept to a minimum for optimum CMR.

## INPUT PROTECTION

The AD620 features $400 \Omega$ of series thin film resistance at its inputs, and will safely withstand input overloads of up to $\pm 15 \mathrm{~V}$ or $\pm 60 \mathrm{~mA}$ for several hours. This is true for all gains, and power on and off, which is particularly important since the signal source and amplifier may be powered separately. For longer time periods, the current should not exceed $6 \mathrm{~mA}\left(\mathrm{I}_{\mathrm{IN}} \leq\right.$ $\mathrm{V}_{\text {IN }} / 400 \Omega$ ). For input overloads beyond the supplies, clamping the inputs to the supplies (using a low leakage diode such as an FD333) will reduce the required resistance, yielding lower noise.

## RF INTERFERENCE

All instrumentation amplifiers can rectify out of band signals, and when amplifying small signals, these rectified voltages act as small dc offset errors. The AD620 allows direct access to the input transistor bases and emitters enabling the user to apply some first order filtering to unwanted RF signals (Figure 38), where $R C \approx 1 /(2 \pi f)$ and where $f \geq$ the bandwidth of the AD620; C $\leq 150 \mathrm{pF}$. Matching the extraneous capacitance at Pins 1 and 8 and Pins 2 and 3 helps to maintain high CMR.


Figure 38. Circuit to Attenuate RF Interference

## AD620

## COMMON-MODE REJECTION

Instrumentation amplifiers like the AD620 offer high CMR, which is a measure of the change in output voltage when both inputs are changed by equal amounts. These specifications are usually given for a full-range input voltage change and a specified source imbalance.

For optimal CMR the reference terminal should be tied to a low impedance point, and differences in capacitance and resistance should be kept to a minimum between the two inputs. In many applications shielded cables are used to minimize noise, and for best CMR over frequency the shield should be properly driven. Figures 39 and 40 show active data guards that are configured to improve ac common-mode rejections by "bootstrapping" the capacitances of input cable shields, thus minimizing the capacitance mismatch between the inputs.


Figure 39. Differential Shield Driver

Figure 40. Common-Mode Shield Driver


## GROUNDING

Since the AD620 output voltage is developed with respect to the potential on the reference terminal, it can solve many grounding problems by simply tying the REF pin to the appropriate "local ground."

In order to isolate low level analog signals from a noisy digital environment, many data-acquisition components have separate analog and digital ground pins (Figure 41). It would be convenient to use a single ground line; however, current through ground wires and PC runs of the circuit card can cause hundreds of millivolts of error. Therefore, separate ground returns should be provided to minimize the current flow from the sensitive points to the system ground. These ground returns must be tied together at some point, usually best at the ADC package as shown.


Figure 41. Basic Grounding Practice

## GROUND RETURNS FOR INPUT BIAS CURRENTS

Input bias currents are those currents necessary to bias the input transistors of an amplifier. There must be a direct return path for these currents; therefore, when amplifying "floating" input


Figure 42a. Ground Returns for Bias Currents with Transformer Coupled Inputs
sources such as transformers, or ac-coupled sources, there must be a dc path from each input to ground as shown in Figure 42. Refer to the Instrumentation Amplifier Application Guide (free from Analog Devices) for more information regarding in amp applications.


Figure 42b. Ground Returns for Bias Currents with Thermocouple Inputs


Figure 42c. Ground Returns for Bias Currents with AC Coupled Inputs

## OUTLINE DIMENSIONS

Dimensions shown in inches and (mm).

## Plastic DIP (N-8) Package



Cerdip (Q-8) Package


## SOIC (SO-8) Package



## Optocoupler, Phototransistor Output, With Base Connection

## Features

- Isolation Test Voltage $5300 \mathrm{~V}_{\mathrm{RMS}}$
- Interfaces with Common Logic Families
- Input-output Coupling Capacitance $<0.5 \mathrm{pF}$
- Industry Standard Dual-in-line 6-pin Package
- Lead-free component
- Component in accordance to RoHS 2002/95/EC and WEEE 2002/96/EC


## Agency Approvals

- UL1577, File No. E52744 System Code H or J, Double Protection
- DIN EN 60747-5-2 (VDE0884) DIN EN 60747-5-5 pending Available with Option 1


## Applications

AC Mains Detection
Reed relay driving
Switch Mode Power Supply Feedback
Telephone Ring Detection
Logic Ground Isolation
Logic Coupling with High Frequency Noise Rejection

## Description

The 4N25 family is an Industry Standard Single Channel Phototransistor Coupler.This family includes the 4N25/ 4N26/ 4N27/ 4N28. Each optocoupler consists of gallium arsenide infrared LED and a silicon NPN phototransistor.
These couplers are Underwriters Laboratories (UL) listed to comply with a $5300 \mathrm{~V}_{\text {RMS }}$ isolation test voltage. This isolation performance is accomplished through special Vishay manufacturing process.
Compliance to DIN EN 60747-5-2(VDE0884)/ DIN EN 60747-5-5 pending partial discharge isolation specification is available by ordering option1.


These isolation processes and the Vishay ISO9001 quality program results in the highest isolation performance available for a commercial plastic phototransistor optocoupler.
The devices are also available in lead formed configuration suitable for surface mounting and are available either on tape and reel, or in standard tube shipping containers.
Note:
For additional design information see Application Note 45 Normalized Curves

## Order Information

| Part | Remarks |
| :---: | :---: |
| 4N25 | CTR > 20 \%, DIP-6 |
| 4N26 | CTR > 20 \%, DIP-6 |
| 4N27 | CTR > 10 \%, DIP-6 |
| 4N28 | CTR > 10 \%, DIP-6 |
| 4N25-X006 | CTR > 20 \%, DIP-6 400 mil (option 6) |
| 4N25-X007 | CTR > 20 \%, SMD-6 (option 7) |
| 4N25-X009 | CTR > 20 \%, SMD-6 (option 9) |
| 4N26-X006 | CTR > 20 \%, DIP-6 400 mil (option 6) |
| 4N26-X007 | CTR > 20 \%, SMD-6 (option 7) |
| 4N26-X009 | CTR > 20 \%, SMD-6 (option 9) |
| 4N27-X007 | CTR > 10 \%, SMD-6 (option 7) |
| 4N27-X009 | CTR > 10 \%, SMD-6 (option 9) |
| 4N28-X009 | CTR > 10 \%, SMD-6 (option 9) |

For additional information on the available options refer to Option Information.

## 4N25/ 4N26/ 4N27/ 4N28

## Vishay Semiconductors

## Absolute Maximum Ratings

$\mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$, unless otherwise specified
Stresses in excess of the absolute Maximum Ratings can cause permanent damage to the device. Functional operation of the device is not implied at these or any other conditions in excess of those given in the operational sections of this document. Exposure to absolute Maximum Rating for extended periods of the time can adversely affect reliability.

## Input

| Parameter | Test condition | Symbol | Value | Unit |
| :--- | :--- | :---: | :---: | :---: |
| Reverse voltage |  | $\mathrm{V}_{\mathrm{R}}$ | 6.0 | V |
| Forward current |  | $\mathrm{I}_{\mathrm{F}}$ | 60 | mA |
| Surge current | $\mathrm{t}<10 \mu \mathrm{~s}$ | $\mathrm{I}_{\text {FSM }}$ | 2.5 | A |
| Power dissipation |  | $\mathrm{P}_{\text {diss }}$ | 100 | mW |

## Output

| Parameter | Test condition | Symbol | Value | Unit |
| :--- | :---: | :---: | :---: | :---: |
| Collector-emitter breakdown voltage |  | $\mathrm{V}_{\text {CEO }}$ | 70 | V |
| Emitter-base breakdown voltage |  | $\mathrm{V}_{\text {EBO }}$ | 7.0 | V |
| Collector current |  | $\mathrm{I}_{\mathrm{C}}$ | 50 | mA |
| Collector currrent | $\mathrm{t}<1.0 \mathrm{~ms}$ | $\mathrm{I}_{\mathrm{C}}$ | mA |  |
| Power dissipation |  | $\mathrm{P}_{\text {diss }}$ | 100 | mW |

## Coupler

| Parameter | Test condition | Symbol | Value | Unit |
| :---: | :---: | :---: | :---: | :---: |
| Isolation test voltage |  | $\mathrm{V}_{\text {ISO }}$ | 5300 | $\mathrm{V}_{\text {RMS }}$ |
| Creepage |  |  | $\geq 7.0$ | mm |
| Clearance |  |  | $\geq 7.0$ | mm |
| Isolation thickness between emitter and detector |  |  | $\geq 0.4$ | mm |
| Comparative tracking index | DIN IEC 112/VDE0303, part 1 |  | 175 |  |
| Isolation resistance | $\mathrm{V}_{\text {IO }}=500 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$ | $\mathrm{R}_{\mathrm{IO}}$ | $10^{12}$ | $\Omega$ |
|  | $\mathrm{V}_{\mathrm{IO}}=500 \mathrm{~V}, \mathrm{~T}_{\mathrm{amb}}=100^{\circ} \mathrm{C}$ | $\mathrm{R}_{10}$ | $10^{11}$ | $\Omega$ |
| Storage temperature |  | $\mathrm{T}_{\text {stg }}$ | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |
| Operating temperature |  | Tamb | -55 to +100 | ${ }^{\circ} \mathrm{C}$ |
| Junction temperature |  | $\mathrm{T}_{\mathrm{j}}$ | 100 | ${ }^{\circ} \mathrm{C}$ |
| Soldering temperature | max. 10 s , dip soldering: distance to seating plane $\geq 1.5 \mathrm{~mm}$ | $\mathrm{T}_{\text {sld }}$ | 260 | ${ }^{\circ} \mathrm{C}$ |

## Electrical Characteristics

$\mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$, unless otherwise specified
Minimum and maximum values are testing requirements. Typical values are characteristics of the device and are the result of engineering evaluation. Typical values are for information only and are not part of the testing requirements.

## Input

| Parameter | Test condition | Symbol | Min | Typ. | Max | Unit |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Forward voltage ${ }^{1)}$ | $\mathrm{I}_{\mathrm{F}}=50 \mathrm{~mA}$ | $\mathrm{~V}_{\mathrm{F}}$ |  | 1.3 | 1.5 | V |
| ${\text { Reverse current }{ }^{1)}}^{\text {Capacitance }}$ | $\mathrm{V}_{\mathrm{R}}=3.0 \mathrm{~V}$ | $\mathrm{I}_{\mathrm{R}}$ |  | 0.1 | 100 | $\mu \mathrm{~A}$ |
| Ca | $\mathrm{V}_{\mathrm{R}}=0 \mathrm{~V}$ | $\mathrm{C}_{\mathrm{O}}$ |  | 25 | pF |  |

${ }^{1)}$ Indicates JEDEC registered values

## Output

| Parameter | Test condition | Part | Symbol | Min | Typ. | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Collector-base breakdown voltage ${ }^{1)}$ | $\mathrm{I}_{\mathrm{C}}=100 \mu \mathrm{~A}$ |  | $\mathrm{BV}_{\mathrm{CBO}}$ | 70 |  |  | V |
| Collector-emitter breakdown voltage ${ }^{1)}$ | $\mathrm{I}_{\mathrm{C}}=1.0 \mathrm{~mA}$ |  | $\mathrm{BV}_{\text {CEO }}$ | 30 |  |  | V |
| Emitter-collector breakdown voltage ${ }^{1)}$ | $\mathrm{I}_{\mathrm{E}}=100 \mu \mathrm{~A}$ |  | $\mathrm{BV}_{\mathrm{ECO}}$ | 7.0 |  |  | V |
| $\mathrm{I}_{\text {CEO }}$ (dark) ${ }^{1 \text { ) }}$ | $\mathrm{V}_{\mathrm{CE}}=10 \mathrm{~V}$, (base open) | 4N25 |  |  | 5.0 | 50 | nA |
|  |  | 4N26 |  |  | 5.0 | 50 | nA |
|  |  | 4N27 |  |  | 5.0 | 50 | nA |
|  |  | 4N28 |  |  | 10 | 100 | nA |
| $\mathrm{I}_{\text {CBO }}(\text { dark })^{1)}$ | $\mathrm{V}_{\mathrm{CB}}=10 \mathrm{~V}$, (emitter open) |  |  |  | 2.0 | 20 | nA |
| Collector-emitter capacitance | $\mathrm{V}_{\mathrm{CE}}=0$ |  | $\mathrm{C}_{\text {CE }}$ |  | 6.0 |  | pF |

${ }^{1)}$ Indicates JEDEC registered values

Coupler

| Parameter | Test condition | Part | Symbol | Min | Typ. | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Isolation voltage ${ }^{1)}$ | Peak, 60 Hz | 4N25 | $\mathrm{V}_{10}$ | 2500 |  |  | V |
|  |  | 4N26 | $\mathrm{V}_{10}$ | 1500 |  |  | V |
|  |  | 4N27 | $\mathrm{V}_{10}$ | 1500 |  |  | V |
|  |  | 4N28 | $\mathrm{V}_{10}$ | 500 |  |  | V |
| Saturation voltage, collectoremitter | $\mathrm{I}_{C E}=2.0 \mathrm{~mA}, \mathrm{I}_{\mathrm{F}}=50 \mathrm{~mA}$ |  | $\mathrm{V}_{\mathrm{CE} \text { (sat) }}$ |  |  | 0.5 | V |
| Resistance, input output ${ }^{1 \text { 1 }}$ | $\mathrm{V}_{10}=500 \mathrm{~V}$ |  | $\mathrm{R}_{1 \mathrm{O}}$ | 100 |  |  | G $\Omega$ |
| Capacitance (input-output) | $\mathrm{f}=1.0 \mathrm{MHz}$ |  | $\mathrm{C}_{10}$ |  | 0.5 |  | pF |

${ }^{1)}$ Indicates JEDEC registered values

## Current Transfer Ratio

| Parameter | Test condition | Part | Symbol | Min | Typ. | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC Current Transfer Ratio ${ }^{1)}$ | $\mathrm{V}_{\mathrm{CE}}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{F}}=10 \mathrm{~mA}$ | 4N25 | $\mathrm{CTR}_{\text {DC }}$ | 20 | 50 |  | \% |
|  |  | 4N26 | $\mathrm{CTR}_{\text {DC }}$ | 20 | 50 |  | \% |
|  |  | 4N27 | $\mathrm{CTR}_{\text {DC }}$ | 10 | 30 |  | \% |
|  |  | 4N28 | $\mathrm{CTR}_{\text {DC }}$ | 10 | 30 |  | \% |

[^2]
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## Switching Characteristics

| Parameter | Test condition | Symbol | Min | Typ. | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rise and fall times | $\mathrm{V}_{\mathrm{CE}}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{F}}=10 \mathrm{~mA}, \mathrm{R}_{\mathrm{L}}=100 \Omega$ | $\mathrm{t}_{\mathrm{r}}, \mathrm{t}_{\mathrm{f}}$ |  | 2.0 |  | $\mu \mathrm{~s}$ |

## Typical Characteristics (Tamb $=25^{\circ} \mathrm{C}$ unless otherwise specified)



Figure 1. Forward Voltage vs. Forward Current


Figure 2. Normalized Non-Saturated and Saturated CTR vs. LED Current

i4n25_03

Figure 3. Normalized Non-saturated and Saturated CTR vs. LED Current

i4n25_04
Figure 4. Normalized Non-saturated and saturated CTR vs. LED Current

i4n25_05
Figure 5. Normalized Non-saturated and saturated CTR vs. LED Current

i4n25_06

Figure 6. Collector-Emitter Current vs. Temperature and LED Current


Figure 7. Collector-Emitter Leakage Current vs.Temp.

${ }^{44 n 25}$. 08
Figure 8. Normalized CTRcb vs. LED Current and Temp.


Figure 9. Normalized Photocurrent vs. $\mathrm{I}_{\mathrm{F}}$ and Temp.


Figure 10. Normalized Non-saturated HFE vs. Base Current and Temperature

## 4N25/ 4N26/ 4N27/ 4N28

## Vishay Semiconductors



Figure 11. Normalized HFE vs. Base Current and Temp.

${ }_{14 n 25}$. 12
Figure 12. Propagation Delay vs. Collector Load Resistor


Figure 13. Switching Timing

4N25/ 4N26/ 4N27/ 4N28

## Package Dimensions in Inches (mm)

For 4N25/26/27..... see DIL300-6 Package dimension in the Package Section.
For 4N28 and for products with an option designator (e.g. 4N25-X001 or 4N26-X007)..... see DIP-6 Package dimensions in the Package Section.

## DIL300-6 Package Dimensions



## DIP-6 Package Dimensions


i178004

## 4N25/ 4N26/ 4N27/ 4N28

## Vishay Semiconductors



## Ozone Depleting Substances Policy Statement

It is the policy of Vishay Semiconductor GmbH to

1. Meet all present and future national and international statutory requirements.
2. Regularly and continuously improve the performance of our products, processes, distribution and operatingsystems with respect to their impact on the health and safety of our employees and the public, as well as their impact on the environment.
It is particular concern to control or eliminate releases of those substances into the atmosphere which are known as ozone depleting substances (ODSs).

The Montreal Protocol (1987) and its London Amendments (1990) intend to severely restrict the use of ODSs and forbid their use within the next ten years. Various national and international initiatives are pressing for an earlier ban on these substances.

Vishay Semiconductor GmbH has been able to use its policy of continuous improvements to eliminate the use of ODSs listed in the following documents.

1. Annex A, B and list of transitional substances of the Montreal Protocol and the London Amendments respectively
2. Class I and II ozone depleting substances in the Clean Air Act Amendments of 1990 by the Environmental Protection Agency (EPA) in the USA
3. Council Decision 88/540/EEC and 91/690/EEC Annex A, B and C (transitional substances) respectively.

Vishay Semiconductor GmbH can certify that our semiconductors are not manufactured with ozone depleting substances and do not contain such substances.

We reserve the right to make changes to improve technical design and may do so without further notice.
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Vishay Semiconductor GmbH, P.O.B. 3535, D-74025 Heilbronn, Germany
Telephone: 49 (0)7131 67 2831, Fax number: 49 (0)7131 672423

## LM741

## Single Operational Amplifier

## Features

－Short circuit protection
－Excellent temperature stability
－Internal frequency compensation
－High Input voltage range
－Null of offset

## Internal Block Diagram



## Schematic Diagram



Absolute Maximum Ratings ( $\mathrm{TA}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ )

| Parameter | Symbol | Value | Unit |
| :--- | :---: | :---: | :---: |
| Supply Voltage | VCC | $\pm 18$ | V |
| Differential Input Voltage | VI(DIFF) | 30 | V |
| Input Voltage | VI | $\pm 15$ | V |
| Output Short Circuit Duration | - | Indefinite | - |
| Power Dissipation | PD | 500 | mW |
| Operating Temperature Range <br> LM741C <br> LM741I | TOPR | $0 \sim+70$ |  |
| Storage Temperature Range | $-40 \sim+85$ | ${ }^{\circ} \mathrm{C}$ |  |

## Electrical Characteristics

( $\mathrm{VCC}=15 \mathrm{~V}, \mathrm{VEE}=-15 \mathrm{~V} . \mathrm{TA}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise specified)

| Parameter | Symbol | Conditions |  | LM741C/LM741I |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. |  |
| Input Offset Voltage | VIo | $\mathrm{Rs} \leq 10 \mathrm{~K} \Omega$ |  | - | 2.0 | 6.0 | mV |
|  |  | RS $\leq 50 \Omega$ |  | - | - | - |  |
| Input Offset Voltage Adjustment Range | VIO(R) | $\mathrm{VCC}= \pm 20 \mathrm{~V}$ |  | - | $\pm 15$ | - | mV |
| Input Offset Current | 1 O |  | - | - | 20 | 200 | nA |
| Input Bias Current | IBIAS | - |  | - | 80 | 500 | nA |
| Input Resistance (Note1) | RI | $\mathrm{Vcc}= \pm 20 \mathrm{~V}$ |  | 0.3 | 2.0 | - | $\mathrm{M} \Omega$ |
| Input Voltage Range | $\mathrm{V}_{1}(\mathrm{R})$ |  | - | $\pm 12$ | $\pm 13$ | - | V |
| Large Signal Voltage Gain | Gv | RL $22 \mathrm{~K} \Omega$ | $\begin{aligned} & \text { VCC }= \pm 20 \mathrm{~V}, \\ & \mathrm{VO}(\mathrm{P}-\mathrm{P})= \pm 15 \mathrm{~V} \\ & \hline \end{aligned}$ | - | - | - | V/mV |
|  |  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}= \pm 15 \mathrm{~V}, \\ & \mathrm{VO}(\mathrm{P}-\mathrm{P})= \pm 10 \mathrm{~V} \end{aligned}$ | 20 | 200 | - |  |
| Output Short Circuit Current | Isc |  | - | - | 25 | - | mA |
| Output Voltage Swing | $\mathrm{V}_{\mathrm{O}}^{(\mathrm{P}-\mathrm{P})}$ | $\mathrm{VCC}= \pm 20 \mathrm{~V}$ | $\mathrm{RL} \geq 10 \mathrm{~K} \Omega$ | - | - | - | V |
|  |  |  | $\mathrm{RL} \geq 2 \mathrm{~K} \Omega$ | - | - | - |  |
|  |  | V CC $= \pm 15 \mathrm{~V}$ | $\mathrm{RL} \geq 10 \mathrm{~K} \Omega$ | $\pm 12$ | $\pm 14$ | - |  |
|  |  |  | $\mathrm{RL} \geq 2 \mathrm{~K} \Omega$ | $\pm 10$ | $\pm 13$ | - |  |
| Common Mode Rejection Ratio | CMRR | $\mathrm{RS} \leq 10 \mathrm{~K} \Omega$, Vcm | $\mathrm{M}= \pm 12 \mathrm{~V}$ | 70 | 90 | - | dB |
|  |  | $\mathrm{RS} \leq 50 \Omega$, VCM | $= \pm 12 \mathrm{~V}$ | - | - | - |  |
| Power Supply Rejection Ratio | PSRR | $\begin{aligned} & \mathrm{VCC}= \pm 15 \mathrm{~V} \\ & \mathrm{Rs} \leq 50 \Omega \end{aligned}$ | $\mathrm{O} \mathrm{VCC}= \pm 15 \mathrm{~V}$ | - | - | - | dB |
|  |  | $\begin{aligned} & \hline \mathrm{VCC}= \pm 15 \mathrm{~V} \\ & \mathrm{RS} \leq 10 \mathrm{~K} \Omega \end{aligned}$ | $\mathrm{O} \mathrm{VCC}= \pm 15 \mathrm{~V}$ | 77 | 96 | - |  |
| Transient Rise Time | TR | Unity Gain |  | - | 0.3 | - | $\mu \mathrm{s}$ |
|  | OS |  |  | - | 10 | - | \% |
| Bandwidth | BW |  | - | - | - | - | MHz |
| Slew Rate | SR | Unity Gain |  | - | 0.5 | - | V/us |
| Supply Current | IcC | $\mathrm{R} \mathrm{L}=\infty \Omega$ |  | - | 1.5 | 2.8 | mA |
| Power Consumption | PC | $\mathrm{VCC}= \pm 20 \mathrm{~V}$ |  | - | - | - | mW |
|  |  | $\mathrm{V} C \mathrm{C}= \pm 15 \mathrm{~V}$ |  | - | 50 | 85 |  |

Note:

1. Guaranteed by design.

## Electrical Characteristics

$\left(0^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 70^{\circ} \mathrm{C} V \mathrm{CC}= \pm 15 \mathrm{~V}\right.$, unless otherwise specified)
The following specification apply over the range of $0^{\circ} \mathrm{C} \leq \mathrm{TA} \leq+70^{\circ} \mathrm{C}$ for the LM 741 C ; and the $-40^{\circ} \mathrm{C} \leq \mathrm{TA} \leq+85^{\circ} \mathrm{C}$ for the LM741I

| Parameter | Symbol | Conditions |  |  | 41C/LI | 7411 | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Typ. | Max. |  |
| Input Offset Voltage | VIO | $\mathrm{Rs} \leq 50 \Omega$ |  | - | - | - | mV |
|  |  | $\mathrm{RS} \leq 10 \mathrm{~K} \Omega$ |  | - | - | 7.5 |  |
| Input Offset Voltage Drift | $\Delta \mathrm{VIO} / \Delta \mathrm{T}$ |  | - | - | - |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Offset Current | 1 IO |  | - | - | - | 300 | nA |
| Input Offset Current Drift | $\Delta \mathrm{l}$ IO/ $\Delta \mathrm{T}$ |  | - | - | - |  | $n A /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | IBIAS |  | - | - | - | 0.8 | $\mu \mathrm{A}$ |
| Input Resistance (Note1) | RI | $\mathrm{VCC}= \pm 20 \mathrm{~V}$ |  | - | - | - | $\mathrm{M} \Omega$ |
| Input Voltage Range | V ( R ) | - |  | $\pm 12$ | $\pm 13$ | - | V |
| Output Voltage Swing | $\mathrm{VO}(\mathrm{P}-\mathrm{P})$ | $\mathrm{VCC}= \pm 20 \mathrm{~V}$ | $\mathrm{R} \mathrm{s} \geq 10 \mathrm{~K} \Omega$ | - | - | - | V |
|  |  |  | $\mathrm{R} \mathrm{S} \geq 2 \mathrm{~K} \Omega$ | - | - | - |  |
|  |  | $\mathrm{VCC}= \pm 15 \mathrm{~V}$ | $\mathrm{R} S \geq 10 \mathrm{~K} \Omega$ | $\pm 12$ | $\pm 14$ | - |  |
|  |  |  | $\mathrm{R} S \geq 2 \mathrm{~K} \Omega$ | $\pm 10$ | $\pm 13$ | - |  |
| Output Short Circuit Current | ISC |  | - | 10 | - | 40 | mA |
| Common Mode Rejection Ratio | CMRR | $\mathrm{RS} \leq 10 \mathrm{~K} \Omega, \mathrm{~V} \mathrm{CM}= \pm 12 \mathrm{~V}$ |  | 70 | 90 | - | dB |
|  |  | $\mathrm{RS} \leq 50 \Omega$, VCM $= \pm 12 \mathrm{~V}$ |  | - | - | - |  |
| Power Supply Rejection Ratio | PSRR | $\begin{aligned} & \mathrm{VCC}= \pm 20 \mathrm{~V} \\ & \text { to } \pm 5 \mathrm{~V} \end{aligned}$ | $\mathrm{RS} \leq 50 \Omega$ | - | - | - | dB |
|  |  |  | $\mathrm{RS} \leq 10 \mathrm{~K} \Omega$ | 77 | 96 | - |  |
| Large Signal Voltage Gain | GV | $\mathrm{Rs} \geq 2 \mathrm{~K} \Omega$ | $\begin{aligned} & \mathrm{VCC}= \pm 20 \mathrm{~V}, \\ & \mathrm{VO}(P-P)= \pm 15 \mathrm{~V} \end{aligned}$ | - | - | - | $\mathrm{V} / \mathrm{mV}$ |
|  |  |  | $\begin{aligned} & \mathrm{VCC}= \pm 15 \mathrm{~V} \\ & \mathrm{VO}(\mathrm{P} . \mathrm{P})= \pm 10 \mathrm{~V} \end{aligned}$ | 15 | - | - |  |
|  |  |  | $\begin{aligned} & \mathrm{VCC}= \pm 15 \mathrm{~V}, \\ & \mathrm{VO}(P-P)= \pm 2 \mathrm{~V} \end{aligned}$ | - | - | - |  |

Note:

1. Guaranteed by design.

## Typical Performance Characteristics



Figure 1. Output Resistance vs Frequency


Figure 3. Input Bias Current vs Ambient Temperature


Figure 5. Input Offset Current vs Ambient Temperature


Figure 2. Input Resistance and Input Capacitance vs Frequency


Figure 4. Power Consumption vs Ambient Temperature


Figure 6. Input Resistance vs Ambient Temperature

## Typical Performance Characteristics (continued)



Figure 7. Normalized DC Parameters vs Ambient Temperature


Figure 9. Frequency Characteristics vs Supply Voltage


Figure 11. Transient Response


Figure 8. Frequency Characteristics vs Ambient Temperature


Figure 10. Output Short Circuit Current vs Ambient Temperature


Figure 12. Common-Mode Rejection Ratio vs Frequency

## Typical Performance Characteristics (continued)



Figure 13. Voltage Follower Large Signal Pulse Response


Figure 14. Output Swing and Input Range vs Supply Voltage

## Mechanical Dimensions

## Package

## 8-DIP



Mechanical Dimensions (Continued)

## Package



## Ordering Information

| Product Number | Package | Operating Temperature |
| :---: | :---: | :---: |
| LM 741 CN | 8 -DIP | $\sim+70^{\circ} \mathrm{C}$ |
| LM 741 CM | $8-\mathrm{SOP}$ |  |
| LM 741 IN | $8-\mathrm{DIP}$ | $-40 \sim+85^{\circ} \mathrm{C}$ |

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2. A critical component in any component of a life support device or system whose failure to perform can be reasonably expected to cause the failure of the life support device or system, or to affect its safety or effectiveness.

## DESCRIPTION

The LM319 series are precision high-speed dual comparators fabricated on a single monolithic chip. They are designed to operate over a wide range of supply voltages down to a single 5 V logic supply and ground. Further, they have higher gain and lower input currents than devices like the $\mu \mathrm{A} 710$. The uncommitted collector of the output stage makes the LM319 compatible with RTL, DTL, and TTL as well as capable of driving lamps and relays at currents up to 25 mA .

Although designed primarily for applications requiring operation from digital logic supplies, the LM319 series are fully specified for power supplies up to $\pm 15 \mathrm{~V}$. It features faster response than the LM111 at the expense of higher power dissipation. However, the high-speed, wide operating voltage range and low package count make the LM319 much more versatile than older devices like the $\mu \mathrm{A} 711$.

