بسم الله الرحمن الرحيم

Palestine Polytechnic University

College of Engineering and Technology

Mechanical Engineering Department

Graduation Project

Self-Balancing Unicycle System on Rough Road

Project Team

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Supervisor

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This project is presented to the Department of Mechanical Engineering at College of Engineering and Technology, for partial fulfillment of the graduate project

Palestine Polytechnic University Hebron-Palestine College of Engineering and Technology Department of Mechanical Engineering

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According to the directions of the project supervisor and by the agreement of all examination committee members, this project is presented to the Department of Mechanical "Engineering at College of Engineering and Technology, for partial fulfillment Bachelor of engineering degree requirements.

Supervisor Signature

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Committee Member Signature

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Project Summary

This system represents a mechatronic system, which contains all the essential components, to be considered a complete mechatronic system. In addition to that, this system represents a challenge in control and implementation, since it must adapt different conditions which are difficult to these systems, such as disturbances, slippage, and motion on rough road (that contains rocks, stones, and other miscellanies). The uniqueness of the SBU (*Self-Balancing Unicycle*) system has drawn interest from many researchers due to the unstable nature of the system.

The system is composed of motor located on a short link, in which this link is attached with a shaft by a roller joint, in which this joint allows a free movement of the link relative to the shaft that is compacted with two wheels (which are joined together by a fixed joint).

SBU system can be considered as an educational tool, since it can be applied for a wide range of classical and modern control techniques. These systems also have many applications, which range widely from robotics to human beings. In transportation, these systems have solid ground, especially in countries with large population that is interested in public transportation and environmental pollution.

In this project, the idea is to design, and prototype SBU system, by using modern control techniques such as state feedback, and interfacing it through PC computer, since the required from this project is testing the effectiveness of control system. The controller will be implemented using commercially available software environments for control system which are MATLAB[®] packages (SIMULINK libraries and xPC Target technique).

Dedication

First of all thanks and praise to "", for patronizing us to work on this project.

This thesis is dedicated to our wonderful parents, who have raised us to be the persons we are today. You have been with us every step of the way, through good times and bad. Thank you for all the unconditional love, guidance, and support that you have always given us, helping us to succeed and instilling in us the confidence that we are capable of doing anything we put our mind to. Thank you for everything.

Thanks for our families for their continued support, encouragement and patience from the first step till the end, and their best wishes to us.

To our teachers for their advices.

To our friends.

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NOMENCLATURES

- \bullet m_w : Mass of the wheel.
- \bullet m_n : Mass of the pendulum and motor and pulleys.
- \bullet \bar{f}_w : Moment of inertia of the wheel about C.O.G.
- \bullet $\mathcal{J}_{\mathcal{D}}$: Moment of inertia of the pendulum and motor about C.O.G.
- \bullet \mathbb{R} : Radius of the wheel.
- \bullet $d_{\mathbf{w}\leftrightarrow\mathbf{n}}$: Viscous damping coefficient between the wheel and pendulum.
- \bullet T : Input torque to the wheel.
- \bullet f_d : Disturbance force acting on the pendulum.
- \bullet f_{fric} : Friction force.
- \bullet $T_{\dot{m}}$: Input torque from the motor.
- \bullet \int_{m} : Equivalent moment of inertia of motor and two pulleys.
- \bullet \mathbf{d}_m : Viscous damping coefficient of the motor.
- \bullet θ : Angular displacement of the wheel.
- \bullet ϕ : Angular displacement of the pendulum.
- \bullet θ_m : Angular displacement of the motor.
- \bullet \dot{n} : The ratio between the radius of pulley1 that is fixed on the motor shaft, to radius of pulley2 that is fixed on unicycle shaft.
- K_w : Kinetic energy of the wheel.
- \bullet K_m : Kinetic energy of the motor.
- K_n : Kinetic energy of the Polly.
- \bullet \overline{F}_w : Potential energy of the wheel.
- \bullet \quad P_m : Potential energy of the motor.
- P_p : Potential energy of the Polly.
- \bullet $D_{w \leftrightarrow p}$: Damping between wheel and Polly.
- \bullet D_m : Damping of the motor.
- \bullet y: Road inclination.
- q: Generalized coordinates describe the system's motion. $q = \varphi \theta^T$
- \bullet \blacksquare \blacksquare represents the power dissipation.
- L: Lagrangian variable (K-P).
- [M]: inertia matrix.
- \bullet [K]: Stiffness matrix.
- [C]: Damping matrix.
- \bullet [B]: Input matrix.
- $[B_d]$: Disturbance matrix.
- x_1 : State vector. $(x_1 = q)$
- x_2 : State vector. $(x_2 = q)$
- \bullet 1 : is the identity matrix.
- \bullet 0 : is the zero matrix.
- y_m : is the measured output vector.
- A: System matrix.
- B: Input matrix.
- C: Output matrix.
- \bullet B_{γ} : road matrix.

Chapter One

SBU System Overview

Contents:

- Introduction
- Recognition of the Need
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- Conceptual Design and Functional Specifications
- Modular Mathematical Model
- Sensors and Actuators Selection
- Control System Design
- Hardware-in-the-Loop Simulation
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	- ▶ Real-Time Simulated Components of HIL
- Time Table For Accomplishing This Project

1.1 Introduction

The Self-Balancing Unicycle (SBU) System represents a mechatronic system that contains all the essential components, to be considered a complete mechatronic system. This system is balancing of one side (xy-plane) of the unicycle by using one cycle for this side, but for the other side (yz-plane), there is no balancing, so it is recommended to use other cycle for balancing the side (xy-plane). In addition to that, this system represents a challenge in control and implementation, since it must adapt different conditions which are difficult to these systems, such as disturbances, slippage, and motion on rough road (that contain rocks, stones, and other miscellanies). The uniqueness of the SBU system has drawn interest from many researches due to the unstable nature of the system. The idea of mobile robot on SBU systems (*Unicycle Robot*) has surfaced in recent years and has attracted interest from control system researchers worldwide, see figure 1.1.

Figure 1.1 Collection of autonomous (mobile) robots on SBU systems

As shown above, these systems consist generally of two-wheeled cycles, that are connected to each other by a connecting shaft, and a link is joined to the shaft by a revolute joint, and this link represent an inverted pendulum system that is common in the field of control engineering, in which the uniqueness and wide application of technology derived from this unstable system has drawn interest of many researches around the world.

As be considered, that SBU system is an educational tool, since it represent an excellent application for a wide range of classical and modern control techniques, these systems also have many practical applications, that ranges widely from robotics (as mentioned above) to human beings. In transportation, these systems have solid ground, particularly in countries with large population that is interested in public transport and environmental pollution, these countries that use the bicycle as a major mean of transport, see figure 1.2.

Principle of operation of Segway, which include movement and balance and all other technical information about it are shown in Appendix B which is

DIY Segway Technical Documentation http://web.mit.edu/first/segway

Figure 1.2 SBU systems in transportation (Segway)

1.2 Recognition of the Need

As mentioned previously, SBU systems have solid ground in education, since it is used for testing various control theories and techniques, such as:

- PID control.
- State Feedback Control.
- Adaptive Control.
- Non-linear Control.

In the near future, personal mobile robots will provide a better life not only to common people but also, to elderly and impaired. In particular, wheeled robots will be expected to provide many convenient and user friendly transport solutions for both people and objects.

The importance of the wheeled mobile robots has long been recognized by the robotics research community, as shown by the numerous robotic competitions and research projects run worldwide in the last decades.

And for autonomous robots on SBU systems, the problem is making a robotic unicycle responds to a reference velocity demand while balancing itself in the pitch direction. The dynamics of the problem were considered and a linear controller was implemented on it. The importance of the subject motivated and continues motivating many projects.

1.3 Literature Review

For the importance of implementing these types of system, as discussed previously, there are some thesis and researches that are related to this topic, particularly when the need of these systems was created, in transportation and robots. Some of these researches are related to the modeling concept, where the others related to control theories applied, but all of these researches did not achieve the overall mechatronic design requirements, which are reliability, maintainability, performance, and cost. This is the reason that make this system can not be applied practically in a wide range, and this section provides a condensed summary of literature reviews on key topics related to SBU system.

1.3.1 Control Systems

Control system development is necessary to guarantee the success in balancing the system, while there is abundance of control strategies that can be applied to stabilize the link, the main aim is to control the system cheaply and effectively without sacrificing the robustness and reliability of the controller. The difference in balance control algorithm implemented depends mostly on how the system is modeled and how the tilt information is obtained.

The control strategies for such system can be divided into two different sections, namely a linear control model or a nonlinear controller model. Linear control methods often linearize the dynamics about a certain operating point. This method is usually sufficient in balancing the system. A nonlinear controller uses the unscathed (without linearization) dynamics model of the system in designing a controller. Although these controllers would provide a more robust system,

the complexity and implementation difficulties of these methods results in most researchers utilizing the linear controller approach.

A literature review found that nonlinear controllers are mostly implemented in solving the balance control problem of a simple pendulum on a cart model or a rotary inverted pendulum. Tarek et al. (1994) developed a Fuzzy Logic controller for balancing an inverted pendulum on a cart. This approach is based on approximate reasoning and knowledge based control. Williams & Matsuoka (1991) used the inverted pendulum model to demonstrate the ability of Neural Networks controller in controlling nonlinear unstable systems.

While simulation results proved that the system can be balanced with both controllers, there is no evidence of implementation of these ideas to verify their findings. Doskocz, Shtessel & Katsinis (1998) implemented a multi-input, multi-output sliding mode controller for a pick and place robotic arm modeled as an inverted pendulum. The researches mentioned above are predominantly purpose built and non-mobile. One of the reasons for that is nonlinear controllers usually requires high computational power.

The linear controllers are more popular among researcher designing similar balancing robots like JOE (Grasser et al, 2002). Linear state space controllers like the Pole-placement controller and the Linear Quadratic Regulators (LQR) are the two most popular control system implemented. The implementation of these controllers can be seen in papers published by Nakajima et al. (1997), Shiroma et al. (1996), Takahashi et al. (2000) and Grasser et al (2002).

In the research titled 'Comparative Study of Control Methods of Single – Rotational Inverted Pendulum' conducted by Xu & Duan (1997) showed that the LQR controller fared better than the pole placement controller in balancing an inverted pendulum mounted on a rotation arm. This is because the LQR controller offers an optimal control over the system's input by taking the states of the system and the control input into account. The arbitrary placement of control poles for Pole-placement controllers might cause the poles to be placed too far into the left-hand plane and cause the system susceptible to noises.¹

 1 This literature review is quoted from the thesis Balancing a Two-Wheeled Autonomous Robot at The University of Western Australia

1.4 Project Objective

Despite of its name, SBU system describes in general systems having usually two parallel driven wheels that are connected to each other by a connecting shaft and a link is joined to the shaft by a revolute joint. Based on Literature surveying that is presented in the previous section, *the main objective of this project*, *is to design, and implement the system to walk on rough road*.

And this main objective comprises inherently, the following aims:

- Investigate the mechanisms involved in balancing.
- To apply skills that are learnt in dynamic and structural (analysis and design) lectures to this problem.
- To develop an understanding of control systems.
- To become familiar with the hardware of control systems and their interfaces.
- To have an impressive project product that can lead to future research.

1.5 Design Process of SBU System

As a mechatronic system, SBU system is the synergistic combination of mechanical engineering, electronics, control systems, and computers and the key element in SBU system is the integration of these areas through the design process, which is called concurrent design.

So, the sequential stages for the design process of SBU system can be demonstrated, in figure1.3.

1.6 Conceptual Design and Functional Specifications

The conceptual design of the system can only be recognized after determining the functional specifications for the system, and for SBU system these specifications can be summarized as in figure 1.4:

Figure 1.4 Functional Specifications of SBU system block diagram

Depending on the specifications that are demonstrated above, conceptual design of SBU system (see figure 1.5) consists of two driven wheels connecting with each other by a connecting shaft, and a link that is represented by an inverted pendulum, where the wheels are rotating and making upon that relative motion between these wheels and the ground, and this will generate a counter torque that stabilize the link, and in addition to that tracking the desired position for the overall unicycle.

Figure 1.5 Conceptual Design of SBU System

1.7 Modular Mathematical Model

Often when engineers design a system to be controlled or optimized, they use a mathematical model. The dynamic performance of physical systems is obtained by utilizing the physical laws of mechanical, electrical, fluid and thermodynamic systems. Engineers generally model physical systems with linear differential equations with constant coefficients when possible.

In mechatronic systems, complex models (such as SBU system model) may be created by connecting the modules, or blocks, together. Each block represent a subsystem that corresponds to some physically or functionally realizable operations that can be encapsulated into a block with input/output limited to input signals, parameters, and output signals. So this modeling is called *modular modeling*.

The modular mathematical model of SBU system will be covered in Chapter Two.

1.8 Sensors and Actuators Selection

Sensors are required to monitor the performance of machines and processes. Using a collection of sensors, one can monitor one or more variables in a process. Some of the more common measurement variables in mechatronic systems are temperature, speed, position, force, torque, and acceleration. The characteristics those are important when one is measuring these variables include dynamics of the sensor, stability, resolution, precision, robustness, size, and signal processing.

Designing a real time closed-loop feedback control system is essential to stabilize the SBU system. Such a control system requires measuring some variables that specify the other states of the system. These measurements are:

- The angular displacement of the wheel.
- The angular displacement of the link.

These measurements were determined depending on the analysis in Chapter Two

To have an accurate and real-time control system, A MMA7260Q Three $Axis^2$ Low-g Micro-machined Accelerometer (see figure 1.6) and an incremental optical encoder (see figure 1.7) that generates 2500 pulse per revolution as a maximum value are selected for the SBU system to measure the tilt angle of the link and the angular displacement of the wheel rotation, respectively.

Figure 1.6 MMA7260Q Three Axis Low-g Micro-machined Accelerometer on its board *Note: The operation of this accelerometer in SBU system will be covered in Chapter Four.*

² In SBU system, it will be used one axis for measuring the tilt angle, and there is no need to use other axis.

Figure 1.7 Rotary optical encoder provided by Panasonic Company

Actuators are another important component of a mechatronic system. Actuators are basically the muscle behind a mechatronic system that accepts a control command (mostly in the form of an electrical signal) and produces a change in the physical system by generating (energy signal) force, motion, heat, flow, etc.

Since the operation of SBU system requires quick changes in the direction of the system velocity and acceleration, which is necessary to stabilize the link vertically and generate the required torque for self balancing process, in addition to tracking process. Also, the selected actuator must have the ability to generate enough torque independently of the speed value. It is important for the selected actuator used in such a system to have a low inertia.

Therefore, AC servo motor with a driver is selected to be the actuator for SBU system.

MSMD042P1S AC servomotor provided by Panasonic Company (see figure 1.8) meets the requirements of low inertia, generated torque independence on the speed, and very fast response.

Figure 1.8 MSMA042AIE AC servomotor and its driver provided by Panasonic Company

1.9 Control System Design

As discussed in the beginning of this chapter, SBU systems are considered as educational tools for modern control system design theories, in addition to classical control theories. Control system development is necessary to guarantee the success in balancing the system, while there is abundance of control strategies that can be applied to stabilize the link, the main aim is to control the system cheaply and effectively without sacrificing the robustness and reliability of the controller.

Any controller applied to an SBU system must guarantee first, the stability of the link vertically. Second, the system position should track a desired input while keeping the link vertically stable. Third, disturbance rejection and robustness are also to be achieved. The possibility for a controller to satisfy these requirements varies according to the control strategy behind it.

The control system design of SBU system will be covered in Chapter Three.

1.10 Hardware-in-the-Loop Simulation

The hardware-in-the-loop simulation (HIL) is characterized by operating real (hardware) components in connection with real-time simulated components. Usually. the control system hardware and software is the real system, as used for series production. The controlled process (consisting of actuators, physical processes, and sensors) can either comprise simulated components or real components. In general, mixtures of the above cases can be realized

In SBU system, HIL will be used in prototyping step, in which the controlled system of SBU will be the real components, while the control system is built as control algorithms, by using MATLAB® / SIMULINK models (see figure 1.9). For that, real- time interfacing circuits, should be used between the plant, and the control system configuration.

In the following sections, HIL components will be discussed in more details, to have an obvious impression about it.

Figure 1.9 HIL configuration for SBU system

1.10.1 Hardware Components of HIL

a. Mechanical Components

Designing the mechanical structure of SBU system and choosing the dimensions and material types, are depending on the functional specifications for each mechanical part. After that, for each part that is designed, it must be analyzed in terms of strength, , elasticity and other material properties, to check that these parts achieve their functions.

Motor Box: which carry the servomotor and its driver, it is fabricated from light metal, it positioned on the link (see figure 1.10).

Figure 1.10 Motor Box

- *Vertical Link:* it will be manufactured from rigid metal in order to carry the box with its contained parts, and connected by its end with the shaft by a rolling bearing (see figure 1.11).

Figure 1.11 Vertical Link

Rolling Bearing: this is a free revolute joint that connect the shaft with the link (see Figure 1.12).

Figure 1.12 Rolling Bearing

- *Pulleys and Non-Slip Belt:* The wheels are driven through a belt connected to pulleys. This will prevent the slipping between the wheels and the belt, through using non-slip *Pulleys and Non-Slip Belt:* The wheels are driven through a belt connected to pulleys.
This will prevent the slipping between the wheels and the belt, through using non-slip
belt, and using pulleys, instead of gears that

Wheels: in which are two wheels, and form the connected part to the ground. The generated torque from motor move these wheels forward, or backward to stabilize the link, and also to track the reference input signal. The most important feature in this mechanical part, is preventing the slippage, as most as possible (see Figure 1.14).

Figure 1.14 Wheel

- *Connecting Shaft:* which is the mechanical component that is used to connect between the two wheels. Usually this part is made from steel, since it has better matiral properties, compared to other materials, and this prevent the bending along the shaft (see Figure 1.15).

b. Electrical Components

The electrical components in the SBU system include sensors, actuator, and the interfacing components that connect between the computer and the other electrical components.

Note: The sensors, and actuator that are used for SBU system was covered in section 1.8, so in this subsection, the discussion will be focused on the interfacing components that is used in SBU system.

Interfacing Devices: usually, these devices are needed for signal conversion between high-power circuits, and low-power circuits. In addition to that, these devices are used for conversion between digital and analog signals. Sometimes, these devices are required for isolation purposes.

The basic interfacing devices of the SBU system are:

Servomotor Driver:

As, it well-known, that servomotor is ac electrical motor that has a neglected dynamic behavior, and that is resulted from built-in controller. This presents a linear relation between input voltage to this motor, and its generated torque.

For that, the servomotor driver contains the controller circuit of the motor, beside the power circuit (see Figure 1.8).

DAQ Hardware:

Data Acquisition Card or DAQ board is a special type of board that plugs into a slot in a desktop personal computer that can be used for many of the tasks. This type of board can generate analog or digital output, in addition to acquisition analog and digital data.

These cards are divided into hardware components, and software components. DAQ hardware, usually include screw terminal, DAQ board plugged through PC computer, and connecting parallel or serial data cable between DAQ board and screw terminal. (see Figure 1.16)

Figure 1.16 DAQ Hardware

1.10.2 Real-Time Simulated Components of HIL

a. xPC Target

xPC Target is a solution for prototyping, testing, and deploying real time systems using standard PC hardware. It is an environment that uses a target PC, separate from a host PC, for running real-time applications. In this environment you use your desktop computer as a host PC with MATLAB[®], SIMULINK, and Stateflow (optional), to create a model using Simulink blocks and Stateflow charts. After creating your model, you can run simulations in non-real time.

xPC Target lets you add I/O blocks to your model and then use the host PC with Real-Time Workshop, Real-Time Workshop Embedded Coder (optional), Stateflow Coder (optional), and a C/C++ compiler to create executable code.

The executable code is downloaded from the host PC to the target PC running the xPC Target real-time kernel. After downloading the executable code, you can run and test your target application in real time.

b. Commercially Available Environment for Information System

This environment is usually used to simulate the control algorithms of the mechatronic system. To achieve that, a set of software packages are used. MATLAB $^{\circledR}$ and SIMULINK provide a wide variety of functions, numerical algorithms, and toolboxes that help significantly not only to design and simulate the control system, but also to build executable real-time applications.

c. DAQ Software

DAQ software is needed in order for the DAQ Hardware to work with a PC. The device driver performs low-level register writes and reads on the hardware.

Time Tables for Accomplishing This Project

First Semester

Second Semester

Chapter Two

Mathematical Model for SBU System on rough road

Contents:

- Introduction
	- Lagrangian method
- Mathematical Model for SBU System on flat road
	- Non-linear Mathematical Model
	- Linearization of Mathematical Model
- Mathematical Model for SBU System on inclined road
	- Non-linear Mathematical Model
	- Linearization of Mathematical Model

2.1 Introduction

The dynamic performance of physical systems is obtained by utilizing the physical laws of mechanical, electrical, fluid and thermodynamic systems. In general physical systems are modeled with nonlinear differential equations with constant or variable coefficients.

Mathematical modeling of SBU system tends to represent all important features of the system and describe its behavior in terms of differential equations. The needed model accuracy (closeness to the actual system) depends on the purpose. Generally a simplified model is needed to study the main characteristics of the system, while a detailed model is needed for precious simulation and predictive studies.

In general, there are two main purposes for modeling a physical system:

- Develop a mathematical model in order to predict the dynamic behavior of the system as accurately as possible. Using numerical solution methods, such a model serves as a tool for extensive evaluation of system behavior without actually using or building the real system.
- Develop models to gain insight into the behavior of the dynamic system qualitatively instead of exact response prediction, i.e. knowledge of stability margins, controllability, observability, and the sensitivity of response to parameter changes, such a model needs not to contain all of the details of the actual system, but only the most essential features so as to provide the needed insight from an engineering stand point.

Therefore two basic models will be derived for the SBU system (for either on flat and inclined road), a simple and linear one for controller design and analysis purposes, and a nonlinear model for testing and simulating the dynamic system response as accurately as possible.