## FEATURES

- Two independent comparators
- Operates from a single 5 V supply
- Typically 80 ns response time at $\pm 15 \mathrm{~V}$
- Minimum fanout of 3 (each side)


## PIN CONFIGURATION

## D, N Packages



- Maximum input current of $1 \mu \mathrm{~A}$ over temperature
- Inputs and outputs can be isolated from system ground
- High common-mode slew rate


## EQUIVALENT SCHEMATIC



## ORDERING INFORMATION

| DESCRIPTION | TEMPERATURE RANGE | ORDER CODE | DWG \# |
| :--- | :---: | :---: | :---: |
| 14-Pin Plastic Small Outline (SO) Package | -25 to $+85^{\circ} \mathrm{C}$ | LM219D | 0175 D |
| 14-Pin Plastic Small Outline (SO) Package | 0 to $+70^{\circ} \mathrm{C}$ | LM319D | 0175 D |
| 14-Pin Plastic Dual In-Line Package (DIP) | 0 to $+70^{\circ} \mathrm{C}$ | LM319N | 0405 B |

## ABSOLUTE MAXIMUM RATINGS

| SYMBOL | PARAMETER | RATING | UNIT |
| :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {S }}$ | Total supply voltage | 36 | V |
|  | Output to negative supply voltage | 36 | V |
|  | Ground to negative supply voltage | 25 | V |
|  | Ground to positive supply voltage | 18 | V |
|  | Differential input voltage | $\pm 5$ | V |
| $\mathrm{V}_{\text {IN }}$ | Input voltage ${ }^{1}$ | $\pm 15$ | V |
|  | Maximum power dissipation, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ (still-air) ${ }^{2}$ <br> N package <br> D package | $\begin{aligned} & 1420 \\ & 1040 \end{aligned}$ | $\begin{gathered} \mathrm{mW} \\ \mathrm{~mW} \end{gathered}$ |
|  | Output short-circuit duration | 10 | s |
| $\mathrm{T}_{\mathrm{A}}$ | $\begin{array}{lr}\text { Operating temperature range } & \text { LM219 } \\ \text { LM319 }\end{array}$ | $\begin{gathered} -25 \text { to }+85 \\ 0 \text { to }+70 \end{gathered}$ | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {STG }}$ | Storage temperature range | -65 to +150 | ${ }^{\circ} \mathrm{C}$ |
| TSOLD | Lead soldering temperature (10sec max) | 300 | ${ }^{\circ} \mathrm{C}$ |

NOTES:

1. For supply voltages less than $\pm 15 \mathrm{~V}$, the absolute maximum rating is equal to the supply voltage.
2. Derate above $25^{\circ} \mathrm{C}$, at the following rates:

N package at $11.4 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$
D package at $8.3 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$
DC ELECTRICAL CHARACTERISTICS
$\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V},-25^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 85^{\circ} \mathrm{C}$ for $\mathrm{LM} 219,0^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 70^{\circ} \mathrm{C}$ for LM 319 , unless otherwise specified.

| SYMBOL | PARAMETER | TEST CONDITIONS | LM219 |  |  | LM319 |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min | Typ | Max | Min | Typ | Max |  |
| $\mathrm{V}_{\mathrm{OS}}$ | Input offset voltage ${ }^{1,2}$ | $\mathrm{R}_{\mathrm{S}} \leq 5 \mathrm{k} \Omega, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ Over temp. |  | 0.7 | $\begin{gathered} 4.0 \\ 7 \end{gathered}$ |  | 2.0 | $\begin{gathered} 8.0 \\ 10 \end{gathered}$ | mV |
| los | Input offset current ${ }^{1,2}$ | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ <br> Over temp. |  | 30 | $\begin{gathered} \hline 75 \\ 100 \\ \hline \end{gathered}$ |  | 80 | $\begin{aligned} & 200 \\ & 300 \\ & \hline \end{aligned}$ | nA |
| $\mathrm{I}_{\mathrm{B}}$ | Input bias current ${ }^{1}$ | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ <br> Over temp. |  | 150 | $\begin{gathered} \hline 500 \\ 1000 \\ \hline \end{gathered}$ |  | 250 | $\begin{aligned} & 1000 \\ & 1200 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{nA} \\ & \mathrm{nA} \end{aligned}$ |
| $\mathrm{A}_{V}$ | Voltage gain | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 8 | 40 |  | 8 | 40 |  | V/mV |
| VoL | Saturation voltage | $\begin{gathered} \mathrm{V}_{\mathrm{IN}_{\mathrm{N}} \leq-10 \mathrm{mV}, \mathrm{I}_{\text {OUT }}=25 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C},} \\ \mathrm{~V}+\geq 4.5 \mathrm{~V}, \mathrm{~V}-=0 \\ \mathrm{~V}_{\text {IN }} \leq-10 \mathrm{mV}, \mathrm{I}_{\text {OUT }}=3.2 \mathrm{~mA} \end{gathered}$ |  | $\begin{gathered} 0.75 \\ 0.3 \end{gathered}$ | $\begin{aligned} & 1.5 \\ & 0.6 \end{aligned}$ |  | $\begin{gathered} 0.75 \\ 0.3 \end{gathered}$ | $\begin{aligned} & 1.5 \\ & 0.4 \end{aligned}$ | V |
| IOH | Output leakage current | $\begin{gathered} \mathrm{V}-=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}} \geq 10 \mathrm{mV} \\ \mathrm{~V}_{\text {OUT }}=35 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \end{gathered}$ |  | 0.2 | 10 |  | 0.2 | 10 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\mathrm{IN}}$ | Input voltage range | $\begin{gathered} \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V} \\ \mathrm{~V}+=5 \mathrm{~V}, \mathrm{~V}-=0 \mathrm{~V} \end{gathered}$ | 1 | $\pm 13$ | 3 | 1 | $\pm 13$ | 3 | V |
| $\mathrm{V}_{\text {ID }}$ | Differential input voltage |  |  |  | $\pm 5$ |  |  | $\pm 5$ | V |
| I+ | Positive supply current | $\mathrm{V}+=5 \mathrm{~V}, \mathrm{~V}-=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 4.3 |  |  | 4.3 |  | mA |
| + | Positive supply current | $\mathrm{V}_{S}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 8.0 | 12.5 |  | 8.0 | 12.5 | mA |
| I- | Negative supply current | $\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  | 3.0 | 5.0 |  | 3.0 | 5.0 | mA |

## NOTES:

1. $V_{O S}$, $l_{\text {Os }}$ and $I_{B}$ specifications apply for a supply voltage range of $V_{S}= \pm 15 \mathrm{~V}$ down to a single 5 V supply.
2. The offset voltages and offset currents given are the maximum values required to drive the output to within 1 V of either supply with a 1 mA load. Thus these parameters define an error band and take into account the worst case effects of voltage gain and input impedance.

## Dual voltage comparator

## AC ELECTRICAL CHARACTERISTICS

| SYMBOL | PARAMETER | TEST CONDITIONS | LIMITS |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min | Typ | Max |  |
| $t_{R}$ | Response time ${ }^{1}$ | $\begin{gathered} \mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C} \\ \mathrm{R}_{\mathrm{L}}=500 \Omega \text { (see test figure) } \end{gathered}$ |  | 80 |  | ns |

NOTES:

1. The response time specified is for a 100 mV step with 5 mV overdrive.

## TEST CIRCUIT



TYPICAL PERFORMANCE CHARACTERISTICS


TYPICAL PERFORMANCE CHARACTERISTICS (Continued)


## TYPICAL APPLICATIONS




## Flex Sensor

## Features

- Angle Displacement Measurement
- Bends and Flexes physically with motion device
- Possible Uses
- Robotics
- Gaming (Virtual Motion)
- Medical Devices
- Computer Peripherals
- Musical Instruments
- Physical Therapy
- Simple Construction
- Low Profile


## Mechanical Specifications

-Life Cycle: >1 million
-Height: $\leq 0.43 \mathrm{~mm}$ (0.017")
-Temperature Range: $-35^{\circ} \mathrm{C}$ to $+80^{\circ} \mathrm{C}$

## Electrical Specifications

-Flat Resistance: 10K Ohms
-Resistance Tolerance: $\pm 30 \%$
-Bend Resistance Range: 60K to 110K Ohms
-Power Rating : 0.50 Watts continuous. 1 Watt Peak

## Dimensional Diagram - Stock Flex Sensor



How to Order - Stock Flex Sensor


How It Works


## BASIC FLEX SENSOR CIRCUIT:



Following are notes from the ITP Flex Sensor Workshop
"The impedance buffer in the [Basic Flex Sensor Circuit] (above) is a single sided operational amplifier, used with these sensors because the low bias current of the op amp reduces errer due to source impedance of the flex sensor as voltage divider. Suggested op amps are the LM358 or LM324."
"You can also test your flex sensor using the simplest circut, and skip the op amp."
"Adjustable Buffer - a potentiometer can be added to the circuit to adjust the sensitivity range."


Figure 1.1
Figure 1.2
"Variable Deflection Threshold Switch - an op amp is used and outputs either high or low depending on the voltage of the inverting input. In this way you can use the flex sensor as a switch without going through a microcontroller."

"Resistance to Voltage Converter - use the sensor as the input of a resistance to voltage converter using a dual sided supply op-amp. A negative reference voltage will give a positive output. Should be used in situations when you want output at a low degree of bending."


- 3-Terminal Regulators
- Output Current up to 1.5 A
- Internal Thermal-Overload Protection

KC (TO-220) PACKAGE
(TOP VIEW)


## - High Power-Dissipation Capability

- Internal Short-Circuit Current Limiting
- Output Transistor Safe-Area Compensation

KTE PACKAGE
(TOP VIEW)


## description/ordering information

This series of fixed-voltage integrated-circuit voltage regulators is designed for a wide range of applications. These applications include on-card regulation for elimination of noise and distribution problems associated with single-point regulation. Each of these regulators can deliver up to 1.5 A of output current. The internal current-limiting and thermal-shutdown features of these regulators essentially make them immune to overload. In addition to use as fixed-voltage regulators, these devices can be used with external components to obtain adjustable output voltages and currents, and also can be used as the power-pass element in precision regulators.

ORDERING INFORMATION

| $\mathrm{T}_{\mathrm{J}}$ | $\begin{gathered} \mathrm{V}_{\mathrm{O}(\mathrm{NOM})}^{(\mathrm{V})} \mathrm{C} \end{gathered}$ | PACKAGE $\dagger$ |  | ORDERABLE PART NUMBER | TOP-SIDE MARKING |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 5 | POWER-FLEX (KTE) | Reel of 2000 | $\mu$ A7805CKTER | $\mu$ A7805C |
|  |  | TO-220 (KC) | Tube of 50 | $\mu \mathrm{A} 7805 \mathrm{CKC}$ | $\mu \mathrm{A} 7805 \mathrm{C}$ |
|  |  | TO-220, short shoulder (KCS) | Tube of 20 | $\mu \mathrm{A} 7805 \mathrm{CKCS}$ |  |
|  | 8 | POWER-FLEX (KTE) | Reel of 2000 | $\mu \mathrm{A} 7808 \mathrm{CKTER}$ | $\mu$ A7808C |
|  |  | TO-220 (KC) | Tube of 50 | $\mu \mathrm{A} 7808 \mathrm{CKC}$ | $\mu A 7808 \mathrm{C}$ |
|  |  | TO-220, short shoulder (KCS) | Tube of 20 | $\mu \mathrm{A} 7808 \mathrm{CKCS}$ |  |
|  | 10 | POWER-FLEX (KTE) | Reel of 2000 | $\mu \mathrm{A} 7810 \mathrm{CKTER}$ | $\mu \mathrm{A} 7810 \mathrm{C}$ |
|  |  | TO-220 (KC) | Tube of 50 | $\mu \mathrm{A} 7810 \mathrm{CKC}$ | $\mu \mathrm{A} 7810 \mathrm{C}$ |
|  | 12 | POWER-FLEX (KTE) | Reel of 2000 | $\mu \mathrm{A} 7812 \mathrm{CKTER}$ | $\mu \mathrm{A} 7812 \mathrm{C}$ |
|  |  | TO-220 (KC) | Tube of 50 | $\mu \mathrm{A} 7812 \mathrm{CKC}$ | $\mu$ A7812C |
|  |  | TO-220, short shoulder (KCS) | Tube of 20 | $\mu$ A7812CKCS |  |
|  | 15 | POWER-FLEX (KTE) | Reel of 2000 | $\mu \mathrm{A} 7815 \mathrm{CKTER}$ | $\mu$ A7815C |
|  |  | TO-220 (KC) | Tube of 50 | $\mu \mathrm{A} 7815 \mathrm{CKC}$ | $\mu \mathrm{A} 7815 \mathrm{C}$ |
|  |  | TO-220, short shoulder (KCS) | Tube of 20 | $\mu$ A7815CKCS |  |
|  | 24 | POWER-FLEX (KTE) | Reel of 2000 | $\mu \mathrm{A} 7824 \mathrm{CKTER}$ | $\mu$ A7824C |
|  |  | TO-220 (KC) | Tube of 50 | $\mu \mathrm{A} 7824 \mathrm{CKC}$ | $\mu \mathrm{A} 7824 \mathrm{C}$ |

†Package drawings, standard packing quantities, thermal data, symbolization, and PCB design guidelines are available at www.ti.com/sc/package.

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## schematic


absolute maximum ratings over virtual junction temperature range (unless otherwise noted) $\dagger$
Input voltage, $\mathrm{V}_{\mathrm{I}}: \mu \mathrm{A} 7824 \mathrm{C}$ ..... 40 V
All others ..... 35 V
Operating virtual junction temperature, $\mathrm{T}_{\mathrm{J}}$ ..... $150^{\circ} \mathrm{C}$
Lead temperature $1,6 \mathrm{~mm}$ ( $1 / 16$ inch) from case for 10 seconds ..... $260^{\circ} \mathrm{C}$
Storage temperature range, $\mathrm{T}_{\text {stg }}$ ..... $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
$\dagger$ Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

## package thermal data (see Note 1)

| PACKAGE | BOARD | $\theta \mathbf{J C}$ | $\theta$ JA |
| :---: | :---: | :---: | :---: |
| POWER-FLEX (KTE) | High K, JESD $51-5$ | $3^{\circ} \mathrm{C} / \mathrm{W}$ | $23^{\circ} \mathrm{C} / \mathrm{W}$ |
| TO-220 (KC/KCS) | High K, JESD $51-5$ | $3^{\circ} \mathrm{C} / \mathrm{W}$ | $19^{\circ} \mathrm{C} / \mathrm{W}$ |

NOTE 1: Maximum power dissipation is a function of $T_{J}(\max ), \theta_{J A}$, and $T_{A}$. The maximum allowable power dissipation at any allowable ambient temperature is $P_{D}=\left(T_{J}(\max )-T_{A}\right) / \theta_{J A}$. Operating at the absolute maximum $T_{J}$ of $150^{\circ} \mathrm{C}$ can affect reliability.

## recommended operating conditions

|  |  | MIN | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{I}} \quad$ Input voltage | $\mu$ A7805C | 7 | 25 | V |
|  | $\mu \mathrm{A} 7808 \mathrm{C}$ | 10.5 | 25 |  |
|  | $\mu \mathrm{A} 810 \mathrm{C}$ | 12.5 | 28 |  |
|  | $\mu$ A7812C | 14.5 | 30 |  |
|  | $\mu \mathrm{A} 8815 \mathrm{C}$ | 17.5 | 30 |  |
|  | $\mu \mathrm{A} 7824 \mathrm{C}$ | 27 | 38 |  |
| IO Output current |  |  | 1.5 | A |
| $\mathrm{T}_{\mathrm{J}} \quad$ Operating virtual junction temperature | $\mu \mathrm{A} 7800 \mathrm{C}$ series | 0 | 125 | ${ }^{\circ} \mathrm{C}$ |

electrical characteristics at specified virtual junction temperature, $\mathrm{V}_{\mathrm{I}}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=500 \mathrm{~mA}$ (unless otherwise noted)

| PARAMETER | TEST CONDITIONS |  | $\mathrm{T}_{\mathbf{J}} \dagger$ | $\mu \mathrm{A} 7805 \mathrm{C}$ |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX |  |
| Output voltage | $\begin{aligned} & \mathrm{l}=5 \mathrm{~mA} \text { to } 1 \mathrm{~A}, \\ & \mathrm{PD}_{\mathrm{D}} \leq 15 \mathrm{~W} \end{aligned}$ | $\mathrm{V}_{\mathrm{I}}=7 \mathrm{~V}$ to 20 V , |  | $25^{\circ} \mathrm{C}$ | 4.8 | 5 | 5.2 | V |
|  |  |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 4.75 |  | 5.25 |  |  |
| Input voltage regulation | $\mathrm{V}_{\mathrm{I}}=7 \mathrm{~V}$ to 25 V |  | $25^{\circ} \mathrm{C}$ |  | 3 | 100 | mV |  |
|  | $\mathrm{V}_{1}=8 \mathrm{~V}$ to 12 V |  |  |  | 1 | 50 |  |  |
| Ripple rejection | $\mathrm{V}_{\mathrm{I}}=8 \mathrm{~V}$ to 18 V , | $\mathrm{f}=120 \mathrm{~Hz}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 62 | 78 |  | dB |  |
| Output voltage regulation | $\mathrm{O}=5 \mathrm{~mA}$ to 1.5 A |  | $25^{\circ} \mathrm{C}$ |  | 15 | 100 | mV |  |
|  | $\mathrm{I}=250 \mathrm{~mA}$ to 75 |  |  |  | 5 | 50 |  |  |
| Output resistance | $\mathrm{f}=1 \mathrm{kHz}$ |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | 0.017 |  | $\Omega$ |  |
| Temperature coefficient of output voltage | $\mathrm{O}=5 \mathrm{~mA}$ |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | -1.1 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |  |
| Output noise voltage | $\mathrm{f}=10 \mathrm{~Hz}$ to 100 k |  | $25^{\circ} \mathrm{C}$ |  | 40 |  | $\mu \mathrm{V}$ |  |
| Dropout voltage | $\mathrm{O}=1 \mathrm{~A}$ |  | $25^{\circ} \mathrm{C}$ |  | 2 |  | V |  |
| Bias current |  |  | $25^{\circ} \mathrm{C}$ |  | 4.2 | 8 | mA |  |
| Bias current change | $\mathrm{V}_{\mathrm{I}}=7 \mathrm{~V}$ to 25 V |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  |  | 1.3 | mA |  |
|  | $\mathrm{I}=5 \mathrm{~mA}$ to 1 A |  |  |  |  | 0.5 |  |  |
| Short-circuit output current |  |  | $25^{\circ} \mathrm{C}$ |  | 750 |  | mA |  |
| Peak output current |  |  | $25^{\circ} \mathrm{C}$ |  | 2.2 |  | A |  |

$\dagger$ Pulse-testing techniques maintain the junction temperature as close to the ambient temperature as possible. Thermal effects must be taken into account separately. All characteristics are measured with a $0.33-\mu \mathrm{F}$ capacitor across the input and a $0.1-\mu \mathrm{F}$ capacitor across the output.

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electrical characteristics at specified virtual junction temperature, $\mathrm{V}_{\mathrm{I}}=14 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=500 \mathrm{~mA}$ (unless otherwise noted)

| PARAMETER | TEST CONDITIONS | TJ $\dagger$ | $\mu \mathrm{A} 7808 \mathrm{C}$ |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX |  |
| Output voltage | $\mathrm{l} \mathrm{l}=5 \mathrm{~mA}$ to $1 \mathrm{~A}, \quad \mathrm{~V}_{\mathrm{I}}=10.5 \mathrm{~V}$ to 23 V,$\mathrm{P}_{\mathrm{D}} \leq 15 \mathrm{~W}$ | $25^{\circ} \mathrm{C}$ | 7.7 | 8 | 8.3 | V |
|  |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 7.6 |  | 8.4 |  |
| Input voltage regulation | $\mathrm{V}_{1}=10.5 \mathrm{~V}$ to 25 V | $25^{\circ} \mathrm{C}$ |  | 6 | 160 | mV |
|  | $\mathrm{V}_{\mathrm{I}}=11 \mathrm{~V}$ to 17 V |  |  | 2 | 80 |  |
| Ripple rejection | $\mathrm{V}_{\mathrm{I}}=11.5 \mathrm{~V}$ to $21.5 \mathrm{~V}, \quad \mathrm{f}=120 \mathrm{~Hz}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 55 | 72 |  | dB |
| Output voltage regulation | $\mathrm{O}=5 \mathrm{~mA}$ to 1.5 A | $25^{\circ} \mathrm{C}$ |  | 12 | 160 | mV |
|  | $\mathrm{O}=250 \mathrm{~mA}$ to 750 mA |  |  | 4 | 80 |  |
| Output resistance | $\mathrm{f}=1 \mathrm{kHz}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | 0.016 |  | $\Omega$ |
| Temperature coefficient of output voltage | $\mathrm{O}=5 \mathrm{~mA}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | -0.8 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| Output noise voltage | $\mathrm{f}=10 \mathrm{~Hz}$ to 100 kHz | $25^{\circ} \mathrm{C}$ |  | 52 |  | $\mu \mathrm{V}$ |
| Dropout voltage | $\mathrm{l}=1 \mathrm{~A}$ | $25^{\circ} \mathrm{C}$ |  | 2 |  | V |
| Bias current |  | $25^{\circ} \mathrm{C}$ |  | 4.3 | 8 | mA |
| Bias current change | $\mathrm{V}_{\mathrm{l}}=10.5 \mathrm{~V}$ to 25 V | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  |  | 1 | mA |
|  | $\mathrm{l} \mathrm{O}=5 \mathrm{~mA}$ to 1 A |  |  |  | 0.5 |  |
| Short-circuit output current |  | $25^{\circ} \mathrm{C}$ |  | 450 |  | mA |
| Peak output current |  | $25^{\circ} \mathrm{C}$ |  | 2.2 |  | A |

$\dagger$ Pulse-testing techniques maintain the junction temperature as close to the ambient temperature as possible. Thermal effects must be taken into account separately. All characteristics are measured with a $0.33-\mu \mathrm{F}$ capacitor across the input and a $0.1-\mu \mathrm{F}$ capacitor across the output.
electrical characteristics at specified virtual junction temperature, $\mathrm{V}_{\mathrm{I}}=17 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=500 \mathrm{~mA}$ (unless otherwise noted)

| PARAMETER | TEST CONDITIONS |  | TJ $\dagger$ | $\mu \mathrm{A} 7810 \mathrm{C}$ |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX |  |
| Output voltage | $\begin{aligned} & \mathrm{l}=5 \mathrm{~mA} \text { to } 1 \mathrm{~A}, \\ & \mathrm{PD}_{\mathrm{D}} \leq 15 \mathrm{~W} \end{aligned}$ | $\mathrm{V}=12.5 \mathrm{~V}$ to 25 V , |  | $25^{\circ} \mathrm{C}$ | 9.6 | 10 | 10.4 | V |
|  |  |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 9.5 | 10 | 10.5 |  |  |
| Input voltage regulation | $\mathrm{V}_{1}=12.5 \mathrm{~V}$ to 28 V |  | $25^{\circ} \mathrm{C}$ |  | 7 | 200 | mV |  |
|  | $\mathrm{V}_{\mathrm{I}}=14 \mathrm{~V}$ to 20 V |  |  |  | 2 | 100 |  |  |
| Ripple rejection | $\mathrm{V}_{1}=13 \mathrm{~V}$ to 23 V , | $\mathrm{f}=120 \mathrm{~Hz}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 55 | 71 |  | dB |  |
| Output voltage regulation | $\mathrm{O}=5 \mathrm{~mA}$ to 1.5 A |  | $25^{\circ} \mathrm{C}$ |  | 12 | 200 | mV |  |
|  | $\mathrm{I}=250 \mathrm{~mA}$ to 750 mA |  |  |  | 4 | 100 |  |  |
| Output resistance | $\mathrm{f}=1 \mathrm{kHz}$ |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | 0.018 |  | $\Omega$ |  |
| Temperature coefficient of output voltage | $\mathrm{O}=5 \mathrm{~mA}$ |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | -1 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |  |
| Output noise voltage | $\mathrm{f}=10 \mathrm{~Hz}$ to 100 kHz |  | $25^{\circ} \mathrm{C}$ |  | 70 |  | $\mu \mathrm{V}$ |  |
| Dropout voltage | $\mathrm{I}=1 \mathrm{~A}$ |  | $25^{\circ} \mathrm{C}$ | 2 |  |  | V |  |
| Bias current |  |  | $25^{\circ} \mathrm{C}$ |  | 4.3 | 8 | mA |  |
| Bias current change | $\begin{array}{\|l} \hline \mathrm{V}_{\mathrm{I}}=12.5 \mathrm{~V} \text { to } 28 \mathrm{~V} \\ \hline \mathrm{I} \mathrm{O}=5 \mathrm{~mA} \text { to } 1 \mathrm{~A} \\ \hline \end{array}$ |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 0.5 |  |  | mA |  |
|  |  |  |  |  |  |  |  |  |  |
| Short-circuit output current |  |  | $25^{\circ} \mathrm{C}$ |  | 400 |  | mA |  |
| Peak output current |  |  | $25^{\circ} \mathrm{C}$ |  | 2.2 |  | A |  |

$\dagger$ Pulse-testing techniques maintain the junction temperature as close to the ambient temperature as possible. Thermal effects must be taken into account separately. All characteristics are measured with a $0.33-\mu \mathrm{F}$ capacitor across the input and a $0.1-\mu \mathrm{F}$ capacitor across the output.
electrical characteristics at specified virtual junction temperature, $\mathrm{V}_{\mathrm{I}}=19 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=500 \mathrm{~mA}$ (unless otherwise noted)

| PARAMETER | TEST CONDITIONS |  | TJ $\dagger$ | $\mu \mathrm{A} 7812 \mathrm{C}$ |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX |  |
| Output voltage | $\begin{aligned} & \mathrm{l} \mathrm{O}=5 \mathrm{~mA} \text { to } 1 \mathrm{~A}, \\ & \mathrm{P}_{\mathrm{D}} \leq 15 \mathrm{~W} \end{aligned}$ | $\mathrm{V}=14.5 \mathrm{~V}$ to 27 V , |  | $25^{\circ} \mathrm{C}$ | 11.5 | 12 | 12.5 | V |
|  |  |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 11.4 |  | 12.6 |  |  |
| Input voltage regulation | $\mathrm{V}_{\mathrm{I}}=14.5 \mathrm{~V}$ to 30 V |  | $25^{\circ} \mathrm{C}$ |  | 10 | 240 | mV |  |
|  | $\mathrm{V}_{1}=16 \mathrm{~V}$ to 22 V |  |  |  | 3 | 120 |  |  |
| Ripple rejection | $\mathrm{V}_{\mathrm{l}}=15 \mathrm{~V}$ to 25 V , | $\mathrm{f}=120 \mathrm{~Hz}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 55 | 71 |  | dB |  |
| Output voltage regulation | $\mathrm{O}=5 \mathrm{~mA}$ to 1.5 A |  | $25^{\circ} \mathrm{C}$ |  | 12 | 240 | mV |  |
|  | $\mathrm{I} \mathrm{O}=250 \mathrm{~mA}$ to 750 mA |  |  |  | 4 | 120 |  |  |
| Output resistance | $\mathrm{f}=1 \mathrm{kHz}$ |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | 0.018 |  | $\Omega$ |  |
| Temperature coefficient of output voltage | $\mathrm{I}=5 \mathrm{~mA}$ |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | -1 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |  |
| Output noise voltage | $\mathrm{f}=10 \mathrm{~Hz}$ to 100 k |  | $25^{\circ} \mathrm{C}$ |  | 75 |  | $\mu \mathrm{V}$ |  |
| Dropout voltage | $\mathrm{O}=1 \mathrm{~A}$ |  | $25^{\circ} \mathrm{C}$ |  | 2 |  | V |  |
| Bias current |  |  | $25^{\circ} \mathrm{C}$ |  | 4.3 | 8 | mA |  |
| Bias current change | $\mathrm{V}_{\mathrm{I}}=14.5 \mathrm{~V}$ to 30 V |  |  |  |  | 1 | mA |  |
| Bias current change | $\mathrm{I}=5 \mathrm{~mA}$ to 1 A |  | $0^{\circ} \mathrm{C}$ to 125 ${ }^{\circ}$ |  |  | 0.5 |  |  |
| Short-circuit output current |  |  | $25^{\circ} \mathrm{C}$ |  | 350 |  | mA |  |
| Peak output current |  |  | $25^{\circ} \mathrm{C}$ |  | 2.2 |  | A |  |

$\dagger$ Pulse-testing techniques maintain the junction temperature as close to the ambient temperature as possible. Thermal effects must be taken into account separately. All characteristics are measured with a $0.33-\mu \mathrm{F}$ capacitor across the input and a $0.1-\mu \mathrm{F}$ capacitor across the output.
electrical characteristics at specified virtual junction temperature, $\mathrm{V}_{\mathrm{I}}=23 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=500 \mathrm{~mA}$ (unless otherwise noted)

| PARAMETER | TEST CONDITIONS | $\mathrm{T}_{\mathbf{J}}{ }^{\dagger}$ | $\mu \mathrm{A} 7815 \mathrm{C}$ |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX |  |
| Output voltage | $\mathrm{l} \mathrm{l}^{\prime}=5 \mathrm{~mA}$ to 1 A,$\mathrm{PD} \leq 15 \mathrm{~W}$ | $25^{\circ} \mathrm{C}$ | 14.4 | 15 | 15.6 | V |
|  |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 14.25 |  | 15.75 |  |
| Input voltage regulation | $\mathrm{V}_{1}=17.5 \mathrm{~V}$ to 30 V | $25^{\circ} \mathrm{C}$ |  | 11 | 300 | mV |
|  | $\mathrm{V}_{\mathrm{I}}=20 \mathrm{~V}$ to 26 V |  |  | 3 | 150 |  |
| Ripple rejection | $\mathrm{V}_{\mathrm{I}}=18.5 \mathrm{~V}$ to $28.5 \mathrm{~V}, \mathrm{f}=120 \mathrm{~Hz}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 54 | 70 |  | dB |
| Output voltage regulation | $\mathrm{I}=5 \mathrm{~mA}$ to 1.5 A | $25^{\circ} \mathrm{C}$ |  | 12 | 300 | mV |
|  | l = 250 mA to 750 mA |  |  | 4 | 150 |  |
| Output resistance | $\mathrm{f}=1 \mathrm{kHz}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | 0.019 |  | $\Omega$ |
| Temperature coefficient of output voltage | $\mathrm{O}=5 \mathrm{~mA}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | -1 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| Output noise voltage | $\mathrm{f}=10 \mathrm{~Hz}$ to 100 kHz | $25^{\circ} \mathrm{C}$ |  | 90 |  | $\mu \mathrm{V}$ |
| Dropout voltage | $\mathrm{O}=1 \mathrm{~A}$ | $25^{\circ} \mathrm{C}$ |  | 2 |  | V |
| Bias current |  | $25^{\circ} \mathrm{C}$ |  | 4.4 | 8 | mA |
| Bias current change | $\mathrm{V}_{\mathrm{I}}=17.5 \mathrm{~V}$ to 30 V | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  |  | 1 | mA |
|  | $\mathrm{I} \mathrm{O}=5 \mathrm{~mA}$ to 1 A |  |  |  | 0.5 |  |
| Short-circuit output current |  | $25^{\circ} \mathrm{C}$ |  | 230 |  | mA |
| Peak output current |  | $25^{\circ} \mathrm{C}$ |  | 2.1 |  | A |

$\dagger$ Pulse-testing techniques maintain the junction temperature as close to the ambient temperature as possible. Thermal effects must be taken into account separately. All characteristics are measured with a $0.33-\mu \mathrm{F}$ capacitor across the input and a $0.1-\mu \mathrm{F}$ capacitor across the output.

## electrical characteristics at specified virtual junction temperature, $\mathrm{V}_{\mathrm{I}}=33 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=500 \mathrm{~mA}$ (unless otherwise noted)

| PARAMETER | TEST CONDITIONS |  | TJ $\dagger$ | $\mu \mathrm{A} 7824 \mathrm{C}$ |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MIN | TYP | MAX |  |
| Output voltage | $\begin{aligned} & \mathrm{IO}=5 \mathrm{~mA} \text { to } 1 \mathrm{~A}, \\ & \mathrm{P}_{\mathrm{D}} \leq 15 \mathrm{~W} \end{aligned}$ | $\mathrm{V}_{\mathrm{I}}=27 \mathrm{~V}$ to 38 V , |  | $25^{\circ} \mathrm{C}$ | 23 | 24 | 25 | V |
|  |  |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 22.8 |  | 25.2 |  |  |
| Input voltage regulation | $\mathrm{V}_{\mathrm{I}}=27 \mathrm{~V}$ to 38 V |  | $25^{\circ} \mathrm{C}$ |  | 18 | 480 | mV |  |
|  | $\mathrm{V}_{1}=30 \mathrm{~V}$ to 36 V |  |  |  | 6 | 240 |  |  |
| Ripple rejection | $\mathrm{V}_{\mathrm{I}}=28 \mathrm{~V}$ to 38 V , | $\mathrm{f}=120 \mathrm{~Hz}$ | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 50 | 66 |  | dB |  |
| Output voltage regulation | $1 \mathrm{O}=5 \mathrm{~mA}$ to 1.5 A |  | $25^{\circ} \mathrm{C}$ |  | 12 | 480 | mV |  |
|  | $\mathrm{I} \mathrm{O}=250 \mathrm{~mA}$ to 750 mA |  |  |  | 4 | 240 |  |  |
| Output resistance | $\mathrm{f}=1 \mathrm{kHz}$ |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | 0.028 |  | $\Omega$ |  |
| Temperature coefficient of output voltage | $\mathrm{O}=5 \mathrm{~mA}$ |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | -1.5 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |  |
| Output noise voltage | $\mathrm{f}=10 \mathrm{~Hz}$ to 100 kHz |  | $25^{\circ} \mathrm{C}$ |  | 170 |  | $\mu \mathrm{V}$ |  |
| Dropout voltage | $\mathrm{I} \mathrm{O}=1 \mathrm{~A}$ |  | $25^{\circ} \mathrm{C}$ |  | 2 |  | V |  |
| Bias current |  |  | $25^{\circ} \mathrm{C}$ |  | 4.6 | 8 | mA |  |
| Bias current change | $\mathrm{V}_{\mathrm{I}}=27 \mathrm{~V}$ to 38 V |  | $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  |  | 1 | mA |  |
| Bias curent change | $\mathrm{l} \mathrm{O}=5 \mathrm{~mA}$ to 1 A |  | 0 to 125 |  |  | 0.5 |  |  |
| Short-circuit output current |  |  | $25^{\circ} \mathrm{C}$ |  | 150 |  | mA |  |
| Peak output current |  |  | $25^{\circ} \mathrm{C}$ |  | 2.1 |  | A |  |

$\dagger$ Pulse-testing techniques maintain the junction temperature as close to the ambient temperature as possible. Thermal effects must be taken into account separately. All characteristics are measured with a $0.33-\mu \mathrm{F}$ capacitor across the input and a $0.1-\mu \mathrm{F}$ capacitor across the output.

## APPLICATION INFORMATION



Figure 1. Fixed-Output Regulator


Figure 2. Positive Regulator in Negative Configuration (V| Must Float)


NOTE A: The following formula is used when $\mathrm{V}_{\mathrm{Xx}}$ is the nominal output voltage (output to common) of the fixed regulator:

$$
\mathrm{V}_{\mathrm{O}}=\mathrm{V}_{\mathrm{xx}}+\left(\frac{\mathrm{V}_{\mathrm{xx}}}{\mathrm{R} 1}+\mathrm{I}_{\mathrm{Q}}\right) \mathrm{R} 2
$$

Figure 3. Adjustable-Output Regulator


Figure 4. Current Regulator

APPLICATION INFORMATION


Figure 5. Regulated Dual Supply

## operation with a load common to a voltage of opposite polarity

In many cases, a regulator powers a load that is not connected to ground but, instead, is connected to a voltage source of opposite polarity (e.g., operational amplifiers, level-shifting circuits, etc.). In these cases, a clamp diode should be connected to the regulator output as shown in Figure 6. This protects the regulator from output polarity reversals during startup and short-circuit operation.


Figure 6. Output Polarity-Reversal-Protection Circuit

## reverse-bias protection

Occasionally, the input voltage to the regulator can collapse faster than the output voltage. This can occur, for example, when the input supply is crowbarred during an output overvoltage condition. If the output voltage is greater than approximately 7 V , the emitter-base junction of the series-pass element (internal or external) could break down and be damaged. To prevent this, a diode shunt can be used as shown in Figure 7.


Figure 7. Reverse-Bias-Protection Circuit


NOTES: A. All linear dimensions are in inches (millimeters).
B. This drawing is subject to change without notice.
C. The center lead is in electrical contact with the thermal tab.
D. Dimensions do not include mold protrusions, not to exceed $0.006(0,15)$.
E. Falls within JEDEC MO-169

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KCS (R-PSFM-T3)

## PLASTIC FLANGE-MOUNT PACKAGE



NOTES: A. All linear dimensions are in inches (millimeters).
B. This drawing is subject to change without notice.
(C) Lead dimensions are not controlled within this area.
D. All lead dimensions apply before solder dip.
E. The center lead is in electrical contact with the mounting tab.

The chamfer is optional.
G Thermal pad contour optional within these dimensions.
(H) Falls within JEDEC TO-220 variation AB, except minimum lead thickness.

KC (R-PSFM-T3)
PLASTIC FLANGE-MOUNT PACKAGE


NOTES: A. All linear dimensions are in inches (millimeters).
B. This drawing is subject to change without notice.
C) Lead dimensions are not controlled within this area.
D. All lead dimensions apply before solder dip.
E. The center lead is in electrical contact with the mounting tab.

The chamfer is optional.
G Thermal pad contour optional within these dimensions.
(H) Falls within JEDEC TO-220 variation AB, except minimum lead thickness.

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## XBee ${ }^{\circledR}$ /XBee-PRO ${ }^{\circledR}$ RF Modules

XBee®/XBee-PRO® RF Modules
RF Module Operation
RF Module Configuration
Appendices


Product Manual v1.xEx - 802.15.4 Protocol
For RF Module Part Numbers: XB24-A...-001, XBP24-A...-001

IEEE ${ }^{\circledR}$ 802.15.4 RF Modules by Digi International


Digi International Inc.
11001 Bren Road East
Minnetonka, MN 55343
877 912-3444 or 952 912-3444
http://www.digi.com

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| Technical Support: | Phone: | (866) 765-9885 toll-free U.S.A. \& Canada (801) 765-9885 Worldwide |
| :---: | :---: | :---: |
|  |  | 8:00 am - 5:00 pm [U.S. Mountain Time] |
|  | Live Chat: | www.digi.com |
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## 1. XBee®/XBee-PRO® RF Modules

The XBee and XBee-PRO RF Modules were engineered to meet IEEE 802.15.4 standards and support the unique needs of low-cost, low-power wireless sensor networks. The modules require minimal power and provide reliable delivery of data between devices.

The modules operate within the ISM 2.4 GHz frequency band and are pin-for-pin compatible with each other.


## Key Features

| Long Range Data Integrity | Low Power |
| :---: | :---: |
| XBee <br> - Indoor/Urban: up to $100^{\prime}$ ( 30 m ) <br> - Outdoor line-of-sight: up to 300' (90 m) <br> - Transmit Power: 1 mW ( 0 dBm ) <br> - Receiver Sensitivity: -92 dBm | XBee <br> - TX Peak Current: $45 \mathrm{~mA}(@ 3.3 \mathrm{~V})$ <br> - RX Current: 50 mA (@3.3 V) <br> - Power-down Current: < $10 \mu \mathrm{~A}$ XBee-PRO |
| XBee-PRO <br> - Indoor/Urban: up to 300' (90 m), 200' (60 $\mathrm{m})$ for International variant <br> - Outdoor line-of-sight: up to 1 mile (1600 $\mathrm{m}), 2500^{\prime}(750 \mathrm{~m})$ for International variant <br> - Transmit Power: 63 mW (18dBm), 10mW (10dBm) for International variant | - TX Peak Current: 250 mA ( 150 mA for international variant) <br> - TX Peak Current (RPSMA module only): 340mA ( 180 mA for international variant <br> - RX Current: $55 \mathrm{~mA}(@ 3.3 \mathrm{~V}$ ) <br> - Power-down Current: < $10 \mu \mathrm{~A}$ <br> ADC and I/O line support |
| - Receiver Sensitivity: -100 dBm <br> RF Data Rate: 250,000 bps <br> Advanced Networking \& Security | Analog-to-digital conversion, Digital I/O I/O Line Passing <br> Easy-to-Use |
| Retries and Acknowledgements <br> DSSS (Direct Sequence Spread Spectrum) | No configuration necessary for out-of box RF communications |
| Each direct sequence channels has over 65,000 unique network addresses available <br> Source/Destination Addressing <br> Unicast \& Broadcast Communications | Free X-CTU Software <br> (Testing and configuration software) <br> AT and API Command Modes for configuring module parameters |
| Point-to-point, point-to-multipoint and peer-to-peer topologies supported | Extensive command set Small form factor |

## Worldwide Acceptance

FCC Approval (USA) Refer to Appendix A [p64] for FCC Requirements.
Systems that contain XBee ${ }^{\circledR} / X B e e-P R O ® ~ R F ~ M o d u l e s ~ i n h e r i t ~ D i g i ~ C e r t i f i c a t i o n s . ~$
ISM (Industrial, Scientific \& Medical) 2.4 GHz frequency band
Manufactured under ISO 9001:2000 registered standards
XBee ${ }^{\circledR} /$ XBee-PRO® RF Modules are optimized for use in the United States, Canada, Australia, Japan, and Europe. Contact Digi for complete list of government agency approvals.

## Specifications

Table 1-01. Specifications of the XBee ${ }^{\circledR} /$ XBee-PRO® RF Modules

| Specification | XBee | XBee-PRO |
| :---: | :---: | :---: |
| Performance |  |  |
| Indoor/Urban Range | Up to $100 \mathrm{ft}(30 \mathrm{~m})$ | Up to 300 ft . 90 m ), up to $200 \mathrm{ft}(60 \mathrm{~m})$ International variant |
| Outdoor RF line-of-sight Range | Up to 300 ft (90 m) | Up to 1 mile ( 1600 m ), up to $2500 \mathrm{ft}(750 \mathrm{~m})$ international variant |
| Transmit Power Output (software selectable) | 1 mW (0 dBm) | $63 \mathrm{~mW}(18 \mathrm{dBm}){ }^{*}$ <br> 10 mW ( 10 dBm ) for International variant |
| RF Data Rate | 250,000 bps | 250,000 bps |
| Serial Interface Data Rate (software selectable) | 1200 bps - 250 kbps (non-standard baud rates also supported) | 1200 bps - 250 kbps (non-standard baud rates also supported) |
| Receiver Sensitivity | -92 dBm (1\% packet error rate) | -100 dBm (1\% packet error rate) |
| Power Requirements |  |  |
| Supply Voltage | 2.8-3.4 V | 2.8-3.4 V |
| Transmit Current (typical) | 45mA (@ 3.3 V) | 250 mA (@3.3 V) ( 150 mA for international variant) RPSMA module only: 340 mA (@3.3 V) ( 180 mA for international variant) |
| Idle / Receive Current (typical) | 50 mA (@ 3.3 V ) | 55 mA (@ 3.3 V ) |
| Power-down Current | < $10 \mu \mathrm{~A}$ | < $10 \mu \mathrm{~A}$ |
| General |  |  |
| Operating Frequency | ISM 2.4 GHz | ISM 2.4 GHz |
| Dimensions | 0.960 " $1.087^{\prime \prime}(2.438 \mathrm{~cm} \times 2.761 \mathrm{~cm})$ | $0.960^{\prime \prime} \times 1.297^{\prime \prime}(2.438 \mathrm{~cm} \times 3.294 \mathrm{~cm})$ |
| Operating Temperature | -40 to $85^{\circ} \mathrm{C}$ (industrial) | -40 to $85^{\circ} \mathrm{C}$ (industrial) |
| Antenna Options | Integrated Whip, Chip or U.FL Connector, RPSMA Connector | Integrated Whip, Chip or U.FL Connector, RPSMA Connector |
| Networking \& Security |  |  |
| Supported Network Topologies | Point-to-point, Point-to-multipoint \& Peer-to-peer |  |
| Number of Channels (software selectable) | 16 Direct Sequence Channels | 12 Direct Sequence Channels |
| Addressing Options | PAN ID, Channel and Addresses | PAN ID, Channel and Addresses |
| Agency Approvals |  |  |
| United States (FCC Part 15.247) | OUR-XBEE | OUR-XBEEPRO |
| Industry Canada (IC) | 4214A XBEE | 4214A XBEEPRO |
| Europe (CE) | ETSI | ETSI (Max. 10 dBm transmit power output)* |
| Japan | R201WW07215214 | R201WW08215111 (Max. 10 dBm transmit power output)* |
| Austraila | C-Tick | C-Tick |

* See Appendix A for region-specific certification requirements.

Antenna Options: The ranges specified are typical when using the integrated Whip ( 1.5 dBi ) and Dipole ( 2.1 dBi ) antennas. The Chip antenna option provides advantages in its form factor; however, it typically yields shorter range than the Whip and Dipole antenna options when transmitting outdoors.For more information, refer to the "XBee Antennas" Knowledgebase Article located on Digi's Support Web site

## Mechanical Drawings

Figure 1-01. Mechanical drawings of the XBee®/XBee-PRO® RF Modules (antenna options not shown)

The XBee and XBee-PRO RF Modules are pin-for-pin compatible.


## Mounting Considerations

The XBee®/XBee-PRO® RF Module was designed to mount into a receptacle (socket) and therefore does not require any soldering when mounting it to a board. The XBee Development Kits contain RS-232 and USB interface boards which use two 20-pin receptacles to receive modules.

Figure 1-02. XBee Module Mounting to an RS-232 Interface Board.


The receptacles used on Digi development boards are manufactured by Century Interconnect. Several other manufacturers provide comparable mounting solutions; however, Digi currently uses the following receptacles:

- Through-hole single-row receptacles Samtec P/N: MMS-110-01-L-SV (or equivalent)
- Surface-mount double-row receptacles Century Interconnect P/N: CPRMSL20-D-0-1 (or equivalent)
- Surface-mount single-row receptacles Samtec P/N: SMM-110-02-SM-S

Digi also recommends printing an outline of the module on the board to indicate the orientation the module should be mounted.

## Pin Signals

 Numbers
(top sides shown - shields on bottom)


Table 1-02. Pin Assignments for the XBee and XBee-PRO Modules
(Low-asserted signals are distinguished with a horizontal line above signal name.)

| Pin \# | Name | Direction | Description |
| :---: | :---: | :---: | :---: |
| 1 | VCC | - | Power supply |
| 2 | DOUT | Output | UART Data Out |
| 3 | DIN/ $\overline{\text { CONFIG }}$ | Input | UART Data In |
| 4 | DO8* | Output | Digital Output 8 |
| 5 | RESET | Input | Module Reset (reset pulse must be at least 200 ns ) |
| 6 | PWMO / RSSI | Output | PWM Output 0 / RX Signal Strength Indicator |
| 7 | PWM1 | Output | PWM Output 1 |
| 8 | [reserved] | - | Do not connect |
| 9 | $\overline{\text { DTR / SLEEP_RQ / DI8 }}$ | Input | Pin Sleep Control Line or Digital Input 8 |
| 10 | GND | - | Ground |
| 11 | AD4 / DIO4 | Either | Analog Input 4 or Digital I/O 4 |
| 12 | $\overline{\text { CTS } / \text { DIO7 }}$ | Either | Clear-to-Send Flow Control or Digital I/O 7 |
| 13 | ON/ $\overline{\text { SLEEP }}$ | Output | Module Status Indicator |
| 14 | VREF | Input | Voltage Reference for A/D Inputs |
| 15 | Associate / AD5 / DIO5 | Either | Associated Indicator, Analog Input 5 or Digital I/O 5 |
| 16 | $\overline{\text { RTS / AD6 / DIO6 }}$ | Either | Request-to-Send Flow Control, Analog Input 6 or Digital I/O 6 |
| 17 | AD3 / DIO3 | Either | Analog Input 3 or Digital I/O 3 |
| 18 | AD2 / DIO2 | Either | Analog Input 2 or Digital I/O 2 |
| 19 | AD1 / DIO1 | Either | Analog Input 1 or Digital I/O 1 |
| 20 | ADO / DIOO | Either | Analog Input 0 or Digital I/O 0 |

* Function is not supported at the time of this release


## Design Notes:

- Minimum connections: VCC, GND, DOUT \& DIN
- Minimum connections for updating firmware: VCC, GND, DIN, DOUT, RTS \& DTR
- Signal Direction is specified with respect to the module
- Module includes a 50k $\Omega$ pull-up resistor attached to $\overline{\text { RESET }}$
- Several of the input pull-ups can be configured using the PR command
- Unused pins should be left disconnected


## Electrical Characteristics

Table 1-03. DC Characteristics (VCC = 2.8-3.4 VDC)


Table 1-04. ADC Characteristics (Operating)

| Symbol | Characteristic | Condition | Min | Typical | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $V_{\text {REFH }}$ | VREF - Analog-to-Digital converter reference range |  | 2.08 | - | $V_{\text {DDAD* }}$ | V |
| $l_{\text {ReF }}$ | VREF - Reference Supply Current | Enabled | - | 200 | - | $\mu \mathrm{A}$ |
|  |  | Disabled or Sleep Mode | - | $<0.01$ | 0.02 | $\mu \mathrm{A}$ |
| $V_{\text {INDC }}$ | Analog Input Voltage ${ }^{1}$ |  | $V_{\text {SSAD }}-0.3$ | - | $V_{\text {DDAD }}+0.3$ | V |

1. Maximum electrical operating range, not valid conversion range.

* $\mathrm{V}_{\text {DDAD }}$ is connected to VCC.

Table 1-05. ADC Timing/Performance Characteristics ${ }^{1}$

| Symbol | Characteristic | Condition | Min | Typical | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{R}_{\text {AS }}$ | Source Impedance at Input ${ }^{2}$ |  | - | - | 10 | $\mathrm{k} \Omega$ |
| $V_{\text {AIN }}$ | Analog Input Voltage ${ }^{3}$ |  | $\mathrm{V}_{\text {REFL }}$ |  | $\mathrm{V}_{\text {REFH }}$ | V |
| RES | Ideal Resolution (1 LSB) ${ }^{4}$ | $2.08 \mathrm{~V} \leq \mathrm{V}_{\text {DDAD }} \leq 3.6 \mathrm{~V}$ | 2.031 | - | 3.516 | mV |
| DNL | Differential Non-linearity ${ }^{5}$ |  | - | $\pm 0.5$ | $\pm 1.0$ | LSB |
| INL | Integral Non-linearity ${ }^{6}$ |  | - | $\pm 0.5$ | $\pm 1.0$ | LSB |
| $\mathrm{E}_{\text {ZS }}$ | Zero-scale Error ${ }^{7}$ |  | - | $\pm 0.4$ | $\pm 1.0$ | LSB |
| $\mathrm{F}_{\mathrm{FS}}$ | Full-scale Error ${ }^{8}$ |  | - | $\pm 0.4$ | $\pm 1.0$ | LSB |
| $\mathrm{E}_{\text {IL }}$ | Input Leakage Error ${ }^{9}$ |  | - | $\pm 0.05$ | $\pm 5.0$ | LSB |
| $\mathrm{E}_{\text {TU }}$ | Total Unadjusted Error ${ }^{10}$ |  | - | $\pm 1.1$ | $\pm 2.5$ | LSB |

1. All ACCURACY numbers are based on processor and system being in WAIT state (very little activity and no IO switching) and that adequate low-pass filtering is present on analog input pins (filter with $0.01 \mu \mathrm{~F}$ to $0.1 \mu \mathrm{~F}$ capacitor between analog input and VREFL). Failure to observe these guidelines may result in system or microcontroller noise causing accuracy errors which will vary based on board layout and the type and magnitude of the activity.
Data transmission and reception during data conversion may cause some degradation of these specifications, depending on the number and timing of packets. It is advisable to test the ADCs in your installation if best accuracy is required.
2. $R_{A S}$ is the real portion of the impedance of the network driving the analog input pin. Values greater than this amount may not fully charge the input circuitry of the ATD resulting in accuracy error.
3. Analog input must be between $V_{\text {REFL }}$ and $V_{\text {REFH }}$ for valid conversion. Values greater than $V_{\text {REFH }}$ will convert to $\$ 3 F F$.
4. The resolution is the ideal step size or $1 \mathrm{LSB}=\left(\mathrm{V}_{\text {REFH }}-\mathrm{V}_{\text {REFL }}\right) / 1024$
5. Differential non-linearity is the difference between the current code width and the ideal code width (1LSB). The current code width is the difference in the transition voltages to and from the current code.
6. Integral non-linearity is the difference between the transition voltage to the current code and the adjusted ideal transition voltage for the current code. The adjusted ideal transition voltage is (Current Code $-1 / 2)^{*}\left(1 /\left(\left(\mathrm{V}_{\mathrm{REFH}}+\mathrm{E}_{\mathrm{FS}}\right)-\left(\mathrm{V}_{\mathrm{REFL}}+\mathrm{E}_{\mathrm{ZS}}\right)\right)\right)$.
7. Zero-scale error is the difference between the transition to the first valid code and the ideal transition to that code. The Ideal transition voltage to a given code is (Code $-1 / 2)^{*}\left(1 /\left(\mathrm{V}_{\text {REFH }}-\mathrm{V}_{\text {REFL }}\right)\right)$.
8. Full-scale error is the difference between the transition to the last valid code and the ideal transition to that code. The ideal transition voltage to a given code is (Code- $1 / 2)^{*}\left(1 /\left(\mathrm{V}_{\text {REFH }}-\mathrm{V}_{\text {REFL }}\right)\right)$.
9. Input leakage error is error due to input leakage across the real portion of the impedance of the network driving the analog pin. Reducing the impedance of the network reduces this error.
10.Total unadjusted error is the difference between the transition voltage to the current code and the ideal straight-line transfer function. This measure of error includes inherent quantization error ( $1 / 2 \mathrm{LSB}$ ) and circuit error (differential, integral, zeroscale, and full-scale) error. The specified value of $\mathrm{E}_{\mathrm{TU}}$ assumes zero $\mathrm{E}_{\mathrm{LL}}$ (no leakage or zero real source impedance).

## 2. RF Module Operation

## Serial Communications

The XBee®/XBee-PRO® RF Modules interface to a host device through a logic-level asynchronous serial port. Through its serial port, the module can communicate with any logic and voltage compatible UART; or through a level translator to any serial device (For example: Through a Digi proprietary RS-232 or USB interface board).

## UART Data Flow

Devices that have a UART interface can connect directly to the pins of the RF module as shown in the figure below.
Figure 2-01. System Data Flow Diagram in a UART-interfaced environment (Low-asserted signals distinguished with horizontal line over signal name.)


## Serial Data

Data enters the module UART through the DI pin (pin 3) as an asynchronous serial signal. The signal should idle high when no data is being transmitted.

Each data byte consists of a start bit (low), 8 data bits (least significant bit first) and a stop bit (high). The following figure illustrates the serial bit pattern of data passing through the module.

Figure 2-02. UART data packet 0x1F (decimal number "31") as transmitted through the RF module Example Data Format is 8 -N-1 (bits - parity - \# of stop bits)


Serial communications depend on the two UARTs (the microcontroller's and the RF module's) to be configured with compatible settings (baud rate, parity, start bits, stop bits, data bits).

The UART baud rate and parity settings on the XBee module can be configured with the BD and SB commands, respectively. See the command table in Chapter 3 for details.

## Transparent Operation

By default, XBee ${ }^{\circledR} /$ XBee-PRO® RF Modules operate in Transparent Mode. When operating in this mode, the modules act as a serial line replacement - all UART data received through the DI pin is queued up for RF transmission. When RF data is received, the data is sent out the DO pin.

## Serial-to-RF Packetization

Data is buffered in the DI buffer until one of the following causes the data to be packetized and transmitted:

1. No serial characters are received for the amount of time determined by the RO (Packetization Timeout) parameter. If $R O=0$, packetization begins when a character is received.
2. The maximum number of characters that will fit in an RF packet (100) is received.
3. The Command Mode Sequence ( $\mathrm{GT}+\mathrm{CC}+\mathrm{GT}$ ) is received. Any character buffered in the DI buffer before the sequence is transmitted.

If the module cannot immediately transmit (for instance, if it is already receiving RF data), the serial data is stored in the DI Buffer. The data is packetized and sent at any RO timeout or when 100 bytes (maximum packet size) are received.

If the DI buffer becomes full, hardware or software flow control must be implemented in order to prevent overflow (loss of data between the host and module).

## API Operation

API (Application Programming Interface) Operation is an alternative to the default Transparent Operation. The frame-based API extends the level to which a host application can interact with the networking capabilities of the module.

When in API mode, all data entering and leaving the module is contained in frames that define operations or events within the module.

Transmit Data Frames (received through the DI pin (pin 3)) include:

- RF Transmit Data Frame
- Command Frame (equivalent to AT commands)

Receive Data Frames (sent out the DO pin (pin 2)) include:

- RF-received data frame
- Command response
- Event notifications such as reset, associate, disassociate, etc.

The API provides alternative means of configuring modules and routing data at the host application layer. A host application can send data frames to the module that contain address and payload information instead of using command mode to modify addresses. The module will send data frames to the application containing status packets; as well as source, RSSI and payload information from received data packets.
The API operation option facilitates many operations such as the examples cited below:
-> Transmitting data to multiple destinations without entering Command Mode
-> Receive success/failure status of each transmitted RF packet
-> Identify the source address of each received packet

[^3]
## Flow Control

Figure 2-03. Internal Data Flow Diagram


## DI (Data In) Buffer

When serial data enters the RF module through the DI pin (pin 3), the data is stored in the DI Buffer until it can be processed.
Hardware Flow Control ( $\overline{\mathbf{C T S}}$ ). When the DI buffer is 17 bytes away from being full; by default, the module de-asserts $\overline{\mathrm{CTS}}$ (high) to signal to the host device to stop sending data [refer to D7 (DIO7 Configuration) parameter]. $\overline{\text { CTS }}$ is re-asserted after the DI Buffer has 34 bytes of memory available.

## How to eliminate the need for flow control:

1. Send messages that are smaller than the DI buffer size (202 bytes).
2. Interface at a lower baud rate [BD (Interface Data Rate) parameter] than the throughput data rate.

## Case in which the DI Buffer may become full and possibly overflow:

If the module is receiving a continuous stream of RF data, any serial data that arrives on the DI pin is placed in the DI Buffer. The data in the DI buffer will be transmitted over-the-air when the module is no longer receiving RF data in the network.

Refer to the RO (Packetization Timeout), BD (Interface Data Rate) and D7 (DIO7 Configuration) command descriptions for more information.

## DO (Data Out) Buffer

When RF data is received, the data enters the DO buffer and is sent out the serial port to a host device. Once the DO Buffer reaches capacity, any additional incoming RF data is lost.
Hardware Flow Control ( $\overline{\mathbf{R T S}}$ ). If $\overline{\mathrm{RTS}}$ is enabled for flow control (D6 (DIO6 Configuration) Parameter $=1$ ), data will not be sent out the DO Buffer as long as $\overline{\mathrm{RTS}}$ (pin 16) is de-asserted.

## Two cases in which the DO Buffer may become full and possibly overflow:

1. If the RF data rate is set higher than the interface data rate of the module, the module will receive data from the transmitting module faster than it can send the data to the host.
2. If the host does not allow the module to transmit data out from the DO buffer because of being held off by hardware or software flow control.

Refer to the D6 (DIO6 Configuration) command description for more information.