In the case of SBU system, the following assumptions are used in deriving their mathematical models:

1. There is no slipping between the two wheels and the ground so, the friction force that affects between the wheels and the ground, is always smaller than $\mu_{min} N$, in which μ_{min}

is the dynamic coefficient of dry friction between the two surfaces, and N is the normal force applied on the wheels, also, this assumption means $x = R\theta$, in which θ is the angle of wheel rotation, and \vec{R} is radius of wheel.

- 2. The air resistance effects on the link, and the wheel, will be neglected.
- 3. The center of gravity of each link is located at the link's axis of symmetry, and the same assumption for the box that is fixed with the links.
- 4. The vibration of box and the link in the y-axis (vertical side of the system) , is very small and considered to be negligible.
- 5. The links are rigid bodies that, it have less elasticity to vibrate in the z-axis (height side of the system), and their oscillations are neglected.
- 6. The mass of non-slipping conveyer is negligible.

In order to obtain the mathematical model of the system, Lagrange method is used to derive the basic differential equations that govern system's dynamics. The main formula and a brief description of this method are presented in the following subsection.

2.1.1 Lagrangian method (Energy based method)

Direct application of Newton's law to each mass in a multi-mass system requires you if' account for the reaction forces explicitly. Then, once all the governing equations have been obtained, the reaction forces must be eliminated algebraically in order to obtain the equations of motion in terms of only the given input and output variables. This is not too difficult to accomplish in many applications, but as the number of masses increases or the kinematic constraints become more complex, it becomes tedious to eliminate the reaction forces.

There is, however, another method available that avoids the need to deal with the reaction forces. This method, due to Lagrange, is briefly presented here so that the reader must be aware that there is more than one way to solve a dynamics problem. The derivation of Lagrange's equations is beyond the scope of this project, and the reader is referred to a text on advanced dynamics for more discussion.

The Lagrangian method is energy based rather than force based, and it requires you to derive expressions for the system's potential and kinetic energies. Denote these energies by P and K , respectively, and define the *Lagrangian* \bf{L} as $\bf{L} = \bf{K} - \bf{P}$. Then Lagrange's equations are

Chapter Two

$$
\frac{d}{dt} \frac{\partial L}{\partial \dot{q}_j} - \frac{\partial L}{\partial q_j} + \frac{\partial D}{\partial \dot{q}_j} = Q_j \qquad j = 1, 2, \dots, n \tag{2-1}
$$

where the variables q_i are a set of generalized coordinates that completely describe the system's motion and *n* is the number of such coordinates. The corresponding velocities are \dot{q}_i , and the q_i terms represent externally applied forces or moments at the coordinates q_i . The term D represents the power dissipation, such as that due to damping, from either a force or moment at that coordinate.

Typical problems with Lagrange formulation:

- It should be established number of degree of freedom first and formulate all energy terms in only those variables. Clearly identify which degrees of freedom are relative coordinates versus absolute coordinates.
- For kinetic energy terms, it should be to formulate absolute velocities before taking derivatives.
- For potential energy terms, it should be noticed that the actual deflection, described by relative and/or absolute coordinates, in spring elements is described.
- There should be only one total kinetic energy equation and one total potential energy equation for the system. The kinetic and potential energy equations should involve only the N generalized coordinates and the constants (mass, damping, stiffness) of the system.
- Apply the Lagrange Equation once for each generalized coordinate. For *degrees of* freedom, N generalized coordinates will yield N equations of motion.

Langrage equation above will be used to derive the mathematical models in the next sections for SBU system on flat road, and on inclined road respectively. The first model will be used for verifying options in addition to control options, while the second model will be used later for controller design and simulation purposes.

2.2 Mathematical Model for SBU System on flat road

In this section, a nonlinear and linear mathematical model of SBU system on flat road will be derived, taking into account, the damping between the wheel shaft and the link. The disturbance effects acting on the link will also be considered.
2.2.1 Non-linear Mathematical Model

In this subsection, mathematical model of the system consists of two second-order nonlinear differential equations, these equations are derived using Lagrange's approach that is discussed in subsection 2.1.1. According to Fig. 2.1, the total kinetic and potential energies of the system can be derived in next page.

Figure 2.1 Self-Balancing Unicycle (SBU) system on flat road

- m_w : mass of the wheel
- $m_{\overline{p}}$: mass of the pendulum and motor and pulleys
- l_{w} : moment of inertia of the wheel about C.O.G
- $\frac{1}{n}$: moment of inertia of the pendulum and motor about C.O.G
- \mathbb{R} : radius of the wheel
- $d_{\mathbf{w} \leftrightarrow \mathbf{p}}$: viscous damping coefficient between the wheel and pendulum
- : input torque to the wheel
- f_d : disturbance force acting on the pendulum
- f_{fric} : friction force
- T_m : input torque from the motor
- J_m : equivalent moment of inertia of motor and two pulleys
- d_m : viscous damping coefficient of the motor
- θ : angular displacement of the wheel
- φ : angular displacement of the pendulum
- θ_m : angular displacement of the motor
- \bullet \bullet \bullet : the ratio between radius of pulley1 that is fixed on the motor shaft, to radius of pulley2 that is fixed on unicycle shaft

By establishing number of degree of freedom for the system above, to use *Lagrangian* method, it is concluded that, there are two independent variables, that can't be substitution in each other, in which these variables called *generalized coordinates*, and can be chosen for system above, θ , φ for control and simulation purposes, that is discussed in Chapter Three later.

So, here there are two generalized coordinates $q_1 = \theta$, $q_2 = \varphi$

The total kinetic energy of the system is the summation of all kinetic energies of all the components of the system, which are, the wheel, the pendulum, the motor and pulleys.

$$
K = K_w + K_p + K_m \tag{2-2}
$$

Where : K_m is the total kinetic energy of motor and pulleys

First, kinetic energy for the wheel:

$$
K_{\rm w} = \frac{1}{2} m_{\rm w} \dot{x}_{\rm w}^2 + \frac{1}{2} m_{\rm w} \dot{y}_{\rm w}^2 + \frac{1}{2} J_{\rm w} \dot{\theta}^2
$$
 (2-3)

And, by substituting x_w and y_w as expressions of the generalized coordinates, that is discussed above, it is concluded the following:

$$
x_w = R\theta \to \dot{x}_w = R\dot{\theta} \tag{2-4}
$$

$$
y_w = 0 \rightarrow \dot{y}_w = 0 \tag{2-5}
$$

Substituting equations $2 - 4$, $2 - 5$ in equation $(2 - 3)$ yields:

$$
K_{\rm w} = \frac{1}{2} m_{\rm w} \ R \dot{\theta}^2 + \frac{1}{2} J_{\rm w} \dot{\theta}^2 \tag{2-6}
$$

Second, kinetic energy for the pendulum:

$$
K_p = \frac{1}{2} m_p \dot{x}_p^2 + \frac{1}{2} m_p \dot{y}_p^2 + \frac{1}{2} J_p \dot{\varphi}^2
$$
 (2-7)

By substituting \dot{x}_p and \dot{y}_p as expressions of the generalized coordinates:

$$
x_p = x_w + l_1 \sin \varphi \to \dot{x}_p = R\dot{\theta} + l_1 \dot{\varphi} \cos \varphi \tag{2-8}
$$

$$
y_p = y_w + l_1 \cos \varphi \to \dot{y}_p = -l_1 \dot{\varphi} \sin \varphi \tag{2-9}
$$

Substituting equations $2 - 8$, $2 - 9$ in equation $(2 - 7)$ yields:

$$
K_p = \frac{1}{2}m_p \ R\dot{\theta} + l_1 \dot{\phi} \cos \varphi^2 + \frac{1}{2}m_p \ -l_1 \dot{\phi} \sin \varphi^2 + \frac{1}{2}l_p \dot{\phi}^2 \tag{2-10}
$$

Third, kinetic energy for the motor and pulleys:

$$
K_m = \frac{1}{2} J_m \dot{\theta}_m^2 \tag{2-11}
$$

Substituting \vec{B}_m as expression of the generalized coordinates:

$$
\theta_m = \frac{1}{n} \ \theta \to \theta_m = \frac{1}{n} \ \theta \tag{2-12}
$$

Substituting equations $2 - 12$ in equation $(2 - 11)$ yields:

$$
K_m = \frac{1}{2} J_m \frac{\theta^2}{n}
$$
 (2-13)

Now, substituting the net equations $2 - 6$, $2 - 10$, and $(2 - 13)$ in equation $2 - 2$ and simplifying it to the next equation:

$$
K = \frac{1}{2} m_w R^2 + m_p R^2 + J_w + \frac{J_m}{n^2} \dot{\theta}^2 + m_p R l_1 \dot{\theta} \dot{\phi} \cos \varphi + \frac{1}{2} m_p l_1^2 + J_p \dot{\phi}^2
$$
 (2-14)

As the same for kinetic energy, the total potential energy of the system is the summation of all potential energies of all the components of the system, which are, the wheel, the pendulum, the motor and pulleys.

$$
P = P_w + P_p + P_m \tag{2-15}
$$

In which, at this case $P_w = P_m = 0$, so equation $(2 - 15)$ will become:

$$
P = P_p = m_p g y_p = m_p g l_1 \cos \varphi \tag{2-16}
$$

Note: \boldsymbol{g} is the gravitational constant.

Finally, computing the power dissipation term to substitute it in *Lagrange's* equation:

$$
D = D_{w \leftrightarrow p} + D_m \tag{2-17}
$$

And since $D_{w \leftrightarrow p}$, D_m are power terms, so it can be written in the following expressions:

$$
D_{w \leftrightarrow p} = \frac{1}{2} d_{w \leftrightarrow p} \quad \dot{\theta}^2 - \dot{\phi}^2 \tag{2-18}
$$

$$
D_m = \frac{1}{2} d_m \theta_m^2 = \frac{1}{2} d_m \frac{\dot{\theta}}{n}^2
$$
 (2-19)

Substituting equations $2 - 18$, $(2 - 19)$ in equation $(2 - 17)$ yields:

$$
D = \frac{1}{2} d_{w \leftrightarrow p} \; \dot{\theta}^2 - \dot{\phi}^2 + \frac{1}{2} d_m \; \frac{\dot{\theta}}{n}^2 \tag{2-20}
$$

Now, evaluating *Lagrangian* term \overline{L} :

$$
L = K - P
$$

\n
$$
L = \frac{1}{2} m_w R^2 + m_p R^2 + J_w + \frac{J_m}{n^2} \dot{\theta}^2 + m_p R l_1 \dot{\theta} \dot{\phi} \cos \varphi + \frac{1}{2} m_p l_1^2 + J_p \dot{\phi}^2
$$

\n
$$
- m_p g l_1 \cos \varphi
$$
 (2-21)

Applying Lagrange's equation for each generalized coordinate, θ and φ , yields:

1. For generalized coordinate θ :

$$
\frac{d}{dt} \frac{\partial L}{\partial \theta} - \frac{\partial L}{\partial \theta} + \frac{\partial D}{\partial \theta} = Q_{\theta}
$$
\n
$$
\Rightarrow \frac{\partial L}{\partial \theta} = 0
$$
\n
$$
\Rightarrow \frac{\partial L}{\partial \theta} = m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{J_{m}}{n^{2}} \dot{\theta} + m_{p}R_{1}\dot{\phi}\cos\varphi
$$
\n
$$
\Rightarrow \frac{\partial D}{\partial \theta} = d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}} \dot{\theta}
$$
\n
$$
\Rightarrow \frac{d}{dt} \frac{\partial L}{\partial \theta} = m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{J_{m}}{n^{2}} \dot{\theta} - m_{p}R_{1}\dot{\phi}^{2}\sin\varphi + m_{p}R_{1}\dot{\phi}\cos\varphi
$$
\n(2-22)

$$
Q_{\theta} = M_{w} \frac{\partial \theta_{w}}{\partial \theta} + F_{w} \frac{\partial x_{w}}{\partial \theta}
$$

 $\rightarrow Q_{\theta} = T_m - f_d R$

So, the *first nonlinear differential equation* of the system will be as the following:

$$
m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{J_{m}}{n^{2}} \ddot{\theta} + m_{p}Rl_{1}\cos\varphi\,\ddot{\varphi} - m_{p}Rl_{1}\dot{\varphi}^{2}\sin\varphi + d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}} \dot{\theta}
$$

= $T_{m} - f_{d}R$ (2-23)

2. For generalized coordinate φ :

$$
\frac{d}{dt} \frac{\partial L}{\partial \phi} - \frac{\partial L}{\partial \phi} + \frac{\partial D}{\partial \phi} = Q_{\varphi}
$$
\n
$$
(2-24)
$$
\n
$$
\Rightarrow \frac{\partial L}{\partial \phi} = m_p g l_1 \sin \varphi - m_p R l_1 \dot{\theta} \dot{\phi} \sin \varphi
$$
\n
$$
\Rightarrow \frac{\partial L}{\partial \dot{\phi}} = m_p R l_1 \dot{\theta} \cos \varphi + m_p l_1^2 + l_p \dot{\phi}
$$
\n
$$
\Rightarrow \frac{\partial D}{\partial \dot{\phi}} = -d_{w \leftrightarrow p} \dot{\phi}
$$
\n
$$
\Rightarrow \frac{d}{dt} \frac{\partial L}{\partial \dot{\phi}} = m_p R l_1 \dot{\theta} \cos \varphi - m_p R l_1 \dot{\phi} \dot{\theta} \sin \varphi + m_p l_1^2 + l_p \dot{\phi}
$$
\n
$$
Q_{\varphi} = M_p \frac{\partial \theta_p}{\partial \phi} + F_p \frac{\partial x_p}{\partial \phi}
$$
\n
$$
\Rightarrow Q_{\varphi} = -T_m - f_d l_2 \cos \varphi
$$
\nAnd *second nonlinear differential equation* of the system will be as the following:

$$
m_p R l_1 \cos \varphi \ddot{\theta} + m_p l_1^2 + l_p \ddot{\varphi} - d_{w \leftrightarrow p} \dot{\varphi} - m_p g l_1 \sin \varphi
$$

=
$$
-T_m - f_d l_2 \cos \varphi
$$
 (2-25)

Nonlinear differential equations $(2 - 23)$ and $(2 - 25)$ that describe Self-Balancing Unicycle (SBU) system on flat road can be written in matrix form as below:

$$
m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{J_{m}}{n^{2}} \quad m_{p}Rl_{1}\cos\varphi \quad \ddot{\theta} + d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}} \quad 0 \quad \dot{\theta}
$$

\n
$$
m_{p}Rl_{1}\cos\varphi \quad m_{p}l_{1}^{2} + J_{p} \quad \dddot{\varphi} + \frac{-m_{p}Rl_{1}\dot{\varphi}^{2}}{m_{p}gl_{1}} \sin\varphi = \frac{1}{-1}T_{m}t + \frac{-R}{-l_{2}\cos\varphi}f_{d} \quad 2-26
$$

Extracting the physical senses from the above equation:

- There is no existence for the friction force in the equation, since this force is a driving force and no slippage between the ground and the wheels.
- The opposite signs for T_m in the model mean that for each degree of freedom, we have the same quantity of T_m but in the opposite direction and this can be explained upon Newton's Third Law.
- In this system corilios forces are vanished since we assume there are no slippage, so there is no relative velocity between the ground and the wheels.
- This means that the slippage is a very important aspect that should be considered well into system implementation.
- We note also that the disturbance force f_d have a coupling effect on θ , and φ and this means no possible for compensating statically this effect on these two degrees of freedom.
- Assuming f_d is a disturbance force acting on the head of the link, since this is has a larger effect than at the foot.

2.2.2 Linearization of Mathematical Model

In order to obtain the equations of motion of dynamic systems, this will need a mathematical description of the forces and moments involved, as functions of displacement or velocity, for example. As well known that, differential equations based on linear models of the forces and moments are much easier to solve than ones based on nonlinear models.

Engineer therefore try to obtain a linear model whenever possible. Sometimes the use of a linear model results in a loss of accuracy, and the engineer must weigh this disadvantage with advantages gained by using a linear model. If the model is nonlinear, it can be obtained a linear model that is an accurate approximation over a limited range of the independent variable.

And in SBU system, there is a limited range of , that it is usually called an *operating point*, and this point in the SBU system is the vertical position of the pendulum, so, the angle φ , and its derivatives are assumed to be very small, that is approximately zero.

This will include that in equation $(2 - 26)$, all nonlinear terms will be linearized depending on the rule that \cong 0 :

 \rightarrow sin $\varphi \cong \varphi$

 \rightarrow cos $\varphi \cong 1$

$$
\rightarrow \dot{\varphi}^2 \cong 0
$$

So, equation $(2 - 26)$ will become as shown below:

$$
m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{J_{m}}{n^{2}} \qquad m_{p}Rl_{1} \qquad \frac{\partial}{\phi} + d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}} \qquad 0 \qquad \frac{\partial}{\phi}
$$

+
$$
\begin{array}{ccc} 0 & m_{p}l_{1}^{2} + J_{p} & \frac{\partial}{\phi} + \frac{J_{w \leftrightarrow p} + \frac{J_{m}}{n^{2}}}{2} & -d_{w \leftrightarrow p} & \frac{\partial}{\phi} \\ + -m_{p}gl_{1} & \varphi = -1 \qquad T_{m} t + \frac{-R}{-l_{2}} f_{d} & (2-27) \end{array}
$$

To have a matrix form of the above with all coordinates, and their derivatives to be in a compact form, it must to get θ , then rewrite the above equation:

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$$
m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{J_{m}}{n^{2}} \t m_{p}Rl_{1} \t \ddot{\theta} + d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}} \t 0 \t \dot{\theta} m_{p}Rl_{1} \t m_{p}l_{1}^{2} + J_{p} \t \ddot{\phi} + \frac{0}{0} - d_{w \leftrightarrow p} \t \dot{\phi} + \frac{0}{0} - m_{p}gl_{1} \t \ddot{\phi} = \frac{1}{-1} T_{m} t + \frac{-R}{-l_{2}} f_{d}
$$
 (2-28)

Here, by defining the vector $\mathbf{q} = \frac{\theta}{\varphi}$, the equation $(2 - 28)$ can be written:

$$
M\ddot{q} + C\dot{q} + Kq = B T_m t + B_d f_d \qquad \qquad 2-29
$$

In which:

- The Inertia matrix is defined as:

$$
M = \frac{m_w R^2 + m_p R^2 + I_w + \frac{I_m}{n^2}}{m_p R I_1} \qquad m_p R I_1 \qquad (2-30)
$$

- The Damping matrix is defined as:

$$
C = \begin{array}{cc} d_{w \leftrightarrow p} + \frac{d_m}{n^2} & 0 \\ 0 & -d_{w \leftrightarrow p} \end{array}
$$
 (2-31)

- The Stiffness matrix is defined as:

$$
K = \begin{bmatrix} 0 & 0 \\ 0 & -m_p g l_1 \end{bmatrix} (2 - 32)
$$

- The Input matrix is defined as:

$$
B = \frac{1}{-1} \tag{2-33}
$$

- The Disturbance matrix is defined as:

$$
B_d = \frac{-R}{-l_2} \tag{2-33}
$$

Note:

From the matrices above, it should be noted that SBU system on flat road has coupling in the inertia matrix and damping matrix, while there is no coupling in the stiffness matrix.

Here, to have a state space representation for the linearized SBU system on flat road, it must have four state variables, which can be chosen θ , φ , $\dot{\theta}$ and $\dot{\varphi}$, and have one input which is the torque $T_m(t)$, and one disturbance force which is f_d , and the stae space model can be derived from the equation $(2 - 29)$, by using the way that is shown underneath:

$$
\rightarrow x_1 = q \tag{2-34}
$$

$$
\rightarrow x_2 = \dot{q} \tag{2-35}
$$

So, by differentiating the equations above, and substituting with each other:

$$
\rightarrow \dot{x}_1 = x_2 \tag{2-36}
$$

$$
\rightarrow x_2 = -M^{-1} K x_1 - M^{-1} C x_2 + M^{-1} B T_m t + M^{-1} B_d f_d \qquad (2-37)
$$

Substitute the equation $2 - 36$ and $(2 - 37)$ in general equations of state space model will yield:

$$
\begin{aligned}\n\ddot{x}_1 &= \mathbf{0}_{2 \times 2} & \mathbf{1}_{2 \times 2} & \mathbf{1}_{2 \times 2} & \mathbf{1}_{2 \times 2} & \mathbf{1}_{2 \times 1} & \mathbf{1}_{
$$

Where:

I: is the identity matrix.

0: is the zero matrix.

 y_m : is the measured output vector.

From the state space model equations above:

$$
A = \frac{0_{2 \times 2}}{M^{-1} K} = \frac{I_{2 \times 2}}{M^{-1} C}
$$
 (2-40)

$$
B = \frac{0_{2 \times 1}}{M^{-1} B} \tag{2-41}
$$

$$
C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \tag{2-42}
$$

$$
B_d = \frac{0_{2 \times 1}}{M^{-1} B_d} \tag{2-43}
$$

Now, it should be measured or established the parameters of the SBU system, to substitute them in the matrices above¹, to locate the eigenvalues of the system, and study its dynamic behavior according to these values , and their locations.

Parameter	Description	Value	Unit
$m_{\scriptscriptstyle W}$	mass of the wheel	1.706	kg
m_p	mass of the pendulum and motor	1.998	kg
R	radius of the wheel	145	mm
Jw	moment of inertia of the wheel about C.O.G	2.260194e-003	$Kg.m^2$
Im	equivalent moment of inertia of motor and pulleys	2.00e-004	$Kg.m^2$

Table 2.1 Estimated parameters of SBU system

	distance between	125.85	mm
	C.O.G of the wheel		
	and C.O.G of the		
	pendulum		
	distance between	280	mm

¹ These values are obtained from CATIA VR® Software, and its approximately equal to the real values.