## ADC and Digital I/O Line Support

The XBee®/XBee-PRO® RF Modules support ADC (Analog-to-digital conversion) and digital I/O line passing. The following pins support multiple functions:
Table 2-01. Pin functions and their associated pin numbers and commands $\mathrm{AD}=$ Analog-to-Digital Converter, DIO = Digital Input/Output
Pin functions not applicable to this section are denoted within (parenthesis).

| Pin Function | Pin\# | AT Command |
| :--- | :--- | :--- |
| AD0 / DIO0 | 20 | D0 |
| AD1 / DIO1 | 19 | D1 |
| AD2 / DIO2 | 18 | D2 |
| AD3 / DIO3 / (COORD_SEL) | 17 | D3 |
| AD4 / DIO4 | 11 | D4 |
| AD5 / DIO5 / (ASSOCIATE) | 15 | D5 |
| DIO6 / (RTS) | 16 | D6 |
| DIO7 / (CTS) | 12 | D7 |
| DI8 / (DTR) / (Sleep_RQ) | 9 | D8 |

To enable ADC and DIO pin functions:

| For ADC Support: | Set ATDn $=2$ |
| :--- | :--- |
| For Digital Input support: | Set ATDn $=3$ |
| For Digital Output Low support: | Set ATDn $=4$ |
| For Digital Output High support: | Set ATDn $=5$ |

## I/O Data Format

I/O data begins with a header. The first byte of the header defines the number of samples forthcoming. The last 2 bytes of the header (Channel Indicator) define which inputs are active. Each bit represents either a DIO line or ADC channel.

Figure 2-04. Header

- Header


Sample data follows the header and the channel indicator frame is used to determine how to read the sample data. If any of the DIO lines are enabled, the first 2 bytes are the DIO sample. The ADC data follows. ADC channel data is represented as an unsigned 10 -bit value right-justified on a 16- bit boundary.
Figure 2-05. Sample Data

## Sample Data

| DIO Line Data is first (if enabled) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | ADC Line Data |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| X | X | X | X | X | X | X | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | ADCn MSB | ADCn LSB |

## API Support

I/O data is sent out the UART using an API frame. All other data can be sent and received using Transparent Operation [refer to p11] or API framing if API mode is enabled (AP >0).
API Operations support two RX (Receive) frame identifiers for I/O data (set 16-bit address to 0xFFFE and the module will do 64-bit addressing):

- $0 \times 82$ for RX (Receive) Packet: 64-bit address I/O
- $0 \times 83$ for RX (Receive) Packet: 16-bit address I/O

The API command header is the same as shown in the "RX (Receive) Packet: 64-bit Address" and "RX (Receive) Packet: 64-bit Address" API types [refer to p63]. RX data follows the format described in the I/O Data Format section [p13].
Applicable Commands: AP (API Enable)

## Sleep Support

Automatic wakeup sampling can be suppressed by setting SO bit 1 . When an RF module wakes, it will always do a sample based on any active ADC or DIO lines. This allows sampling based on the sleep cycle whether it be Cyclic Sleep (SM parameter $=4$ or 5 ) or Pin Sleep (SM = 1 or 2). To gather more samples when awake, set the IR (Sample Rate) parameter.
For Cyclic Sleep modes: If the IR parameter is set, the module will stay awake until the IT (Samples before TX) parameter is met. The module will stay awake for ST (Time before Sleep) time.
Applicable Commands: IR (Sample Rate), IT (Samples before TX), SM (Sleep Mode), IC (DIO Change Detect), SO (Sleep Options)

## DIO Pin Change Detect

When "DIO Change Detect" is enabled (using the IC command), DIO lines 0-7 are monitored. When a change is detected on a DIO line, the following will occur:

1. An RF packet is sent with the updated DIO pin levels. This packet will not contain any ADC samples.
2. Any queued samples are transmitted before the change detect data. This may result in receiving a packet with less than IT (Samples before TX) samples.

Note: Change detect will not affect Pin Sleep wake-up. The D8 pin (DTR/Sleep_RQ/DI8) is the only line that will wake a module from Pin Sleep. If not all samples are collected, the module will still enter Sleep Mode after a change detect packet is sent.

Applicable Commands: IC (DIO Change Detect), IT (Samples before TX)

NOTE: Change detect is only supported when the Dx (DIOx Configuration) parameter equals 3,4 or 5 .

## Sample Rate (Interval)

The Sample Rate (Interval) feature allows enabled ADC and DIO pins to be read periodically on modules that are not configured to operate in Sleep Mode. When one of the Sleep Modes is enabled and the IR (Sample Rate) parameter is set, the module will stay awake until IT (Samples before TX) samples have been collected.

Once a particular pin is enabled, the appropriate sample rate must be chosen. The maximum sample rate that can be achieved while using one A/D line is 1 sample/ms or 1 KHz (Note that the modem will not be able to keep up with transmission when IR \& IT are equal to " 1 " and that configuring the modem to sample at rates greater than once every 20 ms is not recommended).

Applicable Commands: IR (Sample Rate), IT (Samples before TX), SM (Sleep Mode)

## I/O Line Passing

Virtual wires can be set up between XBee®/XBee-PRO® Modules. When an RF data packet is received that contains I/O data, the receiving module can be setup to update any enabled outputs (PWM and DIO) based on the data it receives.

Note that I/O lines are mapped in pairs. For example: ADO can only update PWMO and DI5 can only update DO5. The default setup is for outputs not to be updated, which results in the I/O data being sent out the UART (refer to the IU (Enable I/O Output) command). To enable the outputs to be updated, the IA (I/O Input Address) parameter must be setup with the address of the module that has the appropriate inputs enabled. This effectively binds the outputs to a particular module's input. This does not affect the ability of the module to receive I/O line data from other modules only its ability to update enabled outputs. The IA parameter can also be setup to accept I/O data for output changes from any module by setting the IA parameter to 0xFFFF.
When outputs are changed from their non-active state, the module can be setup to return the output level to it non-active state. The timers are set using the Tn (Dn Output Timer) and PT (PWM Output Timeout) commands. The timers are reset every time a valid I/O packet (passed IA check) is received. The IC (Change Detect) and IR (Sample Rate) parameters can be setup to keep the output set to their active output if the system needs more time than the timers can handle.

Note: DI8 cannot be used for I/O line passing.
Applicable Commands: IA (I/O Input Address), Tn (Dn Output Timeout), PO (PWM0 Configuration), P1 (PWM1 Configuration), M0 (PWM0 Output Level), M1 (PWM1 Output Level), PT (PWM Output Timeout), RP (RSSSI PWM Timer)

## Configuration Example

As an example for a simple A/D link, a pair of RF modules could be set as follows:

```
Remote Configuration
    Base Configuration
    DL = 0x1234
    MY = 0x5678
        D0 = 2
        D1 = 2
        IR = 0\times14
            IT = 5
                    IU = 1 
```

These settings configure the remote module to sample ADO and AD1 once each every 20 ms . It then buffers 5 samples each before sending them back to the base module. The base should then receive a 32-Byte transmission (20 Bytes data and 12 Bytes framing) every 100 ms .

## XBee®/XBee-PRO® Networks

The following terms will be used to explicate the network operations:
Table 2-02. Terms and definitions

| Term | Definition |
| :--- | :--- |
| PAN | Personal Area Network - A data communication network that includes one or more End Devices and <br> optionally a Coordinator. |
| Coordinator | A Full-function device (FFD) that provides network synchronization by polling nodes [NonBeacon <br> (w/ Coordinator) networks only] |
| End Device | When in the same network as a Coordinator - RF modules that rely on a Coordinator for <br> synchronization and can be put into states of sleep for low-power applications. |
| Association | The establishment of membership between End Devices and a Coordinator. Association is only <br> applicable in NonBeacon (w/Coordinator) networks. |

## Peer-to-Peer

By default, XBee®/XBee-PRO RF Modules are configured to operate within a Peer-to-Peer network topology and therefore are not dependent upon Master/Slave relationships. NonBeacon systems operate within a Peer-to-Peer network topology and therefore are not dependent upon Master/ Slave relationships. This means that modules remain synchronized without use of master/server configurations and each module in the network shares both roles of master and slave. Digi's peer-to-peer architecture features fast synchronization times and fast cold start times. This default configuration accommodates a wide range of RF data applications.

Figure 2-06. Peer-to-Peer Architecture

A peer-to-peer network can be established by
 configuring each module to operate as an End Device ( $C E=0$ ), disabling End Device Association on all modules ( $\mathrm{A} 1=0$ ) and setting ID and CH parameters to be identical across the network.

## NonBeacon (w/ Coordinator)

A device is configured as a Coordinator by setting the CE (Coordinator Enable) parameter to " 1 ". Coordinator power-up is governed by the A2 (Coordinator Association) parameter.

In a Coordinator system, the Coordinator can be configured to use direct or indirect transmissions. If the SP (Cyclic Sleep Period) parameter is set to " 0 ", the Coordinator will send data immediately. Otherwise, the SP parameter determines the length of time the Coordinator will retain the data before discarding it. Generally, SP (Cyclic Sleep Period) and ST (Time before Sleep) parameters should be set to match the SP and ST settings of the End Devices.

## Association

Association is the establishment of membership between End Devices and a Coordinator. The establishment of membership is useful in scenarios that require a central unit (Coordinator) to relay messages to or gather data from several remote units (End Devices), assign channels or assign PAN IDs.

An RF data network that consists of one Coordinator and one or more End Devices forms a PAN (Personal Area Network). Each device in a PAN has a PAN Identifier [ID (PAN ID) parameter]. PAN IDs must be unique to prevent miscommunication between PANs. The Coordinator PAN ID is set using the ID (PAN ID) and A2 (Coordinator Association) commands.

An End Device can associate to a Coordinator without knowing the address, PAN ID or channel of the Coordinator. The A1 (End Device Association) parameter bit fields determine the flexibility of an End Device during association. The A1 parameter can be used for an End Device to dynamically set its destination address, PAN ID and/or channel.

For example: If the PAN ID of a Coordinator is known, but the operating channel is not; the A1 command on the End Device should be set to enable the 'Auto_Associate' and 'Reassign_Channel' bits. Additionally, the ID parameter should be set to match the PAN ID of the associated Coordinator.

## Coordinator / End Device Setup and Operation

To configure a module to operate as a Coordinator, set the CE (Coordinator Enable) parameter to '1'. Set the CE parameter of End Devices to '0' (default). Coordinator and End Devices should contain matching firmware versions.

## NonBeacon (w/ Coordinator) Systems

The Coordinator can be configured to use direct or indirect transmissions. If the SP (Cyclic Sleep Period) parameter is set to ' 0 ', the Coordinator will send data immediately. Otherwise, the SP parameter determines the length of time the Coordinator will retain the data before discarding it. Generally, SP (Cyclic Sleep Period) and ST (Time before Sleep) parameters should be set to match the SP and ST settings of the End Devices.

## Coordinator Start-up

Coordinator power-up is governed by the A2 (Coordinator Association) command. On power-up, the Coordinator undergoes the following sequence of events:

## 1. Check A2 parameter- Reassign_PANID Flag

Set (bit $\mathbf{0}=\mathbf{1}$ ) - The Coordinator issues an Active Scan. The Active Scan selects one channel and transmits a request to the broadcast address (0xFFFF) and broadcast PAN ID (0xFFFF). It then listens on that channel for beacons from any Coordinator operating on that channel. The listen time on each channel is determined by the SD (Scan Duration) parameter value.

Once the time expires on that channel, the Active Scan selects another channel and again transmits the BeaconRequest as before. This process continues until all channels have been scanned, or until 5 PANs have been discovered. When the Active Scan is complete, the results include a list of PAN IDs and Channels that are being used by other PANs. This list is used to assign an unique PAN ID to the new Coordinator. The ID parameter will be retained if it is not found in the Active Scan results. Otherwise, the ID (PAN ID) parameter setting will be updated to a PAN ID that was not detected.

Not Set (bit $\mathbf{0}=\mathbf{0}$ ) - The Coordinator retains its ID setting. No Active Scan is performed.

## 2. Check A2 parameter-Reassign_Channel Flag (bit 1)

Set (bit $\mathbf{1}=\mathbf{1}$ ) - The Coordinator issues an Energy Scan. The Energy Scan selects one channel and scans for energy on that channel. The duration of the scan is specified by the SD (Scan Duration) parameter. Once the scan is completed on a channel, the Energy Scan selects the next channel and begins a new scan on that channel. This process continues until all channels have been scanned.
When the Energy Scan is complete, the results include the maximal energy values detected on each channel. This list is used to determine a channel where the least energy was detected. If an Active Scan was performed (Reassign_PANID Flag set), the channels used by the detected PANs are eliminated as possible channels. Thus, the results of the Energy Scan and the Active Scan (if performed) are used to find the best channel (channel with the least energy that is not used by any detected PAN). Once the best channel has been selected, the CH (Channel) parameter value is updated to that channel.

Not Set (bit $\mathbf{1}=\mathbf{0}$ ) - The Coordinator retains its CH setting. An Energy Scan is not performed.

## 3. Start Coordinator

The Coordinator starts on the specified channel (CH parameter) and PAN ID (ID parameter). Note, these may be selected in steps 1 and/or 2 above. The Coordinator will only allow End Devices to associate to it if the A2 parameter "AllowAssociation" flag is set. Once the Coordinator has successfully started, the Associate LED will blink 1 time per second. (The LED is solid if the Coordinator has not started.)

## 4. Coordinator Modifications

Once a Coordinator has started:
Modifying the A2 (Reassign_Channel or Reassign_PANID bits), ID, CH or MY parameters will cause the Coordinator's MAC to reset (The Coordinator RF module (including volatile RAM) is not reset). Changing the A2 AllowAssociation bit will not reset the Coordinator's MAC. In a nonbeaconing system, End Devices that associated to the Coordinator prior to a MAC reset will have knowledge of the new settings on the Coordinator. Thus, if the Coordinator were to change its ID, CH or MY settings, the End Devices would no longer be able to communicate with the nonbeacon Coordinator. Once a Coordinator has started, the ID, CH, MY or A2 (Reassign_Channel or Reassign_PANID bits) should not be changed.

## End Device Start-up

End Device power-up is governed by the A1 (End Device Association) command. On power-up, the End Device undergoes the following sequence of events:

1. Check A1 parameter - AutoAssociate Bit

Set (bit $2=1$ ) - End Device will attempt to associate to a Coordinator. (refer to steps 2-3).
Not Set (bit $2=\mathbf{0}$ ) - End Device will not attempt to associate to a Coordinator. The End Device will operate as specified by its ID, CH and MY parameters. Association is considered complete and the Associate LED will blink quickly ( 5 times per second). When the AutoAssociate bit is not set, the remaining steps (2-3) do not apply.

## 2. Discover Coordinator (if Auto-Associate Bit Set)

The End Device issues an Active Scan. The Active Scan selects one channel and transmits a BeaconRequest command to the broadcast address (0xFFFF) and broadcast PAN ID (0xFFFF). It then listens on that channel for beacons from any Coordinator operating on that channel. The listen time on each channel is determined by the SD parameter.

Once the time expires on that channel, the Active Scan selects another channel and again transmits the BeaconRequest command as before. This process continues until all channels have been scanned, or until 5 PANs have been discovered. When the Active Scan is complete, the results include a list of PAN IDs and Channels that are being used by detected PANs.

The End Device selects a Coordinator to associate with according to the A1 parameter "Reassign_PANID" and "Reassign_Channel" flags:

Reassign_PANID Bit Set (bit $\mathbf{0}=\mathbf{1}$ )- End Device can associate with a PAN with any ID value.
Reassign_PANID Bit Not Set (bit $\mathbf{0}=\mathbf{0}$ ) - End Device will only associate with a PAN whose ID setting matches the ID setting of the End Device.
Reassign_Channel Bit Set (bit $\mathbf{1}=\mathbf{1}$ ) - End Device can associate with a PAN with any CH value.
Reassign_Channel Bit Not Set (bit $\mathbf{1}=\mathbf{0}$ )- End Device will only associate with a PAN whose CH setting matches the CH setting of the End Device.

After applying these filters to the discovered Coordinators, if multiple candidate PANs exist, the End Device will select the PAN whose transmission link quality is the strongest. If no valid Coordinator is found, the End Device will either go to sleep (as dictated by its SM (Sleep Mode) parameter) or retry Association.
Note - An End Device will also disqualify Coordinators if they are not allowing association (A2 AllowAssociation bit); or, if the Coordinator is not using the same NonBeacon scheme as the End Device. (They must both be programmed with NonBeacon code.)

## 3. Associate to Valid Coordinator

Once a valid Coordinator is found (step 2), the End Device sends an AssociationRequest message to the Coordinator. It then waits for an AssociationConfirmation to be sent from the Coordinator. Once the Confirmation is received, the End Device is Associated and the Associate LED will blink rapidly (2 times per second). The LED is solid if the End Device has not associated.

## 4. End Device Changes once an End Device has associated

Changing A1, ID or CH parameters will cause the End Device to disassociate and restart the Association procedure.
If the End Device fails to associate, the AI command can give some indication of the failure.

## XBee®/XBee-PRO® Addressing

Every RF data packet sent over-the-air contains a Source Address and Destination Address field in its header. The RF module conforms to the 802.15 .4 specification and supports both short 16 -bit addresses and long 64-bit addresses. A unique 64-bit IEEE source address is assigned at the factory and can be read with the SL (Serial Number Low) and SH (Serial Number High) commands. Short addressing must be configured manually. A module will use its unique 64-bit address as its Source Address if its MY (16-bit Source Address) value is "0xFFFF" or "0xFFFE".
To send a packet to a specific module using 64-bit addressing: Set the Destination Address (DL + DH ) of the sender to match the Source Address ( $\mathrm{SL}+\mathrm{SH}$ ) of the intended destination module.
To send a packet to a specific module using 16-bit addressing: Set DL (Destination Address Low) parameter to equal the MY parameter of the intended destination module and set the DH (Destination Address High) parameter to ' 0 '.

## Unicast Mode

By default, the RF module operates in Unicast Mode. Unicast Mode is the only mode that supports retries. While in this mode, receiving modules send an ACK (acknowledgement) of RF packet reception to the transmitter. If the transmitting module does not receive the ACK, it will re-send the packet up to three times or until the ACK is received.
Short 16-bit addresses. The module can be configured to use short 16-bit addresses as the Source Address by setting ( $M Y<0 \times F F F E$ ). Setting the DH parameter ( $D H=0$ ) will configure the Destination Address to be a short 16-bit address (if DL < 0xFFFE). For two modules to communicate using short addressing, the Destination Address of the transmitter module must match the MY parameter of the receiver.

The following table shows a sample network configuration that would enable Unicast Mode communications using short 16 -bit addresses.
Table 2-03. Sample Unicast Network Configuration (using 16-bit addressing)

| Parameter | RF Module 1 | RF Module 2 |
| :---: | :---: | :---: |
| MY (Source Address) | $0 \times 01$ | $0 \times 02$ |
| DH (Destination Address High) | 0 | 0 |
| DL (Destination Address Low) | $0 \times 02$ | $0 \times 01$ |

Long 64-bit addresses. The RF module's serial number (SL parameter concatenated to the SH parameter) can be used as a 64-bit source address when the MY (16-bit Source Address) parameter is disabled. When the MY parameter is disabled (MY = 0xFFFF or OxFFFE), the module's source address is set to the 64-bit IEEE address stored in the SH and SL parameters.
When an End Device associates to a Coordinator, its MY parameter is set to 0xFFFE to enable 64bit addressing. The 64-bit address of the module is stored as SH and SL parameters. To send a packet to a specific module, the Destination Address (DL + DH) on the sender must match the Source Address (SL + SH) of the desired receiver.

## Broadcast Mode

Any RF module within range will accept a packet that contains a broadcast address. When configured to operate in Broadcast Mode, receiving modules do not send ACKs (Acknowledgements) and transmitting modules do not automatically re-send packets as is the case in Unicast Mode.

To send a broadcast packet to all modules regardless of 16 -bit or 64 -bit addressing, set the destination addresses of all the modules as shown below.
Sample Network Configuration (All modules in the network):

- DL (Destination Low Address) $=0 x 0000 F F F F$
- DH (Destination High Address) $=0 \times 00000000$ (default value)

[^4] " $0 x$ " prefix). Leading zeros may be omitted.

## Modes of Operation

XBee®/XBee-PRO® RF Modules operate in five modes.
Figure 2-07. Modes of Operation


## Idle Mode

When not receiving or transmitting data, the RF module is in Idle Mode. The module shifts into the other modes of operation under the following conditions:

- Transmit Mode (Serial data is received in the DI Buffer)
- Receive Mode (Valid RF data is received through the antenna)
- Sleep Mode (Sleep Mode condition is met)
- Command Mode (Command Mode Sequence is issued)

Transmit/Receive Modes

## RF Data Packets

Each transmitted data packet contains a Source Address and Destination Address field. The Source Address matches the address of the transmitting module as specified by the MY (Source Address) parameter (if MY >=0xFFFE), the SH (Serial Number High) parameter or the SL (Serial Number Low) parameter. The <Destination Address> field is created from the DH (Destination Address High) and DL (Destination Address Low) parameter values. The Source Address and/or Destination Address fields will either contain a 16 -bit short or long 64 -bit long address.
The RF data packet structure follows the 802.15 .4 specification.
[Refer to the XBee/XBee-PRO Addressing section for more information]

## Direct and Indirect Transmission

There are two methods to transmit data:

- Direct Transmission - data is transmitted immediately to the Destination Address
- Indirect Transmission - A packet is retained for a period of time and is only transmitted after the destination module (Source Address = Destination Address) requests the data.
Indirect Transmissions can only occur on a Coordinator. Thus, if all nodes in a network are End Devices, only Direct Transmissions will occur. Indirect Transmissions are useful to ensure packet delivery to a sleeping node. The Coordinator currently is able to retain up to 2 indirect messages.


## Direct Transmission

A Coordinator can be configured to use only Direct Transmission by setting the SP (Cyclic Sleep Period) parameter to " 0 ". Also, a Coordinator using indirect transmissions will revert to direct transmission if it knows the destination module is awake.
To enable this behavior, the ST (Time before Sleep) value of the Coordinator must be set to match the ST value of the End Device. Once the End Device either transmits data to the Coordinator or polls the Coordinator for data, the Coordinator will use direct transmission for all subsequent data transmissions to that module address until ST time occurs with no activity (at which point it will revert to using indirect transmissions for that module address). "No activity" means no transmission or reception of messages with a specific address. Global messages will not reset the ST timer.

## Indirect Transmission

To configure Indirect Transmissions in a PAN (Personal Area Network), the SP (Cyclic Sleep Period) parameter value on the Coordinator must be set to match the longest sleep value of any End Device. The sleep period value on the Coordinator determines how long (time or number of beacons) the Coordinator will retain an indirect message before discarding it.
An End Device must poll the Coordinator once it wakes from Sleep to determine if the Coordinator has an indirect message for it. For Cyclic Sleep Modes, this is done automatically every time the module wakes (after SP time). For Pin Sleep Modes, the A1 (End Device Association) parameter value must be set to enable Coordinator polling on pin wake-up. Alternatively, an End Device can use the FP (Force Poll) command to poll the Coordinator as needed.

## CCA (Clear Channel Assessment)

Prior to transmitting a packet, a CCA (Clear Channel Assessment) is performed on the channel to determine if the channel is available for transmission. The detected energy on the channel is compared with the CA (Clear Channel Assessment) parameter value. If the detected energy exceeds the CA parameter value, the packet is not transmitted.
Also, a delay is inserted before a transmission takes place. This delay is settable using the RN (Backoff Exponent) parameter. If RN is set to " 0 ", then there is no delay before the first CCA is performed. The RN parameter value is the equivalent of the "minBE" parameter in the 802.15 .4 specification. The transmit sequence follows the 802.15 .4 specification.
By default, the MM (MAC Mode) parameter $=0$. On a CCA failure, the module will attempt to resend the packet up to two additional times.
When in Unicast packets with RR (Retries) $=0$, the module will execute two CCA retries. Broadcast packets always get two CCA retries.

## Acknowledgement

If the transmission is not a broadcast message, the module will expect to receive an acknowledgement from the destination node. If an acknowledgement is not received, the packet will be resent up to 3 more times. If the acknowledgement is not received after all transmissions, an ACK failure is recorded.

## Sleep Mode

Sleep Modes enable the RF module to enter states of low-power consumption when not in use. In order to enter Sleep Mode, one of the following conditions must be met (in addition to the module having a non-zero SM parameter value):

- Sleep_RQ (pin 9) is asserted and the module is in a pin sleep mode ( $\mathrm{SM}=1,2$, or 5 )
- The module is idle (no data transmission or reception) for the amount of time defined by the ST (Time before Sleep) parameter. [NOTE: ST is only active when SM = 4-5.]
Table 2-04. Sleep Mode Configurations

| Sleep Mode Setting | Transition into Sleep Mode | Transition out of Sleep Mode (wake) | Characteristics | Related Commands | Power Consumption |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pin Hibernate (SM = 1) | Assert (high) Sleep_RQ (pin 9) | De-assert (low) Sleep_RQ | Pin/Host-controlled / NonBeacon systems only / Lowest Power | (SM) | $\begin{aligned} & <10 \mu \mathrm{~A}(@ 3.0 \\ & \text { VCC) } \end{aligned}$ |
| $\begin{aligned} & \text { Pin Doze } \\ & (\mathrm{SM}=2) \end{aligned}$ | Assert (high) Sleep_RQ (pin 9) | De-assert (low) Sleep_RQ | Pin/Host-controlled $/$ NonBeacon systems only / Fastest wake-up | (SM) | < $50 \mu \mathrm{~A}$ |
| Cyclic Sleep $(S M=4)$ | Automatic transition to Sleep Mode as defined by the SM (Sleep Mode) and ST (Time before Sleep) parameters. | Transition occurs after the cyclic sleep time interval elapses. The time interval is defined by the SP (Cyclic Sleep Period) parameter. | RF module wakes in pre-determined time intervals to detect if RF data is present / When SM $=5$ | (SM), SP, ST | $<50 \mu \mathrm{~A}$ when sleeping |
| Cyclic Sleep $(S M=5)$ | Automatic transition to Sleep Mode as defined by the SM (Sleep Mode) and ST (Time before Sleep) parameters or or on a falling edge transition of the SLEEP_RQ pin. | Transition occurs after the cyclic sleep time interval elapses. The time interval is defined by the SP (Cyclic Sleep Period) parameter. | RF module wakes in pre-determined time intervals to detect if $R F$ data is present. Module also wakes on a falling edge of SLEEP_RQ | (SM), SP, ST | $<50 \mu \mathrm{~A}$ when sleeping |

The SM command is central to setting Sleep Mode configurations. By default, Sleep Modes are disabled ( $\mathrm{SM}=0$ ) and the module remains in Idle/Receive Mode. When in this state, the module is constantly ready to respond to serial or RF activity.

## Pin/Host-controlled Sleep Modes

The transient current when waking from pin sleep ( $\mathrm{SM}=1$ or 2 ) does not exceed the idle current of the module. The current ramps up exponentially to its idle current.

## Pin Hibernate (SM = 1)

- Pin/Host-controlled
- Typical power-down current: < $10 \mu \mathrm{~A}$ (@3.0 VCC)
- Wake-up time: 13.2 msec

Pin Hibernate Mode minimizes quiescent power (power consumed when in a state of rest or inactivity). This mode is voltage level-activated; when Sleep_RQ (pin 9) is asserted, the module will finish any transmit, receive or association activities, enter Idle Mode, and then enter a state of sleep. The module will not respond to either serial or RF activity while in pin sleep.
To wake a sleeping module operating in Pin Hibernate Mode, de-assert Sleep_RQ (pin 9). The module will wake when Sleep_RQ is de-asserted and is ready to transmit or receive when the CTS line is low. When waking the module, the pin must be de-asserted at least two 'byte times' after CTS goes low. This assures that there is time for the data to enter the DI buffer.

## Pin Doze (SM = 2)

- Pin/Host-controlled
- Typical power-down current: < $50 \mu \mathrm{~A}$
- Wake-up time: 2 msec

Pin Doze Mode functions as does Pin Hibernate Mode; however, Pin Doze features faster wake-up time and higher power consumption.

To wake a sleeping module operating in Pin Doze Mode, de-assert Sleep_RQ (pin 9). The module will wake when Sleep_RQ is de-asserted and is ready to transmit or receive when the CTS line is
low. When waking the module, the pin must be de-asserted at least two 'byte times' after CTS goes low. This assures that there is time for the data to enter the DI buffer.

## Cyclic Sleep Modes

## Cyclic Sleep Remote (SM = 4)

- Typical Power-down Current: < $50 \mu \mathrm{~A}$ (when asleep)
- Wake-up time: 2 msec

The Cyclic Sleep Modes allow modules to periodically check for RF data. When the SM parameter is set to ' 4 ', the module is configured to sleep, then wakes once a cycle to check for data from a module configured as a Cyclic Sleep Coordinator ( $\mathrm{SM}=0, \mathrm{CE}=1$ ). The Cyclic Sleep Remote sends a poll request to the coordinator at a specific interval set by the SP (Cyclic Sleep Period) parameter. The coordinator will transmit any queued data addressed to that specific remote upon receiving the poll request.
If no data is queued for the remote, the coordinator will not transmit and the remote will return to sleep for another cycle. If queued data is transmitted back to the remote, it will stay awake to allow for back and forth communication until the ST (Time before Sleep) timer expires.
Also note that $\overline{\mathrm{CTS}}$ will go low each time the remote wakes, allowing for communication initiated by the remote host if desired.

## Cyclic Sleep Remote with Pin Wake-up (SM = 5)

Use this mode to wake a sleeping remote module through either the RF interface or by the deassertion of Sleep_RQ for event-driven communications. The cyclic sleep mode works as described above (Cyclic Sleep Remote) with the addition of a pin-controlled wake-up at the remote module. The Sleep_RQ pin is edge-triggered, not level-triggered. The module will wake when a low is detected then set $\overline{\mathrm{CTS}}$ low as soon as it is ready to transmit or receive.

Any activity will reset the ST (Time before Sleep) timer so the module will go back to sleep only after there is no activity for the duration of the timer. Once the module wakes (pin-controlled), further pin activity is ignored. The module transitions back into sleep according to the ST time regardless of the state of the pin.
[Cyclic Sleep Coordinator (SM = 6)]

- Typical current $=$ Receive current
- Always awake

NOTE: The SM=6 parameter value exists solely for backwards compatibility with firmware version 1.x60. If backwards compatibility with the older firmware version is not required, always use the CE (Coordinator Enable) command to configure a module as a Coordinator.

This mode configures a module to wake cyclic sleeping remotes through RF interfacing. The Coordinator will accept a message addressed to a specific remote 16 or 64-bit address and hold it in a buffer until the remote wakes and sends a poll request. Messages not sent directly (buffered and requested) are called "Indirect messages". The Coordinator only queues one indirect message at a time. The Coordinator will hold the indirect message for a period 2.5 times the sleeping period indicated by the SP (Cyclic Sleep Period) parameter. The Coordinator's SP parameter should be set to match the value used by the remotes.

## Command Mode

To modify or read RF Module parameters, the module must first enter into Command Mode - a state in which incoming characters are interpreted as commands. Two Command Mode options are supported: AT Command Mode [refer to section below] and API Command Mode [p57].

## AT Command Mode

## To Enter AT Command Mode:

Send the 3-character command sequence "+++" and observe guard times before and after the command characters. [Refer to the "Default AT Command Mode Sequence" below.]

Default AT Command Mode Sequence (for transition to Command Mode):

- No characters sent for one second [GT (Guard Times) parameter $=0 \times 3 \mathrm{E} 8$ ]
- Input three plus characters ("+++") within one second [CC (Command Sequence Character) parameter $=0 \times 2 \mathrm{~B}$.]
- No characters sent for one second [GT (Guard Times) parameter $=0 \times 3 \mathrm{E} 8$ ]

All of the parameter values in the sequence can be modified to reflect user preferences.

NOTE: Failure to enter AT Command Mode is most commonly due to baud rate mismatch. Ensure the 'Baud' setting on the "PC Settings" tab matches the interface data rate of the RF module. By default, the $B D$ parameter $=3(9600 \mathrm{bps})$.

## To Send AT Commands:

Send AT commands and parameters using the syntax shown below.
Figure 2-08. Syntax for sending AT Commands


To read a parameter value stored in the RF module's register, omit the parameter field.
The preceding example would change the RF module Destination Address (Low) to " $0 \times 1 \mathrm{~F}$ ". To store the new value to non-volatile (long term) memory, subsequently send the WR (Write) command.

For modified parameter values to persist in the module's registry after a reset, changes must be saved to non-volatile memory using the WR (Write) Command. Otherwise, parameters are restored to previously saved values after the module is reset.

System Response. When a command is sent to the module, the module will parse and execute the command. Upon successful execution of a command, the module returns an "OK" message. If execution of a command results in an error, the module returns an "ERROR" message.

## To Exit AT Command Mode:

1. Send the ATCN (Exit Command Mode) command (followed by a carriage return).
[OR]
2. If no valid AT Commands are received within the time specified by CT (Command Mode Timeout) Command, the RF module automatically returns to Idle Mode.

For an example of programming the RF module using AT Commands and descriptions of each configurable parameter, refer to the RF Module Configuration chapter [p26].

# 3. RF Module Configuration 

## Programming the RF Module

Refer to the Command Mode section [p25] for more information about entering Command Mode, sending AT commands and exiting Command Mode. For information regarding module programming using API Mode, refer to the API Operation sections [p57].

## Programming Examples

## Setup

The programming examples in this section require the installation of Digi's X-CTU Software and a serial connection to a PC. (Digi stocks RS-232 and USB boards to facilitate interfacing with a PC.)

1. Install Digi's X-CTU Software to a PC by double-clicking the "setup_X-CTU.exe" file. (The file is located on the Digi CD and www.digi.com/xctu.)
2. Mount the RF module to an interface board, then connect the module assembly to a PC.
3. Launch the X-CTU Software and select the 'PC Settings' tab. Verify the baud and parity settings of the Com Port match those of the RF module.
NOTE: Failure to enter AT Command Mode is most commonly due to baud rate mismatch.
Ensure the 'Baud' setting on the 'PC Settings' tab matches the interface data rate of the RF module. By default, the BD parameter $=3$ (which corresponds to 9600 bps ).

## Sample Configuration: Modify RF Module Destination Address

Example: Utilize the X-CTU "Terminal" tab to change the RF module's DL (Destination Address Low) parameter and save the new address to non-volatile memory.
After establishing a serial connection between the RF module and a PC [refer to the 'Setup' section above], select the "Terminal" tab of the X-CTU Software and enter the following command lines ('CR' stands for carriage return):

Method 1 (One line per command)

```
Send AT Command
+++
ATDL <Enter>
ATDL1AOD <Enter>
ATWR <Enter>
ATCN <Enter>
```

```
System Response
OK <CR> (Enter into Command Mode)
{current value} <CR> (Read Destination Address Low)
OK <CR> (Modify Destination Address Low)
OK <CR> (Write to non-volatile memory)
OK <CR> (Exit Command Mode)
```

Method 2 (Multiple commands on one line)

| Send AT Command | System Response |
| :--- | :--- |
| +++ | OK <CR $>$ (Enter into Command Mode) |
| ATDL <Enter> | \{current value $\}<C R>$ (Read Destination Address Low) |
| ATDL1AOD,WR,CN <Enter> | $O K<C R>O K<C R>O K<C R>$ |

## Sample Configuration: Restore RF Module Defaults

Example: Utilize the X-CTU "Modem Configuration" tab to restore default parameter values. After establishing a connection between the module and a PC [refer to the 'Setup' section above], select the "Modem Configuration" tab of the X-CTU Software.

1. Select the 'Read' button.
2. Select the 'Restore' button.

## Remote Configuration Commands

The API firmware has provisions to send configuration commands to remote devices using the Remote Command Request API frame (see API Operation). This API frame can be used to send commands to a remote module to read or set command parameters.

The API firmware has provisions to send configuration commands (set or read) to a remote module using the Remote Command Request API frame (see API Operations). Remote commands can be issued to read or set command parameters on a remote device.

## Sending a Remote Command

To send a remote command, the Remote Command Request frame should be populated with values for the 64 bit and 16 bit addresses. If 64 bit addressing is desired then the 16 bit address field should be filled with 0xFFFE. If any value other than 0xFFFE is used in the 16 bit address field then the 64 bit address field will be ignored and 16 bit addressing will be used. If a command response is desired, the Frame ID should be set to a non-zero value.

## Applying Changes on Remote

When remote commands are used to change command parameter settings on a remote device, parameter changes do not take effect until the changes are applied. For example, changing the $B D$ parameter will not change the actual serial interface rate on the remote until the changes are applied. Changes can be applied using remote commands in one of three ways:

Set the apply changes option bit in the API frame
Issue an AC command to the remote device
Issue a WR + FR command to the remote device to save changes and reset the device.

## Remote Command Responses

If the remote device receives a remote command request transmission, and the API frame ID is non-zero, the remote will send a remote command response transmission back to the device that sent the remote command. When a remote command response transmission is received, a device sends a remote command response API frame out its UART. The remote command response indicates the status of the command (success, or reason for failure), and in the case of a command query, it will include the register value.
The device that sends a remote command will not receive a remote command response frame if:
The destination device could not be reached
The frame ID in the remote command request is set to 0 .

## Command Reference Tables

XBee ${ }^{\circledR} /$ /XBee-PRO® RF Modules expect numerical values in hexadecimal. Hexadecimal values are designated by a " $0 x$ " prefix. Decimal equivalents are designated by a "d" suffix. Commands are contained within the following command categories (listed in the order that their tables appear):

- Special
- Networking \& Security
- RF Interfacing
- Sleep (Low Power)
- Serial Interfacing
- I/O Settings
- Diagnostics
- AT Command Options

All modules within a PAN should operate using the same firmware version.

## Special

Table 3-01. XBee-PRO Commands - Special

| AT <br> Command | Command <br> Category | Name and Description | Parameter Range | Default |
| :--- | :--- | :--- | :--- | :--- |
| WR | Special | Write. Write parameter values to non-volatile memory so that parameter modifications <br> persist through subsequent power-up or reset. <br> Note: Once WR is issued, no additional characters should be sent to the module until <br> after the response "OKlr" is received. | - | - |
| RE | Special | Restore Defaults. Restore module parameters to factory defaults. | - |  |
| FR $\left(v 1 . \times 80^{*}\right)$ | Special | Software Reset. Responds immediately with an OK then performs a hard reset <br> $\sim 100 \mathrm{~ms}$ later. | - | - |

* Firmware version in which the command was first introduced (firmware versions are numbered in hexadecimal notation.)

Networking \& Security
Table 3-02. XBee®/XBee-PRO® Commands - Networking \& Security (Sub-categories designated within \{brackets\})

| AT Command | Command Category | Name and Description | Parameter Range | Default |
| :---: | :---: | :---: | :---: | :---: |
| CH | Networking \{Addressing\} | Channel. Set/Read the channel number used for transmitting and receiving data between RF modules (uses 802.15.4 protocol channel numbers). | $\begin{aligned} & 0 \times 0 \mathrm{~B}-0 \times 1 \mathrm{~A}(\mathrm{XBee}) \\ & 0 \times 0 \mathrm{C}-0 \times 17 \text { (XBee-PRO) } \end{aligned}$ | 0x0C (12d) |
| ID | Networking \{Addressing\} | PAN ID. Set/Read the PAN (Personal Area Network) ID. Use 0xFFFF to broadcast messages to all PANs. | 0-0xFFFF | $\begin{aligned} & 0 \times 3332 \\ & (13106 \mathrm{~d}) \end{aligned}$ |
| DH | Networking \{Addressing\} | Destination Address High. SetRead the upper 32 bits of the 64 -bit destination address. When combined with DL , it defines the destination address used for transmission. To transmit using a 16 -bit address, set DH parameter to zero and DL less than 0xFFFF. $0 x 000000000000 F F F F$ is the broadcast address for the PAN. | 0-0xFFFFFFFF | 0 |
| DL | Networking \{Addressing\} | Destination Address Low. Set/Read the lower 32 bits of the 64-bit destination address. When combined with DH, DL defines the destination address used for transmission. To transmit using a 16 -bit address, set DH parameter to zero and DL less than 0xFFFF. $0 x 000000000000$ FFFF is the broadcast address for the PAN. | 0-0xFFFFFFFF | 0 |
| MY | Networking \{Addressing\} | 16-bit Source Address. Set/Read the RF module 16-bit source address. Set MY = OxFFFF to disable reception of packets with 16 -bit addresses. 64 -bit source address (serial number) and broadcast address ( $0 \times 000000000000 \mathrm{FFFF}$ ) is always enabled. | 0-0xFFFF | 0 |
| SH | Networking \{Addressing\} | Serial Number High. Read high 32 bits of the RF module's unique IEEE 64-bit address. 64-bit source address is always enabled. | 0-0xFFFFFFFF [read-only] | Factory-set |
| SL | Networking \{Addressing\} | Serial Number Low. Read low 32 bits of the RF module's unique IEEE 64 -bit address. 64-bit source address is always enabled. | 0-0xFFFFFFFF [read-only] | Factory-set |
| RR (v1.xA0*) | Networking \{Addressing\} | XBee Retries. Set/Read the maximum number of retries the module will execute in addition to the 3 retries provided by the 802.15.4 MAC. For each XBee retry, the 802.15.4 MAC can execute up to 3 retries. | 0-6 | 0 |
| RN | Networking \{Addressing\} | Random Delay Slots. Set/Read the minimum value of the back-off exponent in the CSMA-CA algorithm that is used for collision avoidance. If $\mathrm{RN}=0$, collision avoidance is disabled during the first iteration of the algorithm (802.15.4-macMinBE). | 0-3 [exponent] | 0 |
| MM ( v1. $\times 80^{*}$ ) | Networking \{Addressing\} | MAC Mode. MAC Mode. Set/Read MAC Mode value. MAC Mode enables/disables the use of a Digi header in the 802.15.4 RF packet. When Modes 0 or 3 are enabled ( $\mathrm{MM}=0,3$ ), duplicate packet detection is enabled as well as certain AT commands. Please see the detailed MM description on page 47 for additional information. | $\begin{aligned} & 0-3 \\ & 0=\text { Digi Mode } \\ & 1=802.15 .4 \text { (no ACKs) } \\ & 2=802.15 .4 \text { (with ACKs) } \\ & 3=\text { Digi Mode (no ACKs) } \end{aligned}$ | 0 |
| $\mathrm{NI}\left(\mathrm{v1} . \times 80^{*}\right)$ | Networking \{Identification\} | Node Identifier. Stores a string identifier. The register only accepts printable ASCII data. A string can not start with a space. Carriage return ends command. Command will automatically end when maximum bytes for the string have been entered. This string is returned as part of the ND (Node Discover) command. This identifier is also used with the DN (Destination Node) command. | 20-character ASCII string | - |
| ND ( v1. . $80{ }^{*}$ ) | Networking \{Identification\} | Node Discover. Discovers and reports all RF modules found. The following information is reported for each module discovered (the example cites use of Transparent operation (AT command format) - refer to the long ND command description regarding differences between Transparent and API operation). <br> MY<CR> <br> SH<CR> <br> SL<CR> <br> DB<CR> <br> N $<$ CR > < CR > <br> The amount of time the module allows for responses is determined by the NT parameter. In Transparent operation, command completion is designated by a <CR> (carriage return). ND also accepts a Node Identifier as a parameter. In this case, only a module matching the supplied identifier will respond. If ND self-response is enabled ( $\mathrm{NO}=1$ ) the module initititing the node discover will also output a response for itself. | optional 20-character NI value |  |
| NT ( v1.xA0*) | Networking \{Identification\} | Node Discover Time. Set/Read the amount of time a node will wait for responses from other nodes when using the ND (Node Discover) command. | 0x01-0xFC [x 100 ms ] | 0x19 |

Table 3-02. XBee ${ }^{\circledR} /$ XBee-PRO ${ }^{\circledR}$ Commands - Networking \& Security (Sub-categories designated within $\{$ brackets $\}$ )

| AT |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Command |  |  |  |  |
| NO (v1xC5) | Command <br> Category | Name and Description <br> Networking <br> Ildentification $\}$ | Node Discover Options. Enables node discover self-response on the module. | Parameter Range |

Table 3-02. XBee ${ }^{\circledR} /$ XBee-PRO ${ }^{\circledR}$ Commands - Networking \& Security (Sub-categories designated within \{brackets\})

| AT <br> Command | Command Category | Name and Description | Parameter Range | Default |
| :---: | :---: | :---: | :---: | :---: |
| Al ( v1.x80*) | Networking \{Association\} | Association Indication. Read errors with the last association request: <br> 0x00-Successful Completion - Coordinator successfully started or End Device association complete <br> $0 \times 01$ - Active Scan Timeout <br> 0x02 - Active Scan found no PANs <br> 0x03 - Active Scan found PAN, but the CoordinatorAllowAssociation bit is not set <br> $0 \times 04$ - Active Scan found PAN, but Coordinator and End Device are not configured to support beacons <br> $0 \times 05$ - Active Scan found PAN, but the Coordinator ID parameter does not match the ID parameter of the End Device <br> 0x06-Active Scan found PAN, but the Coordinator CH parameter does not match the CH parameter of the End Device <br> 0x07-Energy Scan Timeout <br> 0x08-Coordinator start request failed <br> $0 \times 09$ - Coordinator could not start due to invalid parameter <br> $0 \times 0 \mathrm{~A}$ - Coordinator Realignment is in progress <br> 0x0B - Association Request not sent <br> 0x0C - Association Request timed out - no reply was received <br> 0x0D - Association Request had an Invalid Parameter <br> 0x0E - Association Request Channel Access Failure. Request was not transmitted CCA failure <br> 0x0F - Remote Coordinator did not send an ACK after Association Request was sent <br> $0 \times 10$ - Remote Coordinator did not reply to the Association Request, but an ACK was received after sending the request <br> 0x11-[reserved] <br> $0 \times 12$ - Sync-Loss - Lost synchronization with a Beaconing Coordinator <br> $0 \times 13$ - Disassociated - No longer associated to Coordinator <br> 0xFF - RF Module is attempting to associate | 0-0x13 [read-only] | - |
| DA ( v1.x80*) | Networking \{Association\} | Force Disassociation. End Device will immediately disassociate from a Coordinator (if associated) and reattempt to associate. | - | - |
| FP ( v1.x80*) | Networking \{Association\} | Force Poll. Request indirect messages being held by a coordinator. | - | - |
| AS ( v1.x80*) | Networking \{Association\} | Active Scan. Send Beacon Request to Broadcast Address (0xFFFF) and Broadcast PAN (0xFFFF) on every channel. The parameter determines the time the radio will listen for Beacons on each channel. A PanDescriptor is created and returned for every Beacon received from the scan. Each PanDescriptor contains the following information: <br> CoordAddress (SH, SL)<CR> <br> CoordPanID (ID)<CR> <br> CoordAddrMode <CR> <br> $0 \times 02=16$-bit Short Address <br> $0 \times 03=64$-bit Long Address <br> Channel (CH parameter) <CR> <br> SecurityUse<CR> <br> ACLEntry<CR> <br> SecurityFailure<CR> <br> SuperFrameSpec<CR> (2 bytes): <br> bit 15 - Association Permitted (MSB) <br> bit 14 - PAN Coordinator <br> bit 13 - Reserved <br> bit 12 - Battery Life Extension <br> bits 8-11-Final CAP Slot <br> bits 4-7 - Superframe Order <br> bits 0-3-Beacon Order <br> GtsPermit<CR> <br> RSSI<CR> (RSSI is returned as -dBm ) <br> TimeStamp<CR> (3 bytes) <br> <CR> <br> A carriage return $<C R>$ is sent at the end of the AS command. The Active Scan is capable of returning up to 5 PanDescriptors in a scan. The actual scan time on each channel is measured as Time $=\left[\left(2^{\wedge} \text { SD PARAM }\right)^{*} 15.36\right] \mathrm{ms}$. Note the total scan time is this time multiplied by the number of channels to be scanned (16 for the XBee and 13 for the XBee-PRO). Also refer to SD command description. | 0-6 | - |
| ED ( v1.x80*) | Networking \{Association\} | Energy Scan. Send an Energy Detect Scan. This parameter determines the length of scan on each channel. The maximal energy on each channel is returned \& each value is followed by a carriage return. An additional carriage return is sent at the end of the command. The values returned represent the detected energy level in units of -dBm . The actual scan time on each channel is measured as Time $=\left[\left(2^{\wedge} E D\right)^{*} 15.36\right] \mathrm{ms}$. Note the total scan time is this time multiplied by the number of channels to be scanned (refer to SD parameter). | 0-6 | - |
| EE ( v1.xA0*) | Networking \{Security\} | AES Encryption Enable. Disable/Enable 128-bit AES encryption support. Use in conjunction with the KY command. | 0-1 | 0 (disabled) |
| KY ( v1.xA0*) | Networking \{Security\} | AES Encryption Key. Set the 128-bit AES (Advanced Encryption Standard) key for encrypting/decrypting data. The KY register cannot be read. | 0 - (any 16-Byte value) | - |

[^5]
## RF Interfacing

Table 3-03. XBee/XBee-PRO Commands - RF Interfacing

| AT <br> Command | Command Category | Name and Description | Parameter Range | Default |
| :---: | :---: | :---: | :---: | :---: |
| PL | RF Interfacing | Power Level. Select/Read the power level at which the RF module transmits conducted power. | $\begin{aligned} 0-4 & (\text { XBee } / \text { XBee-PRO) } \\ 0 & =-10 / 10 \mathrm{dBm} \\ 1 & =-6 / 12 \mathrm{dBm} \\ 2 & =-4 / 14 \mathrm{dBm} \\ 3 & =-2 / 16 \mathrm{dBm} \\ 4 & =0 / 18 \mathrm{dBm} \end{aligned}$ <br> XBee-PRO International variant: $\text { PL=4: } 10 \text { dBm }$ $\text { PL=3: } 8 \text { dBm }$ $\text { PL=2: } 2 \text { dBm }$ $\mathrm{PL}=1:-3 \mathrm{dBm}$ $\mathrm{PL}=0:-3 \mathrm{dBm}$ | 4 |
| CA (v1.x80*) | RF Interfacing | CCA Threshold. Set/read the CCA (Clear Channel Assessment) threshold. Prior to transmitting a packet, a CCA is performed to detect energy on the channel. If the detected energy is above the CCA Threshold, the module will not transmit the packet. | 0x24-0x50 [-dBm] | $\begin{aligned} & 0 \times 2 \mathrm{C} \\ & (-44 \mathrm{dBm}) \end{aligned}$ |

* Firmware version in which the command was first introduced (firmware versions are numbered in hexadecimal notation.)


## Sleep (Low Power)

Table 3-04. XBee ${ }^{\circledR} /$ XBee-PRO ${ }^{\circledR}$ Commands - Sleep (Low Power)

| AT <br> Command | Command Category | Name and Description | Parameter Range | Default |
| :---: | :---: | :---: | :---: | :---: |
| SM | Sleep (Low Power) | Sleep Mode. Set/Read Sleep Mode configurations. | 0-5 <br> $0=$ No Sleep <br> 1 = Pin Hibernate <br> 2 = Pin Doze <br> 3 = Reserved <br> 4 = Cyclic sleep remote <br> 5 = Cyclic sleep remote w/ pin wake-up <br> $6=$ [Sleep Coordinator] for backwards compatibility w/ v1.x6 only; otherwise, use CE command. | 0 |
| SO | Sleep (Low Power) | Sleep Options Set/Read the sleep mode options. <br> Bit 0 - Poll wakeup disable <br> 0 - Normal operations. A module configured for cyclic sleep will poll for data on waking. <br> 1 - Disable wakeup poll. A module configured for cyclic sleep will not poll for data on waking. <br> Bit 1 - ADC/DIO wakeup sampling disable. <br> 0 - Normal operations. A module configured in a sleep mode with ADC/DIO sampling enabled will automatically perform a sampling on wakeup. <br> 1 - Suppress sample on wakeup. A module configured in a sleep mode with ADC/DIO sampling enabled will not automatically sample on wakeup. | 0-4 | 0 |
| ST | Sleep (Low Power) | Time before Sleep. <NonBeacon firmware> Set/Read time period of inactivity (no serial or RF data is sent or received) before activating Sleep Mode. ST parameter is only valid with Cyclic Sleep settings (SM = 4-5). <br> Coordinator and End Device ST values must be equal. <br> Also note, the GT parameter value must always be less than the ST value. (If GT > ST, the configuration will render the module unable to enter into command mode.) If the ST parameter is modified, also modify the GT parameter accordingly. | 1-0xFFFF [x 1 ms ] | $\begin{aligned} & 0 \times 1388 \\ & (5000 \mathrm{~d}) \end{aligned}$ |
| SP | Sleep (Low Power) | Cyclic Sleep Period. <NonBeacon firmware> Set/Read sleep period for cyclic sleeping remotes. Coordinator and End Device SP values should always be equal. To send Direct Messages, set SP $=0$. <br> End Device - SP determines the sleep period for cyclic sleeping remotes. Maximum sleep period is 268 seconds ( $0 \times 68 \mathrm{~B} 0$ ). <br> Coordinator - If non-zero, SP determines the time to hold an indirect message before discarding it. A Coordinator will discard indirect messages after a period of ( 2.5 * SP). | 0-0x68B0 [x 10 ms ] | 0 |
| DP (1.x80*) | Sleep (Low Power) | Disassociated Cyclic Sleep Period. <NonBeacon firmware> End Device - Set/Read time period of sleep for cyclic sleeping remotes that are configured for Association but are not associated to a Coordinator. (i.e. If a device is configured to associate, configured as a Cyclic Sleep remote, but does not find a Coordinator, it will sleep for DP time before reattempting association.) Maximum sleep period is 268 seconds ( $0 \times 68 B 0$ ). DP should be $>0$ for NonBeacon systems. | 1-0x68B0 [x 10 ms ] | $\begin{aligned} & 0 \times 3 E 8 \\ & (1000 \mathrm{~d}) \end{aligned}$ |

* Firmware version in which the command was first introduced (firmware versions are numbered in hexadecimal notation.)


## Serial Interfacing

Table 3-05. XBee-PRO Commands - Serial Interfacing

| AT <br> Command | Command Category | Name and Description | Parameter Range | Default |
| :---: | :---: | :---: | :---: | :---: |
| BD | Serial Interfacing | Interface Data Rate. Set/Read the serial interface data rate for communications between the RF module serial port and host. <br> Request non-standard baud rates with values above 0x80 using a terminal window. Read the BD register to find actual baud rate achieved. | $\begin{aligned} & 0-7 \text { (standard baud rates) } \\ & 0=1200 \text { bps } \\ & 1=2400 \\ & 2=4800 \\ & 3=9600 \\ & 4=19200 \\ & 5=38400 \\ & 6=57600 \\ & 7=115200 \\ & \text { 0x80 - 0x3D090 } \\ & \text { (non-standard baud rates up to } \\ & 250 \text { Kbps) } \end{aligned}$ | 3 |
| RO | Serial Interfacing | Packetization Timeout. Set/Read number of character times of inter-character delay required before transmission. Set to zero to transmit characters as they arrive instead of buffering them into one RF packet. | 0-0xFF [x character times] | 3 |
| AP (v1.x80*) | Serial Interfacing | API Enable. Disable/Enable API Mode. | $\begin{aligned} & 0-2 \\ & 0=\text { Disabled } \\ & 1=\text { API enabled } \\ & 2=\text { API enabled (w/escaped } \\ & \text { control characters) } \end{aligned}$ | 0 |
| NB | Serial Interfacing | Parity. Set/Read parity settings. | 0-4 <br> $0=8$-bit no parity <br> $1=8$-bit even <br> $2=8$-bit odd <br> $3=8$-bit mark <br> 4 = 8-bit space | 0 |
| PR (v1.x80*) | Serial Interfacing | Pull-up Resistor Enable. Set/Read bitfield to configure internal pull-up resistor status for I/O lines <br> Bitfield Map: <br> bit 0 - AD4/DIO4 (pin11) <br> bit 1 - AD3 / DIO3 (pin17) <br> bit 2 - AD2/DIO2 (pin18) <br> bit 3 - AD1/DIO1 (pin19) <br> bit 4 - ADO / DIOO (pin20) <br> bit 5 - RTS / AD6 / DIO6 (pin16) <br> bit 6 - DTR / SLEEP_RQ / DI8 (pin9) <br> bit 7 - DIN/CONFIG (pin3) <br> Bit set to "1" specifies pull-up enabled; "0" specifies no pull-up | 0-0xFF | 0xFF |

* Firmware version in which the command was first introduced (firmware versions are numbered in hexadecimal notation.)