By substituting the values of table above into general equations of state space model, it will result the following matrices:

$$
\dot{\mathbf{x}} = \begin{bmatrix} 0 & 0 & 1.0000 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1.0000 & \mathbf{x} + \mathbf{0} & 0 & 0 \\ 0 & -71.8243 & -0.0179 & -0.0001 & 45.1495 & T_m t + \mathbf{0} & 0.1830 & f_d \\ 0 & 65.8677 & 0.0086 & 0.0001 & -28.0718 & -1.8321 \end{bmatrix}
$$
\n
$$
\mathbf{y}_m = \begin{bmatrix} \mathbf{y}_1 \\ \mathbf{y}_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \mathbf{x}
$$
\nWhere $\mathbf{x} = \begin{bmatrix} \theta \\ \theta \\ \phi \\ \phi \end{bmatrix}$

2.3 Mathematical Model for SBU System on inclined road

In this section, a nonlinear and linear mathematical model of SBU system on inclined road will be derived. This model is used for purposes of controller design, as is discussed in Chapter will be derived. This model is used for purposes of controller design, as is discussed in Chapter
Three in more details. This model is derived by taking into account, the damping between the wheel shaft and the link. The disturbance effects acting on the link will also be considered.

The modeling process for SBU system on rough road is based on a simple hypothesis, that is having rough road can be accomplished by using inclined road with different incline angle. This angle is assumed constant while the mathematical model is done, but it can be varied through simulation process, to easy the model deriving process, as explained in this section. wheel shaft and the link. The disturbance effects acting on the link will also be considered.
The modeling process for SBU system on rough road is based on a simple hypothesis, that is
having rough road can be accomplished

2.3.1 Non-linear Mathematical Model

In this subsection, mathematical model of the system consists of two second-order nonlinear differential equations, these equations are derived using Lagrange's approach that is discussed in subsection 2.1.1. According to Fig. 2.2, the total kinetic and potential energies of the system can be derived as follows: this section, a nonlinear and linear mathematical model of SBU system

ederived. This model is used for purposes of controller design, as is dis-

in more details. This model is derived by taking into account, the dam

sha

Figure 2.2 Self-Balancing Unicycle (SBU) system on inclined road All parameters in this figure will have the same description as in **Figure 2.1**

The total kinetic energy of the system is the summation of all kinetic energies of all the components of the system, which are, the wheel, the pendulum, the motor and pulleys.

$$
K = K_w + K_p + K_m \tag{2-43}
$$

First, kinetic energy for the wheel:

$$
K_{\rm w} = \frac{1}{2} m_{\rm w} \dot{x}_{\rm w}^2 + \frac{1}{2} m_{\rm w} \dot{y}_{\rm w}^2 + \frac{1}{2} J_{\rm w} \dot{\theta}^2
$$
 (2-44)

And, by substituting \dot{x}_w and \dot{y}_w as expressions of the generalized coordinates, that is discussed above, it is concluded the following:

$$
x_w = R\theta \cos \gamma \to \dot{x}_w = R\dot{\theta} \cos \gamma \tag{2-45}
$$

$$
y_w = R\theta \sin \gamma \to \dot{y}_w = R\dot{\theta} \sin \gamma \tag{2-46}
$$

Substituting equations $2 - 45$, $2 - 46$ in equation $(2 - 44)$ yields:

$$
K_{w} = \frac{1}{2} m_{w} R \dot{\theta} \cos \gamma^{2} + \frac{1}{2} m_{w} R \dot{\theta} \sin \gamma^{2} + \frac{1}{2} J_{w} \dot{\theta}^{2}
$$
 (2-47)

Second, kinetic energy for the pendulum:

$$
K_p = \frac{1}{2} m_p \dot{x}_p^2 + \frac{1}{2} m_p \dot{y}_p^2 + \frac{1}{2} J_p \dot{\varphi}^2
$$
 (2-48)

By substituting \dot{x}_p and \dot{y}_p as expressions of the generalized coordinates:

$$
x_p = x_w + l_1 \sin \varphi \to \dot{x}_p = R\dot{\theta} \cos \gamma + l_1 \dot{\varphi} \cos \varphi \tag{2-49}
$$

$$
y_p = y_w + l_1 \cos \varphi \to \dot{y}_p = R\dot{\theta} \sin \gamma - l_1 \dot{\varphi} \sin \varphi \tag{2-50}
$$

Substituting equations $2 - 49$, $2 - 50$ in equation $(2 - 48)$ yields:

$$
K_p = \frac{1}{2} m_p \ R\dot{\theta} \cos \gamma + l_1 \dot{\phi} \cos \varphi^2 + \frac{1}{2} m_p \ R\dot{\theta} \sin \gamma - l_1 \dot{\phi} \sin \varphi^2 + \frac{1}{2} l_p \dot{\phi}^2
$$
 (2-51)

Third, kinetic energy for the motor and pulleys:

$$
K_m = \frac{1}{2} J_m \dot{\theta}_m^2 \tag{2-52}
$$

Substituting \vec{B}_m as expression of the generalized coordinates:

$$
\theta_m = \frac{1}{n} \ \theta \to \dot{\theta}_m = \frac{1}{n} \ \dot{\theta} \tag{2-53}
$$

Substituting equations $2 - 53$ in equation $(2 - 52)$ yields:

$$
K_m = \frac{1}{2} I_m \frac{\theta^2}{n}
$$
 (2-54)

Now, substituting the net equations $2 - 47$, $2 - 51$, and $(2 - 54)$ in equation $2 - 43$ and simplifying it to the next equation:

$$
K = \frac{1}{2} m_w R^2 + m_p R^2 + I_w + \frac{I_m}{n^2} \dot{\theta}^2 + m_p R I_1 \dot{\theta} \dot{\phi} \cos \gamma \cos \varphi - \sin \gamma \sin \varphi
$$

+ $\frac{1}{2} m_p I_1^2 + I_p \dot{\phi}^2$ (2-55)

As the same for kinetic energy, the total potential energy of the system is the summation of all potential energies of all the components of the system, which are, the wheel, the pendulum, the motor and pulleys.

$$
P = P_w + P_p + P_m \tag{2-56}
$$

First, potential energy for the wheel:

$$
P_w = m_w g y_w = m_w g \ R\theta \sin \gamma \tag{2-57}
$$

Second, potential energy for the pendulum:

$$
P_p = m_p g y_p = m_p g R \theta \sin \gamma + l_1 \cos \varphi \tag{2-58}
$$

Third, potential energy for the motor and pulleys:

$$
P_m = 0
$$
, since the mass of motor and pulleys are included in m_p (2-59)

Now, substituting the net equations $2 - 57$, $2 - 58$, and $(2 - 59)$ in equation $2 - 56$ and simplifying it to the next equation:

$$
P = m_w g R \sin \gamma + m_p g R \sin \gamma \ \theta + m_p g l_1 \cos \varphi \tag{2-60}
$$

Finally, computing the power dissipation term to substitute it in *Lagrange's* equation:

$$
D = D_{w \leftrightarrow p} + D_m \tag{2-61}
$$

And since $D_{w \leftrightarrow p}$, D_m are power terms, so it can be written in the following expressions:

$$
D_{w \leftrightarrow p} = \frac{1}{2} d_{w \leftrightarrow p} \quad \theta^2 - \dot{\phi}^2 \tag{2-62}
$$

$$
D_m = \frac{1}{2} d_m \theta_m^2 = \frac{1}{2} d_m \frac{\dot{\theta}}{n}^2
$$
 (2-63)

Substituting equations $2 - 62$, $(2 - 63)$ in equation $(2 - 61)$ yields:

$$
D = \frac{1}{2} d_{w \leftrightarrow p} \; \dot{\theta}^2 - \dot{\phi}^2 + \frac{1}{2} d_m \; \frac{\dot{\theta}}{n}^2 = \frac{1}{2} d_{w \leftrightarrow p} + \frac{d_m}{n^2} \; \dot{\theta}^2 - \frac{1}{2} d_{w \leftrightarrow p} \dot{\phi}^2 \tag{2-64}
$$

Now, evaluating *Lagrangian* term \overline{L} :

$$
L = K - P
$$

\n
$$
L = \frac{1}{2} m_w R^2 + m_p R^2 + J_w + \frac{J_m}{n^2} \dot{\theta}^2 + m_p R l_1 \dot{\theta} \dot{\phi} \cos \gamma \cos \varphi - \sin \gamma \sin \varphi
$$

\n
$$
+ \frac{1}{2} m_p l_1^2 + J_p \dot{\phi}^2 - m_w g R \sin \gamma + m_p g R \sin \gamma \theta - m_p g l_1 \cos \varphi
$$
 (2-65)

Applying Lagrange's equation for each generalized coordinate, θ and φ , yields:

1. For generalized coordinate θ :

$$
\frac{d}{dt} \frac{\partial L}{\partial \theta} - \frac{\partial L}{\partial \theta} + \frac{\partial D}{\partial \theta} = Q_{\theta}
$$
\n
$$
\Rightarrow \frac{\partial L}{\partial \theta} = -m_{w}gR\sin\gamma + m_{p}gR\sin\gamma
$$
\n
$$
\Rightarrow \frac{\partial L}{\partial \theta} = m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{I_{m}}{n^{2}} \quad \theta + m_{p}Rl_{1}\phi \cos\gamma\cos\varphi - \sin\gamma\sin\varphi
$$
\n
$$
\Rightarrow \frac{\partial D}{\partial \theta} = d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}} \quad \theta
$$
\n
$$
\Rightarrow \frac{d}{dt} \frac{\partial L}{\partial \theta} = m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{I_{m}}{n^{2}} \quad \theta - m_{p}Rl_{1}\phi^{2}\cos\gamma\sin\varphi + m_{p}Rl_{1}\ddot{\varphi}\cos\gamma\cos\varphi
$$
\n
$$
-m_{p}Rl_{1}\dot{\varphi}^{2}\sin\gamma\cos\varphi - m_{p}Rl_{1}\ddot{\varphi}\sin\gamma\sin\varphi
$$
\n
$$
Q_{\theta} = M_{w} \frac{\partial \theta_{w}}{\partial \theta} + F_{w} \frac{\partial x_{w}}{\partial \theta}
$$
\n
$$
\Rightarrow Q_{\theta} = T_{m} - f_{d}R
$$
\n(2 - 66)

So, the *first nonlinear differential equation* of the system will be as the following:

$$
m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{J_{m}}{n^{2}} \ddot{\theta} + m_{p}Rl_{1} \cos\gamma\cos\varphi - \sin\gamma\sin\varphi \ddot{\varphi}
$$

-
$$
m_{p}Rl_{1} \cos\gamma\sin\varphi + \sin\gamma\cos\varphi \dot{\varphi}^{2} + m_{w}gR\sin\gamma + m_{p}gR\sin\gamma
$$

+
$$
d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}} \dot{\theta} = T_{m} - f_{d}R
$$
 (2-67)

2. For generalized coordinate φ :

$$
\frac{d}{dt} \frac{\partial L}{\partial \dot{\phi}} - \frac{\partial L}{\partial \phi} + \frac{\partial D}{\partial \dot{\phi}} = Q_{\varphi}
$$
\n
$$
(2 - 68)
$$
\n
$$
\frac{\partial L}{\partial \phi} = m_{p}g l_{1} \sin \varphi - m_{p}R l_{1} \dot{\theta} \dot{\phi} \cos \gamma \sin \varphi + \sin \gamma \cos \varphi
$$
\n
$$
\frac{\partial L}{\partial \dot{\phi}} = m_{p}R l_{1} \dot{\theta} \cos \gamma \cos \varphi - \sin \gamma \sin \varphi + m_{p}l_{1}^{2} + l_{p} \dot{\phi}
$$
\n
$$
\frac{\partial D}{\partial \dot{\phi}} = -d_{w \leftrightarrow p} \dot{\phi}
$$
\n
$$
\frac{d}{dt} \frac{\partial L}{\partial \dot{\phi}} = -m_{p}R l_{1} \dot{\theta} \dot{\phi} \cos \gamma \sin \varphi + m_{p}R l_{1} \ddot{\theta} \cos \gamma \cos \varphi - m_{p}R l_{1} \dot{\theta} \dot{\phi} \sin \gamma \cos \varphi
$$
\n
$$
-m_{p}R l_{1} \ddot{\theta} \sin \gamma \sin \varphi + m_{p}l_{1}^{2} + l_{p} \ddot{\varphi}
$$
\n
$$
Q_{\varphi} = M_{p} \frac{\partial \theta_{p}}{\partial \varphi} + F_{p} \frac{\partial x_{p}}{\partial \varphi}
$$
\n(2 - 68)

 $Q_{\varphi} = -T_m - f_d l_2 \cos \varphi$

And *second nonlinear differential equation* of the system will be as the following:

$$
-m_p R l_1 \dot{\theta} \dot{\phi} \cos \gamma \sin \varphi + m_p R l_1 \ddot{\theta} \cos \gamma \cos \varphi - m_p R l_1 \dot{\theta} \dot{\phi} \sin \gamma \cos \varphi - m_p R l_1 \ddot{\theta} \sin \gamma \sin \varphi
$$

+
$$
m_p l_1^2 + l_p \ddot{\phi} - m_p g l_1 \sin \varphi + m_p R l_1 \dot{\theta} \dot{\phi} \cos \gamma \sin \varphi + \sin \gamma \cos \varphi
$$

-
$$
d_{w \leftrightarrow p} \dot{\phi} = -T_m - f_d l_2 \cos \varphi
$$
 (2-69)

Nonlinear differential equations $(2 - 67)$ and $(2 - 69)$ that describe Self-Balancing Unicycle (SBU) system on inclined road can be written in matrix form as below:

$$
m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{Im}{n^{2}} \t m_{p}Rl_{1} \cos \gamma \cos \varphi - \sin \gamma \sin \varphi \quad \ddot{\theta}
$$

\n
$$
m_{p}Rl_{1} \cos \gamma \cos \varphi - \sin \gamma \sin \varphi \t m_{p}l_{1}^{2} + J_{p} \qquad \ddot{\varphi}
$$

\n
$$
+ \frac{d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}}}{0} \t 0 \t \theta
$$

\n
$$
-d_{w \leftrightarrow p} \qquad \ddot{\varphi}
$$

\n
$$
+ \frac{-m_{p}Rl_{1} \cos \gamma \sin \varphi + \sin \gamma \cos \varphi \dot{\varphi}^{2} + m_{w}gR \sin \gamma + m_{p}gR \sin \gamma}{-m_{p}g l_{1} \sin \varphi}
$$

\n
$$
= \frac{1}{-1} T_{m} t + \frac{-R}{-l_{2} \cos \varphi} f_{d} \qquad (2-70)
$$

2.3.2 Linearization of Mathematical Model

Using the assumption that is used in subsection 2.2.2 for linearization, equation $(2 - 70)$ can be written as in the following form:

$$
m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{J_{m}}{n^{2}} \quad m_{p}Rl_{1} \cos \gamma \quad \theta \quad + \quad d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}} \quad 0 \quad \theta
$$

\n
$$
m_{p}Rl_{1} \cos \gamma \quad m_{p}l_{1}^{2} + J_{p} \quad \phi \quad 0 \quad -d_{w \leftrightarrow p} \quad \phi
$$

\n
$$
+ \quad m_{w}gR \sin \gamma + m_{p}gR \sin \gamma \quad = \quad 1 \quad T_{m} \quad t \quad + \quad -R \quad J_{2} \quad f_{d} \quad (2-71)
$$

and rewriting the above equation in more compact form, as in the following equation:

$$
m_{w}R^{2} + m_{p}R^{2} + J_{w} + \frac{J_{m}}{n^{2}} \quad m_{p}Rl_{1} \cos \gamma \quad \ddot{\theta} + d_{w \leftrightarrow p} + \frac{d_{m}}{n^{2}} \quad 0 \quad \dot{\theta}
$$

\n
$$
m_{p}Rl_{1} \cos \gamma \quad m_{p}l_{1}^{2} + J_{p} \quad \ddot{\phi} + 0 \quad -d_{w \leftrightarrow p} \quad \ddot{\phi}
$$

\n
$$
+ \quad 0 \quad 0 \quad \theta
$$

\n
$$
+ \quad 0 \quad -m_{p}gl_{1} \quad \varphi
$$

\n
$$
= \quad \frac{1}{-1} T_{m} t + \frac{-R}{-l_{2}} f_{d} + \quad m_{w} g R + m_{p} g R \quad \sin \gamma \qquad (2-72)
$$

Here, by defining the vector $\mathbf{q} = \frac{\theta}{\varphi}$, the equation $(2 - 72)$ can be written:

$$
M\ddot{\mathbf{q}} + C\dot{\mathbf{q}} + K\mathbf{q} = B T_m t + B_d f_d + B_y \sin\gamma
$$
 2-73

In which:

- The Inertia matrix is defined as:

$$
M = \frac{m_w R^2 + m_p R^2 + I_w + \frac{I_m}{n^2}}{m_p R l_1 \cos \gamma} \qquad (2-74)
$$

$$
m_p R l_1 \cos \gamma
$$

- The Damping matrix is defined as:

$$
C = \begin{array}{cc} d_{w \leftrightarrow p} + \frac{d_m}{n^2} & 0 \\ 0 & -d_{w \leftrightarrow p} \end{array}
$$
 (2-75)

- The Stiffness matrix is defined as:

$$
K = \begin{bmatrix} 0 & 0 \\ 0 & -m_p g l_1 \end{bmatrix} \tag{2-76}
$$

- The Input matrix is defined as:

$$
B = \frac{1}{-1} \tag{2-77}
$$

- The Disturbance matrix is defined as:

$$
B_d = \frac{-R}{-l_2} \tag{2-78}
$$

- The Inclination angle matrix is defined as:

$$
B_y = \frac{m_w g R + m_p g R}{0} \tag{2-79}
$$

Note:

From the matrices above, it should be noted that SBU system on iclined road has coupling in the inertia matrix and damping matrix, while there is no coupling in the stiffness matrix.

Here, to have a state space representation for the linearized SBU system on inclined road, it must have four state variables, which can be chosen θ , φ , $\dot{\theta}$ and $\dot{\varphi}$, and have one input which is the torque $T_m(t)$, and one disturbance force which is f_d , and another disturbance from the inclination angle γ and the stae space model can be derived from the equation $(2 - 73)$, by using the way that is shown underneath:

$$
\rightarrow x_1 = q \tag{2-80}
$$

$$
\rightarrow x_2 = \dot{q} \tag{2-81}
$$

So, by differentiating the equations above, and substituting with each other:

$$
\rightarrow \dot{x}_1 = x_2
$$

\n
$$
\rightarrow \dot{x}_2 =
$$

\n
$$
- M^{-1} K x_1 - M^{-1} C x_2 + M^{-1} B T_m t + M^{-1} B_d f_d + M^{-1} B_y \sin \gamma
$$
 (2-83)

Substitute the equation $2 - 82$ and $(2 - 83)$ in general equations of state space model will yield:

$$
\begin{aligned}\n\ddot{x}_1 &= \mathbf{0}_{2 \times 2} & \mathbf{I}_{2 \times 2} & \mathbf{I}_{2 \times 2} & \mathbf{I}_{2} & \mathbf{I}_{
$$

Where:

I: is the identity matrix.

0: is the zero matrix.

 y_m : is the measured output vector.

From the state space model equations above:

$$
A = \frac{0_{2 \times 2}}{M^{-1} K} - \frac{I_{2 \times 2}}{M^{-1} C}
$$
 (2-86)

$$
B = \frac{0_{2 \times 1}}{M^{-1} B} \tag{2-87}
$$

$$
C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \tag{2-88}
$$

$$
B_d = \frac{0_{2 \times 1}}{M^{-1} B_d} \tag{2-89}
$$

$$
B_{\gamma} = \frac{0_{2 \times 1}}{M^{-1} B_{\gamma}} \tag{2-90}
$$

Using parameters of SBU system in Table 2.1, there are numerical values of state space representation of the system and eigenvalues also, as bellow(assuming $\gamma = 0$):

$$
\begin{array}{rcl}\n\dot{x}_1 & = & 0 & 0 & 1.0000 & 0 & 0 & 0 \\
\dot{x}_2 & = & 0 & -71.8243 & -0.0179 & -0.0001 & x_2 + 45.1495 & T_m \ t + \frac{0}{-0.1830} \ f_d \\
 & = & 0 & 65.8677 & 0.0086 & 0.0001 & -28.0718 & -1.8321 \\
 & & & & & \\
\end{array}
$$
\n
$$
\begin{array}{rcl}\n\dot{x}_1 & = & 0 & 0 & 0 \\
\hline\n & 65.8677 & 0.0086 & 0.0001 & -28.0718 & -1.8321 \\
 & & & & \\
\end{array}
$$
\n
$$
\begin{array}{rcl}\n\dot{x}_1 & = & 0 & 0 & 0 \\
\hline\n & 121.2035 & \sin \gamma \text{ (assuming } \gamma = 0) \\
 & & & & \\
\hline\n & & & & \\
\mathbf{y}_m = & \mathbf{y}_1 = & 0 & 0 & 0 & \mathbf{x}_1 \\
 & \mathbf{y}_2 = & 0 & 1 & 0 & 0 & \mathbf{x}_2\n\end{array}
$$

Chapter Three

Mechanical Components, Electrical and Computer Interfacing Components, and Information System of SBU System

Contents:

- Introduction
- Mechanical Components
	- \triangleright Structure Parts
	- \triangleright Ball Bearing
	- Non-slip Belt
	- \triangleright Pulleys
	- \triangleright Wheels
- Electrical and Computer Interfacing Components
	- \triangleright AC Servomotor and its driver
	- Micro-machined Accelerometer
	- Optical Digital Encoder
	- Data Acquisition Cards
- Information System
	- MATLAB® and SIMULINK
	- xPC Target

3.1 Introduction

As a mechatronic system, mechanical components and considerations are important in SBU system. These components include the structure parts that are designed and manufactured by the machine operations and processes, and also mechanical components include other components that are already available. The duty is how to compromise between these two main kinds of components.

Also, SBU system has electrical components, in which these components include the actuator which represents the muscle of the control system, and the sensors which represent the eye of the control system. In addition to that the electrical components of SBU system include the circuits and cards that are essential for interfacing the control system of SBU system with the controller which is in this case PC computer.