## I/O Settings

Table 3-06. XBee-PRO Commands - I/O Settings (sub-category designated within \{brackets\})

| AT <br> Command | Command Category | Name and Description | Parameter Range | Default |
| :---: | :---: | :---: | :---: | :---: |
| D8 | I/O Settings | DI8 Configuration. Select/Read options for the DI8 line (pin 9) of the RF module. | $\begin{gathered} 0-1 \\ 0=\text { Disabled } \\ 3=D I \\ (1,2,4 \& 5 \mathrm{n} / \mathrm{a}) \end{gathered}$ | 0 |
| D7 (v1.x80*) | I/O Settings | DIO7 Configuration. Select/Read settings for the DIO7 line (pin 12) of the RF module. Options include CTS flow control and I/O line settings. | $\begin{aligned} 0 & -1 \\ 0 & =\text { Disabled } \\ 1 & =\text { CTS Flow Control } \\ 2 & =(n / a) \\ 3 & =\text { DI } \\ 4 & =\text { DO low } \\ 5 & =\text { DO high } \\ 6 & =\text { RS485 Tx Enable Low } \\ 7 & =\text { RS485 Tx Enable High } \end{aligned}$ | 1 |
| D6 (v1.x80*) | I/O Settings | DIO6 Configuration. Select/Read settings for the DIO6 line (pin 16) of the RF module. Options include RTS flow control and I/O line settings. | ```0-1 0 = Disabled 1 = RTS flow control 2=(n/a) 3 = DI 4 = DO low 5 = DO high``` | 0 |

Table 3-06. XBee-PRO Commands - I/O Settings (sub-category designated within \{brackets\})

| AT <br> Command | Command Category | Name and Description | Parameter Range | Default |
| :---: | :---: | :---: | :---: | :---: |
| D5 (v1.x80*) | I/O Settings | DIO5 Configuration. Configure settings for the DIO5 line (pin 15) of the RF module. Options include Associated LED indicator (blinks when associated) and I/O line settings. | $\begin{aligned} 0 & -1 \\ 0 & =\text { Disabled } \\ 1 & =\text { Associated indicator } \\ 2 & =\text { ADC } \\ 3 & =\text { DI } \\ 4 & =\text { DO low } \\ 5 & =\text { DO high } \end{aligned}$ | 1 |
| $\begin{aligned} & \text { D0 - D4 } \\ & \text { (v1.xA0*) } \end{aligned}$ | I/O Settings | (DIO4-DIO4) Configuration. Select/Read settings for the following lines: ADO/DIOO (pin 20), AD1/DIO1 (pin 19), AD2/DIO2 (pin 18), AD3/DIO3 (pin 17), AD4/DIO4 (pin 11). Options include: Analog-to-digital converter, Digital Input and Digital Output. | $\begin{aligned} 0-1 & - \text { Disabled } \\ 0 & =(n / a) \\ 2 & =A D C \\ 3 & =D I \\ 4 & =\text { DO low } \\ 5 & =\text { DO high } \end{aligned}$ | 0 |
| IU (v1.xA0*) | I/O Settings | I/O Output Enable. Disables/Enables I/O data received to be sent out UART. The data is sent using an API frame regardless of the current AP parameter value. | $\begin{aligned} & 0-1 \\ & 0=\text { Disabled } \\ & 1=\text { Enabled } \end{aligned}$ | 1 |
| IT (v1.xA0*) | I/O Settings | Samples before TX. Set/Read the number of samples to collect before transmitting data. Maximum number of samples is dependent upon the number of enabled inputs. | 1-0xFF | 1 |
| IS (v1.xA0*) | I/O Settings | Force Sample. Force a read of all enabled inputs (DI or ADC). Data is returned through the UART. If no inputs are defined ( DI or ADC), this command will return error. | 8-bit bitmap (each bit represents the level of an I/O line setup as an output) | - |
| 10 (v1.xA0*) | I/O Settings | Digital Output Level. Set digital output level to allow DIO lines that are setup as outputs to be changed through Command Mode. | - | - |
| IC (v1.xA0*) | I/O Settings | DIO Change Detect. Set/Read bitfield values for change detect monitoring. Each bit enables monitoring of DIO0-DIO7 for changes. If detected, data is transmitted with DIO data only. Any samples queued waiting for transmission will be sent first. | 0-0xFF [bitfield] | 0 (disabled) |
| $\mathrm{IR}\left(\mathrm{v} 1 . \mathrm{xA0}{ }^{*}\right)$ | I/O Settings | Sample Rate. Set/Read sample rate. When set, this parameter causes the module to sample all enabled inputs at a specified interval. | 0-0xFFFF [x 1 msec ] | 0 |
| IA (v1.xA0*) | I/O Settings $\{1 / 0$ Line Passing\} | I/O Input Address. Set/Read addresses of module to which outputs are bound. Setting all bytes to 0xFF will not allow any received I/O packet to change outputs. Setting address to 0xFFFF will allow any received I/O packet to change outputs. | 0-0xFFFFFFFFFFFFFFFFF | OxFFFFFFF FFFFFFFFF |
| $\begin{aligned} & \text { T0-T7 } \\ & \left(\mathrm{v} 1 . \mathrm{xA} 0^{*}\right) \end{aligned}$ | I/O Settings \{l/O Line Passing\} | (D0 - D7) Output Timeout. Set/Read Output timeout values for lines that correspond with the D0-D7 parameters. When output is set (due to I/O line passing) to a nondefault level, a timer is started which when expired will set the output to it default level. The timer is reset when a valid I/O packet is received. | 0-0xFF [x 100 ms ] | 0xFF |
| P0 | I/O Settings $\{1 / 0$ Line Passing\} | PWM0 Configuration. Select/Read function for PWM0 pin. | $\begin{aligned} 0-2 & =\text { Disabled } \\ 1 & =\text { RSSI } \\ 2 & =\text { PWM Output } \end{aligned}$ | 1 |
| P1 (v1.xA0*) | I/O Settings $\{1 / 0$ Line Passing\} | PWM1 Configuration. Select/Read function for PWM1 pin. | $\begin{aligned} 0-2 & =\text { Disabled } \\ 0 & =\text { RSSI } \\ 2 & =\text { PWM Output } \end{aligned}$ | 0 |
| M0 (v1.xA0*) | I/O Settings \{1/O Line Passing\} | PWM0 Output Level. Set/Read the PWM0 output level. | 0-0x03FF | - |
| M1 (v1.xA0*) | I/O Settings \{l/O Line Passing\} | PWM1 Output Level. Set/Read the PWM1 output level. | 0-0x03FF | - |
| PT (v1.xA0*) | I/O Settings $\{1 / 0$ Line Passing\} | PWM Output Timeout. Set/Read output timeout value for both PWM outputs. When PWM is set to a non-zero value: Due to I/O line passing, a time is started which when expired will set the PWM output to zero. The timer is reset when a valid I/O packet is received.] | 0-0xFF [x 100 ms ] | 0xFF |
| RP | I/O Settings $\{1 / 0$ Line Passing\} | RSSI PWM Timer. Set/Read PWM timer register. Set the duration of PWM (pulse width modulation) signal output on the RSSI pin. The signal duty cycle is updated with each received packet and is shut off when the timer expires.] | 0-0xFF [x 100 ms ] | 0x28 (40d) |

* Firmware version in which the command was first introduced (firmware versions are numbered in hexadecimal notation.)


## Diagnostics

Table 3-07. XBee®/XBee-PRO® Commands - Diagnostics

| AT <br> Command | Command <br> Category | Name and Description | Parameter Range | Default |
| :--- | :--- | :--- | :--- | :--- |
| VR | Diagnostics | Firmware Version. Read firmware version of the RF module. | $0-0 x F F F F$ [read-only] | Factory-set |
| VL (v1.x80*) | Diagnostics | Firmware Version - Verbose. Read detailed version information (including application <br> build date, MAC, PHY and bootloader versions). The VL command has been <br> deprecated in version 10C9. It is not supported in firmware versions after 10C8 | - | - |

Table 3-07. XBee ${ }^{\circledR} /$ XBee-PRO ${ }^{\circledR}$ Commands - Diagnostics

| AT <br> Command | Command Category | Name and Description | Parameter Range | Default |
| :---: | :---: | :---: | :---: | :---: |
| HV (v1.x80*) | Diagnostics | Hardware Version. Read hardware version of the RF module. | 0-0xFFFFF [read-only] | Factory-set |
| DB | Diagnostics | Received Signal Strength. Read signal level [in dB] of last good packet received (RSSI). Absolute value is reported. (For example: $0 \times 58=-88 \mathrm{dBm}$ ) Reported value is accurate between -40 dBm and RX sensitivity. | $\begin{aligned} & \text { 0x17-0x5C (XBee) } \\ & 0 \times 24-0 \times 64 \text { (XBee-PRO) } \\ & \text { [read-only] } \end{aligned}$ | - |
| EC (v1.x80*) | Diagnostics | CCA Failures. Reset/Read count of CCA (Clear Channel Assessment) failures. This parameter value increments when the module does not transmit a packet because it detected energy above the CCA threshold level set with CA command. This count saturates at its maximum value. Set count to "0" to reset count. | 0-0xFFFF | - |
| EA (v1.x80*) | Diagnostics | ACK Failures. Reset/Read count of acknowledgment failures. This parameter value increments when the module expires its transmission retries without receiving an ACK on a packet transmission. This count saturates at its maximum value. Set the parameter to " 0 " to reset count. | 0-0xFFFF | - |
| ED (v1.x80*) | Diagnostics | Energy Scan. Send 'Energy Detect Scan'. ED parameter determines the length of scan on each channel. The maximal energy on each channel is returned and each value is followed by a carriage return. Values returned represent detected energy levels in units of -dBm. Actual scan time on each channel is measured as Time $=\left[\left(2^{\wedge} \mathrm{SD}\right)\right.$ * 15.36] ms . Total scan time is this time multiplied by the number of channels to be scanned. | 0-6 | - |

* Firmware version in which the command was first introduced (firmware versions are numbered in hexadecimal notation.)


## AT Command Options

| AT Command | Command Category | Name and Description | Parameter Range | Default |
| :---: | :---: | :---: | :---: | :---: |
| CT | AT Command Mode Options | Command Mode Timeout. Set/Read the period of inactivity (no valid commands received) after which the RF module automatically exits AT Command Mode and returns to Idle Mode. | 2-0xFFFF [x 100 ms ] | 0x64 (100d) |
| CN | AT Command Mode Options | Exit Command Mode. Explicitly exit the modul from AT Command Mode. | -- | -- |
| AC (v1.xA0*) | AT Command Mode Options | Apply Changes. Explicitly apply changes to queued parameter value(s) and reinitialize module. | -- | -- |
| GT | AT Command Mode Options | Guard Times. Set required period of silence before and after the Command Sequence Characters of the AT Command Mode Sequence (GT+CC + GT). The period of silence is used to prevent inadvertent entrance into AT Command Mode. | 2-0x0CE4 [x 1 ms ] | $\begin{aligned} & \text { 0x3E8 } \\ & \text { (1000d) } \end{aligned}$ |
| CC | AT Command Mode Options | Command Sequence Character. Set/Read the ASCII character value to be used between Guard Times of the AT Command Mode Sequence (GT+CC+GT). The AT Command Mode Sequence enters the RF module into AT Command Mode. | 0-0xFF | $\begin{aligned} & 0 \times 2 \mathrm{~B} \\ & (++ \text { ' } \mathrm{ASCII}) \end{aligned}$ |

[^6]
## Command Descriptions

Command descriptions in this section are listed alphabetically. Command categories are designated within " < >" symbols that follow each command title. XBee®/XBee-PRO® RF Modules expect parameter values in hexadecimal (designated by the "0x" prefix).
All modules operating within the same network should contain the same firmware version.

## A1 (End Device Association) Command

<Networking \{Association\}> The A1 command is used to set and read association options for an End Device.
Use the table below to determine End Device behavior in relation to the A1 parameter.

AT Command: ATA1
Parameter Range: 0 - 0x0F [bitfield]
Default Parameter Value: 0
Related Commands: ID (PAN ID), NI (Node Identifier), CH (Channel), CE (Coordinator Enable), A2 (Coordinator Association)
Minimum Firmware Version Required: v1.x80

| Bit number | End Device Association Option |
| :---: | :---: |
| 0 - ReassignPanID | 0 - Will only associate with Coordinator operating on PAN ID that matches Node Identifier |
|  | 1 - May associate with Coordinator operating on any PAN ID |
| 1 - ReassignChannel | 0 - Will only associate with Coordinator operating on Channel that matches CH setting |
|  | 1 - May associate with Coordinator operating on any Channel |
| 2 - AutoAssociate | 0 - Device will not attempt Association |
|  | 1 - Device attempts Association until success Note: This bit is used only for Non-Beacon systems. End Devices in a Beaconing system must always associate to a Coordinator |
| 3 - PollCoordOnPinWake | 0 - Pin Wake will not poll the Coordinator for pending (indirect) Data |
|  | 1 - Pin Wake will send Poll Request to Coordinator to extract any pending data |
| 4-7 | [reserved] |

## A2 (Coordinator Association) Command

<Networking \{Association\}> The A2 command is used to set and read association options of the Coordinator.
Use the table below to determine Coordinator behavior in relation to the A2 parameter.

## AT Command: ATA2

Parameter Range: 0-7 [bitfield]
Default Parameter Value: 0
Related Commands: ID (PAN ID), NI (Node Identifier), CH (Channel), CE (Coordinator Enable), A1 (End Device Association), AS Active Scan), ED (Energy Scan)
Minimum Firmware Version Required: v1.x80

| Bit number | End Device Association Option |
| :--- | :--- |
| 0 - ReassignPanID | 0 - Coordinator will not perform Active Scan to locate available PAN ID. It will operate on ID <br> (PAN ID). |
|  |  |
|  | $0-$ Coordinator will not perform Energy Scan to determine free channel. It will operate on the <br> channel determined by the CH parameter. |
|  | 1 - Coordinator will perform Energy Scan to find a free channel, then operate on that channel. |
| $2-$ AllowAssociate | $0-$ Coordinator will not allow any devices to associate to it. |
| $3-7$ | 1 - Coordinator will allow devices to associate to it. |

The binary equivalent of the default value ( $0 \times 06$ ) is 00000110 . 'Bit 0 ' is the last digit of the sequence.

## AC (Apply Changes) Command

<AT Command Mode Options> The AC command is used to explicitly apply changes to module parameter values. 'Applying changes' means that

AT Command: ATAC
Minimum Firmware Version Required: v1.xA0 the module is re-initialized based on changes made to its parameter values. Once changes are applied, the module immediately operates according to the new parameter values.
This behavior is in contrast to issuing the WR (Write) command. The WR command saves parameter values to non-volatile memory, but the module still operates according to previously saved values until the module is re-booted or the CN (Exit AT Command Mode) command is issued.

Refer to the "AT Command - Queue Parameter Value" API type for more information.

## AI (Association Indication) Command

<Networking \{Association\}> The AI command is used to indicate occurrences of errors during the last association request.
Use the table below to determine meaning of the returned values.

| AT Command: ATAI |
| :--- |
| Parameter Range: $0-0 \times 13$ [read-only] |
| Related Commands: AS (Active Scan), ID (PAN |
| ID), CH (Channel), ED (Energy Scan), A1 (End |
| Device Association), A2 (Coordinator |
| Association), CE (Coordinator Enable) |
| Minimum Firmware Version Required: v1.x80 |


| Returned Value (Hex) | Association Indication |
| :--- | :--- |
| $0 \times 00$ | Successful Completion - Coordinator successfully started or End Device association complete |
| $0 \times 01$ | Active Scan Timeout |
| $0 \times 02$ | Active Scan found no PANs |
| $0 \times 03$ | Active Scan found PAN, but the Coordinator Allow Association bit is not set |
| $0 \times 04$ | Active Scan found PAN, but Coordinator and End Device are not configured to support beacons |
| $0 \times 05$ | Active Scan found PAN, but Coordinator ID (PAN ID) value does not match the ID of the End Device |
| $0 \times 06$ | Active Scan found PAN, but Coordinator CH (Channel) value does not match the CH of the End Device |
| $0 \times 07$ | Energy Scan Timeout |
| $0 \times 08$ | Coordinator start request failed |
| Ox09 | Coordinator could not start due to Invalid Parameter |
| Ox0A | Coordinator Realignment is in progress |
| Ox0B | Association Request not sent |
| $0 \times 0 C$ | Association Request timed out - no reply was received |
| $0 \times 0 D$ | Association Request had an Invalid Parameter |
| $0 \times 0$ E | Association Request Channel Access Failure - Request was not transmitted - CCA failure |
| Ox0F | Remote Coordinator did not send an ACK after Association Request was sent |
| $0 \times 10$ | Remote Coordinator did not reply to the Association Request, but an ACK was received <br> after sending the request |
| $0 \times 11$ | [reserved] |
| $0 \times 12$ | Sync-Loss - Lost synchronization with a Beaconing Coordinator |
| $0 \times 13$ | Disassociated - No longer associated to Coordinator |
| $0 \times F F$ | RF Module is attempting to associate |

## AP (API Enable) Command

<Serial Interfacing> The AP command is used to enable the RF module to operate using a framebased API instead of using the default Transparent (UART) mode.

| AT Command: ATAP |
| :--- |
| Parameter Range:0-2  <br> Parameter Configuration <br> 0 Disabled <br> (Transparent operation) <br> 1 API enabled <br> 2 API enabled <br> (with escaped characters) <br> Default Parameter Value:0  <br> Minimum Firmware Version Required: v1.x80  |

Refer to the API Operation section when API operation is enabled (AP = 1 or 2 ).

## AS (Active Scan) Command

<Network \{Association\}> The AS command is used to send a Beacon Request to a Broadcast (0xFFFF) and Broadcast PAN (0xFFFF) on every channel. The parameter determines the amount of time the RF module will listen for Beacons on each channel. A 'PanDescriptor' is created and returned for every Beacon received from the

AT Command: ATAS

Parameter Range: 0-6
Related Command: SD (Scan Duration), DL (Destination Low Address), DH (Destination High Address), ID (PAN ID), CH (Channel)

Minimum Firmware Version Required: v1.x80 scan. Each PanDescriptor contains the following information:

CoordAddress (SH + SL parameters)<CR> (NOTE: If MY on the coordinator is set less than 0xFFFF, the MY value is displayed)
CoordPanID (ID parameter)<CR>
CoordAddrMode <CR>
$0 \times 02=16$-bit Short Address
$0 \times 03=64$-bit Long Address
Channel (CH parameter) <CR>
SecurityUse<CR>
ACLEntry<CR>
SecurityFailure<CR>
SuperFrameSpec<CR> (2 bytes):
bit 15 - Association Permitted (MSB)
bit 14 - PAN Coordinator
bit 13 - Reserved
bit 12 - Battery Life Extension
bits 8-11 - Final CAP Slot
bits 4-7-Superframe Order
bits 0-3-Beacon Order
GtsPermit<CR>
RSSI<CR> (- RSSI is returned as -dBm)
TimeStamp<CR> (3 bytes)
<CR> (A carriage return <CR> is sent at the end of the AS command.
The Active Scan is capable of returning up to 5 PanDescriptors in a scan. The actual scan time on each channel is measured as Time $=[(2 \wedge$ (SD Parameter $)) * 15.36]$ ms. Total scan time is this time multiplied by the number of channels to be scanned ( 16 for the XBee, 12 for the XBee-PRO).

NOTE: Refer the scan table in the SD description to determine scan times. If using API Mode, no <CR>'s are returned in the response. Refer to the API Mode Operation section.

## BD (Interface Data Rate) Command

<Serial Interfacing> The BD command is used to set and read the serial interface data rate used between the RF module and host. This parameter determines the rate at which serial data is sent to the module from the host. Modified interface data rates do not take effect until the CN (Exit AT Command Mode) command is issued and the system returns the 'OK' response.
When parameters 0-7 are sent to the module, the respective interface data rates are used (as shown in the table on the right).
The RF data rate is not affected by the BD parameter. If the interface data rate is set higher than the RF data rate, a flow control configuration may need to be implemented.

## Non-standard Interface Data Rates:

## AT Command: ATBD

Parameter Range:0-7 (standard rates) $0 \times 80-0 \times 3$ D090 (non-standard rates up to 250 Kbps)

| Parameter | Configuration (bps) |
| :---: | :---: |
| 0 | 1200 |
| 1 | 2400 |
| 2 | 4800 |
| 3 | 9600 |
| 4 | 19200 |
| 5 | 38400 |
| 6 | 57600 |
| 7 | 115200 |

Default Parameter Value:3

Any value above $0 \times 07$ will be interpreted as an actual baud rate. When a value above $0 \times 07$ is sent, the closest interface data rate represented by the number is stored in the BD register. For example, a rate of 19200 bps can be set by sending the following command line "ATBD4B00". NOTE: When using Digi's X-CTU Software, non-standard interface data rates can only be set and read using the X-CTU 'Terminal' tab. Non-standard rates are not accessible through the 'Modem Configuration' tab.

When the BD command is sent with a non-standard interface data rate, the UART will adjust to accommodate the requested interface rate. In most cases, the clock resolution will cause the stored BD parameter to vary from the parameter that was sent (refer to the table below). Reading the BD command (send "ATBD" command without an associated parameter value) will return the value actually stored in the module's $B D$ register.
Parameters Sent Versus Parameters Stored

| BD Parameter Sent (HEX) | Interface Data Rate (bps) | BD Parameter Stored (HEX) |
| :---: | :---: | :---: |
| 0 | 1200 | 0 |
| 4 | 19,200 | 4 |
| 7 | $115,200^{*}$ | 7 |
| 12 C | 300 | 12 B |
| 1 C200 | 115,200 | 1 B207 |

* The 115,200 baud rate setting is actually at 111,111 baud ( $-3.5 \%$ target UART speed).


## CA (CCA Threshold) Command

<RF Interfacing> CA command is used to set and read CCA (Clear Channel Assessment) thresholds.

Prior to transmitting a packet, a CCA is performed to detect energy on the transmit channel. If the detected energy is above the CCA Threshold, the RF module will not transmit the packet.

AT Command: ATCA
Parameter Range: $0-0 \times 50$ [-dBm]
Default Parameter Value: 0x2C
(-44 decimal dBm)
Minimum Firmware Version Required: v1.x80

## CC (Command Sequence Character) Command

<AT Command Mode Options> The CC command is used to set and read the ASCII character used between guard times of the AT Command Mode Sequence (GT + CC + GT). This sequence enters

AT Command: ATCC
Parameter Range: 0-0xFF the RF module into AT Command Mode so that data entering the module from the host is recognized as commands instead of payload.

Default Parameter Value: 0x2B (ASCII "+") Related Command: GT (Guard Times)

The AT Command Sequence is explained further in the AT Command Mode section.

## CE (Coordinator Enable) Command

<Networking \{Association\} The CE command is used to set and read the behavior (End Device vs. Coordinator) of the RF module.
AT Command: ATCE

| Parameter Range:0 - |  |
| :---: | :---: |
| Parameter | Configuration |
| 0 | End Device |
| 1 | Coordinator |
| Default Parameter Value:0 |  |
| Minimum Firmware Version Required: v1.x80 |  |

## CH (Channel) Command

<Networking \{Addressing\}> The CH command is used to set/read the operating channel on which RF connections are made between RF modules. The channel is one of three addressing options available to the module. The other options are the PAN ID (ID command) and destination addresses (DL \& DH commands).

## AT Command: ATCH

Parameter Range: 0x0B-0x1A (XBee) $0 \times 0 C-0 \times 17$ (XBee-PRO)
Default Parameter Value: $0 \times 0 \mathrm{C}$ ( 12 decimal)
Related Commands: ID (PAN ID), DL (Destination Address Low, DH (Destination Address High)

In order for modules to communicate with each other, the modules must share the same channel number. Different channels can be used to prevent modules in one network from listening to transmissions of another. Adjacent channel rejection is 23 dB .

The module uses channel numbers of the 802.15 .4 standard.
Center Frequency $=2.405+(\mathrm{CH}-11 \mathrm{~d}) * 5 \mathrm{MHz}$
(d = decimal)

Refer to the XBee/XBee-PRO Addressing section for more information.

## CN (Exit Command Mode) Command

<AT Command Mode Options> The CN command is used to explicitly exit the RF module from AT Command Mode.

AT Command: ATCN

AT Command: ATCT
Parameter Range:2-0xFFFF
[ x 100 milliseconds]
Default Parameter Value: 0x64 (100 decimal (which equals 10 decimal seconds))
Number of bytes returned: 2
Related Command: CN (Exit Command Mode)

## D0 - D4 (DIOn Configuration) Commands

<I/O Settings> The D0, D1, D2, D3 and D4 commands are used to select/read the behavior of their respective AD/DIO lines (pins 20, 19, 18, 17
and 11 respectively).
Options include:

- Analog-to-digital converter
- Digital input
- Digital output

AT Commands:
ATD0, ATD1, ATD2, ATD3, ATD4
Parameter Range:0-5

| Parameter | Configuration |
| :---: | :---: |
| 0 | Disabled |
| 1 | $\mathrm{n} / \mathrm{a}$ |
| 2 | ADC |
| 3 | DI |
| 4 | DO low |
| 5 | DO high |

Default Parameter Value:0
Minimum Firmware Version Required: 1.x.A0

## D5 (DIO5 Configuration) Command

<I/O Settings> The D5 command is used to select/read the behavior of the DIO5 line (pin 15).

Options include:

- Associated Indicator (LED blinks when the module is associated)
- Analog-to-digital converter
- Digital input
- Digital output

| AT Command: ATD5 |
| :--- |
| Parameter Range:0-5 |


| Parameter | Configuration |
| :---: | :---: |
| 0 | Disabled |
| 1 | Associated Indicator |
| 2 | ADC |
| 3 | DI |
| 4 | DO low |
| 5 | DO high |

Default Parameter Value: 1
Parameters 2-5 supported as of firmware version 1.xA0

## D6 (DIO6 Configuration) Command

<I/O Settings> The D6 command is used to select/read the behavior of the DIO6 line (pin 16).
Options include:

- RTS flow control
- Analog-to-digital converter
- Digital input
- Digital output
AT Command: ATD6
Parameter Range:0 - 5

| Parameter | Configuration |
| :---: | :---: |
| 0 | Disabled |
| 1 | RTS Flow Control |
| 2 | $\mathrm{n} / \mathrm{a}$ |
| 3 | DI |
| 4 | DO low |
| 5 | DO high |

Default Parameter Value:0
Parameters 3-5 supported as of firmware version 1.xA0

## D7 (DIO7 Configuration) Command

<I/O Settings> The D7 command is used to select/read the behavior of the DIO7 line (pin 12).
Options include:

- CTS flow control
- Analog-to-digital converter
- Digital input
- Digital output
- RS485 TX Enable (this output is 3 V CMOS level, and is useful in a 3 V CMOS to RS485 conversion circuit)

AT Command: ATD7
Parameter Range:0-5

| Parameter | Configuration |
| :---: | :---: |
| 0 | Disabled |
| 1 | CTS Flow Control |
| 2 | $\mathrm{n} / \mathrm{a}$ |
| 3 | DI |
| 4 | DO low |
| 5 | DO high |
| 6 | RS485 TX Enable Low |
| 7 | RS485 TX Enable High |

Default Parameter Value: 1
Parameters 3-7 supported as of firmware version 1.x.A0

## D8 (DI8 Configuration) Command

<I/O Settings> The D8 command is used to select/read the behavior of the DI8 line (pin 9). This command enables configuring the pin to function as a digital input. This line is also used with Pin Sleep.

AT Command: ATD8
Parameter Range:0-5

| $(1,2,4 \& 5 \mathrm{n} / \mathrm{a})$ |  |
| :---: | :---: |
| Parameter | Configuration |
| 0 | Disabled |
| 3 | DI |

## DA (Force Disassociation) Command

<(Special)> The DA command is used to immediately disassociate an End Device from a Coordinator and reattempt to associate.

AT Command: ATDA
Minimum Firmware Version Required: v1.x80

## DB (Received Signal Strength) Command

<Diagnostics> DB parameter is used to read the received signal strength (in dBm ) of the last RF packet received. Reported values are accurate between -40 dBm and the RF module's receiver sensitivity.
Absolute values are reported. For example: $0 \times 58=-88 \mathrm{dBm}$ (decimal). If no packets have been received (since last reset, power cycle or sleep event), " 0 " will be reported.

## DH (Destination Address High) Command

<Networking \{Addressing\}> The DH command is used to set and read the upper 32 bits of the RF module's 64-bit destination address. When combined with the DL (Destination Address Low) parameter, it defines the destination address used for transmission.

An module will only communicate with other

## AT Command: ATDH

Parameter Range: 0 - 0xFFFFFFFF
Default Parameter Value: 0
Related Commands: DL (Destination Address Low), CH (Channel), ID (PAN VID), MY (Source Address) modules having the same channel (CH parameter), PAN ID (ID parameter) and destination address (DH + DL parameters).

To transmit using a 16-bit address, set the DH parameter to zero and the DL parameter less than 0xFFFF. 0x000000000000FFFF (DL concatenated to DH) is the broadcast address for the PAN.
Refer to the XBee/XBee-PRO Addressing section for more information.

## DL (Destination Address Low) Command

<Networking \{Addressing\}> The DL command is used to set and read the lower 32 bits of the RF module's 64-bit destination address. When combined with the DH (Destination Address High) parameter, it defines the destination address used for transmission.

A module will only communicate with other mod-
AT Command: ATDL
Parameter Range: 0-0xFFFFFFFF
Default Parameter Value: 0
Related Commands: DH (Destination Address High), CH (Channel), ID (PAN VID), MY (Source Address)
ules having the same channel (CH parameter), PAN ID (ID parameter) and destination address (DH + DL parameters).

To transmit using a 16-bit address, set the DH parameter to zero and the DL parameter less than 0xFFFF. 0x000000000000FFFF (DL concatenated to DH) is the broadcast address for the PAN.
Refer to the XBee/XBee-PRO Addressing section for more information.

## DN (Destination Node) Command

<Networking \{Identification\}> The DN command is used to resolve a NI (Node Identifier) string to a physical address. The following events occur upon successful command execution:

AT Command: ATDN
Parameter Range: 20-character ASCII String
Minimum Firmware Version Required: v1.x80

1. DL and DH are set to the address of the module with the matching NI (Node Identifier).
2. ' $O K$ ' is returned.
3. RF module automatically exits AT Command Mode.

If there is no response from a modem within 200 msec or a parameter is not specified (left blank), the command is terminated and an 'ERROR' message is returned.

DP (Disassociation Cyclic Sleep Period) Command
<Sleep Mode (Low Power)>

## NonBeacon Firmware

End Device - The DP command is used to set and read the time period of sleep for cyclic sleeping remotes that are configured for Association but are not associated to a Coordinator. (i.e. If a device is configured to associate, configured as a Cyclic Sleep remote, but does not find a Coordinator; it will sleep for DP time before reattempting association.) Maximum sleep period is 268 seconds ( $0 \times 68$ B0). DP should be $>0$ for NonBeacon systems.

## EA (ACK Failures) Command

<Diagnostics> The EA command is used to reset and read the count of ACK (acknowledgement) failures. This parameter value increments when the module expires its transmission retries without receiving an ACK on a packet transmission. This count saturates at its maximum value.

Set the parameter to " 0 " to reset count.

AT Command: ATDP
Parameter Range: $1-0 \times 68$ B0
[x 10 milliseconds]

Default Parameter Value:0×3E8
(1000 decimal)
Related Commands: SM (Sleep Mode), SP (Cyclic Sleep Period), ST (Time before Sleep)
Minimum Firmware Version Required: v1.x80

AT Command: ATEA
Parameter Range:0-0xFFFF

Minimum Firmware Version Required: v1.x80

## EC (CCA Failures) Command

<Diagnostics> The EC command is used to read and reset the count of CCA (Clear Channel Assessment) failures. This parameter value increments when the RF module does not transmit a packet due to the detection of energy that is above the CCA threshold level (set with CA command). This count saturates at its maximum value.

Set the EC parameter to "0" to reset count.

## ED (Energy Scan) Command

<Networking \{Association\}> The ED command is used to send an "Energy Detect Scan". This parameter determines the length of scan on each channel. The maximal energy on each channel is returned and each value is followed by a carriage return. An additional carriage return is sent at the end of the command.

AT Command: ATEC
Parameter Range:0 - 0xFFFF
Related Command: CA (CCA Threshold)
Minimum Firmware Version Required: v1.x80

The values returned represent the detected energy level in units of -dBm. The actual scan time on each channel is measured as Time $=[(2 \wedge$ ED PARAM $) * 15.36] \mathrm{ms}$.

Note: Total scan time is this time multiplied by the number of channels to be scanned. Also refer to the SD (Scan Duration) table. Use the SC (Scan Channel) command to choose which channels to scan.

## EE (AES Encryption Enable) Command

<Networking \{Security\}> The EE command is used to set/read the parameter that disables/ enables 128-bit AES encryption.

AT Command: ATEE
Parameter Range:0-1

| Parameter | Configuration |
| :--- | :---: |
| 0 | Disabled |
| 1 | Enabled |
| Default Parameter Value:0 |  |
| Related Commands: KY (Encryption Key), AP |  |
| (API Enable), MM (MAC Mode) |  |
| Minimum Firmware Version Required: v1.xA0 |  | always use its 64-bit long address as the source address for RF packets. This does not affect how the MY (Source Address), DH (Destination Address High) and DL (Destination Address Low) parameters work

If MM (MAC Mode) > 0 and AP (API Enable) parameter > 0:
With encryption enabled and a 16-bit short address set, receiving modules will only be able to issue $R X$ (Receive) 64-bit indicators. This is not an issue when $M M=0$.

If a module with a non-matching key detects RF data, but has an incorrect key: When encryption is enabled, non-encrypted RF packets received will be rejected and will not be sent out the UART.

Transparent Operation --> All RF packets are sent encrypted if the key is set.
API Operation --> Receive frames use an option bit to indicate that the packet was encrypted.

## FP (Force Poll) Command

<Networking (Association)> The FP command is used to request indirect messages being held by a Coordinator.

AT Command: ATFP
Minimum Firmware Version Required: v1.x80

## FR (Software Reset) Command

<Special> The FR command is used to force a software reset on the RF module. The reset simulates powering off and then on again the module.

AT Command: ATFR
Minimum Firmware Version Required: v1.x80

## GT (Guard Times) Command

<AT Command Mode Options> GT Command is used to set the DI (data in from host) time-ofsilence that surrounds the AT command sequence character (CC Command) of the AT Command Mode sequence (GT + CC + GT).
The DI time-of-silence is used to prevent inadvertent entrance into AT Command Mode.

Refer to the Command Mode section for more information regarding the AT Command Mode Sequence.

## HV (Hardware Version) Command

<Diagnostics> The HV command is used to read the hardware version of the RF module.

AT Command: ATHV
Parameter Range:0 - 0xFFFF [Read-only]
Minimum Firmware Version Required: v1.x80

## IA (I/O Input Address) Command

$<\mathrm{I} / \mathrm{O}$ Settings \{I/O Line Passing\}> The IA command is used to bind a module output to a specific address. Outputs will only change if received from this address. The IA command can be used to set/read both 16 and 64-bit addresses.

Setting all bytes to 0xFF will not allow the reception of any I/O packet to change outputs. Setting the IA address to 0xFFFF will cause the module to accept all I/O packets.

AT Command: ATGT
Parameter Range:2-0x0CE4
[x 1 millisecond]
Default Parameter Value:0x3E8
(1000 decimal)
Related Command: CC (Command Sequence Character)
$\qquad$

AT Command: ATIA
Parameter Range:0-0xFFFFFFFFFFFFFFFF
Default Parameter Value:0xFFFFFFFFFFFFFFFF (will not allow any received I/O packet to change outputs)

Minimum Firmware Version Required: v1.xA0

AT Command: ATIC
Parameter Range:0 - 0xFF [bitfield]
Default Parameter Value:0 (disabled)
Minimum Firmware Version Required: 1.xA0
<I/O Settings> Set/Read bitfield values for change detect monitoring. Each bit enables monitoring of DIOO - DIO7 for changes.

If detected, data is transmitted with DIO data only. Any samples queued waiting for transmission will be sent first.

Refer to the "ADC and Digital I/O Line Support" sections of the "RF Module Operations" chapter for more information.

## ID (Pan ID) Command

<Networking \{Addressing\}> The ID command is used to set and read the PAN (Personal Area Network) ID of the RF module. Only modules with matching PAN IDs can communicate with each other. Unique PAN IDs enable control of which RF packets are received by a module.
Setting the ID parameter to 0xFFFF indicates a global transmission for all PANs. It does not indicate a global receive.

## IO (Digital Output Level) Command

<I/O Settings> The IO command is used to set digital output levels. This allows DIO lines setup as outputs to be changed through Command Mode.

AT Command: ATIO
Parameter Range: 8-bit bitmap
(where each bit represents the level of an I/O line that is setup as an output.)
Minimum Firmware Version Required: v1.xA0

## IR (Sample Rate) Command

<I/O Settings> The IR command is used to set/ read the sample rate. When set, the module will sample all enabled DIO/ADC lines at a specified interval. This command allows periodic reads of the ADC and DIO lines in a non-Sleep Mode setup. A sample rate which requires transmissions at a rate greater than once every 20 ms is not recommended.

AT Command: ATIR
Parameter Range: 0 - 0xFFFF [x 1 msec ] (cannot guarantee 1 ms timing when $\mathrm{IT}=1$ )

Default Parameter Value:0
Related Command: IT (Samples before TX)
Minimum Firmware Version Required: v1.xA0

Example: When IR $=0 \times 14$, the sample rate is 20 ms (or 50 Hz ).

## IS (Force Sample) Command

<I/O Settings> The IS command is used to force a read of all enabled DIO/ADC lines. The data is returned through the UART.

When operating in Transparent Mode ( $\mathrm{AP}=0$ ), the data is retuned in the following format:

AT Command: ATIS
Parameter Range: 1-0xFF
Default Parameter Value: 1
Minimum Firmware Version Required: v1.xA0

All bytes are converted to ASCII:
number of samples <CR>
channel mask<CR>
DIO data<CR> (If DIO lines are enabled<CR>
ADC channel Data<cr> <-This will repeat for every enabled ADC channel<CR>
$<C R>$ (end of data noted by extra $<\mathrm{CR}>$ )
When operating in API mode (AP >0), the command will immediately return an 'OK' response. The data will follow in the normal API format for DIO data.

## IT (Samples before TX) Command

<I/O Settings> The IT command is used to set/ read the number of DIO and ADC samples to collect before transmitting data.
One ADC sample is considered complete when all enabled ADC channels have been read. The mod-

AT Command: ATIT
Parameter Range: 1-0xFF
Default Parameter Value: 1
Minimum Firmware Version Required: v1.xA0 ule can buffer up to 93 Bytes of sample data.
Since the module uses a 10 -bit A/D converter, each sample uses two Bytes. This leads to a maximum buffer size of 46 samples or $I T=0 \times 2 E$.

When Sleep Modes are enabled and IR (Sample Rate) is set, the module will remain awake until IT samples have been collected.

## IU (I/O Output Enable) Command

$<\mathrm{I} / \mathrm{O}$ Settings> The IU command is used to disable/enable I/O UART output. When enabled (IU $=1$ ), received I/O line data packets are sent out the UART. The data is sent using an API frame regardless of the current AP parameter value.
AT Command: ATIU

| Parameter Range:0-1 |  |
| :---: | :---: |
| Parameter | Configuration |
| 1 | Disabled - <br> Received I/O line data <br> packets will be NOT <br> sent out UART. |
| 1 | Enabled - <br> Received I/O line data <br> will be sent out UART |
| Default Parameter Value:1 |  |
| Minimum Firmware Version Required: 1.xAO |  |

## KY (AES Encryption Key) Command

<Networking \{Security\}> The KY command is used to set the 128 -bit AES (Advanced Encryption Standard) key for encrypting/decrypting data. Once set, the key cannot be read out of the module by any means.
The entire payload of the packet is encrypted

## AT Command: ATKY

Parameter Range:0 - (any 16-Byte value)
Default Parameter Value:0
Related Command: EE (Encryption Enable)
Minimum Firmware Version Required: v1.xA0 using the key and the CRC is computed across the ciphertext. When encryption is enabled, each packet carries an additional 16 Bytes to convey the random CBC Initialization Vector (IV) to the receiver(s). The KY value may be " 0 " or any 128 -bit value. Any other value, including entering KY by itself with no parameters, is invalid. All ATKY entries (valid or not) are received with a returned 'OK'.

A module with the wrong key (or no key) will receive encrypted data, but the data driven out the serial port will be meaningless. A module with a key and encryption enabled will receive data sent from a module without a key and the correct unencrypted data output will be sent out the serial port. Because CBC mode is utilized, repetitive data appears differently in different transmissions due to the randomly-generated IV.
When queried, the system will return an 'OK' message and the value of the key will not be returned.

## MO (PWMO Output Level) Command

<I/O Settings> The M0 command is used to set/ read the output level of the PWMO line (pin 6).
Before setting the line as an output:

1. Enable PWMO output $(P O=2)$
2. Apply settings (use CN or AC)

The PWM period is $64 \mu \mathrm{sec}$ and there are $0 \times 03 \mathrm{FF}$ ( 1023 decimal) steps within this period. When M0 = 0 ( $0 \%$ PWM), 0x01FF (50\% PWM), 0x03FF (100\% PWM), etc.

AT Command: ATMO
Parameter Range:0 - 0x03FF [steps]
Default Parameter Value:0
Related Commands: P0 (PWMO Enable), AC
(Apply Changes), CN (Exit Command Mode)
Minimum Firmware Version Required: v1.xA0

## M1 (PWM1 Output Level) Command

<I/O Settings> The M1 command is used to set/ read the output level of the PWM1 line (pin 7).

Before setting the line as an output:

1. Enable PWM1 output ( $\mathrm{P} 1=2$ )
2. Apply settings (use CN or AC )

AT Command: ATM 1
Parameter Range:0-0x03FF
Default Parameter Value:0
Related Commands: P1 (PWM1 Enable), AC (Apply Changes), CN (Exit Command Mode)

Minimum Firmware Version Required: v1.xA0

## MM (MAC Mode) Command

<Networking \{Addressing\}> The MM command is used to set and read the MAC Mode value. The MM command disables/enables the use of a Digi header contained in the 802.15.4 RF packet. By default ( $\mathrm{MM}=0$ ), Digi Mode is enabled and the module adds an extra header to the data portion of the 802.15.4 packet. This enables the following features:

- ND and DN command support
- Duplicate packet detection when using ACKs
- "RR command
- "DIO/AIO sampling support

The MM command allows users to turn off the use of the extra header. Modes 1 and 2 are strict

Note: When MM=0 or 3, application and CCA failure retries are not supported.

## MY (16-bit Source Address) Command

AT Command: ATMM
Parameter Range:0-3

| Parameter | Configuration |
| :---: | :---: |
| 0 | Digi Mode (802.15.4 + <br> Digi header) |
| 1 | 802.15 .4 (no ACKs) |
| 2 | 802.15 .4 (with ACKs) |
| 3 | Digi Mode (no ACKs) |

Default Parameter Value:0
Related Commands: ND (Node Discover), DN (Destination Node)

Minimum Firmware Version Required: v1.x80
802.15.4 modes. If the Digi header is disabled, ND and DN parameters are also disabled.
<Networking \{Addressing\}> The MY command is used to set and read the 16 -bit source address of the RF module.
By setting MY to 0xFFFF, the reception of RF packets having a 16 -bit address is disabled. The 64-bit address is the module's serial number and is always enabled.

NB (Parity) Command
<Serial Interfacing> The NB command is used to select/read the parity settings of the RF module for UART communications.
Note: the module does not actually calculate and check the parity; it only interfaces with devices at the configured parity and stop bit settings.

AT Command: ATMY
Parameter Range: 0-0xFFFF
Default Parameter Value: 0
Related Commands: DH (Destination Address High), DL (Destination Address Low), CH (Channel), ID (PAN ID)

AT Command: ATNB
Parameter Range: 0-4

| Parameter | Configuration |
| :---: | :---: |
| 0 | 8 -bit no parity |
| 1 | 8 -bit even |
| 2 | 8 -bit odd |
| 3 | 8 -bit mark |
| 4 | 8 -bit space |

Default Parameter Value: 0
Number of bytes returned: 1

## ND (Node Discover) Command

<Networking \{Identification\}> The ND command is used to discover and report all modules on its current operating channel (CH parameter) and PAN ID (ID parameter). ND also accepts an NI (Node Identifier) value as a parameter. In this case, only a module matching the supplied identifier will respond.

ND uses a 64-bit long address when sending and

## AT Command: ATND

Range: optional 20-character NI value
Related Commands: CH (Channel), ID (Pan ID), MY (Source Address), SH (Serial Number High), SL (Serial Number Low), NI (Node Identifier), NT (Node Discover Time)
Minimum Firmware Version Required: v1.x80 responding to an ND request. The ND command causes a module to transmit a globally addressed ND command packet. The amount of time allowed for responses is determined by the NT (Node Discover Time) parameter.
In AT Command mode, command completion is designated by a carriage return (0x0D). Since two carriage returns end a command response, the application will receive three carriage returns at the end of the command. If no responses are received, the application should only receive one carriage return. When in API mode, the application should receive a frame (with no data) and status (set to 'OK') at the end of the command. When the ND command packet is received, the remote sets up a random time delay (up to 2.2 sec ) before replying as follows:
Node Discover Response (AT command mode format - Transparent operation):
MY (Source Address) value<CR>
SH (Serial Number High) value<CR>
SL (Serial Number Low) value<CR>
DB (Received Signal Strength) value $<C R>$
NI (Node Identifier) value<CR>
<CR> (This is part of the response and not the end of command indicator.)
Node Discover Response (API format - data is binary (except for NI)):
2 bytes for MY (Source Address) value
4 bytes for SH (Serial Number High) value
4 bytes for SL (Serial Number Low) value
1 byte for DB (Received Signal Strength) value
NULL-terminated string for NI (Node Identifier) value (max 20 bytes w/out NULL terminator)

## NI (Node Identifier) Command

<Networking \{Identification\}> The NI command is used to set and read a string for identifying a particular node.
Rules:

- Register only accepts printable ASCII data.
- A string can not start with a space.
- A carriage return ends command
- Command will automatically end when maximum bytes for the string have been entered. This string is returned as part of the ND (Node Discover) command. This identifier is also used with the DN (Destination Node) command.

NO (Node Discover Options) Command
<Networking \{Identification\}> The NO command is used to suppress/include a self-response to Node Discover commands. When $\mathrm{NO}=1$ a module doing a Node Discover will include a response entry for itself.

AT Command: ATNI
Parameter Range: 20-character ASCII string
Related Commands: ND (Node Discover), DN (Destination Node)
Minimum Firmware Version Required: v1.x80

## NT (Node Discover Time) Command

<Networking \{Identification\}> The NT command is used to set the amount of time a base node will wait for responses from other nodes when using the ND (Node Discover) command. The NT value is transmitted with the ND command.

Remote nodes will set up a random hold-off time based on this time. The remotes will adjust this time down by 250 ms to give each node the ability to respond before the base ends the command. Once the ND command has ended, any response received on the base will be discarded.

## P0 (PWM0 Configuration) Command

$<\mathrm{I} / \mathrm{O}$ Setting \{I/O Line Passing\}> The PO command is used to select/read the function for PWMO (Pulse Width Modulation output 0). This command enables the option of translating incoming data to a PWM so that the output can be translated back into analog form.

With the IA (I/O Input Address) parameter correctly set, ADO values can automatically be passed to PWMO.

AT Command: ATNT
Parameter Range: $0 \times 01-0 \times F C$
[ $\times 100 \mathrm{msec}$ ]

Default: 0×19 (2.5 decimal seconds)
Related Commands: ND (Node Discover)
Minimum Firmware Version Required: 1.xA0

AT Command: ATPO
The second character in the command is the number zero ("0"), not the letter " 0 ".
Parameter Range: 0-2

| Parameter | Configuration |
| :---: | :---: |
| 0 | Disabled |
| 1 | RSSI |
| 2 | PWM0 Output |

Default Parameter Value: 1 passed to PWMO.

## P1 (PWM1 Configuration) Command

$<\mathrm{I} / \mathrm{O}$ Setting \{I/O Line Passing\} $>$ The P1 command is used to select/read the function for PWM1 (Pulse Width Modulation output 1). This command enables the option of translating incoming data to a PWM so that the output can be translated back into analog form.
With the IA (I/O Input Address) parameter correctly set, AD1 values can automatically be passed to PWM1.

AT Command: ATP1
Parameter Range: 0-2

| Parameter | Configuration |
| :---: | :---: |
| 0 | Disabled |
| 1 | RSSI |
| 2 | PWM1 Output |

Default Parameter Value: 0
Minimum Firmware Version Required: v1.xA0

## PL (Power Level) Command

<RF Interfacing> The PL command is used to select and read the power level at which the RF module transmits conducted power.
When operating in Europe, XBee-PRO 802.15.4 modules must operate at or below a transmit power output level of 10 dBm . Customers have 2 choices for transmitting at or below 10dBm:

- Order the standard XBeePRO module and change the PL command to "0" (10dBm),
- Order the International variant of the XBee-PRO module, which has a maximum transmit output power of 10 dBm .


## PR (Pull-up Resistor) Command

<Serial Interfacing> The PR command is used to set and read the bit field that is used to configure internal the pull-up resistor status for I/O lines. "1" specifies the pull-up resistor is enabled. " 0 " specifies no pull up.

AT Command: ATPR
Parameter Range: 0-0xFF
Default Parameter Value: 0xFF
(all pull-up resistors are enabled)
Minimum Firmware Version Required: v1.x80
bit 0 - AD4/DIO4 (pin 11)
bit 1 - AD3/DIO3 (pin 17)
bit 2 - AD2/DIO2 (pin 18)
bit 3 - AD1/DIO1 (pin 19)
bit 4 - ADO/DIOO (pin 20)
bit 5 - AD6/DIO6 (pin 16)
bit 6 - DI8 (pin 9)
bit 7 - DIN/CONFIG (pin 3)
For example: Sending the command "ATPR 6F" will turn bits $0,1,2,3,5$ and 6 ON; and bits $4 \& 7$ will be turned OFF. (The binary equivalent of " $0 \times 6 \mathrm{~F}$ " is " 01101111 ". Note that 'bit 0 ' is the last digit in the bitfield.

## PT (PWM Output Timeout) Command

<I/O Settings \{I/O Line Passing\}> The PT command is used to set/read the output timeout value for both PWM outputs.

When PWM is set to a non-zero value: Due to I/O line passing, a time is started which when expired will set the PWM output to zero. The timer is reset when a valid I/O packet is received.

AT Command: ATPT
Parameter Range: 0 - 0xFF [x 100 msec ]
Default Parameter Value: 0xFF
Minimum Firmware Version Required: 1.xA0

## RE (Restore Defaults) Command

<(Special)> The RE command is used to restore all configurable parameters to their factory

AT Command: ATRE default settings. The RE command does not write restored values to non-volatile (persistent) memory. Issue the WR (Write) command subsequent to issuing the RE command to save restored parameter values to non-volatile memory.

## RN (Random Delay Slots) Command

<Networking \& Security> The RN command is used to set and read the minimum value of the back-off exponent in the CSMA-CA algorithm. The CSMA-CA algorithm was engineered for collision

AT Command: ATRN
Parameter Range: 0-3 [exponent]
Default Parameter Value: 0 avoidance (random delays are inserted to prevent data loss caused by data collisions).
If $R N=0$, collision avoidance is disabled during the first iteration of the algorithm (802.15.4macMinBE).

CSMA-CA stands for "Carrier Sense Multiple Access - Collision Avoidance". Unlike CSMA-CD (reacts to network transmissions after collisions have been detected), CSMA-CA acts to prevent data collisions before they occur. As soon as a module receives a packet that is to be transmitted, it checks if the channel is clear (no other module is transmitting). If the channel is clear, the packet is sent over-the-air. If the channel is not clear, the module waits for a randomly selected period of time, then checks again to see if the channel is clear. After a time, the process ends and the data is lost.

## RO (Packetization Timeout) Command

<Serial Interfacing> RO command is used to set and read the number of character times of intercharacter delay required before transmission.

| AT Command: ATRO |  |
| :---: | :---: |
|  | Parameter Range: 0 - 0xFF [ x character times |
|  | - 3 |

RF transmission commences when data is detected in the DI (data in from host) buffer and

Default Parameter Value: 3
RO character times of silence are detected on the
UART receive lines (after receiving at least 1 byte).
RF transmission will also commence after 100 Bytes (maximum packet size) are received in the DI buffer.

Set the RO parameter to ' 0 ' to transmit characters as they arrive instead of buffering them into one RF packet.

## RP (RSSI PWM Timer) Command

$<\mathrm{I} / \mathrm{O}$ Settings \{I/O Line Passing\}> The RP command is used to enable PWM (Pulse Width Modulation) output on the RF module. The output is calibrated to show the level a received RF signal is above the sensitivity level of the module. The
 PWM pulses vary from 24 to $100 \%$. Zero percent means PWM output is inactive. One to $24 \%$ percent means the received RF signal is at or below the published sensitivity level of the module. The following table shows levels above sensitivity and PWM values.

The total period of the PWM output is $64 \mu \mathrm{~s}$. Because there are 445 steps in the PWM output, the minimum step size is 144 ns .
PWM Percentages

| dB above Sensitivity | PWM percentage <br> (high period / total period) |
| :---: | :---: |
| 10 | $41 \%$ |
| 20 | $58 \%$ |
| 30 | $75 \%$ |

A non-zero value defines the time that the PWM output will be active with the RSSI value of the last received RF packet. After the set time when no RF packets are received, the PWM output will be set low ( 0 percent PWM) until another RF packet is received. The PWM output will also be set low at power-up until the first RF packet is received. A parameter value of 0xFF permanently enables the PWM output and it will always reflect the value of the last received RF packet.

## RR (XBee Retries) Command

<Networking \{Addressing\}> The RR command is used set/read the maximum number of retries the module will execute in addition to the 3 retries provided by the 802.15.4 MAC. For each XBee retry, the 802.15.4 MAC can execute up to 3

AT Command: ATRR
Parameter Range: 0-6
Default: 0
Minimum Firmware Version Required: 1.xA0 retries.

This values does not need to be set on all modules for retries to work. If retries are enabled, the transmitting module will set a bit in the Digi RF Packet header which requests the receiving module to send an ACK (acknowledgement). If the transmitting module does not receive an ACK within 200 msec , it will re-send the packet within a random period up to 48 msec . Each XBee retry can potentially result in the MAC sending the packet 4 times ( 1 try plus 3 retries). Note that retries are not attempted for packets that are purged when transmitting with a Cyclic Sleep Coordinator.

## SC (Scan Channels) Command

<Networking \{Association\}> The SC command is used to set and read the list of channels to scan for all Active and Energy Scans as a bit field.

This affects scans initiated in command mode [AS (Active Scan) and ED (Energy Scan) commands] and during End Device Association and Coordinator startup.

| bit $0-0 \times 0 B$ | bit $4-0 \times 0 F$ | bit $8-0 \times 13$ | bit $12-0 \times 17$ |
| :--- | :--- | :--- | :--- |
| bit $1-0 \times 0 C$ | bit $5-0 \times 10$ | bit $9-0 \times 14$ | bit $13-0 \times 18$ |
| bit $2-0 \times 0 D$ | bit $6-0 \times 11$ | bit $10-0 \times 15$ | bit $14-0 \times 19$ |
| bit $3-0 \times 0 E$ | bit $7-0 \times 12$ | bit $11-0 \times 16$ | bit $15-0 \times 1 A$ |

AT Command: ATSC XBee-PRO) PRO channels) (Scan Duration)

## SD (Scan Duration) Command

<Networking \{Association\}> The SD command is used to set and read the exponent value that determines the duration (in time) of a scan.
End Device (Duration of Active Scan during Association) - In a Beacon system, set SD = BE of the Coordinator. SD must be set at least to the highest BE parameter of any Beaconing Coordinator with which an End Device or Coordinator wish to discover.

Coordinator - If the 'ReassignPANID' option is set on the Coordinator [refer to A2 parameter], the SD parameter determines the length of time the Coordinator will scan channels to locate existing PANs. If the 'ReassignChannel' option is set, SD determines how long the Coordinator will perform an Energy Scan to determine which channel it will operate on.

Scan Time is measured as ((\# of Channels to Scan) * $\left.\left(2^{\wedge} \mathrm{SD}\right) * 15.36 \mathrm{~ms}\right)$. The number of channels to scan is set by the SC command. The XBee RF Module can scan up to 16 channels (SC $=$ $0 \times F F F F$ ). The XBee PRO RF Module can scan up to 12 channels ( $\mathrm{SC}=0 \times 1$ FFE).
Examples: Values below show results for a 12-channel scan

| If $S D=0$, time $=0.18 \mathrm{sec}$ | $S D=8$, time $=47.19 \mathrm{sec}$ |
| :--- | :--- |
| $S D=2$, time $=0.74 \mathrm{sec}$ | $S D=10$, time $=3.15 \mathrm{~min}$ |
| $S D=4$, time $=2.95 \mathrm{sec}$ | $S D=12$, time $=12.58 \mathrm{~min}$ |
| $S D=6$, time $=11.80 \mathrm{sec}$ | $S D=14$, time $=50.33 \mathrm{~min}$ |

## SH (Serial Number High) Command

<Diagnostics> The SH command is used to read the high 32 bits of the RF module's unique IEEE 64-bit address.
The module serial number is set at the factory and is read-only.

AT Command: ATSH
Parameter Range: 0 - 0xFFFFFFFF [read-only]
Related Commands: SL (Serial Number Low), MY (Source Address)

## SL (Serial Number Low) Command

<Diagnostics> The SL command is used to read the low 32 bits of the RF module's unique IEEE 64-bit address.

The module serial number is set at the factory and is read-only.

Parameter Range: 1-0xFFFF [Bitfield]
(bits $0,14,15$ are not allowed when using the

Default Parameter Value: 0x1 FFE (all XBee-

Related Commands: ED (Energy Scan), SD

Minimum Firmware Version Required: v1.x80

AT Command: ATSD
Parameter Range: $0-0 \times 0 F$
Default Parameter Value: 4
Related Commands: ED (Energy Scan), SC (Scan Channel)
Minimum Firmware Version Required: v1.x80

## SM (Sleep Mode) Command

<Sleep Mode (Low Power)> The SM command is used to set and read Sleep Mode settings. By default, Sleep Modes are disabled ( $\mathrm{SM}=0$ ) and the RF module remains in Idle/ Receive Mode. When in this state, the module is constantly ready to respond to either serial or RF activity.

* The Sleep Coordinator option (SM=6) only exists for backwards compatibility with firmware version 1.x06 only. In all other cases, use the CE command to enable a Coordinator.

AT Command: ATSM

| Parameter Range: $0-6$ |  |
| :---: | :---: |
| Parameter | Configuration |
| 0 | Disabled |
| 1 | Pin Hibernate |
| 2 | Pin Doze |
| 3 | (reserved) |
| 4 | Cyclic Sleep Remote |
| 5 | Cyclic Sleep Remote <br> (with Pin Wake-up) |
| 6 | Sleep Coordinator* |

Default Parameter Value: 0

## SO (Sleep Mode Command)

Sleep (Low Power) Sleep Options Set/Read the sleep mode options.

Bit 0 - Poll wakeup disable

- 0 - Normal operations. A module configured for cyclic sleep will poll for data on waking.
- 1 - Disable wakeup poll. A module configured for cyclic sleep will not poll for data on waking.

AT Command: ATSO

| Parameter <br> Range: | $0-4$ |
| :--- | :--- |

Default Parameter Value:
Related Commands: SM (Sleep Mode), ST
(Time before Sleep), DP (Disassociation Cyclic Sleep Period, BE (Beacon Order)

Bit 1-ADC/DIO wakeup sampling disable.

- 0 - Normal operations. A module configured in a sleep mode with ADC/DIO sampling enabled will automatically perform a sampling on wakeup.
- 1 - Suppress sample on wakeup. A module configured in a sleep mode with ADC/DIO sampling enabled will not automatically sample on wakeup.


## SP (Cyclic Sleep Period) Command

<Sleep Mode (Low Power)> The SP command is used to set and read the duration of time in which a remote RF module sleeps. After the cyclic sleep period is over, the module wakes and checks for data. If data is not present, the module goes back to sleep. The maximum sleep period is 268 seconds (SP = 0x68B0).
The SP parameter is only valid if the module is configured to operate in Cyclic Sleep ( $\mathrm{SM}=4-6$ ).
Coordinator and End Device SP values should
always be equal.
To send Direct Messages, set SP $=0$.

## NonBeacon Firmware

End Device - SP determines the sleep period for cyclic sleeping remotes. Maximum sleep period is 268 seconds (0x68B0).
Coordinator - If non-zero, SP determines the time to hold an indirect message before discarding it. A Coordinator will discard indirect messages after a period of (2.5*SP).

## ST (Time before Sleep) Command

<Sleep Mode (Low Power)> The ST command is used to set and read the period of inactivity (no serial or RF data is sent or received) before activating Sleep Mode.

## NonBeacon Firmware

Set/Read time period of inactivity (no serial or RF data is sent or received) before activating Sleep
Mode. ST parameter is only valid with Cyclic Sleep settings (SM = 4-5).

Coordinator and End Device ST values must be equal.

AT Command: ATST
Parameter NonBeacon Firmware: Range: 1 - 0xFFFF [x 1 millisecond]
Default Parameter Value:
Related Commands: SM (Sleep Mode), ST (Time before Sleep)

## T0-T7 ((D0-D7) Output Timeout) Command

$<\mathrm{I} / \mathrm{O}$ Settings \{I/O Line Passing $\gg$ The T0, T1, T2, T3, T4, T5, T6 and T7 commands are used to set/read output timeout values for the lines that correspond with the D0 - D7 parameters. When output is set (due to I/O line passing) to a nondefault level, a timer is started which when expired, will set the output to its default level. The timer is reset when a valid I/O packet is received. The Tn parameter defines the permissible amount of time to stay in a non-default (active) state. If $\mathrm{Tn}=0$, Output Timeout is disabled (output levels are held indefinitely).

## VL (Firmware Version - Verbose)

<Diagnostics> The VL command is used to read detailed version information about the RF module. The information includes:
application build date; MAC, PHY and bootloader versions; and build dates. This command was removed from firmware 1 xC 9 and later versions.