In any mechatronic system such as SBU system, the software components have a significant importance. So, availability of some software tools in any software environment will facilitate the controller design process and getting the experimental results for this system. MATLAB® and SIMULINK tools will be used for this system. And to achieve high real-time abilities that are required for dealing with such rapid dynamic system, a special tool will be used which is xPC Target that is already available in SIMULINK libraries.

Figure 3.1 show the Self-Balancing Unicycle System

3.2 Mechanical Components

Mechanical systems are connected with the behavior of matter under the action of forces. Such systems are categorized as rigid, deformable, or fluid in nature.

Most mechatronic applications involve rigid-body systems. In SBU system, there are some components that are manufactured by some machining processes, in which will be covered in structure parts, and other components that are brought from the market, which will be covered in the other subsections.

3.2.1 Structure Parts

Designing the mechanical structure of SBU system and choosing the dimensions and material types, are depending on the functional specifications for each mechanical part. After that, for each part that is designed, it must be analyzed in terms of strength, elasticity and other material properties, to check that these parts achieve their functions.

Figure 3.1 Self- Balancing Unicycle System

The following are the main parts that are designed and manufactured in SBU system:

- 1. *The link:* it was designed and manufactured from rigid material (which is aluminum) in order to achieve the following: (see figure 3.2)
- Carrying the motor.
- Resisting the counter torque that is generated from the motor.

- Transiting the torque from the motor to the overall link, with the same degree of effect.
- Reducing the inertia as possible as it can.
- Reducing the link thickness to facilitate joining the motor with this link.
- Having the same dimensions of motor plate to be compatible with it.
- Resisting the tension in the non-slip belt between the pulleys.

Figure 3.2 The link (all dimensions are in mm)

- 2. *The Supports:* these mechanical parts were designed and manufactured from rigid material (which is aluminum) to achieve the following: (see figure 3.3)
- Carrying the motor and the link.
- Resisting the static forces resulted from the tension in the non-slip belt between the pulleys, by converting this tension stress into shear stress.
- Transiting the torque from the link to the housing elements of bearings (which are connected rigidly with the supports) with the same degree of effect.
- Reducing the inertia through the reducing the dimensions of these elements.

Figure 3.3 The Supports (all dimensions are in mm)

- 3. *Housing of Ball Bearing:* these mechanical parts were designed and manufactured from rigid material (which is aluminum) to achieve the following: (see figure 3.4)
- Carrying the motor, the link, and the supports.
- Resisting the static forces resulted from the tension in the non-slip belt between the pulleys.
- Transiting the torque from the supports to the bearings with the same degree of effect.
- Reducing the inertia as possible as it can, by reducing the dimensions of these components.
- Having the same dimensions of Ball bearings with specified clearance to be compatible with it.
- Having the same thickness of Ball bearings to be compatible with it.

Figure 3.4 The Housing of Ball Bearings (all dimensions are in mm)

- 4. *Connecting Shaft:* this mechanical component was designed and manufactured from rigid material (which is aluminum) to achieve the following: (see figure 3.5)
- Carrying the motor, the link, the supports, and the housings with the bearings.
- Resisting the static forces resulted from the tension in the non-slip belt between the pulleys.
- Having the same dimensions of inside diameter of bearing with specified clearance to be compatible with it.
- Having the length as small as possible, and at the same, compromising it with the dimensions of motor, link and supports.
- Reducing the inertia as possible as it can, by reducing the dimensions of this component.

Figure 3.5 The connecting Shaft (all dimensions are in mm)

3.2.2 Ball Bearings

In SBU system, the function of these bearings is to fix the connecting shaft with the link, permitting them to rotate with minimal possible friction.

Two sets of these bearings will be used in this project. In order to reduce the friction at these bearings, the lubricant and its keepers are removed as shown in figure 3.6.

Figure 3.6 Ball Bearings used in SBU system

3.2.3 Non-Slip Belt

This part will be used in SBU system, for transiting the motion from the motor to the connecting shaft. The measurement of the shaft rotation will depend on the motor's encoder, so this belt have a big mission which is preventing the slip between the pulley of motor and the other on the shaft. See figure 3.7

Figure 3.7 Timing Belt used in SBU system

3.2.4 Pulleys

In SBU system, another part must be considered to prevent the slippage between the connecting shaft and the motor shaft, which are the pulleys. See figure 3.8.

For the ball bearings and the arrangement of the pulleys and the belt, that are previously mentioned, two essential requirements should be satisfied:

- Friction coefficient between the moving parts should be at the minimum possible value.
- Very high friction between the belt and the pulleys, so as to prevent any slippage.

Meeting these specifications is important; therefore this motor will be able to deal with the quick motion reversals during the operation of the system.

Figure 3.8 Timing Pulley used in SBU system

3.2.5 Wheels

In which are two wheels, and form the connected part to the ground. The generated torque from motor move these wheels forward, or backward to stabilize the link, and also to track the reference input signal. The most important feature in this mechanical part is preventing the slippage. See figure 3.9

Also, to prevent the slippage between the wheels and the ground, some arrangement will be used in SBU system during the real implementation.

Figure 3.9 Wheels used in SBU

3.3 Electrical and Computer Interfacing Components

Electrical systems are concerned with the behavior of three fundamental quantities: charge, current, and voltage (potential).

In SBU system, electrical components include the actuator which is the servomotor and its driver connections with the power and the controller. Also electrical components include the sensors which are the accelerometer that used for estimating the tilt angle of the link, and optical digital encoder used for measuring the rotation angle of the wheel. In addition to that the electrical components of SBU system include the circuits and cards that are essential for interfacing the control system of SBU system with the controller which is in this case PC computer.

In the following subsections, all these electrical components will be covered.

3.3.1 AC Servomotor and its driver

Single phase AC servo motor with a driver is selected to be the actuator for SBU system. Since the operation of SBU system requires quick changes in the direction of the system velocity and acceleration, which is necessary to stabilize the link vertically and generate the required torque for self balancing process, in addition to tracking process. Also, the selected actuator must have the ability to generate enough torque independently of the speed value. It is important for the selected actuator used in such a system to have a low inertia.

AC servomotor provided by Panasonic Company (see figure 3.10 and figure 3.11) meets the requirements of low inertia, generated torque independence on the speed, and very fast response.

Figure 3.10 Configuration of AC servomotor

The Ac servomotor used with the SBU system has the following specifications:

- Motor model is MSMD042P1S.
- Driver model is MBDDT2210.

- The rated power of the motor is 400 watt, with 3000 rpm as a rated speed, thus the rated torque will be 1.3 N.m.
- Motor rated voltage is 200 volt, single phase.
- The encoder provided with this model is an incremental encoder that generates 2500 pulse per revolution as a maximum value.
- Allowable radial and thrust loads on the shaft of the motor during operation are: Radial load $=$ 245N. Thrust load $=$ 98 N.

Figure 3.11 Configuration of servomotor driver

Motor and driver connections in torque control mode will be discussed in more details in appendix F.

3.3.2 Micro-machined Accelerometer

An accelerometer is a device that is used to measure the acceleration in its sensing axes relative to freefall. Single- and multi-axis accelerometers are available, in which in these devices, magnitude and direction of acceleration can be detected. Accelerometers are usually used to sense orientation, vibration and shock $_{[1]}$.

Accurate tracking for dynamic systems is a challenging task. However, what is required from the SBU system is accurate tracking, especially in its dynamic behavior. A unique method to have an accurate tracking is achieved by validating experimentally the accelerometer dynamic behavior.

Micro-machined accelerometers are commercially successful micro-sensors that are the silicon micro-fabricated accelerometers. In various forms these micro-sensors can measure acceleration ranges from well below one to around a thousand meters per square second with resolutions of one part in $10,000_{[2]}$.

Principle of Operation of Micro-machined Accelerometer

These sensors incorporate a micro-machined suspended proof mass that is subjected to an inertial force in response to an acceleration, which causes deflection of the supporting flexures. One means of measuring the deflection is by utilizing piezoresisteive strain gages (see figure 3.12)

Figure 3.12 Principle of operation for micro-machined accelerometer

Measuring Tilt with Accelerometer

Accelerometers are used to measure the tilt of an object. Accelerometers can be used for measuring both dynamic and static measurements of acceleration. Tilt is a static measurement where gravity is the acceleration being measured, see figure 3.13. Therefore, to achieve the highest degree resolution of a tilt measurement, high-sensitivity accelerometer is required.

STATIC ACCELERATION

Figure 3.13 Static Acceleration for accelerometers as tilt sensors

Three Axis Low-g Micro-machined Accelerometer provided by Freescale Semiconductor Company (see figure 3.14) meets the requirements of low-g, high sensitivity, and high bandwidth response.

Figure 3.14 Configuration of micro-machined accelerometer

The Freescale MMA6200Q and MMA7260Q series accelerometers are good solutions for XY and XYZ tilt sensing. These devices provide a sensitivity of 800 mV/g in 3.3 V applications. All of these accelerometers will experience acceleration in the range of $+1g$ to $-1g$ as the device is tilted from -90 degrees to $+90$ degrees, as in figure 3.14.

The Micro-machined Accelerometer used with the SBU system has the following features:

- Micro-machined Accelerometer model is MMA7260Q.
- Micro-machined Accelerometer Board has dimensions 6mm x 6mm x 1.45mm.
- Selectable Sensitivity (1.5g/2g/4g/6g).
- Low Current Consumption: 500 μA.
- Sleep Mode: 3 μA.
- Low Voltage Operation: 2.2 V _ 3.6 V.
- Bandwidth response: 350 Hz
- High Sensitivity (800 mV/g $@1.5$ g).
- Fast Turn on Time.
- High Sensitivity (1.5 g).
- Integral Signal Conditioning with Low Pass Filter (on board).
- Robust Design, High Shocks Survivability.

Typical applications of this Micro-machined Accelerometer are:

- Navigation and Dead Reckoning: E-Compass Tilt Compensation.
- Gaming: Tilt and Motion Sensing, Event Recorder.
- Robotics: Motion Sensing.
- Other applications are mentioned in Appendix D.

Other information about Micro-machined Accelerometer is in Appendix D.

3.3.3 Optical Digital Encoder

An encoder is a device that converts angular displacement into digital signals. The most popular type of encoders is the optical one, which consists of a rotating disk, a light

source, and a photo detector. This disk, which is fixed on the rotating shaft, has patterns of codes. When the disk rotates, these patterns break off the light emitted onto the photo detector, generating a digital signal.

Usually in optical encoders, there are two basic channels that generate digital signals, are called phase A, B. These channels used to sense the direction of the rotation besides the angular displacement as shown figure 3.15. Usually this encoder has a third phase which is phase Z that used for generating signals having information about the number of completed cycles.

Figure 3.15 Basic Configuration of optical encoder

In SBU system, this type of optical encoder will be used to measure the angular displacement of the wheels.

The optical encoder that is used in SBU system has the following specifications:

- The encoder provided with the servomotor is an incremental encoder that generates 2500 pulse per revolution as a maximum value.
- The digital signals that are generated from this encoder have 12-volts amplitude (see figure 3.16).

Figure 3.16 Digital Signal generated from motor encoder

3.3.4 Data Acquisition Cards

Data Acquisition Card (DAQ) is an interfacing card used to enter signals to PC computers or to generate signals from PC computers by using some useful software packages. In SBU system two data acquisition cards are used, one is supplied by National Instruments, while the other by Measurement Computing. Also, for SBU system MATLAB $^{\circledR}$ packages will be used for real-time applications with these cards.

In this section, these two cards that are used in SBU system will be discussed.

1.4 NI 6024E

This card is classified as a general-purpose data acquisition card. In SBU system this card is used for entering the analog signal of accelerometer to the controller (PC computer). Also, this card is used for sending analog signal from the computer to the servo driver to generate the required torque signal. Also, this card is used for entering the analog signals which have information about the actual torque generated from the servomotor to the computer. Figure 3.17 shows NI 6024E that is used in SBU system.

Figure 3.17 NI 6024E used in SBU System

2.4 PCI-QUAD04

The PCI-QUAD04 is a PCI plug-in board that provides inputs and decoupling for up to four incremental quadrature encoders. The PCI-QUAD04 can also be used as a high speed pulse counter for general counting application. It uses one PCI slot and a 37 pin connector for up to four channels. Each incremental quadrature encoders connects to an input channel on the board through a DB37 female connector on the board's rear panel. Channels 1 through 4 connect to the DB37 connector on the rear panel bracket.

Figure 3.18 PCI-QUAD04

3.4 Information System

As a mechatronic application, computer and information system are essential components of the SBU system. These components include, in addition to the PC hardware used for controller design, a set of software packages that is used to design, simulate, and control the system. These packages are represented by MATLAB® and SIMULINK, and xPC target techniques.

3.4.1 MATLAB® and SIMULINK

This environment is usually used to simulate the control algorithms of the mechatronic system. To achieve that, a set of software packages are used. MATLAB® and SIMULINK provide a wide variety of functions, numerical algorithms, and toolboxes that help significantly not only to design and simulate the control system, but also to build executable real-time applications.

3.4.2 xPC Target

xPC Target is a solution for prototyping, testing, and deploying real time systems using standard PC hardware. It is an environment that uses a target PC, separate from a host PC, for running real-time applications. In this environment you use your desktop computer as a host PC with MATLAB[®], SIMULINK, and Stateflow (optional), to create a model using Simulink blocks and Stateflow charts. After creating your model, you can run simulations in non-real time.

xPC Target lets you add I/O blocks to your model and then use the host PC with Real- Time Workshop, Real-Time Workshop Embedded Coder (optional), Stateflow Coder (optional), and a C/C++ compiler to create executable code.

The executable code is downloaded from the host PC to the target PC running the xPC Target real-time kernel. After downloading the executable code, you can run and test your target application in real time.

Chapter Four

Control System Design and Simulation Results of SBU System on Rough Road

Contents:

- Introduction
- Control Methods for SBU system
	- **► PID Control**
	- **► State Feedback Control**
	- \triangleright Adaptive Control
	- Non-linear Control
- Control Theory for SBU system
	- **≻ State Space Model**
	- ▶ Robust Tracking and Disturbance Rejection **Controller**
- Full-Order State Observer Design
- Control System Design Process for SBU system on flat road
- Simulation Results of SBU system on flat road
- Control System Design Process for SBU system on inclined road
- Simulation Results of SBU system on inclined road

4.1 Introduction

As discussed in Chapter One, SBU systems are considered as educational tools for classical and modern control system design theories, for that reason this chapter will introduce review discussion about the concepts of controller design that can be applied to these systems.

Control design process of SBU system can be divided into two basic divisions, one for stabilization the link, that means rejection all disturbances that affect this link (in certain limits) and saving the link stable about its operating point, and in addition for all that reject the disturbances that is formed from the nature of rough road. While the other division is specified for tracking the system for specified position.

In fact, this kind of systems, have some complex aspects

- The SBU system is unstable inherently, in its open-loop form, and this is resulted from the gravity effect on the link which is an inverted pendulum.
- On rough road, this system affected by many disturbances, that disturb the system response, in which is modeled mathematically by an inclined road with variable angle.
- This system have nonlinearity behavior, resulted from the terms that is omitted from the state space model in Chapter Two, in which these nonlinearities affect on the overall response of the system.
- The hardware limitations that are related to SBU system, such as the rated torque generated from the motor, add other difficulties to the control system, which is considering these limitations.
- The control system of SBU system will calculate the required motor torque on the link that opposite the gravity force that affect on this link.
- The disturbances affecting on the system are not measurable in direct form, and this add another function to the system, which is estimating the disturbances.
- As it was noted from state space model in Chapter Two, the SBU system has four states, that are not measured by sensors, so they must be estimated, and this a new task for control system.
- Robustness is another aspect that must be considered in control system design.

The following sections in this chapter talks about control methods and their characteristics that make these methods applicable for SBU system, and then control theory that will be implemented in this project, will be discussed. Then, upcoming sections will start the control system design process, first for the SBU system on flat road, and then on inclined road. Finally the end of this chapter contain simulation and testing the control system model behavior that is build using SIMULINK toolboxes in MATLAB® software.

4.2 Control Methods for SBU system

As stated earlier, SBU system have some complex aspects and challenges in terms of its control, due to the fact that, inherently open-loop unstable, with highly-nonlinear behavior. These add functions for a control system which is both interesting and challenging.

So, there are some control methods, that can be applied for SBU system control, that will be discussed later, they are accomplished with *real-time software interfacing*, but the SBU system can be also controlled by analog controller that have more difficulties resulted from finding the physical elements, and it must be noted that all control methods that are discussed below are *device control*.

The following subsections will discuss briefly the most important control methods that are defined above.

4.2.1 PID Control

A closed loop control system is one that determines an error in the desired and actual condition and creates a correction control command to remove this error. PID control demonstrates three ways of looking at this error and correcting it, as shown in Figure 4.1. The first way is the P, the proportional term. This term represents the control action made by the microcontroller in proportion to the error. In other words, the bigger the error, the bigger the correction. The I is for the integral of the error over time. The integral term produces a correction that considers the time the error has been present. Stated in other words, the longer the error continues, the bigger the correction. Lastly, the D stands for derivative. In the derivative term, the corrective action is related to the derivative or change of the error with respect to time. Stated in other words, the faster the error is changing, the bigger the correction. Control systems can use

P, PI, PD, or PID in creating corrective actions. The problem generally is "tuning" the system by selecting the proper values in the terms.

Figure 4.1 Control system scheme using PID controller

But for MIMO systems, this controller is not recommended, since it has some complex aspects, in addition to this type of controller is not recommended also for unstable systems (such as SBU system), since it has more overshoot in dynamical response.

4.2.2 State Feedback Control

This type of control depends on design of control systems in state space based on the pole placement method and the quadratic optimal regulator method. The pole-placement method is somewhat similar to the root-locus method in that placing closed-loop poles at desired locations. The basic difference is that in the root-locus design, the process is placing only the dominant closed-loop poles at the desired locations, while in the pole-placement design placing all closedloop poles at desired locations.

So, this method of control needs to have information about all the states of the system, and this may not be realized physically, the state observer can be used to estimate the states that can not be measured, based on the knowledge of the output and the input driving the system.

For MIMO systems (such as SBU system), this control system design is recommended, since there are two divisions of control system design (regulating and tracking input signal), as shown in Figure 4.2.

Figure 4.2 Servo control system (regulation and tracking) by state feedback & full-order state observer

4.2.3 Adaptive Control

The term adapt means "to change (oneself) so that one's behavior will conform to new or changed circumstances." The words "adaptive systems" and "adaptive control" have been used as early as 1950.

The design of autopilots for high-performance aircraft was one of the primary motivations for active research on adaptive control in the early 1950s. Aircraft operate over a wide range of speeds and altitudes, and their dynamics are nonlinear and conceptually time varying. For a given operating point, specified by the aircraft speed (Mach number) and altitude, the complex aircraft dynamics can be approximated by a linear model of the same form as below. For example, for an operating point *i*, the linear aircraft model has the following form:

$$
\dot{\mathbf{x}} = \mathbf{A}_i \mathbf{x} + \mathbf{B}_i \mathbf{u} \tag{4-1. a}
$$

$$
y = C_i x + D_i u \tag{4-1.b}
$$

where A_i , B_i , C_i , and D_i are functions of the operating point *i*. As the aircraft goes through different flight conditions, the operating point changes leading to different values for A , B , C , and D

Because the output response $y(t)$ carries information about the state x as well as the parameters, one may argue that in principle, a sophisticated feedback controller should be able to learn about parameter changes by processing $y(t)$ and use the appropriate gains to accommodate them. This argument led to a feedback control structure on which adaptive control is based. The controller structure consists of a feedback loop and a controller with adjustable gains as shown in Chapter Four
them. This argument led to a feedback control structure on which adaptive controlleis based. The
controller structure consists of a feedback loop and a controller with adjustable gains as shown in
Figure 4.3. disturbance dynamics distinguishes one scheme from another.

Figure 4.3 Adaptive controller structures with adjustable gains

4.2.4 Non-linear Control

Processes in reality like SBU system, robots and space crafts typically have strong non-linear Processes in reality like SBU system, robots and space crafts typically have strong non-linear
dynamics. In control theory it is sometimes possible to linearize such classes of systems and apply linear techniques, but in many cases is desirable to expand the sight beyond linear theories, permitting the control of nonlinear systems. These normally take advantage of results based on *Lyapunov's theory*. apply linear techniques, but in many cases is desirable to expand the sight beyond linear theories,
permitting the control of nonlinear systems. These normally take advantage of results based on
Lyapunov's theory.
4.3 Con Chapter Four

Singure and led to a feedback control structure on which adaptive control is based. The

numeral structure consists of a feedback loop and a controller with adjustable gains as shown in

gure 4.3. The way of

4.3 Control Theory for SBU system

In this section state feedback control theories, including robust tracking and disturbance rejection controller design, and full-order state observer for the system states are discussed. These theories are used to design stabilization and tracking controller, which is described at the introduction of this chapter, for both SBU system on flat road, and SBU system on inclined road.

4.3.1 State Space Model

In control engineering, a state space representation is a mathematical model of a physical system as a set of input, output and state variables related by first-order differential equations. To abstract from the number of inputs, outputs and states, the variables are expressed as vectors and the differential and algebraic equations are written in matrix form. The state space representation

(also known as the "time-domain approach") also provides a convenient and compact way to model and analyze systems with multiple inputs and outputs. Unlike the frequency domain approach, the use of the state space representation is not limited to time-invariant systems with linear components and zero initial conditions. "State Space" refers to the space whose axes are the state variables.

To obtain the state-space representation for any system, the state variables of the system, its inputs, outputs, in addition to the state and output equations are to be determined. The general linear time invariant state space model that is used throughout this chapter is:

$$
\dot{\mathbf{x}} = A\mathbf{x} + B\mathbf{u} + B_d F_d \tag{4-2. a}
$$

$$
y = Cx + Du \tag{4-2.b}
$$

Where:

- : The state vector, $\in R^{4\times 1}$
- : The controlled input vector, $\in R^{1\times 1}$
- : The output vector, $\in R^{2\times 1}$
- : The disturbance vector, $\in R^{1 \times 1}$
- : The system matrix, $\in R^{4 \times 4}$
- : The input matrix, $\in R^{4\times 1}$
- : The disturbance matrix, $\in R^{4\times 1}$
- : The output matrix, $\in R^{2\times 4}$
- **D**: The feed-forward matrix, this matrix is mostly a zero matrix, since all the transfer functions of physical systems relating the outputs to the inputs are strictly proper rational functions.

4.3.2 Robust Tracking and Disturbance Rejection Controller

The state equation and transfer function developed to describe a plant may change due to change of load, environment, or aging. Thus plant parameter variations often occur in practice. The equation used in the design is often called the *nominal equation*. The feed-forward gain computed for the nominal plant transfer functions may not yield the same result for non-nominal plant transfer functions. Then the output will not track asymptotically any step reference input. Such a tracking is said to be *nonrobust*.

The problem is to design an overall system so that the output $y(t)$ will track asymptotically any step reference input even with the presence of a disturbance F_d and with plant parameter variations. This is called *robust tracking and disturbance rejection*.

In SBU system, the problem is to design a state feedback controller that is able to track a desired reference signal of the wheel position, while keeping the pendulum (link) stabilized in its vertical position, even with the presence, to some extent, of disturbances and changes in plant parameters. The function of such a controller is divided into two divisions related to two different problems:

- *1. Regulator Problem:* which is to find a state feedback gain so that the response (that is caused by some nonzero initial conditions and disturbances) will die out at desired rate, this problem is applied in SBU system in the case of stabilizing the pendulum (link) in its vertical position.
- *2. Tracking Problem:* which is to design an overall system so that $y(t)$ approaches the reference signal $r(t)$ at steady state, and this problem is applied in SBU system in the case of tracking the wheel a desired reference signal. This problem have two aspects:
	- *a.* Asymptotic Tracking Problem: which is to design an overall system so that $y(t)$ approaches the reference signal $r(t) = a \quad \forall t \ge 0$ as t approaches infinity, it is clear that if $r(t) = 0$ then the tracking problem reduces to the regulator problem.
	- *b. Servomechanism Problem:* This is tracking non-constant reference signal.

It should be noted that the maximum number of signals that can be tracked equals the number of independent inputs of the system. In the case of SBU system, there is only one actuator acting on the system, so it is possible for only one output to track a desired input signal, which is the wheel position, while other states are just regulated.

Based on the previous discussion, the *Augmented System Model* as follows: $\dot{x} = (A - BK)x + Bk_1r$ (4 – 3. a) $= C_{track} x$ (4 – 3. b) Where:

$$
K = [k_1 \quad k_2 \quad \dots \quad k_n] \quad n : number of states
$$
\n
$$
A_a = A - BK \quad , \quad B_a = Bk_1
$$
\n
$$
(4 - 4.b)
$$
\n
$$
(4 - 4.b)
$$

 $C_{track} = [1 \space zeros]$, which corresponds to the wheel position.

Figure 4.4 shows the control system configuration,

for SBU System

To check the possibility of the closed loop eigenvalues of the system A_a to be placed arbitrarily; so as to achieve stability and the desired transient response, the controllability of the system is checked. This can be done by finding that the matrix $\begin{bmatrix} A - \lambda I & B \end{bmatrix}$ has a full row rank for each eigenvalue λ of the system. In another way, the controllability of the system is checked by calculating the controllability matrix (C_M) , such that:

$$
C_M = \begin{bmatrix} B & AB & \dots & A^{n-1}B \end{bmatrix} \tag{4-5}
$$

Note: In control system design for SBU system, the controllability of the pair (A, B) can be checked by using MATLAB® function (*ctrb*), then the rank of this matrix will be checked also, by using function (*rank*).

If the controllability matrix has a full row rank (number of rows that is rank, is equal to the number of system states), then the system is controllable, and it is possible to find a gain matrix \boldsymbol{K} , shown in Figure 4.4, so that to obtain the desired performance criteria, for achieving stability at the desired operating point, meeting the transient specifications, without moving beyond the practical constraints mentioned in Chapter One.

To find the desired gain matrix **K**, *Pole Placement Method* will be used.

Topology for Pole Placement:

In order to lay the groundwork for the approach, consider a plant represented in state space by

$$
\dot{\mathbf{x}} = A\mathbf{x} + B\mathbf{u} \tag{4-6. a}
$$
\n
$$
\mathbf{y} = C\mathbf{x} \tag{4-6. b}
$$

So, to apply pole-placement methodology to plants, (which is represented in phase-variable form such as SBU system) it should be taken the following steps:

- 1. Represent the plant in phase-variable form.
- 2. Feedback each phase variable to the input of the plant through a gain, k_i .
- 3. Find the characteristic equation for the closed-loop system represented in step2.
- 4. Decide upon all closed-loop pole locations and determine an equivalent characteristic equation.
- 5. Equate like coefficient of the characteristic equations from step 3 and 4 and solve for k_1 .

But, the selection of the closed-loop pole locations of the system should take into account the following constraints:

- The location of the open-loop zeros and poles.
- The damping ratio of the poles should be large enough in order to reduce the oscillation of system response.
- The real part should not be placed far away from the imaginary axis, since a choice like this will result in large gain values, that means a large driving torque, and this will exceeds the motor rated torque.
- It is recommended to have only a conjugate poles from the desired poles to make easy the controlling of the transient response.
- The bandwidth frequency of the system should be kept small enough, so as to make the system less sensitive to noise.

Note: In control system design for SBU system, after determining the desired poles, MATLAB[®] function (*place*) will be used to calculate the necessary gain values.

4.4 Full-Order State Observer Design

In the pole-placement approach to the design of control systems, it is assumed that all state variables are available for feedback. In practice, however, not all state variables are available for feedback. Then, there is need to estimate unavailable state variables. Estimation of immeasurable state variables is commonly called *observation*. A computer program that estimates or observes the state variable is called a *state observer*, or simply an *observer*. If the state observer observes all state variables of the system, regardless of whether some state variables are available for direct measurement, it is called a *full-order state observer*.

Based on the previous discussion, a state observer estimates the state variables based on the measurement of the output and control variables. Here the concept of *observability* plays an important role, where state observers can be designed if and only if the observability condition is satisfied.

Usually the observability of the pair (A, C) can be checked by the observability matrix (O_M) , such that:

$$
O_M = \frac{CA}{CA}
$$
 (4-7)

After determining the observability matrix (O_M) , if it has a full column rank, then system is fully observable.

Notes:

- In control system design for SBU system, the matrix (O_M) can be calculated by using MATLAB® function (*obsv*), then its rank is found.
- The following discussion of state observer, will use the notation \bar{x} to designate the observed state vector.

Observer Design Process:

Figure 4.5 shows the basic concept of observer design. The measured outputs of the system are compared to those estimated, and then error signal is feedback to the observer. In order to increase the convergence speed of the error signal, which is making the observer outputs match those measured as fast as possible, the dynamics of the observer should be made much faster than that of the controlled system.

The state equation of the observer is found form Figure 4.5 as follows:

$$
\widetilde{\mathbf{x}} = A\widetilde{\mathbf{x}} + B\mathbf{u} + L(\mathbf{y} - \widetilde{\mathbf{y}}) \tag{4-8. a}
$$

$$
\widetilde{\mathbf{x}} = A\widetilde{\mathbf{x}} + Bu + LC(\mathbf{x} - \widetilde{\mathbf{x}}) \tag{4-8.b}
$$

While for the linear system: $x = Ax + Bu$ (4 – 9)

The error signal between the measured and observed state is: $\hat{z} = x - \tilde{x}$ (4 - 10)

Subtracting the state equation of the observer from the state equation for linear system will include:

$$
\tilde{e} = (A - LC)\tilde{e} \tag{4-11}
$$

Thus, the function of design engineer, is choosing an appropriate gain vector (L) , the poles of the characteristic equation can be placed far to the left from those of the controlled system, so as to achieve the desired speed of the observer.

Note: In control system design for SBU system, after determining the desired poles for the observer, MATLAB[®] function (*place*) will be used to calculate the necessary gain vector (\bf{L}).

4.5 Control System Design Process for SBU system on flat road

In this section, all theories and procedures that are discussed in the previous sections, will be applied in this section for SBU system on flat road.

The first step in control system design process is the state-space modeling, in which this step is accomplished in Chapter Two, so it is enough to rewrite this model again in this chapter:

Chapter Four

$$
\vec{x} = \begin{pmatrix}\n0 & 0 & 1.0000 & 0 & 0 & 0 & 0 \\
0 & 0 & 0 & 1.0000 & \vec{x} + 0 & 0 & 0 & 0 \\
0 & -71.8243 & -0.0179 & -0.0001 & + 45.1495 & T_m(t) + -0.1830 & f_a \\
0 & 65.8677 & 0.0086 & 0.0001 & -28.0718 & -1.8321\n\end{pmatrix}
$$
\n
$$
y_m = \begin{pmatrix}\ny_1 \\
y_2\n\end{pmatrix} = \begin{pmatrix}\n1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 0 & 0 \\
0 & 0 & 0 & 0\n\end{pmatrix} \vec{x}
$$
\n
$$
y_{track} = \begin{bmatrix}\n1 & 0 & 0 & 0 \\
0 & 0 & 0 & 0 \\
0 & 0 & 0 & 0\n\end{bmatrix} \vec{x}
$$
\n(4-12)

The eigenvalues of the system (uncontrolled system) can be obtained by using the MATLAB® function (*eig*) as below:

```
eigenvalues=eig(A)
eigenvalues =
         0 % this system's kind is type No.1
   8.1113 % this system is open loop unstable
   -8.1205
   -0.0085 % this eigenvalue is not recommended
```
It can be easily seen that the system is type 1 and unstable.

Based on equation $(4 - 3)$ the equation $(4 - 12)$ will be written as below:

$$
\vec{x} = (A - BK)\vec{x} + Bk_1r + B_df_d
$$
\n
$$
y_{track} = \begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix}\vec{x}
$$
\n(4-13. a)\n(4-13. b)

Then, next step is checking the controllability matrix (C_M) by using the MATLAB[®] function (*ctrb*) as below:

```
co=ctrb(A,B);cm=rank(co)
cm =4 % this system is full controllable
```
Now, the next step is finding the gains of matrix \boldsymbol{K} , this will be accomplished by using MATLAB® function (*place*) , but for that it must be determined the desire eigenvalues of the system, in which are $[-7 \quad -10 \quad -4 \quad -3]$, then the function can be used as below:

```
p=[-7 -10 -4 -3];k=place(A,B,p)
k=-0.8771 -10.9091 -0.7240 -2.0187k1=k(1)k1 =-0.8771
k(1)=0;k =0 -10.9091 -0.7240 -2.0187k(1) k(2) k(3) k(4)
```
The next step is full-order state observer design, in which this is accomplished by the error dynamic equation that is cleared in equation $(4 - 11)$, in this equation it is important to put the eigenvalues of the error matrix far to the left from those of the controlled system, and it is recommended to put them too far, to have a large speed in error dynamic, that will mask its behavior.

So, by using MATLAB[®] function (*place*) again, the gains of the matrix **L** can be determined, but for that, the eigenvalues of the error matrix must be chosen as follow $[-70$ -100 -40 -30], then the function can be used as below:

```
poles=10*[-7 -10 -4 -3];
L=place(A',Cm',poles)' % where cm is the measured output matrix
L =1.0e+003 *
   0.1031 0.0110
   0.0105 0.1368
   2.2620 0.4760
   0.5131 3.9004
```
Finally, the control system of SBU system on flat road is now ready for simulation in the next section.

4.6 Simulation Results of SBU system on flat road

The next step in controller design process is simulation. This step is significant importance to check whether the resulted system response meets the design specifications or not. Using the controller and observer design results, with the system model derived in Chapter Two, MATLAB® and SIMULINK are used to simulate system performance. Then simulation is very significant, in comparing between the nonlinear model behavior of the system with the linear model performance, in which this step will be applied for SBU system on flat road, also.

The simulink model of SBU system on flat road is shown in Figure 4.7.

The initial conditions, desired input, and disturbance acting on the system are assumed as follows:

- The initial angle of the link is 0.1 rad.
- All initial other conditions are zero.
- The desired input of the unicycle is 10 m.
- There is a disturbing force acting on the link equal to 1N acting on small interval $[4 -$ 4.1] sec.

The simulation results were as follows:

Figure 4.6 Driving motor torque

Figure 4.9 Link angle behavior with time

x

Figure 4.11 Nonlinearities effect on unicycle position with time

Figure 4.12 Nonlinearities effect on link angle with time

The results that can be noticed from the previous figures:

- Zero steady-state error in unicycle position, and that is resulted from the system model type number (Figure 4.8).
- Very small differences between linear and nonlinear model behavior (Figure 4.10, 4.11, 4.12).
- The observer model behavior is very fast compared to the controlled plant behavior, so the observer effect on the controlled plant is too small, and can be neglected.
- The system model did not exceed the saturation limit of motor torque, so the motor can operate the system in easy way (Figure 4.7).

4.7 Control System Design Process for SBU system on inclined road

In this section, all theories and procedures that are discussed for SBU system on flat road, will be applied in this section for SBU system on inclined road.

The first step in control system design process is the state-space modeling, in which this step is accomplished in Chapter Two, so it is enough to rewriting this model again in this chapter:

$$
\vec{x} = \begin{bmatrix} 0 & 0 & 0 & 1.0000 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1.0000 & \vec{x} + 0 & 0 & 0 \\ 0 & -71,8243 & -0.0179 & -0.0001 & \vec{x} + 45.1495 & T_m(t) + -0.1830 & f_a + 0 & 0 \\ 0 & 65.8677 & 0.0086 & 0.0001 & -28.0718 & -1.8321 \\ 0 & 0 & \vec{x} & \vec{x} & \vec{x} \\ 121.2035 & \sin \gamma & -58.1777 & \vec{x} \\ \hline\n\end{bmatrix}
$$
\n
$$
\vec{y}_m = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & \vec{x} \\ 0 & 1 & 0 & 0 & 0 & \vec{x} \\ 0 & 0 & 0 & 0 & \vec{x} \\ \hline\n\end{bmatrix}
$$
\n
$$
\vec{y}_r = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & \vec{x} \\ 0 & 0 & 0 & 0 & 0 & \vec{x} \\ 0 & 0 & 0 & 0 & 0 & \vec{x} \\ 0 & 0 & 0 & 0 & 0 & 0 & \vec{x} \end{bmatrix}
$$
\n
$$
(4 - 14)
$$

Depending on the above model, it should be determined the eigenvalues of the system $(\gamma = 0^{\degree})$, to have well-known notice about these eigenvalues, and this can be achieved by using the MATLAB® function (*eig*) as below:

```
eigenvalues=eig(A)
eigenvalues =
         0 % this system's kind is type No.1
    8.1113 % this system is open loop unstable
   -8.1205
   -0.0085 % this eigenvalue is not recommended
```
Based on equation $(4 - 3)$ the equation $(4 - 14)$ will be written as in equation $(4 - 15)$:

```
\vec{x} = (A - BK)\vec{x} + Bk_1r + B_df_d + B_{\gamma}\sin\gammay_{track} = \begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix}\vec{x} (4 - 15)
```
Then, next step is checking the controllability matrix (C_M) by using the MATLAB[®] function (*ctrb*) as below:

```
co=ctrb(A,B);cm=rank(co)
cm =
```
4 % this system is full controllable

Now, the next step is finding the gains of matrix \bf{K} , this will be accomplished by using MATLAB® function (*place*) , but for that it must be determined the desire eigenvalues of the system, in which are $[-7 \quad -10 \quad -4 \quad -3]$, then the function can be used as below:

```
p=[-7 -10 -4 -3];k=place(A,B,p);
k=-0.8771 -10.9091 -0.7240 -2.0187
```
The next step is full-order state observer design, in which this is accomplished by the error dynamic equation that is cleared in equation $(4 - 3)$, in this equation it is important to put the eigenvalues of the error matrix far to the left from those of the controlled system, and it is recommended to put them too far, to have a large speed in error dynamic, that will mask its behavior.

So, by using MATLAB[®] function (*place*) again, the gains of the matrix **L** can be determined, but for that, the eigenvalues of the error matrix must be chosen as follow $[-70 \quad -100 \quad -40 \quad -30]$, then the function can be used as below:

```
poles=10*[-7 -10 -4 -3];
L=place(A',Cm',poles)' % where cm is the measured output matrix
L =1.0e+003 *
   0.1031 0.0110
   0.0105 0.1368
   2.2620 0.4760
   0.5131 3.9004
```
Finally, the control system of SBU system on inclined road is now ready for simulation in the next section.

4.8 Simulation Results of SBU system on inclined road

The next step in controller design process is simulation. This step is significant importance to check whether the resulted system response meets the design specifications or not. Using the controller and observer design results, with the system model derived in Chapter Two, MATLAB® and SIMULINK are used to simulate system performance. Then simulation is very significant, in comparing between the nonlinear model behavior of the system with the linear model performance, in which this step will be applied for SBU system on inclined road, also.

The simulink model of SBU system on flat road is shown in Figure 4.13.

The initial conditions, desired input, and disturbance acting on the system are assumed as follows:

- The initial angle of the link is 0.1 rad.
- All initial other conditions are zero.
- The desired input of the unicycle is 10 m.
- There is a disturbing force acting on the link equal to 1N acting on small interval [4 4.1] sec.
- The road is flat initially, and after 2 seconds the road will be inclined by (0.1) rad angle, and this road will continue for 1 second, and then the road will be inclined to 0.2 rad angle, and will continue for 1 second, and then the road will be flat again till the end of simulation time.

The simulation results were as follows:

Figure 4.15 Unicycle position with time

Figure 4.16 Link angle behavior with time

Figure 4.17 Nonlinearities effect on motor torque with time

Figure 4.18 Nonlinearities effect on link angle with time

Figure 4.19 Nonlinearities effect on unicycle position with time

The results that can be noticed from the previous figures:

- Zero steady-state error in unicycle position and that is resulted from the nature of the system plant, which is type one (Figure 4.15).
- Very small differences between linear and nonlinear model behavior (Figures 4.17, 4.18, 4.19).
- The observer model behavior is very fast compared to the controlled plant behavior, so the observer effect on the controlled plant is too small, and can be neglected.
- The system model did not exceed the saturation limit of motor torque, so the motor can operate the system in easy way (Figure 4.14).

Chapter Five

Experimental Results of SBU System

Contents:

- Introduction
- Accelerometer Tests and Experiments
- SBU System on Flat Road Experiments
- SBU System on Inclined Road Experiments

5.1 Introduction

As mentioned in chapter one, SBU systems have solid ground in education, since it is used for testing various control theories and techniques, such as:

- PID control.
- State Feedback Control.
- Adaptive Control.
- Non-linear Control.

In which comparisons between these control systems depend on transient response characteristics, disturbance rejection ability, and robustness of these control systems.

Figure 5.1 shows SBU system that is implemented in the lab, this system consists of the mechanical components that construct the structure of the system. In addition to servomotor and the servo driver, and the accelerometer that is used for measuring link's angle and the optical encoder that is used for measuring the rotation angle of the wheels.

Besides that, SBU system composed of interfacing circuits that connect the actuator (servomotor driver) and the sensors with the controller (PC target), since the real-time-controller is implemented using xPC target technique. These interfacing circuits are two Data Acquisition Cards which are NI6024E, and PCI-Quad04.

Figure 5.1 SBU System in the Lab.

For preparing the SBU system for being controlled, there are some considerations and tests which are:

- Fixing an absorber plate between the link and the motor, which is used for suppressing the vibrations that are resulted from the motor movements that will affect the accelerometer readings, and make the accelerometer signal has some peaks in which can be called shocks.
- Increasing the tension force in the belt, so as to protect the system from the internal slippage between the pulleys.
- Using a coarse surface for moving the system to protect the system from the slippage between the surface and the wheels.
- Keeping the high power cables away from low power wires (which carry information signals), to ensure the correctness of the information signals.
- Using a battery for operating the accelerometer, to reduce noise effects resulted from using the power supply in the Lab.
- Fixing the motor cable and sensors wires away from the system, since these wires are not inserted in the model, so it is a disturbance.
- Preparing the servomotor for torque control mode by installing the required parameters to the servo driver, as in appendix F.
- Preparing the connection between the host and target PCs to use xPC target technique, as demonstrated in section 5.4.2
- Modifying the SIMULINK models and making them ready for being converted to a real-time application using MATLAB[®], s real-time workshop, xPC target toolboxes, and C++ compiler.
- Determining the conversion factors to convert the measured quantities from pulses to radians, by using the encoder's resolution (number of pulses per revolution).
- Putting the accelerometer inside a special package, and using non-conducting materials to cover the accelerometer board, so to eliminate noise effects as possible as.
- Executing tests and experiments for the accelerometer, to determine the effectiveness of the accelerometer for measuring the tilt angle of the link, in addition to calibrating it.

In the upcoming sections, state feedback controllers are applied practically for SBU system in the once by using derivatives for acquainting about the velocity states, and two measurement position states. Also, state feedback controllers are applied practically for SBU system by using an extended observer. After that the results where be compared.

But before implementation the controllers, experiments will be executed for determining effectiveness of the accelerometer for measuring the tilt angle of the link, in addition to calibrating it.

5.2 Accelerometer Tests and Experiments

As stated later, accelerometers are used to measure the tilt of an object. Accelerometers can be used for measuring both dynamic and static measurements of acceleration. Tilt is a static measurement where gravity is the acceleration being measured.

The duty for using the accelerometer as a tilt sensor is how the device will be mounted in the end application. This will allow you to achieve the highest degree resolution for a given solution due to the nonlinearity of the technology. First, you need to know what the sensing axis is for the accelerometer. See figure 5.2 to see where the sensing axes are for the MMA7260Q.