AT Command: ATVL
Parameter Range:0-0xFF
[ x 100 milliseconds]
Default Parameter Value: 0x28 (40 decimal)
Minimum Firmware Version Required: v1.x80 - v1.xC8

AT Commands: ATTO - ATT7
Parameter Range:0-0xFF [x 100 msec ]
Default Parameter Value:0xFF
Minimum Firmware Version Required: v1.xA0

## VR (Firmware Version) Command

<Diagnostics> The VR command is used to read which firmware version is stored in the module.

## AT Command: ATVR

Parameter Range: 0 - 0xFFFF [read only]
XBee version numbers will have four significant digits. The reported number will show three or four numbers and is stated in hexadecimal notation. A version can be reported as " $A B C$ " or " $A B C D$ ". Digits $A B C$ are the main release number and $D$ is the revision number from the main release. " $D$ " is not required and if it is not present, a zero is assumed for D . " B " is a variant designator. The following variants exist:

- "0" = Non-Beacon Enabled 802.15.4 Code
- "1" = Beacon Enabled 802.15.4 Code


## WR (Write) Command

<(Special)> The WR command is used to write configurable parameters to the RF module's non-

AT Command: ATWR volatile memory. Parameter values remain in the module's memory until overwritten by subsequent use of the WR Command.

If changes are made without writing them to non-volatile memory, the module reverts back to previously saved parameters the next time the module is powered-on.

NOTE: Once the WR command is sent to the module, no additional characters should be sent until after the "OK/r" response is received.

## API Operation

By default, XBee®/XBee-PRO® RF Modules act as a serial line replacement (Transparent Operation) - all UART data received through the DI pin is queued up for RF transmission. When the module receives an RF packet, the data is sent out the DO pin with no additional information.
Inherent to Transparent Operation are the following behaviors:

- If module parameter registers are to be set or queried, a special operation is required for transitioning the module into Command Mode.
- In point-to-multipoint systems, the application must send extra information so that the receiving module(s) can distinguish between data coming from different remotes.
As an alternative to the default Transparent Operation, API (Application Programming Interface) Operations are available. API operation requires that communication with the module be done through a structured interface (data is communicated in frames in a defined order). The API specifies how commands, command responses and module status messages are sent and received from the module using a UART Data Frame.


## API Frame Specifications

Two API modes are supported and both can be enabled using the AP (API Enable) command. Use the following AP parameter values to configure the module to operate in a particular mode:

- AP $=0$ (default): Transparent Operation (UART Serial line replacement) API modes are disabled.
- AP = 1: API Operation
- AP = 2: API Operation (with escaped characters)

Any data received prior to the start delimiter is silently discarded. If the frame is not received correctly or if the checksum fails, the data is silently discarded.

API Operation (AP parameter $=1$ )
When this API mode is enabled ( $\mathrm{AP}=1$ ), the UART data frame structure is defined as follows:
Figure 3-01. UART Data Frame Structure:

| Start Delimiter <br> (Byte 1) | Length <br> (Bytes 2-3) | Frame Data <br> (Bytes 4-n) | Checksum <br> (Byte $\mathrm{n}+1$ 1) |  |
| :---: | :---: | :---: | :---: | :---: |
| 0x7E | MSB | LSB | API-specific Structure | 1 Byte |

MSB $=$ Most Significant Byte, LSB $=$ Least Significant Byte
API Operation - with Escape Characters (AP parameter = 2)
When this API mode is enabled ( $\mathrm{AP}=2$ ), the UART data frame structure is defined as follows:
Figure 3-02. UART Data Frame Structure - with escape control characters:


Escape characters. When sending or receiving a UART data frame, specific data values must be escaped (flagged) so they do not interfere with the UART or UART data frame operation. To escape an interfering data byte, insert 0x7D and follow it with the byte to be escaped XOR'd with $0 \times 20$.

## Data bytes that need to be escaped:

- 0x7E - Frame Delimiter
- 0x7D - Escape
- $0 \times 11$ - XON
- 0x13 - XOFF

Example - Raw UART Data Frame (before escaping interfering bytes): $0 \times 7 \mathrm{E} 0 \times 000 \times 020 \times 230 \times 110 \times C B$
$0 \times 11$ needs to be escaped which results in the following frame:
$0 x 7 E 0 x 000 x 020 x 230 x 7 D 0 x 310 x C B$
Note: In the above example, the length of the raw data (excluding the checksum) is $0 \times 0002$ and the checksum of the non-escaped data (excluding frame delimiter and length) is calculated as: $0 \times F F-(0 \times 23+0 \times 11)=(0 x F F-0 \times 34)=0 \times C B$.

## Checksum

To test data integrity, a checksum is calculated and verified on non-escaped data.
To calculate: Not including frame delimiters and length, add all bytes keeping only the lowest 8 bits of the result and subtract from 0xFF.

To verify: Add all bytes (include checksum, but not the delimiter and length). If the checksum is correct, the sum will equal 0xFF.

## API Types

Frame data of the UART data frame forms an API-specific structure as follows:


The cmdID frame (API-identifier) indicates which API messages will be contained in the cmdData frame (Identifier-specific data). Refer to the sections that follow for more information regarding the supported API types. Note that multi-byte values are sent big endian.

## Modem Status

API Identifier: $0 \times 8 \mathrm{~A}$
RF module status messages are sent from the module in response to specific conditions.
Figure 3-04. Modem Status Frames


## AT Command

API Identifier Value: 0x08
The "AT Command" API type allows for module parameters to be queried or set. When using this command ID, new parameter values are applied immediately. This includes any register set with the "AT Command - Queue Parameter Value" (0x09) API type.
Figure 3-05. AT Command Frames


Figure 3-06. Example: API frames when reading the DL parameter value of the module.


Figure 3-07. Example: API frames when modifying the DL parameter value of the module.


## AT Command - Queue Parameter Value

API Identifier Value: 0x09
This API type allows module parameters to be queried or set. In contrast to the "AT Command" API type, new parameter values are queued and not applied until either the "AT Command" (0x08) API type or the AC (Apply Changes) command is issued. Register queries (reading parameter values) are returned immediately.
Figure 3-08. AT Command Frames
(Note that frames are identical to the "AT Command" API type except for the API identifier.)


## AT Command Response

API Identifier Value: 0x88
Response to previous command.
In response to an AT Command message, the module will send an AT Command Response message. Some commands will send back multiple frames (for example, the ND (Node Discover) and AS (Active Scan) commands). These commands will end by sending a frame with a status of ATCMD_OK and no cmdData.

Figure 3-09. AT Command Response Frames.


Figure 3-10. AT Command Response Frames.


## Remote AT Command Request

API Identifier Value: $0 \times 17$
Allows for module parameter registers on a remote device to be queried or set
Figure 3-11. Remote AT Command Request


## Remote Command Response

API Identifier Value: 0x97
If a module receives a remote command response RF data frame in response to a Remote AT Command Request, the module will send a Remote AT Command Response message out the UART. Some commands may send back multiple frames--for example, Node Discover (ND) command.

Figure 3-12. Remote AT Command Response.


## TX (Transmit) Request: 64-bit address

API Identifier Value: $0 \times 00$
A TX Request message will cause the module to send RF Data as an RF Packet.
Figure 3-13. TX Packet (64-bit address) Frames


| Frame ID (Byte 5) | Destination Address (By | Options (Byte 14) | RF Data (Byte(s) 15-n) |
| :---: | :---: | :---: | :---: |
| Identifies the UART data frame for the host to correlate with a subsequent ACK (acknowledgement). Setting Frame ID to '0' will disable response frame. | MSB first, LSB last. <br> Broadcast = 0x000000000000FFFF | $0 \times 01$ = Disable ACK <br> 0x04 = Send packet with Broadcast Pan ID <br> All other bits must be set to 0 . | Up to 100 Bytes per packet |

## TX (Transmit) Request: 16-bit address

API Identifier Value: $0 \times 01$
A TX Request message will cause the module to send RF Data as an RF Packet.
Figure 3-14. TX Packet (16-bit address) Frames


Frame ID (Byte 5)
Identifies the UART data frame for the host to correlate with a subsequent ACK (acknowledgement). Setting Frame ID to '0' will disable response frame.

Destination Address (Bytes 6-7)
MSB first, LSB last.
Broadcast $=0 \times$ FFFF

Options (Byte 8)
$0 \times 01=$ Disable ACK $0 \times 04=$ Send packet with Broadcast Pan ID Up to 100 Bytes per packet All other bits must be set to 0 .

RF Data (Byte(s) 9-n)

## TX (Transmit) Status

API Identifier Value: 0x89
When a TX Request is completed, the module sends a TX Status message. This message will indicate if the packet was transmitted successfully or if there was a failure.

Figure 3-15. TX Status Frames


NOTES:

- "STATUS = 1 " occurs when all retries are expired and no ACK is received.
- If transmitter broadcasts (destination address $=0 x 000000000000$ FFFF), only "STATUS = 0 or 2 " will be returned.
- "STATUS $=3$ " occurs when Coordinator times out of an indirect transmission. Timeout is defined as ( $2.5 \times$ SP (Cyclic Sleep Period) parameter value).


## RX (Receive) Packet: 64-bit Address

API Identifier Value: 0x80
When the module receives an RF packet, it is sent out the UART using this message type.
Figure 3-16. RX Packet (64-bit address) Frames


## RX (Receive) Packet: 16-bit Address

API Identifier Value: $0 \times 81$
When the module receives an RF packet, it is sent out the UART using this message type.
Figure 3-17. RX Packet (16-bit address) Frames


| Source Address (Bytes 5-6) | RSSI(Byte 7) | Options (Byte 8) | RF Data (Byte(s) 9-n) |
| :---: | :---: | :---: | :---: |
| MSB (most significant byte) first, LSB (least significant) last | Received Signal Strength Indicator Hexadecimal equivalent of (-dBm) value. (For example: If RX signal strength $=-40$ dBm, "0x28" (40 decimal) is returned) | bit 0 [reserved] <br> bit 1 = Address broadcast <br> bit $2=$ PAN broadcast <br> bits 3-7 [reserved] | Up to 100 Bytes per packet |

# Appendix A: Agency Certifications 

## United States (FCC)

XBee $® /$ XBee-PRO® RF Modules comply with Part 15 of the FCC rules and regulations. Compliance with the labeling requirements, FCC notices and antenna usage guidelines is required.

To fulfill FCC Certification requirements, the OEM must comply with the following regulations:

1. The system integrator must ensure that the text on the external label provided with this device is placed on the outside of the final product [Figure A-01].
2. $\mathrm{XBee} ® / \mathrm{BB}$ ee- $\mathrm{PRO} ®$ RF Modules may only be used with antennas that have been tested and approved for use with this module [refer to the antenna tables in this section].

## OEM Labeling Requirements

A
WARNING: The Original Equipment Manufacturer (OEM) must ensure that FCC labeling requirements are met. This includes a clearly visible label on the outside of the final product enclosure that displays the contents shown in the figure below.

Figure 4-01. Required FCC Label for OEM products containing the XBee®/XBee-PRO® RF Module
Contains FCC ID: OUR-XBEE/OUR-XBEEPRO**
The enclosed device complies with Part 15 of the FCC Rules. Operation is subject to the following two conditions: (i.) this device may not cause harmful interference and (ii.) this device must accept any interference received, including interference that may cause undesired operation.

* The FCC ID for the XBee is "OUR-XBEE". The FCC ID for the XBee-PRO is "OUR-XBEEPRO".


## FCC Notices

IMPORTANT: The XBee®/XBee-PRO® RF Module has been certified by the FCC for use with other products without any further certification (as per FCC section 2.1091). Modifications not expressly approved by Digi could void the user's authority to operate the equipment.
IMPORTANT: OEMs must test final product to comply with unintentional radiators (FCC section 15.107 \& 15.109) before declaring compliance of their final product to Part 15 of the FCC Rules.

IMPORTANT: The RF module has been certified for remote and base radio applications. If the module will be used for portable applications, the device must undergo SAR testing.

This equipment has been tested and found to comply with the limits for a Class B digital device, pursuant to Part 15 of the FCC Rules. These limits are designed to provide reasonable protection against harmful interference in a residential installation. This equipment generates, uses and can radiate radio frequency energy and, if not installed and used in accordance with the instructions, may cause harmful interference to radio communications. However, there is no guarantee that interference will not occur in a particular installation.
If this equipment does cause harmful interference to radio or television reception, which can be determined by turning the equipment off and on, the user is encouraged to try to correct the interference by one or more of the following measures: Re-orient or relocate the receiving antenna, Increase the separation between the equipment and receiver, Connect equipment and receiver to outlets on different circuits, or Consult the dealer or an experienced radio/TV technician for help.

## FCC-Approved Antennas (2.4 GHz)

XBee/XBee-PRO RF Modules can be installed using antennas and cables constructed with standard connectors (TypeN, SMA, TNC, etc.) if the installation is performed professionally and according to FCC guidelines. For installations not performed by a professional, non-standard connectors (RPSMA, RPTNC, etc) must be used.
The modules are FCC-approved for fixed base station and mobile applications on channels $0 \times 0 B-0 \times 1 \mathrm{~A}$ (XBee) and $0 \times 0 \mathrm{C}-0 \times 17$ (XBee-PRO). If the antenna is mounted at least 20 cm ( 8 in. ) from nearby persons, the application is considered a mobile application. Antennas not listed in the table must be tested to comply with FCC Section 15.203 (Unique Antenna Connectors) and Section 15.247 (Emissions).
XBee RF Modules ( $\mathbf{1} \mathbf{~ m W}$ ): XBee Modules have been tested and approved for use with all of the antennas listed in the tables below (Cable-loss IS NOT required).
XBee-PRO RF Modules ( $\mathbf{6 0} \mathbf{~ m W}$ ): XBee-PRO Modules have been tested and approved for use with the antennas listed in the tables below (Cable-loss IS required when using antennas listed in the second table.

The antennas in the tables below have been approved for use with this module. Digi does not carry all of these antenna variants. Contact Digi Sales for available antennas.


| Part Number | Type (Description) | Gain | Application* | Vlin. Separation |
| :--- | :--- | :--- | :--- | :--- |
| A24-HASM-450 | Dipole (Half-wave articulated RPSMA - 4.5") | 2.1 dBi | Fixed/Mobile | 20 cm |
| A24-HABSM | Dipole (Articulated RPSMA) | 2.1 dBi | Fixed | 20 cm |
| A24-HABUF-P5I | Dipole (Half-wave articulated bulkhead mount U.FL. w/ 5" pigtail) | 2.1 dBi | Fixed | 20 cm |
| A24-HASM-525 | Dipole (Half-wave articulated RPSMA - 5.25") | 2.1 dBi | Fixed/Mobile | 20 cm |
| A24-QI | Monopole (Integrated whip) | 1.5 dBi | Fixed | 20 cm |

Antennas approved for use with the XBee RF Modules (Cable-loss is required)

| Part Number | Type (Description) | Gain | Application* | Vin. Separation | Required Cabe-oss |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Omni-Directional Class Antennas |  |  |  |  |  |
| A24-Y6NF | Yagi (6-element) | 8.8 dBi | Fixed | 2 m | 1.7 dB |
| A24-Y7NF | Yagi (7-element) | 9.0 dBi | Fixed | 2 m | 1.9 dB |
| A24-Y9NF | Yagi (9-element) | 10.0 dBi | Fixed | 2 m | 2.9 dB |
| A24-Y10NF | Yagi (10-element) | 11.0 dBi | Fixed | 2 m | 3.9 dB |
| A24-Y12NF | Yagi (12-element) | 12.0 dBi | Fixed | 2 m | 4.9 dB |
| A24-Y13NF | Yagi (13-element) | 12.0 dBi | Fixed | 2 m | 4.9 dB |
| A24-Y15NF | Yagi (15-element) | 12.5 dBi | Fixed | 2 m | 5.4 dB |
| A24-Y16NF | Yagi (16-element) | 13.5 dBi | Fixed | 2 m | 6.4 dB |
| A24-Y16RM | Yagi (16-element, RPSMA connector) | 13.5 dBi | Fixed | 2 m | 6.4 dB |
| A24-Y18NF | Yagi (18-element) | 15.0 dBi | Fixed | 2 m | 7.9 dB |
| Omni-Directional Class Antennas |  |  |  |  |  |
| A24-C1 | Surface Mount | $-1.5 \mathrm{dBi}$ | Fixed/Mobile | 20 cm | - |
| A24-F2NF | Omni-directional (Fiberglass base station) | 2.1 dBi | Fixed/Mobile | 20 cm |  |
| A24-F3NF | Omni-directional (Fiberglass base station) | 3.0 dBi | Fixed/Mobile | 20 cm |  |
| A24-F5NF | Omni-directional (Fiberglass base station) | 5.0 dBi | Fixed/Mobile | 20 cm |  |
| A24-F8NF | Omni-directional (Fiberglass base station) | 8.0 dBi | Fixed | 2 m |  |
| A24-F9NF | Omni-directional (Fiberglass base station) | 9.5 dBi | Fixed | 2 m | 0.2 dB |
| A24-F10NF | Omni-directional (Fiberglass base station) | 10.0 dBi | Fixed | 2 m | 0.7 dB |
| A24-F12NF | Omni-directional (Fiberglass base station) | 12.0 dBi | Fixed | 2 m | 2.7 dB |
| A24-F15NF | Omni-directional (Fiberglass base station) | 15.0 dBi | Fixed | 2 m | 5.7 dB |
| A24-W7NF | Omni-directional (Base station) | 7.2 dBi | Fixed | 2 m |  |
| A24-M7NF | Omni-directional (Mag-mount base station) | 7.2 dBi | Fixed | 2 m |  |
| Panel Class Antennas |  |  |  |  |  |
| A24-P8SF | Flat Panel | 8.5 dBi | Fixed | 2 m | 1.5 dB |
| A24-P8NF | Flat Panel | 8.5 dBi | Fixed | 2 m | 1.5 dB |
| A24-P13NF | Flat Panel | 13.0 dBi | Fixed | 2 m | 6 dB |
| A24-P14NF | Flat Panel | 14.0 dBi | Fixed | 2 m | 7 dB |
| A24-P15NF | Flat Panel | 15.0 dBi | Fixed | 2 m | 8 dB |
| A24-P16NF | Flat Panel | 16.0 dBi | Fixed | 2 m | 9 dB |

Antennas approved for use with the XBee®/XBee-PRO® RF Modules (Cable-loss is required)

| Part Number | Type (Description) | Gain | Application | Vlin. Separation | Required Cable-loss |
| :--- | :--- | :--- | :--- | :--- | :--- |
| A24-C1 | Surface Mount | -1.5 dBi | Fixed/Mobile | 20 cm | - |
| A24-Y4NF | Yagi (4-element) | 6.0 dBi | Fixed | 2 m | 8.1 dB |
| A24-Y6NF | Yagi (6-element) | 8.8 dBi | Fixed | 2 m | 10.9 dB |
| A24-Y7NF | Yagi (7-element) | 9.0 dBi | Fixed | 2 m | 11.1 dB |
| A24-Y9NF | Yagi (9-element) | 10.0 dBi | Fixed | 2 m | 12.1 dB |
| A24-Y10NF | Yagi (10-element) | 11.0 dBi | Fixed | 2 m | 13.1 dB |
| A24-Y12NF | Yagi (12-element) | 12.0 dBi | Fixed | 2 m | 14.1 dB |
| A24-Y13NF | Yagi (13-element) | 12.0 dBi | Fixed | 2 m | 14.1 dB |
| A24-Y15NF | Yagi (15-element) | 12.5 dBi | Fixed | 2 m | 14.6 dB |
| A24-Y16NF | Yagi (16-element) | 13.5 dBi | Fixed | 2 m | 15.6 dB |
| A24-Y16RM | Yagi (16-element, RPSMA connector) | 13.5 dBi | Fixed | 2 m | 15.6 dB |
| A24-Y18NF | Yagi (18-element) | 15.0 dBi | Fixed | 2 m | 17.1 dB |
| A24-F2NF | Omni-directional (Fiberglass base station) | 2.1 dBi | Fixed/Mobile | 20 cm | 4.2 dB |
| A24-F3NF | Omni-directional (Fiberglass base station) | 3.0 dBi | Fixed/Mobile | 20 cm | 5.1 dB |
| A24-F5NF | Omni-directional (Fiberglass base station) | 5.0 dBi | Fixed/Mobile | 20 cm | 7.1 dB |
| A24-F8NF | Omni-directional (Fiberglass base station) | 8.0 dBi | Fixed | 2 m | 10.1 dB |
| A24-F9NF | Omni-directional (Fiberglass base station) | 9.5 dBi | Fixed | 2 m | 11.6 dB |
| A24-F10NF | Omni-directional (Fiberglass base station) | 10.0 dBi | Fixed | 2 m | 12.1 dB |
| A24-F12NF | Omni-directional (Fiberglass base station) | 12.0 dBi | Fixed | 2 m | 14.1 dB |
| A24-F15NF | Omni-directional (Fiberglass base station) | 15.0 dBi | Fixed | 2 m | 17.1 dB |
| A24-W7NF | Omni-directional (Base station) | 7.2 dBi | Fixed | 2 m | 9.3 dB |
| A24-M7NF | Omni-directional (Mag-mount base station) | 7.2 dBi | Fixed | 2 m | 9.3 dB |
| A24-P8SF | Flat Panel | 8.5 dBi | Fixed | 2 m | 8.6 dB |
| A24-P8NF | Flat Panel | 8.5 dBi | Fixed | 2 m | 8.6 dB |
| A24-P13NF | Flat Panel | 13.0 dBi | Fixed | 2 m | 13.1 dB |
| A24-P14NF | Flat Panel | 14.0 dBi | Fixed | 2 m | 14.1 dB |
| A24-P15NF | Flat Panel | 15.0 dBi | Fixed | 2 m | 15.1 dB |
| A24-P16NF | Flat Panel | 16.0 dBi | Fixed | 2 m | 16.1 dB |
| A24-P19NF | Flat Panel | 19.0 dBi | Fixed | 2 m | 19.1 dB |

* If using the RF module in a portable application (For example - If the module is used in a handheld device and the antenna is less than 20 cm from the human body when the device is operation): The integrator is responsible for passing additional SAR (Specific Absorption Rate) testing based on FCC rules 2.1091 and FCC Guidelines for Human Exposure to Radio Frequency Electromagnetic Fields, OET Bulletin and Supplement C. The testing results will be submitted to the FCC for approval prior to selling the integrated unit. The required SAR testing measures emissions from the module and how they affect the person.


## RF Exposure

WARNING: To satisfy FCC RF exposure requirements for mobile transmitting devices, a separation distance of 20 cm or more should be maintained between the antenna of this device and persons during device operation. To ensure compliance, operations at closer than this distance is not recommended. The antenna used for this transmitter must not be co-located in conjunction with any other antenna or transmitter.

The preceding statement must be included as a CAUTION statement in OEM product manuals in order to alert users of FCC RF Exposure compliance.

## Europe (ETSI)

The XBee RF Modules have been certified for use in several European countries. For a complete list, refer to www.digi.com

If the XBee RF Modules are incorporated into a product, the manufacturer must ensure compliance of the final product to the European harmonized EMC and low-voltage/safety standards. A Declaration of Conformity must be issued for each of these standards and kept on file as described in Annex II of the R\&TTE Directive.

Furthermore, the manufacturer must maintain a copy of the XBee user manual documentation and ensure the final product does not exceed the specified power ratings, antenna specifications, and/ or installation requirements as specified in the user manual. If any of these specifications are exceeded in the final product, a submission must be made to a notified body for compliance testing to all required standards.

## OEM Labeling Requirements

The 'CE' marking must be affixed to a visible location on the OEM product.

## CE Labeling Requirements

The CE mark shall consist of the initials "CE" taking the following form:

- If the CE marking is reduced or enlarged, the proportions given in the above graduated drawing must be respected.
- The CE marking must have a height of at least 5 mm except where this is not possible on account of the nature of the apparatus.
- The CE marking must be affixed visibly, legibly, and indelibly.


## Restrictions

Power Output: When operating in Europe, XBee-PRO 802.15.4 modules must operate at or below a transmit power output level of 10 dBm . Customers have two choices for transmitting at or below 10dBm:
a. Order the standard XBee-PRO module and change the PL command to 0 ( 10 dBm )
b. Order the International variant of the XBee-PRO module, which has a maximum transmit output power of 10 dBm ( $@ \mathrm{PL}=4$ ).

Additionally, European regulations stipulate an EIRP power maximum of $12.86 \mathrm{dBm}(19 \mathrm{~mW})$ for the XBee-PRO and 12.11 dBm for the XBee when integrating antennas.

France: Outdoor use limited to 10 mW EIRP within the band $2454-2483.5 \mathrm{MHz}$.
Norway: Norway prohibits operation near Ny-Alesund in Svalbard. More information can be found at the Norway Posts and Telecommunications site (www.npt.no).

## Declarations of Conformity

Digi has issued Declarations of Conformity for the XBee RF Modules concerning emissions, EMC and safety. Files can be obtained by contacting Digi Support.

Important Note:
Digi does not list the entire set of standards that must be met for each country. Digi customers assume full responsibility for learning and meeting the required guidelines for each country in their distribution market. For more information relating to European compliance of an OEM product incorporating the XBee RF Module, contact Digi, or refer to the following web sites:

CEPT ERC 70-03E - Technical Requirements, European restrictions and general requirements: Available at www.ero.dk/.
R\&TE Directive - Equipment requirements, placement on market: Available at www.ero.dk/.

## Approved Antennas

When integrating high-gain antennas, European regulations stipulate EIRP power maximums. Use the following guidelines to determine which antennas to design into an application.

## XBee-PRO RF Module

The following antenna types have been tested and approved for use with the XBee Module:

## Antenna Type: Yagi

RF module was tested and approved with 15 dBi antenna gain with 1 dB cable-loss (EIRP Maximum of 14 dBm ). Any Yagi type antenna with 14 dBi gain or less can be used with no cable-loss.

## Antenna Type: Omni-directional

RF module was tested and approved with 15 dBi antenna gain with 1 dB cable-loss (EIRP Maxi-
mum of 14 dBm ). Any Omni-directional type antenna with 14 dBi gain or less can be used with no cable-loss.

## Antenna Type: Flat Panel

RF module was tested and approved with 19 dBi antenna gain with 4.8 dB cable-loss (EIRP Maximum of 14.2 dBm ). Any Flat Panel type antenna with 14.2 dBi gain or less can be used with no cable-loss.

XBee-PRO RF Module (@ 10 dBm Transmit Power, PL parameter value must equal 0, or use International variant)

The following antennas have been tested and approved for use with the embedded XBee-PRO RF Module:

- Dipole ( 2.1 dBi , Omni-directional, Articulated RPSMA, Digi part number A24-HABSM)
- Chip Antenna (-1.5 dBi)
- Attached Monopole Whip ( 1.5 dBi )

The RF modem encasement was designed to accommodate the RPSMA antenna option.

## Canada (IC)

## Labeling Requirements

Labeling requirements for Industry Canada are similar to those of the FCC. A clearly visible label on the outside of the final product enclosure must display the following text:

## Contains Model XBee Radio, IC: 4214A-XBEE

Contains Model XBee-PRO Radio, IC: 4214A-XBEEPRO
The integrator is responsible for its product to comply with IC ICES-003 \& FCC Part 15, Sub. B Unintentional Radiators. ICES-003 is the same as FCC Part 15 Sub. B and Industry Canada accepts FCC test report or CISPR 22 test report for compliance with ICES-003.

## Japan

In order to gain approval for use in Japan, the XBee RF module or the International variant of the XBee-PRO RF module (which has 10 dBm transmit output power) must be used.

## Labeling Requirements

A clearly visible label on the outside of the final product enclosure must display the following text:

## ID: 005NYCA0378

# Appendix B. Additional Information 

## 1-Year Warranty

XBee®/XBee-PRO® RF Modules from Digi Intenational, Inc. (the "Product") are warranted against defects in materials and workmanship under normal use, for a period of 1-year from the date of purchase. In the event of a product failure due to materials or workmanship, Digi will repair or replace the defective product. For warranty service, return the defective product to Digi, shipping prepaid, for prompt repair or replacement.
The foregoing sets forth the full extent of Digi's warranties regarding the Product. Repair or replacement at Digi's option is the exclusive remedy. THIS WARRANTY IS GIVEN IN LIEU OF ALL OTHER WARRANTIES, EXPRESS OR IMPLIED, AND DIGI SPECIFICALLY DISCLAIMS ALL WARRANTIES OF MERCHANTABILITY OR FITNESS FOR A PARTICULAR PURPOSE. IN NO EVENT SHALL DIGI, ITS SUPPLIERS OR LICENSORS BE LIABLE FOR DAMAGES IN EXCESS OF THE PURCHASE PRICE OF THE PRODUCT, FOR ANY LOSS OF USE, LOSS OF TIME, INCONVENIENCE, COMMERCIAL LOSS, LOST PROFITS OR SAVINGS, OR OTHER INCIDENTAL, SPECIAL OR CONSEQUENTIAL DAMAGES ARISING OUT OF THE USE OR INABILITY TO USE THE PRODUCT, TO THE FULL EXTENT SUCH MAY BE DISCLAIMED BY LAW. SOME STATES DO NOT ALLOW THE EXCLUSION OR LIMITATION OF INCIDENTAL OR CONSEQUENTIAL DAMAGES. THEREFORE, THE FOREGOING EXCLUSIONS MAY NOT APPLY IN ALL CASES. This warranty provides specific legal rights. Other rights which vary from state to state may also apply.

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[^1]:    One Technology Way, P.O. Box 9106, Norwood, MA 02062-9106, U.S.A. Tel: 781/329-4700 World Wide Web Site: http://www.analog.com Fax: 781/326-8703
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[^2]:    1) Indicates JEDEC registered value
[^3]:    To implement API operations, refer to API sections [p57].

[^4]:    NOTE: When programming the module, parameters are entered in hexadecimal notation (without the

[^5]:    * Firmware version in which the command was first introduced (firmware versions are numbered in hexadecimal notation.)

[^6]:    * Firmware version in which the command was first introduced (firmware versions are numbered in hexadecimal notation.)