Figure5.2 Sensing Axis for the MMA7260Q Accelerometer with X, Y, and Z-Axis for Sensing Acceleration

To obtain the most resolution per degree of change, the accelerometer should be mounted with the sensitive axis parallel to the plane of movement where the most sensitivity is desired.

The typical output of capacitive, micro-machined accelerometers is a sine function. Figure 5.3 shows the analog output voltage from the accelerometer for degrees of tilt from -90° to +90°. The change in degrees of tilt directly corresponds to a change in the acceleration due to a changing component of gravity acted on the accelerometer. 22

Figure5.3 Typical Output of X, Y, and Z-Axis Accelerometers

1

 $x - 2y =$

axia

 2005

Ways for Calculating the Degree of Tilt:

1. Using Lookup Table:

 1 These results are obtained from Freescale Semiconductor Company, and more information in Appendix E

The acceleration is compared to the zero g offset to determine if it is a positive or negative acceleration, e.g., if value is greater than the offset then the acceleration seeing a positive acceleration, so the offset is subtracted from the value and the resulting value is then used with a lookup table to determine the corresponding degree of tilt. If the acceleration is negative, then the value is subtracted from the offset to determine the amount of negative acceleration and then passed to the lookup table.

2. Using Tilt Algorithm:

$$
V_{out} = V_{offset} + \frac{\Delta V}{\Delta g} \times 1.0g \times \sin \varphi \tag{5-1}
$$

 V_{out} : Accelerometer Output in Volts

V_{offset}: Accelerometer 0g Offset

 ΔV , Consitiv Δg : Sensitivity

1.0 q : Earth. s Gravity

: Angle of Tilt

In SBU system, the tilt angle of the link will be calculated by using the second way which is the equation above, see figure 5.4.

X-axis reads 0g, Y-axis reads -1g

X now sees some gravity

X reads slightly positive X reads slightly negative

Figure5.4 Accelerometer as a tilt sensor

For the accelerometer that is used in SBU system, two main experiments will be executed in the Lab. Once for determining the sensitivity of the accelerometer experimentally, and the second for testing the accelerometer effectiveness for the required frequency to the controlled system.

Note: in the previous semester, another experiment was executed for testing the accelerometer effectiveness for the required frequency to the controlled system but this experiment produced bad results. (We can talk about this in the discussion)

Determining the sensitivity of the accelerometer:

In this experiment, we used a protractor, and joined the accelerometer with this protractor (see figure 5.5). By turning the accelerometer clockwise, and counterclockwise and recording the voltage at each time, the sensitivity gain was computed as follows:

$$
V_{offset} = V_{zero \ degree} = 1.2 \nu \quad \text{for } Y - axis
$$
\n
$$
V_{ten \ degree \ clockwise} = 1.3180 \nu
$$

And by using equation $5 - 1$, this will produce $\frac{\Delta V}{\Delta \theta} = 0.67$ $\overline{\Delta g} = 0.6797$

Figure5.5 Calculating the sensitivity gain for the accelerometer in the Lab.
- Testing the accelerometer effectiveness for the required frequency to the controlled system:

For the closed loop of SBU system, the dominant poles are selected at $-1 \pm j$ and that means that the natural frequency of the system is 1.4142 rad/sec = 0.2251 Hz.

As mentioned in chapter three that the accelerometer has a bandwidth response of 350 Hz = 2200 rad/sec. For SBU system that is really too enough, but this experiment is to check *experimentally* the effectiveness of the accelerometer in SBU system.

In this experiment, we used a compound pendulum that is connected with a revolute joint, and fixed the accelerometer at this pendulum (see figure 5.6). Rotating the pendulum clockwise and counterclockwise by hand, yielded the results in figure 5.7.

Figure5.6 Checking the frequency of the accelerometer in the Lab.

From figure 5.7, we note that the frequency that can be reached by this experiment is approximately 2Hz, and for SBU system this is really enough, since the required frequency as discussed above is 0.2251Hz.

Note: In figure 5.7, also we can notice that the accelerometer signal is nearly pure, and this because of using the analog filters (hardware filters, and software filters).

Figure5.7 Accelerometer Response in the experiment

5.3 SBU System on Flat Road Experiments

In this section the robust tracking and disturbance rejection controller designed in Chapter Four, is applied practically to the SBU system on flat road. But the change is using an extended observer instead of an observer. Using the extended observer will give true information about the states of the system, in addition to compensate the disturbance and nonlinearities effects.

The change of using the controller that is discussed in Chapter Four and the application in this experiment, is the gain values that are related to the poles locations, which are selected to be much smaller than those used in Chapter Four. The problem with applying high gains to the real system is the unmodeled dynamics of the cable, which cause some oscillations. In addition to that, high gains will cause some problem from noise effects in the Lab.

To avoid the problems mentioned above, lower gains will be used, although these gains will affect on the stability and transient response of the controlled system.

Control system gains and poles are as follows:

- Poles: $-1 j$ $-1 + j$ -3 -3.1
- Gains of feedback matrix: $-0.0115 -1.9541 -0.0191 -0.1344$

The following figures show the input torque, wheel angle of rotation, and tilt angle of the link which are obtained from the controller applied to the SBU system on flat road. It must be noted that there is a dead zone conception which is used for the tilt angle signal. These figures are obtained for a regulation control system only.

Figure5.8 Input Torque

Figure5.9 Wheel angle

Based on the previous figures, it is clear that the controller managed to **Figure5.10** Tilt Anglestabilize the link at the inverted position, and also stabilize the wheels at the zero

position. The main problems encountered during controlling the SBU system can be summarized as follows:

- 1. There is a steady state error can be noticed in input torque, and wheel angle, and this is resulted from mounting the accelerometer on the link.
- 2. The cable of the servomotor, its encoder, and the accelerometer represent a continuous disturbance to the control system
- 3. Using the low pass filters for estimating the true signal from the accelerometer will result some delay, where the amount of delay is inversely proportional to the filter's cutoff frequency.
- 4. The errors caused by using the extended observer are parameters uncertainty, initial conditions effects.
- 5. The estimated disturbance from the extended observer is not shown here, since it doesn't make sense, because of Lab. Noise.
- 6. The static compensation of the disturbance was not used here, since this increased the control efforts. The disturbance rejection can be accomplished depending on the robustness of the control system.

5.4 SBU System on Inclined Road Experiments

In this section the robust tracking and disturbance rejection controller designed in Chapter Four, is applied practically to the SBU system on inclined road. But the change is using an extended observer instead of an observer. Using the extended observer will give true information about the states of the system, in addition to compensate the disturbance and nonlinearities effects.

Also, lower gains will be used for this system, although these gains will affect on the stability and transient response of the controlled system.

Control system gains and poles are as follows:

- Poles: $-1 j$ $-1 + j$ -3 -3.1
- Gains of feedback matrix: $-0.0115 -1.9541 -0.0191 -0.1344$

The following figures show the input torque, wheel angle of rotation, and tilt angle of the link which are obtained from the controller applied to the SBU system on flat road. It must be noted that there is a dead zone conception which is used for the tilt angle signal. These figures are obtained for a tracking control system only, in which there is a nail in the road.

Figure5.13 Tilt Angle

Based on the previous figures, it is clear that the controller managed to stabilize the link at the inverted position, and also track the wheels at the desired position. The main results obtained during controlling the SBU on system can be summarized as follows:

- 1. It must be noted that the control system succeeded in passing over a road with some miscellanies (such as nails).
- 2. These results are obtained without applying a static compensation for the disturbances, but only depending on the robustness of the control system.
- 3. All the problems that mentioned in Section 5.3 can be repeated here.

Chapter Six

Conclusions and Recommendations for Future Works

Contents:

- Considerations and Conclusions
- Recommendations for Future Work
- Problems Encountered

6.1 Considerations and Conclusions

In this project, Self-Balancing Unicycle System (SBU) is implemented, tested and controlled. The results related to mechanical structure, electrical and computer interfacing components, control theory, and all other related techniques are obtained.

Beginning with the mechanical structure of the system, there are many considerations. Usually, these considerations are validated to make the system ready for being controlled. These considerations consternate on making the system close as possible to the mathematical model, which is derived in Chapter Two. In this model, no slippage between the ground and the wheels, and no slippage between the pulleys and the belt, since these slippages cannot be measured. So, this means that the wheels are always in contact with the ground. And there are other considerations which are discussed in Chapter five.

Related to electrical and computer interfacing components, there are some significant modifications which operates the servomotor in torque control mode, since the dynamic of the servomotor is not considered in the model of the system. Also, some interfacing circuits are required to increase the protection of some components from overload fluctuating. Such as NI 6024E that is used in SBU system with isolation circuit, at the channel that generates the torque command signal.

Also, for servo driver in SBU system, noise filter is used to minimize the effect of noise and harmonic voltages in the main power lines.

The accelerometer in SBU system cannot be used alone without some analog filters. These filters are usually low-pass filters, in which cutoff frequency is tuned upon speed requirements and filters effectiveness for noise immunity.

In order to measure the unicycle position by measuring the wheel rotation, incremental encoder is installed with special data acquisition card (PCI-QUAD04) that is provided by Measurement Computing.

Testing and calibrating the accelerometer through some experiments that are discussed in Chapter Five will produce information about the effectiveness of this sensor to be used inside control loop, and its bandwidth response.

State feedback control theories are then applied and tested in SBU system. In which these control systems are designed based on linearzed mathematical model, for nonlinear systems, this will produce some errors in control systems. But for systems such as SBU system without highly nonlinear effects, linear control systems can operate well and give useful results.

For SBU system experimentation, the results produced by using derivatives for estimating the velocities compared with the results produced by using extended observer. After comparison the results produced by using extended observer is more accurate than using derivatives, and this can be explained by the quantity of information that can be extracted about the signals than derivatives.

By using extended observer for SBU system, other information can be extracted as the disturbances, and noise (white noise). This will permit for disturbance compensation.

xPC target package that is already available in MATLAB is used in SBU system, for logging data from real-time applications, and also sending data to real time applications. For that, this technique has a wide range in real-time controllers as used in SBU system. Using this technique facilitate noticing the results on line from the users, and modifying the parameter of the model, without need to rebuild again.

6.2 Recommendations for Future Work

Further improvements on SBU system can be accomplished through acquisition true estimation for the tilt angle of the link. Accelerometer is not enough for having true estimation for the tilt angle, since accelerometers usually used for low- frequency range. This is because of the tilt angle is extracted only from the gravity vector resulted from the accelerometer, and using the dynamic acceleration is not recommended using the accelerometer. And using the integration through estimating the tilt angle by using accelerometer has some problems, resulted from the accumulative nature of the integration.

The recommended way for estimating the true angle of tilt can be achieved, by using also the gyroscope. This will enable the system to estimate the tilt angle at any frequency, and also true estimation is done.

This merging between the accelerometer and the gyroscope for estimating the tilt angle can be accomplished as shown in figure 6.1.

Figure 6.1 Recommended Approach for using Accelerometer and Gyroscope for estimating tilt angle.

6.3 Problems Encountered

The main problem that encountered in SBU system is estimating the true angle of tilt from accelerometer as discussed above.

Other problem is the unmodeled cable dynamics, which causes a continuous disturbance. This problem can be solved through using wireless DAQ, battery with interfacing circuit for the servomotor.

The noise signals is another problem in the Lab. that caused wrong measurements of the tilt angle, in addition to servomotor vibrations. The noise signals in the lab. are not white noise, that can be solved by Kalman Filter.

* This approach was used from students in MIT as a graduation project, and it produced good results, for more information http://web.mit.edu/first/segway

Appendix A

Inclined Road Implementation

The examination of the SBU system on an inclined road in the lab is unattainable so we have built a system for this purpose, which is consisting of two plates with a motor.

The two plates are made from strengthened wax, dimension of the first plate is (50×50) cm, and the other one is (50×47) cm, which are strong enough for holding the SBU system, they are connected by two revolute joints where a servomotor can be position controlled.

The servomotor which drives the two plates is a DC motor with an encoder for position, and has the following features:

The encoder characteristics:

DIY Segway Technical Documentation

Rev. 0, 8/23/2007

Note/Warning/Disclaimer: Segways, like any large machines, can be dangerous if appropriate safety precautions are not observed. DIY Segways, including this one, are *particularly* dangerous because they often lack the redundant safety features of commercial Segways. This technical documentation is intended for informational, not instructional, purposes. Attempt/build at your own risk!

Overview

Building a DIY Segway-like scooter was an incredibly fun project, and we would like to share the experience with others in as much detail as possible. The intention of the technical documentation is not to provide step-by-step instructions on how to build this particular machine, but to share some of the resources that made it possible. Hopefully, others will find these resources useful in their own projects, self-balancing or otherwise. If you have further questions or comments about our project, please contact:

seg-info@mit.edu

Files

In **segspecs.zip**, you can find the following files:

- **segspecs.pdf**: This document.
- **BOM.pdf**: Bill of materials, including supplier and vendor information.
- **PCB.zip**: PCB manufacturing files, in gerber format.
- **CAD.zip**: All of the SolidWorks files, plus a few .dxf files of the base plate waterjet cut.
- **SegwayDash.zip**: The custom VB dashboard source (used for wireless debugging).
- **controller.pdf**: Some more visual notes on the custom controller.
- **filter.pdf**: A detailed explanation of the digital filter we used to estimate angle from sensors.
- **segwaycode.c**: The actual code implemented on the PIC microcontroller for control.

Quick Specifications:

Overall Footprint: 27"x15" **Wheel Diameter:** 12.5" **Ground Clearance:** 5" **Weight:** 52 lbs. with battery, 39 lbs. without **Rider Capacity:** 250 lbs. **Peak Motor Power:** 343 W (0.46 HP) each **Peak Motor Torque:** 2.45 N-m (347 ozf-in) each **Max. Continuous Motor Current:** 40 A each **Gear ratio:** 16:1 **Theoretical Top Speed:** 5 m/s (11 MPH) **Software-Limited Top Speed:** ~3 m/s (~7 MPH) **Battery:** 12V Sealed Lead-Acid, 18 A-hr **Normal-Usage Battery Life: ~**45-60 min **Controller Update Rate:** 100 Hz **Telemetry Transmit Rate:** 15 Hz **Telemetry Transmit Range:** 300 ft **Total Materials Cost:** <\$1,000 **Number of Cup Holders:** 2

Base Plate Design and Fabrication

The base plate is really the key to much of the mechanical construction of our machine. All of the tricky alignment of motors, gearboxes, and bearings was consolidated onto one piece to be precisely machined. The base is made from $\frac{1}{4}$ -thick 6061 aluminum plate (vendor: McMaster Carr¹). It has been pointed out to use several times that there are much cheaper alternative materials and/or vendors. One easy and inexpensive alternative is Big Blue Saw², which offers waterjet cutting straight from CAD files and has reasonable prices which include material costs. They offer a wide range of materials and thicknesses, as well. (Clear polycarbonate base, anyone?) The plate itself contributes only partially to the rigidity of the base. Most of the strength comes from two 1"x1"x1/8" aluminum box extrusion cross-beams. Placing the bearings as close as possible to the edge of the base ensures that the load is carried directly from the wheels into these two cross beams without causing significant deflection of the drive shaft or motors.

The base plate was collaboratively designed in SolidWorks³ and cut on the waterjet at the MIT Hobby Shop⁴. Holes for mounting the motors, bearings, handlebar, electronics, and cross-beams were included, as well as the now-famous cup holders. It weighs approximately 7 lbs. A .dxf file of the plate is available in **CAD.zip**.

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Motors and Gearboxes

Picking motors was one of the first things we did. After briefly considering larger, more powerfully $24V$ NPC⁵ motors such as those used on Trevor Blackwell's inspirational design $⁶$, we chose</sup> to use the familiar and inexpensive 12V CIM motors provided in the FIRST Robotics kit of parts. At just under $\frac{1}{2}$ HP peak output each, they were a compromise that we thought would work okay with our lightweight design. They also offered the advantage of being compatible with a compact 16:1 in-line planetary gearbox (vendor: BaneBots⁷).

BaneBots also sells a two-motor adaptor for this gearbox, creating potential for a design with twice the power. Backlash in the gearbox is noticeable, but it is less than five degrees. Note that these gearboxes have some well-known assembly quirks, particularly the axial alignment of the motor pinion gear, so read the BaneBots documentation carefully.

Coupling, Axle, and Bearings

Our original design called for a flexible coupling between the 1/2" gearbox shaft and the 5/8" drive shaft, to allow for misalignment and minimize shock loading on the gears. The problem we encountered with this design was that in order to accommodate two bearings, spaced out enough to support the drive shaft, our total width would be

http://www.mcmaster.com

² http://www.bigbluesaw.com

³ http://solidworks.com/pages/products/edu/studenteditionsoft ware.html

⁴ http://hobbyshop.mit.edu

⁵ http://www.npcrobotics.com

⁶ http://www.tlb.org/scooter.html

⁷ http://www.banebots.com

over 32". Besides looking somewhat ridiculous, this would cause problems getting through doors.

We pretty quickly decided to give up on the flexible coupling in order to get the width under 30". With a rigid coupling between the gearbox and the drive shaft, the bearing on the gearbox provides a second point of support for the rigidly-coupled shafts. Quick calculations indicated that with a 5/8" steel keyed drive shaft and bearing placed as close to the edge of the base as possible, there was enough support in the system so that the gearbox would not be damaged by deflection of the shaft. (We've also seen these gearboxes survive under much less adequate constraints on FIRST robots.)

We did not know how the rigid coupling would affect alignment and shock loading transmitted to the gearbox. We bought some shim stock in case the alignment was a problem, but wound up not using it. As for shock loading, we'll have to wait and see how well the carrier plates inside the gearbox hold up. So far, they seem okay.

One major design oversight was the fact that the motor actually sticks out a bit further than the edge of the gearbox. We had to shim up the gearbox and bearings with sheet metal to allow for this, although it could easily have been avoided by cutting a slot or milling a pocket on the base plate for the motor to rest in.

Wheels

Based on our motor torque/speed characteristics, we needed to use relatively small wheels to get adequate performance. We chose 12.5" pneumatic wheels made by Skyway⁸ because they were inexpensive, light, and had the 5/8" keyed hub we needed. Skyway has been a long-time supplier for FIRST teams and offers special pricing for them.

Handlebar

The handlebar was supposed to be the easy part…until the decision to go for lean steering. Aside from that part, it is just a piece of $80/20^9$ 1"x2" extrusion. This stuff is great because it allows easy adjustment via sliding t-nuts, making height and angle modifications simple. We cut a few custom brackets for it on the waterjet out of the leftover aluminum from the base plate (see CAD files).

As for the lean-steering joint, we went through a bunch of iterations, including one with a combination of compression and tension springs that sounded like an old Buick suspension. The current design uses four strips of ¼" polycarbonate as leaf springs to center the steering joint. The forward/backward rigidity of the joint is workable, but not great and is something to look at for future modification.

⁸ http://www.skywaytuffwheels.com

 $9 \overline{\text{http://www.8020.net}}$

Battery and Power Electronics

All of the power electronics on our machine are FIRST-legal kit components. The power source is a 12V, 18 A-h sealed lead-acid motorcycle battery that weighs 13 lbs. It is connected to a 120A main breaker with 6-gauge wire, then to a distribution block. Each motor line has a 40A circuit breaker. The controller also has a 40A breaker, but it is also protected by a 1A thermal polyswitch. The grounds are grouped together in the remaining slot of the distribution block. (Notice the aluminum ground jumper? Not the most elegant solution, but it works.) The chassis is *not* grounded.

The motor controllers are the reliable Innovation First¹⁰ Victor 884 model found in the FIRST kit. Aside from being virtually indestructible (they have survived being rained on), they can supply 40A continuous and much higher peak currents without ever getting hot thanks to fans directly cooling the MOSFETs. They are driven by

1-2ms PWM signals, the same signal used by RC servos. These signals are easily generated by the PIC controller. The speed controllers can be updated at up to 100Hz.

Sensors, Signal Electronics, and Controller

We made use of three sensors: a gyroscope and an accelerometer for balancing, and a second accelerometer for steering. Unlike the commercial Segway, ours has no redundant sensors – you pretty much need all three to be working correctly for it to be rideable.

The sensors are all from the Analog Devices¹¹ iMEMS line (see B.O.M.). They report an analog voltage between 0V and 5V to the controller, with neutral angle or zero rate being near 2.5V, although each requires some calibration with regards to the exact offset. The gyroscope is used simply to measure angular rate. The accelerometer is used to indirectly measure the direction of the force of gravity, since it is really sensing force per unit mass along a given axis. This, along with a small angle approximation, gives an estimate of the angle to horizontal.

The controller is based on the PIC16F877 board of the Machine Science¹² starter kit. It is protected by a 1A thermal polyswitch, a diode to prevent reversing polarity, and a large filter capacitor before the 5V regulator (LM7805). The PCB was drawn out it out in a freeware program called Free $PCB¹³$ and manufactured by Advanced

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¹¹ http://www.analog.com
¹² http://www.machinescience.org
¹³ http://www.freepcb.com

¹⁰ http://www.ifirobotics.com

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Circuits¹⁴, which has an excellent student discount of \$33/board. The PCB layout and Gerber files are available in **PCB.zip**.

The CPU clock for the PIC is generated by a 4 MHz oscillator. (Compare this to 4 GHz Pentiums…) The actual instruction and timer clock is $\frac{1}{4}$ of that, 1 MHz. This is relatively slow even for a microcontroller, and in a future upgrade we plan to move to a faster microprocessor. But even with the current setup and a good amount of floatingpoint control math, we can keep our control loop running at 100 Hz.

One thing we think is fairly unique about our controller is that its interface is *entirely* wireless. It can be reprogrammed without attaching any cables to the Segway and can transmit data from the sensors or controller to a laptop for debugging. This is all done via MaxStream15's XBee radios. In a future mod, it might even be capable of wireless self-balancing control with no rider.

Signal Filtering

There are a number of problems with using direct sensor data for control. For one, with two half-horsepower electric motors on the same power and ground line as the controller, there is bound to be noise in the system even with a 6800μF power supply filter capacitor for the controller.

There are also physical reasons why the data from the accelerometers and gyroscope has to be filtered. The accelerometers measure a change in angle by the component of the force of gravity along their sensitive axis (horizontal). But they also report other horizontal accelerations from the motors or, in the case of steering, wiggling of the handlebar. The gyroscope measures angular rate and can be used to estimate angle by integration, multiplying the rate by the small time step to get the small change in angle each time through the program loop. But this method can lead to drift: the angle changes slowly over time if the sensor is not perfectly zeroed (which it never is).

For the steering, we implemented the simple hardware solution of adding capacitance to the output filter of the accelerometer, creating a "lowpass filter" that smoothes out short periods of acceleration and lets through only the long term effects of gravity. The ADXL203 data sheet explains how to do this. We've been experimenting with capacitors in the 4.7-10μF range.

For the balance controller, though, this method would cause too much lag in the angle estimate. Most self-balancing robot / homemade Segway sites refer to some kind of digital filter which combines the accelerometer and gyroscope data to get a clean, fast angle estimate. The Kalman Filter is often offered as a possibility, although nobody ever seems to take the time to explain it. (And for good reason: It is mathematically complicated and would not run on a PIC.) Our solution is a much simpler software filter that we are just going to call a "digital complementary filter" for lack of any known technical reference to it. It is actually the same as the filter implemented in the Balancing Robot Wheeley¹⁶ project.

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¹⁴ http://www.4pcb.com
¹⁵ http://www.maxstream.net

"After a lot of trials and calibration the performance of the Kalman filter was not satisfying. I developed another simple filter again on trial and error."

-Balancing Robot Wheeley page

Although it is fairly simple to explain, we will leave it out of this document and instead point you to **filter.pdf** for a more colorful explanation.

Balance Control

For all the controller setup (timers, wireless communication, etc.) and signal conditioning, the actual balance control is a fairly short bit of code:

motor $+=$ (KP * angle) + (KD * (float)gz_vel);

It's a "PD" controller, standing for Proportional + Derivative. The motor output is scaled proportionally to the (filtered) angle estimate and its derivative, the angular velocity measurement. Using the angle alone would have a similar effect, but with more oscillations. This of it this way: The angle term provides a spring-like effect $(F = kx)$ restoring the base to the horizontal position, while the angular velocity term is more like a damper. There are a lot of great references¹⁷ available on PID control theory.

There is more to be done after the simple PD controller, some of which we've gotten to and some of which we are still working on. For one, steering must be taken into account. This is done simply by adding an offset to one motor and subtracting it from the other. Also, motor values must be limited so as not to overflow their variable types or exceed the limits of the motor controllers.

One major piece of control that we have yet to add to our code is the speed limiter. Ideally, the controller should push back harder if you try to lean forward/backwards at high speed, to prevent you from getting into a condition where the motors can no longer catch up to you. Testing this bit is difficult, so we've put it off so far and worked only at low speeds. **Do not try to take a DIY Segway up to high speeds without a helmet/pads/etc. because you are almost guaranteed to fall off.** Best to think of it as an extreme sport…

The current controller code, with comments, is in this zip: **segwaycode.c**.

Design Notes

If you've made it this far through the documentation, you deserve a nice summary of what worked and what still needs work on this project. This way, when you are working on your own project, you can learn from our successes and not-so-successes. So, in no particular order, things that worked really well:

- The base. It is light, but wonderfully rigid and easily supports the load of the rider *jumping* on, even with the simpler onebearing setup. The cross-beams take all of the weight and the bearing/gearbox alignment stays true. Designing it in SolidWorks and machining it on the waterjet paid off big time.
- The sensors. Yes, they are noisy analog sensors. But with some signal conditioning, they absolutely work. They are also tiny and dirt cheap now. We had an ADIS16350 digital IMU, but decided not to use it because these are far simpler.
- The XBee radios. These things are so easy to use and cut debugging time in half, easily.
- The Victor884 speed controllers. After an hour of riding, the motors get pretty hot, but the speed controllers are always cool to the touch. They are incredibly efficient and robust. Only minor issue is the dead band, but we accommodate for that in software.

¹⁷ http://www.chiefdelphi.com/media/papers/1823

http://www.chiefdelphi.com/media/papers/1911

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And things that could be better:

- The motors. They may be just a bit underpowered for this type of application. For normal operation on flat surfaces, they work great. Speed bumps, turning on rough terrain, etc, not as well. But they are consistent with the lightweight, compact design and serve their purpose.
- The microcontroller. The Machine Science online IDE is excellent, but we are eager to move from the PIC to their new development environment for the Atmel AVR line. These have more code space and are significantly faster (and cheaper).
- Steering. A combination of mechanical and control problems still need to be worked out. We got the kinks out of the joint, finally, but are still working on getting the steering to be smooth and controlled at any speed. The dead band on the motor drivers makes turning while coasting a somewhat involuntary adventure, but that should be fixable in software.

Wrap-Up

This was a great project and we think proves that even seemingly complicated technology is within reach for high school-level engineering projects. We're not suggesting that everyone go out and build a Segway (although wouldn't that be interesting), but the technologies we used can be applied to any number of cool projects that we can't wait to see.

Appendix C

M-FILE code

```
%% Control System Design
mw=0.8060;
mp=1.998;
Jw=0.0081;
Jp=0.01100788;
R=0.145;l=0;r=R+(1/(2*pi));
l1=0.1258509705;
12=0.28;
dwp=5.8000e-005;
%dwp=0.0012;
dm=5.8e-009;
%dm=5.8e-005;
g=9.81;n=1;
[M] = [ (mw * r^2 + mp * r^2 + Jw) mp * r * 11; mp * r * 11 (mp * 11^2 + Jp) ];[d] = [ (dwp) 0:0 -1*dwp];[K]=[0 \ 0:0 \ -1*mp*q*11];[b]=[1;-1];[bd] = [-1*r;-1*12];[bn] = [0; -1];zero=[0 0;0 0];
I=[1 0; 0 1];A = [zero I; -1 * inv([M]) * [K] -1 * inv([M]) * [d]];B = [0;0;inv([M]) * [b]];Bd=[0;0;inv([M])*[bd]];Bn=[0:0,inv(M)*(bn)];Btot=[B Bd Bn];
Cm=[1 0 0 0;0 1 0 0];
```

```
C=[1 0 0 0];N=[Bd \; Bn];
Ae=[A N:zeros(2,4) zeros(2,2)];
Be=[B;0;0];Ce = [Cm \text{ zeros}(2,1) \text{ zeros}(2,1)];
~8p=[-0.5+0.5*1 -0.5-0.5*1 -2.5 -2.6];~8p=[-3+3*1 -3-3*1 -6 -7.5];
%k=place(A,B,p);
a1=mw*r^2+mp*r^2+Jw;
a2=mp*11^2+Jp;
```

```
%% Observer Design
\text{poles}=10*(-7 -10 -4 -3];%L=place(A',Cm',poles)';
Q=[0 0 0 12.0900 0 0]';
T=[1 0 0 0 0 0;0 1 0 0 0 0;0 0 2 0 0 0;1 10 100 1000
10000 100000;0 1 20 300 4000 50000;0 0 2 60 1200 20000];
ftrack=inv(T)*Q;
f0=ftrack(1);
f1=ftrack(2);
f2=ftrack(3);f3=ftrack(4);f4=ftrack(5);f5=ftrack(6);ts = 0.01;Qe=[1000 0 0 0 0 0;0 10000 0 0 0 0;0 0 1000 0 0 0;0 0 0
1000 0 0;0 0 0 0 10^9 0;0 0 0 0 0 10^9];
Re=[1 0; 0 1];Le=lqr(Ae',Ce',Qe,Re)';
k=place(A,B,[-1+i,-1-i,-3,-3.1]);
k1=k(1);k(1)=0;kn1=0.1471;
kn2=0.6873;
```
±**1.5g - 6g Three Axis Low-g Micromachined Accelerometer**

The MMA7260Q low cost capacitive micromachined accelerometer features signal conditioning, a 1-pole low pass filter, temperature compensation and g-Select which allows for the selection among 4 sensitivities. Zero-g offset full scale span and filter cut-off are factory set and require no external devices. Includes a Sleep Mode that makes it ideal for handheld battery powered electronics.

Features

- Selectable Sensitivity (1.5g/2g/4g/6g)
- Low Current Consumption: 500 µA
- Sleep Mode: 3 µA
- Low Voltage Operation: 2.2 V $-$ 3.6 V
- 6mm x 6mm x 1.45mm QFN
- High Sensitivity (800 mV/g @1.5 g)
- Fast Turn On Time
- High Sensitivity (1.5 g)
- Integral Signal Conditioning with Low Pass Filter
- Robust Design, High Shocks Survivability
- Pb-Free Terminations
- Environmentally Preferred Package
- Low Cost

Typical Applications

- HDD MP3 Player : Freefall Detection
- Laptop PC : Freefall Detection, Anti-Theft
- Cell Phone : Image Stability, Text Scroll, Motion Dialing, E-Compass
- Pedometer : Motion Sensing
- PDA : Text Scroll
- Navigation and Dead Reckoning : E-Compass Tilt Compensation
- Gaming : Tilt and Motion Sensing, Event Recorder
- Robotics : Motion Sensing

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Figure 2. Simplified Accelerometer Functional Block Diagram

Table 1. Maximum Ratings

(Maximum ratings are the limits to which the device can be exposed without causing permanent damage.)

1. Dropped onto concrete surface from any axis.

ELECTRO STATIC DISCHARGE (ESD)

WARNING: This device is sensitive to electrostatic discharge.

Although the Freescale accelerometer contains internal 2000 V ESD protection circuitry, extra precaution must be taken by the user to protect the chip from ESD. A charge of over 2000 volts can accumulate on the human body or associated test equipment. A charge of this magnitude can

alter the performance or cause failure of the chip. When handling the accelerometer, proper ESD precautions should be followed to avoid exposing the device to discharges which may be detrimental to its performance.

Table 2. Operating Characteristics

Unless otherwise noted: $-20^{\circ}C \leq T_A \leq 85^{\circ}C$, 2.2 V \leq V_{DD} \leq 3.6 V, Acceleration = 0g, Loaded output⁽¹⁾

1. For a loaded output, the measurements are observed after an RC filter consisting of a 1.0 kΩ resistor and a 0.1 µF capacitor to ground.

2. These limits define the range of operation for which the part will meet specification.

3. Within the supply range of 2.2 and 3.6 V, the device operates as a fully calibrated linear accelerometer. Beyond these supply limits the device may operate as a linear device but is not guaranteed to be in calibration.

4. This value is measured with g-Select in 1.5g mode.

5. The device can measure both + and - acceleration. With no input acceleration the output is at midsupply. For positive acceleration the output will increase above $V_{DD}/2$. For negative acceleration, the output will decrease below $V_{DD}/2$.

6. The response time between 10% of full scale Vdd input voltage and 90% of the final operating output voltage.

7. The response time between 10% of full scale Sleep Mode input voltage and 90% of the final operating output voltage.

8. A measure of the device's ability to reject an acceleration applied 90° from the true axis of sensitivity.

PRINCIPLE OF OPERATION

The Freescale accelerometer is a surface-micromachined integrated-circuit accelerometer.

The device consists of two surface micromachined capacitive sensing cells (g-cell) and a signal conditioning ASIC contained in a single integrated circuit package. The sensing elements are sealed hermetically at the wafer level using a bulk micromachined cap wafer.

The g-cell is a mechanical structure formed from semiconductor materials (polysilicon) using semiconductor processes (masking and etching). It can be modeled as a set of beams attached to a movable central mass that move between fixed beams. The movable beams can be deflected from their rest position by subjecting the system to an acceleration (Figure 3) .

As the beams attached to the central mass move, the distance from them to the fixed beams on one side will increase by the same amount that the distance to the fixed beams on the other side decreases. The change in distance is a measure of acceleration.

The g-cell beams form two back-to-back capacitors (Figure 3). As the center beam moves with acceleration, the distance between the beams changes and each capacitor's value will change, $(C = A\varepsilon/D)$. Where A is the area of the beam, ε is the dielectric constant, and D is the distance between the beams.

The ASIC uses switched capacitor techniques to measure the g-cell capacitors and extract the acceleration data from the difference between the two capacitors. The ASIC also signal conditions and filters (switched capacitor) the signal, providing a high level output voltage that is ratiometric and proportional to acceleration.

Figure 3. Simplified Transducer Physical Model

SPECIAL FEATURES

g-Select

The g-Select feature allows for the selection among 4 sensitivities present in the device. Depending on the logic input placed on pins 1 and 2, the device internal gain will be changed allowing it to function with a 1.5g, 2g, 4g, or 6g sensitivity (Table 3). This feature is ideal when a product has applications requiring different sensitivities for optimum performance. The sensitivity can be changed at anytime during the operation of the product. The g-Select1 and g-Select2 pins can be left unconnected for applications requiring only a 1.5g sensitivity as the device has an internal pulldown to keep it at that sensitivity (800mV/g).

Sleep Mode

The 3 axis accelerometer provides a Sleep Mode that is ideal for battery operated products. When Sleep Mode is active, the device outputs are turned off, providing significant reduction of operating current. A low input signal on pin 12 (Sleep Mode) will place the device in this mode and reduce the current to 3uA typ. For lower power consumption, it is recommended to set g-Select1 and g-Select2 to 1.5g mode. By placing a high input signal on pin 12, the device will resume to normal mode of operation.

Filtering

The 3 axis accelerometer contains onboard single-pole switched capacitor filters. Because the filter is realized using switched capacitor techniques, there is no requirement for external passive components (resistors and capacitors) to set the cut-off frequency.

Ratiometricity

Ratiometricity simply means the output offset voltage and sensitivity will scale linearly with applied supply voltage. That is, as supply voltage is increased, the sensitivity and offset increase linearly; as supply voltage decreases, offset and sensitivity decrease linearly. This is a key feature when interfacing to a microcontroller or an A/D converter because it provides system level cancellation of supply induced errors in the analog to digital conversion process.

BASIC CONNECTIONS

Pin Descriptions

Table 4. Pin Descriptions

PCB Layout

Figure 6. Recommended PCB Layout for Interfacing Accelerometer to Microcontroller

NOTES:

- 1. Use 0.1 μ F capacitor on V_{DD} to decouple the power source.
- 2. Physical coupling distance of the accelerometer to the microcontroller should be minimal.
- 3. Flag underneath package is connected to ground.
- 4. Place a ground plane beneath the accelerometer to reduce noise, the ground plane should be attached to all of the open ended terminals shown in Figure 6.
- 5. Use an RC filter with 1.0 k Ω and 0.1 µF on the outputs of the accelerometer to minimize clock noise (from the switched capacitor filter circuit).
- 6. PCB layout of power and ground should not couple power supply noise.
- 7. Accelerometer and microcontroller should not be a high current path.
- 8. A/D sampling rate and any external power supply switching frequency should be selected such that they do not interfere with the internal accelerometer sampling frequency (11 kHz for the sampling frequency). This will prevent aliasing errors.

MMA7260Q

MINIMUM RECOMMENDED FOOTPRINT FOR SURFACE MOUNTED APPLICATIONS

Surface mount board layout is a critical portion of the total design. The footprint for the surface mount packages must be the correct size to ensure proper solder connection interface between the board and the package.

With the correct footprint, the packages will self-align when subjected to a solder reflow process. It is always recommended to design boards with a solder mask layer to avoid bridging and shorting between solder pads.

PACKAGE DIMENSIONS

MMA7260Q

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Measuring Tilt with Low-g Accelerometers

by: Michelle Clifford and Leticia Gomez Sensor Products, Tempe, AZ

INTRODUCTION

This application note describes how accelerometers are used to measure the tilt of an object. Accelerometers can be used for measuring both dynamic and static measurements of acceleration. Tilt is a static measurement where gravity is the acceleration being measured. Therefore, to achieve the highest degree resolution of a tilt measurement, a low-g, highsensitivity accelerometer is required. The Freescale MMA6200Q and MMA7260Q series accelerometers are good solutions for XY and XYZ tilt sensing. These devices provide a sensitivity of 800 mV/g in 3.3 V applications. The MMA2260D and MMA1260D are also good solutions for 5 V applications providing a sensitivity of 1200mV/g for X and Z, respectively. All of these accelerometers will experience acceleration in the range of +1g to -1g as the device is tilted from -90 degrees to +90 degrees.

 $1g = 9.8$ m/s

MODULE

A simple tilt application can be implemented using an 8 or 10-bit microcontroller that has 1 or 2 ADC channels to input the analog output voltage of the accelerometers and general purpose I/O pins for displaying the degrees either on a PC through a communication protocol or on an LCD. See Figure 1 for a typical block diagram. Some applications may not require a display at all. These applications may only require an I/O channel to send a signal for turning on or off a device at a determined angle range.

Figure 1. Typical Tilt Application Block Diagram

MOUNTING CONSIDERATIONS

Device selection depends on the angle of reference and how the device will be mounted in the end application. This will allow you to achieve the highest degree resolution for a given solution due to the nonlinearity of the technology. First, you need to know what the sensing axis is for the accelerometer. See Figure 2 to see where the sensing axes are for the

MMA7260Q. To obtain the most resolution per degree of change, the IC should be mounted with the sensitive axis parallel to the plane of movement where the most sensitivity is desired. For example, if the degree range that an application will be measuring is only 0° to 45° and the PCB will be mounted perpendicular to gravity, then an X-Axis device

would be the best solution. If the degree range was 0° to 45° and the PCB will be mounted perpendicular to gravity, then a Z-Axis device would be the best solution. This is understood more when thinking about the output response signal of the device and the nonlinearity.

MMA7260Q Accelerometer With X, Y, and Z-Axis for Sensing Acceleration

Tilted X-Axis Accelerometer

Tilted Z-Axis Accelerometer

NONLINEARITY

As seen in Figure 5, the typical output of capacitive, micromachined accelerometers is more like a sine function. The figure shows the analog output voltage from the accelerometer for degrees of tilt from -90° to +90°. The change in degrees of tilt directly corresponds to a change in the acceleration due to a changing component of gravity acted on the accelerometer. The slope of the curve is actually the sensitivity of the device.

As the device is tilted from 0°, the sensitivity decreases. You see this in the graph as the slope of output voltage decreases for an increasing tilt towards 90°. Because of this nonlinearity, the degree resolution of the application must be determined at 0° and 90° to ensure the lowest resolution is still within the required application resolution. This will be explained more in the following section.

CALCULATING DEGREE OF TILT

In order to determine the angle of tilt, θ, the A/D values from the accelerometer are sampled by the ADC channel on the microcontroller. The acceleration is compared to the zero g offset to determine if it is a positive or negative acceleration, e.g., if value is greater than the offset then the acceleration is seeing a positive acceleration, so the offset is subtracted from the value and the resulting value is then used with a lookup table to determine the corresponding degree of tilt (See Table1 for a typical 8-bit lookup table), or the value is passed to a tilt algorithm. If the acceleration is negative, then the value is subtracted from the offset to determine the amount of negative acceleration and then passed to the lookup table or algorithm. One solution can measure 0° to 90° of tilt with a single axis accelerometer, or another solution can measure 360° of tilt with two axis configuration (XY, X and Z), or a single axis configuration (e.g. X or Z), where values in two directions are converted to degrees and compared to determine the quadrant that they are in. A tilt solution can be solved by either implementing an arccosine function, an arcsine function, or a look-up table depending on the power of the microcontroller and the accuracy required by the application. For simplicity, we will use the equation: $θ = arcsin(x)$. The arcsin(y) can determine the range from 0° to 180°, but it cannot discriminate the angles in range from 0° to 360°, e.g. arcsin(45°) = arcsin(135º). However, the sign of x and y can be used to determine which quadrant the angle is in. By this means, we can calculate the angle $β$ in one quadrant $(0-90°)$ using $arcsin(y)$ and then determine θ in the determined quadrant.

Figure 6. The Quadrants of a 360 Degree Rotation

Figure 7. An Example of Tilt in the First Quadrant

[1]
$$
V_{\text{OUT}} = V_{\text{OFFSET}} + \left(\frac{\Delta V}{\Delta g} \times 1.0 g \times \sin \theta\right)
$$

where: V_{OUT} = Accelerometer Output in Volts V_{OFF} = Accelerometer 0g Offset ∆V/∆g = Sensitivity $1g =$ Earth's Gravity θ = Angle of Tilt

Solving for the angle:

$$
[2] \quad \theta = \arcsin\left(\frac{V_{\text{OUT}} - V_{\text{OFFSET}}}{\frac{\Delta V}{\Delta g}}\right)
$$

This equation can be used with the MMA6260Q as an example:

$$
V_{\text{OUT}} = 1650 \text{mV} + 800 \text{mV} \times \sin \theta
$$

Where the angle can be solved by

$$
\theta = \arcsin\left(\frac{V_{\text{OUT}} - 1650 \text{mV}}{800 \text{mV/g}}\right)
$$

From this equation, you can see that at 0° the accelerometer output voltage would be 1650mV and at 90° the accelerometer output would be 2450mV.

INTERFACING TO ADC

An 8-Bit ADC

An 8-bit ADC cuts 3.3V supply into 255 steps of 12.9mV for each step. Therefore, by taking one ADC reading of the MMA6260Q at 0g (0°of tilt for an x-axis device) and 1g (90° of tilt for an x-axis device), would result in the following:

- 0° : 1650mV + 12.9mV = 1662.9mV, which is 0.92° resolution
- 90°: 2450mV+ 12.9mV = 2462.9mV,

which is 6.51° resolution

Due to the nonlinearity discussed earlier, you will see that the accelerometer is most sensitive when the sensing axis is closer to 0°, and less sensitive when closer to 90°. Therefore, the system provides a 0.92 degree resolution at the highest sensitivity point (0 degrees), and a 6.51 degree resolution at the lowest sensitivity point (90°).

A 10-Bit ADC

A 10-bit ADC cuts 3.3V supply into 1023 steps of 3.2mV for each step. Therefore, by taking one ADC reading of the MMA6260Q again at 0g (0° of tilt for an x-axis device), would now result in the following:

- 0° : 1650mV + 3.2mV = 1653.2mV
- 90° 2450mV + 3.2mV = 2453.2mV

This results in a 0.229 degree resolution at the highest sensitivity point (0°) and a 3.26 degree resolution at the lowest sensitivity point (90°).

A 12-Bit ADC

A 12-bit ADC cuts 3.3V supply into 4095 steps of 0.8mV for each step. Therefore, by taking one ADC reading of the MMA6260Q again at 0g (0° of tilt for an x-axis device), would now result in the following:

- 0° : 1650mV + 0.8mV = 1650.8mV
- 90°: 2450mV + 0.8mV = 2450.8mV

This results in a 0.057 degree resolution at the highest sensitivity point (0°) and 1.63 degree resolution at the lowest sensitivity point (90°). However, for 0.8mV changes, the noise factor becomes the factor to consider during design. How much noise the system has will depend on how much resolution you can get with a higher bit count.

TILT APPLICATIONS

There are many applications where tilt measurements are required or will enhance its functionality. In the cell phone market and handheld electronics market, tilt applications can be used for controlling menu options, e-compass compensation, image rotation, or function selection in response to different tilt measurements. In the medical markets, tilt is used for making blood pressure monitors more accurate. They can also be used for feedback for tilting hospital beds or chairs. A tilt controller can also be used for an easier way to control this type of equipment. Accelerometers for tilt measurements can also be designed into a multitude of products, such as game controllers, virtual reality input devices, HDD portable products, computer mouse, cameras, projectors, washing machines, and personal navigation systems.

NOTES

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NOTES

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Instruction Manual AC Servo Motor and Driver MINAS A4 Series

- •Thank you for buying and using Panasonic AC Servo Motor and Driver, MINAS A4 Series.
- •Read through this Instruction Manual for proper use, especially read "Precautions for Safety" (P.8 to 11) without fail for safety purpose.
- •Keep this Manual at an easily accessible place so as to be referred anytime as necessary.

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Safety Precautions Observe the Following Instructions Without Fail

Observe the following precautions in order to avoid damages on the machinery and injuries to the operators and other personnel during the operation.

• In this document, the following symbols are used to indicate the level of damages or injuries which might be incurred by the misoperation ignoring the precautions.

DANGER Indicates a potentially hazardous situation which, if not avoided, will result in death or serious injury.

CAUTION Indicates a potentially hazardous situation which, if not avoided, will result in minor injury or property damage.

•The following symbols represent "MUST NOT" or "MUST" operations which you have to observe. (Note that there are other symbols as well.)

Represents "MUST NOT" operation which is inhibited.

Represents "MUST" operation which has to be executed.

DANGER

Do not subject the Product to water, corrosive or flammable gases, and combustibles.

Failure to observe this instruction could result in fire.

Do not put your hands in the servo driver.

Failure to observe this instruction could result in burn and electrical shocks.

Do not drive the motor with external power.

Failure to observe this instruction could result in fire.

Do not subject the cables to excessive force, heavy object, or pinching force, nor damage the cables.

Failure to observe this instruction could result in electrical shocks, damages and breakdowns.

Do not touch the rotating portion of the motor while it is running.

Failure to observe this instruction could result in injuries.

Do not touch the motor, servo driver and external regenerative resistor of the driver, since they become very hot.

Rotating portion

Failure to observe this instruction could result in burns.

DANGER

Do not place combustibles near by the motor, driver and regenerative resistor.

Failure to observe this instruction could result in fire.

Ground the earth terminal of the motor and driver without fail.

Failure to observe this instruction could result in electrical shocks.

Install an emergency stop circuit externally so that you can stop the operation and shut off the power immediately.

Failure to observe this instruction could result in injuries, electrical shocks, fire, breakdowns and damages.

Install and mount the Product and machinery securely to prevent any possible fire or accidents incurred by earthquake.

Failure to observe this instruction could result in electrical shocks, injuries and fire.

Check and confirm the safety of the operation after the earthquake.

Failure to observe this instruction could result in electrical shocks, injuries and fire.

Mount the motor, driver and regenerative resistor on incombustible material such as metal.

Failure to observe this instruction could result in fire.

Do not place the console close to a heating unit such as a heater or a large wire wound resistor.

Failure to observe this instruction could result in fire and breakdowns.

Install an over-current protection, earth leakage breaker, over-temperature protection and emergency stop apparatus without fail.

Failure to observe this instruction could result in electrical shocks, injuries and fire.

Turn off the power and wait for a longer time than the specified time, before transporting, wiring and inspecting the driver.

Failure to observe this instruction could result in electrical shocks.

Turn off the power and make it sure that there is no risk of electrical shocks before transporting, wiring and inspecting the motor.

Failure to observe this instruction could result in electrical shocks.

Wiring has to be carried out by the qualified and authorized specialist.

Failure to observe this instruction could result in electrical shocks.

Make the correct phase sequence of the motor and correct wiring of the encoder.

Failure to observe this instruction could result in injuries breakdowns and damages.

Safety Precautions Observe the Following Instructions Without Fail

ACAUTION

Do not hold the motor cable or motor shaft during the transportation.

Failure to observe this instruction could result in injuries.

Never run or stop the motor with the electro-magnetic contactor installed in the main power side.

Failure to observe this instruction could result in breakdowns.

Do not give strong impact shock to the motor shaft.

Failure to observe this \mathbb{R} instruction could result in breakdowns.

Do not approach to the machine since it may suddenly restart after the power resumption.

Design the machine to secure the safety for the operator even at a sudden restart.

Failure to observe this instruction could result in injuries.

Do not use the built-in brake as a "Braking" to stop the moving load.

Failure to observe this instruction could result in injuries and breakdowns.

Do not modify, disassemble nor repair the Product.

Failure to observe this instruction could result in fire, electrical shocks and injuries.

Do not block the heat dissipating holes or put the foreign particles into them.

Failure to observe this instruction could result in electrical shocks and fire.

Do not step on the Product nor place the heavy object on them.

Failure to observe this instruction could result in electrical shocks, injuries, breakdowns and damages.

Do not turn on and off the main power of the driver repeatedly.

Failure to observe this instruction could result in breakdowns.

Do not make an extreme gain adjustment or change of the drive. Do not keep the machine running/operating unstably.

Failure to observe this instruction could result in iniuries.

Do not give strong impact shock to the Product.

Failure to observe this instruction could result in breakdowns.

Do not pull the cables with excessive force.

Failure to observe this instruction could result in breakdowns.

ACAUTION

Use the motor and the driver in the specified combination.

Failure to observe this instruction could result in fire.

Use the eye bolt of the motor for transportation of the motor only, and never use this for transportation of the machine.

Failure to observe this instruction could result in injuries and breakdowns.

Make an appropriate mounting of the Product matching to its weight and output rating.

Failure to observe this instruction could result in injuries and breakdowns.

Keep the ambient temperature below the permissible temperature for the motor and driver.

Failure to observe this instruction could result in breakdowns.

Connect the brake control relay to the relay which is to shut off at emergency stop in series.

Failure to observe this instruction could result in injuries and breakdowns.

When you dispose the batteries, observe any applicable regulations or laws after insulating them with tape.

Make a wiring correctly and securely.

Failure to observe this instruction could result in fire and electrical shocks.

Observe the specified mounting method and direction.

Failure to observe this instruction could result in breakdowns.

Observe the specified voltage.

Failure to observe this instruction could result in electrical shocks, injuries and fire.

Execute the trial run without connecting the motor to the machine system and fix the motor. After checking the operation, connect to the machine system again.

Failure to observe this instruction could result in injuries.

When any error occurs, remove the cause and release the error after securing the safety, then restart.

Failure to observe this instruction could result in injuries.

This Product shall be treated as Industrial Waste when you dispose.

Maintenance and Inspection

• Routine maintenance and inspection of the driver and motor are essential for the proper and safe operation.

Notes on Maintenance and Inspection

- 1) Turn on and turn off should be done by operators or inspectors themselves.
- 2) Internal circuit of the driver is kept charged with high voltage for a while even after power-off. Turn off the power and allow 15 minutes or longer after LED display of the front panel has gone off, before performing maintenance and inspection.
- 3) Disconnect all of the connection to the driver when performing megger test (Insulation resistance measurement) to the driver, otherwise it could result in breakdown of the driver.

Inspection Items and Cycles

General and normal running condition

Ambient conditions : 30˚C (annual average), load factor of 80% or lower, operating hours of 20 hours or less per day.

Perform the daily and periodical inspection as per the items below.

<Note> Inspection cycle may change when the running conditions of the above change.

Guideline for Parts Replacement

Use the table below for a reference. Parts replacement cycle varies depending on the actual operating conditions. Defective parts should be replaced or repaired when any error have occurred.

Disassembling for inspection and repair should be carried out only by authorized dealers or service company.

Introduction

Outline

MINAS-A4 Series with wide output range from 50W to 5kW, are the high speed, high functionality AC servo drivers and motors. Thanks to the adoption of a new powerful CPU, A4 Series now realize velocity response frequency of 1kHz, and contribute to the development of a high-speed machine and drastic shortening of tact-time.

Standard line-up includes full-closed control and auto-gain tuning function and the motors with 2500P/r incremental encoder and 17-bit absolute/incremental encoder.

A4 Series have also improved the user-friendliness by offering a console (option) which enables you to monitor the rotational speed display, set up parameters, trial run (JOG running) and copy parameters.

A4 Series can support various applications and their requirement by featuring automated gain tuning function, damping control which achieves a stable "Stop Performance" even in low-stiffness machine and high speed motor.

This document is designed for the customer to exploit the versatile functions of A4 Series to full extent.

Cautions

1) Any part or whole of this document shall not be reproduced without written permission from us.

2) Contents of this document are subject to change without notice.

On Opening the Product Package

- Make sure that the model is what you have ordered.
- Check if the product is damaged or not during transportation.
- Check if the instruction manual is attached or not.
- Check if the power connector and motor connecters (CN X1 and CN X2 connectors) are attached or not (A to D-frame).

Contact to a dealer if you find any failures.

Check of the Driver Model

Check of the Motor Model Contents of Name Plate Panasonic Model CONT. TORQUE 0.64 Nm AC SERVO MOTOR
MODELNO. MSMD5AZS1S AC SERVO MOTOR RATING S1
MODELNO. **MSMD5AZS1S** INS. CLASS B (TÜV) A (UL)
INPUT 30AC 92 V IP65 Serial Number Rated input voltage/current 92 V
 1.6 A
 0.2 kW
 100 Hz e.g.): 0411 0001 1.65
CONNECTION
SER No. RATED OUTPUT RATED FREQ. 0.2 kW SER No. ⁰⁴¹¹⁰⁰⁰¹ ²⁰⁰ Hz RATED REV. 3000 r/min Lot number Rated output Month of production Rated rotational speed Year of production (Lower 2 digits of AD year) **Model Designation** $\underbrace{S\quad M\quad D}\quad \underbrace{5\quad A}\quad \underbrace{7}_{\frac{7}{2}}\quad \underbrace{S}_{\frac{8}{2}}\quad \underbrace{1\quad B}\quad \underbrace{S}_{\frac{10}{2}}$ 11 to $12 \overline{}$ Special specifications (letters and numbers) Motor structure -**Symbol Type** Design order Ultra low inertia MAMA 1: Standard (100W to 750W) Low inertia MQMA (100W to 400W) Voltage specifications Low inertia MSMD Motor rated output **Symbol Specifications** (50W to 750W) 100 V Low inertia **Symbol Output Symbol Output** 1 MSMA (1.0kW to 5.0kW) 50W 5A 15 1.5kW 200 V 2 Middle inertia 20 100W 2.0kW 01 MDMA 100/200 common (1.0kW to 5.0kW) 02 200W 25 2.5kW Z (50W only) **High inertia** 400W MHMA 04 30 3.0kW (500W to 5.0kW) 05 500W 40 4.0kW Middle inertia 08 750W 45 4.5kW MFMA (400W to 4.5kW) 09 900W 50 5.0kW Middle inertia **MGMA** 10 1.0kW (900W to 4.5kW) Rotary encoder specifications **Specifications Symbol Format Pulse count Resolution Wire count** P 2500P/r 10,000 Incremental 5-wire S 17bit 131,072 7-wire Absolute/Incremental common

Motor structure MSMD, MQMA MAMA

*1 The product with oil seal is a special order product. *2 Key way with center tap.

Products are standard stock items or build to order litems. For details, inquire of the dealer.

MSMA, MDMA, MFMA, MGMA, MHMA

Introduction

Check of the Combination of the Driver and the Motor

This drive is designed to be used in a combination with the motor which are specified by us. Check the series name of the motor, rated output torque, voltage specifications and encoder specifications.

Incremental Specifications, 2500P/r

<Remarks> Do not use in other combinations than those listed below.

<Note>

Suffix of " * " in the applicable motor model represents the motor structure.

Absolute/Incremental Specifications, 17-bit

<Remarks> Do not use in other combinations than those listed below.

<Notes>

1) Suffix of " * " in the applicable motor model represents the motor structure.

2) Default of the driver is set for the incremental encoder specifications.

When you use in absolute, make the following operations.

- a) Install a battery for absolute encoder. (refer to P.314, "Options" of Supplement.)
- b) Switch the parameter Pr0B (Absolute encoder setup) from "1 (default)" to "0".
- 3) No wiring for back up battery is required when you use the absolute 17-bit encoder in incremental.

Parts Description

Driver

e.g.) : MADDT1207 (Single phase, 200V, 200W : A-frame)

• C and D-frame

e.g.) : MCDDT1207 (Single/3-phase, 200V, 750W : C-frame)

X1 and X2 are attached in A to D-frame driver.

<Note>

[Before Using the Products]

<Note> For details of each model, refer to "Dimensions " (P.324 to 326) of Supplement. e.g.) : MFDDTB3A2 (3-phase, 200V, 5.0kW : F-frame)

Parts Description

Motor

- MSMD 50W to 750W
- MAMA 100W to 750W
- MQMA 100W to 400W

e.g.) : Low inertia type (MSMD series, 50W)

<Note>

For details of each model, refer to "Dimensions " (P.327 to P.341) of Supplement.

Console

Main Body

<Note>

Console is an option (Part No.: DV0P4420).

Display/Touch panel

Mode switching button : Switches the mode among the following 6 modes.

- (1) Monitor mode
- (2) Parameter setup mode
- (3) EEPROM write mode
- (4) Normal auto-gain tuning mode
- (5) AUX function mode
	- Trial run (JOG mode)
	- Alarm clear
- (6) Copy mode
	- Parameter copy from the servo driver to the console
	- Parameter copy from the console to the servo driver

How to Install

Install the driver and the motor properly to avoid a breakdown or an accident.

Driver

Installation Place

- 1) Indoors, where the products are not subjected to rain or direct sun beams. The products are not waterproof.
- 2) Where the products are not subjected to corrosive atmospheres such as hydrogen sulfide, sulfurous acid, chlorine, ammonia, chloric gas, sulfuric gas, acid, alkaline and salt and so on, and are free from splash of inflammable gas, grinding oil, oil mist, iron powder or chips and etc.
- 3) Well-ventilated and low humidity and dust-free place.
- 4) Vibration-free place

Environmental Conditions

How to Install

- 1) Rack-mount type. Install in vertical position, and reserve enough space around the servo driver for ventilation. Base mount type (rear mount) is standard (A to D-frame)
- 2) Use the optional mounting bracket when you want to change the mounting face.
	- A to D-frame

e.g.) In case of C-frame

Fastening torque of earth screws (M4) to be 0.39 to 0.59N•m.

E and F-frame

Mounting Direction and Spacing

- Reserve enough surrounding space for effective cooling.
- Install fans to provide uniform distribution of temperature in the control panel.
- Observe the environmental conditions of the control panel described in the next page.

<Note>

It is recommended to use the conductive paint when you make your own mounting bracket, or repaint after peeling off the paint on the machine for installing the products, in order to make noise countermeasure.

Caution on Installation

We have been making the best effort to ensure the highest quality, however, application of exceptionally large external noise disturbance and static electricity, or failure in input power, wiring and components may result in unexpected action. It is highly recommended that you make a fail-safe design and secure the safety in the operative range.

There might be a chance of smoke generation due to the failure of these products. Pay an extra attention when you apply these products in a clean room environment.

Motor

Installation Place

Since the conditions of location affect a lot to the motor life, select a place which meets the conditions below.

- 1) Indoors, where the products are not subjected to rain or direct sun beam. The products are not waterproof.
- 2) Where the products are not subjected to corrosive atmospheres such as hydrogen sulfide, sulfurous acid, chlorine, ammonia, chloric gas, sulfuric gas, acid, alkaline and salt and so on, and are free from splash of inflammable gas, grinding oil, oil mist, iron powder or chips and etc.
- 3) Where the motor is free from grinding oil, oil mist, iron powder or chips.
- 4) Well-ventilated and humid and dust-free place, far apart from the heat source such as a furnace.
- 5) Easy-to-access place for inspection and cleaning.
- 6) Vibration-free place.
- 7) Avoid enclosed place. Motor may gets hot in those enclosure and shorten the motor life.

Environmental Conditions

*1 Ambient temperature to be measured at 5cm away from the motor.

*2 Permissible temperature for short duration such as transportation.

How to Install

You can mount the motor either horizontally or vertically as long as you observe the followings.

- 1) Horizontal mounting
- Mount the motor with cable outlet facing downward for water/oil countermeasure.
- 2) Vertical mounting
	- Use the motor with oil seal (non-standard) when mounting the motor with gear reducer to prevent the reducer oil/grease from entering to the motor.
- 3) For mounting dimensions, refer to P.326 to 340 "Dimensions".

Oil/Water Protection

- 1) Don't submerge the motor cable to water or oil.
- 2) Install the motor with the cable outlet facing downward.
- 3) Avoid a place where the motor is subjected to oil or water.
- 4) Use the motor with an oil seal when used with the gear reducer, so that the oil may not enter to the motor through shaft.

Stress to Cables

- 1) Avoid a stress application to the cable outlet and connecting portion by bending or self-weight.
- 2) Especially in an application where the motor itself travels, fix the attached cable and contain the extension junction cable into the bearer so that the stress by bending can be minimized.
- 3) Take the cable bending radius as large as possible. (Minimum R20mm)

Permissible Load to Output Shaft

- 1) Design the mechanical system so that the applied radial load and/or thrust load to the motor shaft at installation and at normal operation can meet the permissible value specified to each model.
- 2) Pay an extra attention when you use a rigid coupling. (Excess bending load may damage the shaft or deteriorate the bearing life.
- 3) Use a flexible coupling with high stiffness designed exclusively for servo application in order to make a radial thrust caused by micro misalignment smaller than the permissible value.
- 4) For permissible load of each model, refer to P.342, "List of Permissible Load to Output Shaft" of Supplement.

Notes on Installation

- 1) Do not apply direct impact to the shaft by hammer while attaching/detaching a coupling to and from the motor shaft.
	- (Or it may damage the encoder mounted on the other side of the shaft.)
- 2) Make a full alignment. (incomplete alignment may cause vibration and damage the bearing.)
- 3) If the motor shaft is not electrically grounded, it may cause electrolytic corrosion to the bearing depending on the condition of the machine and its mounting environment, and may result in the bearing noise. Check and verification by customer is required.

the Products Before Using

Before Using
the Products

Console

Installation Place

- 1) Indoors, where the products are not subjected to rain or direct sun beam. The products are not waterproof.
- 2) Where the products are not subjected to corrosive atmospheres such as hydrogen sulfide, sulfurous acid, chlorine, ammonia, chloric gas, sulfuric gas, acid, alkaline and salt and so on, and are free from splash of inflammable gas, grinding oil, oil mist, iron powder or chips and etc.
- 3) Well-ventilated and low humidity and dust-free place.
- 4) Easy-to-access place for inspection and cleaning

Environmental Conditions

<Cautions>

- Do not give strong impact to the products.
- Do not drop the products.
- Do not pull the cables with excess force.
- Avoid the place near to the heat source such as a heater or a large winding resistor.

How to Connect

<Remarks>

- Connect the console connector securely to CN X4 connector of the driver
- Never pull the cable to plug in or plug out.

[Preparation]

 LR

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System Configuration and Wiring

Overall Wiring (Connecting Example of C-frame, 3-phase)

• Wiring of the Main Circuit

(Note that no regenerative resister is equipped in Frame A and B type. **Install an external regenerative resister on incombustible material, such as metal.** Follow the same wiring connection as the above.)

• When you connect an external regenerative resister, set up Parameter No. 6C to 1 or 2.

Regenerative resistor (optional) <Remarks>

When you use an external regenerative resister, install an external protective apparatus, such as thermal fuse without fail.

connection for other occasions. (see page for connection.)

Thermal fuse and thermostat are built in to the regenerative resistor (Option). If the thermal fuse is activated, it will not resume.

System Configuration and Wiring

Overall Wiring (Connecting Example of E-frame)

• Wiring of the Main Circuit

disconnect a short bar between B1 and B2, then connect **the external regenerative resister** between P and B2.

Install an external regenerative resister on incombustible material, such as metal . Follow the same wiring connection as the above.

• When you connect an external regenerative resister, set up Parameter No. 6C to 1 or 2.

Regenerative resistor (optional) <Remarks>

When you use an external regenerative resister, install an external protective apparatus, such as thermal fuse without fail.

Ground (earth)

Thermal fuse and thermostat are built in to the regenerative resistor (Option). If the thermal fuse is activated, it will not resume.

System Configuration and Wiring

Driver and List of Applicable Peripheral Equipments

[Preparation]

Preparation

Preparation

• Select a single and 3-phase common specifications according to the power source.

 • Manufacturer of circuit breaker and magnetic contactor : Matsushita Electric Works. To comply to EC Directives, install a circuit breaker between the power and the noise filter without fail, and the circuit breaker should conform to IEC Standards and UL recognized (Listed and ω marked). 5000Arms, 240V is the maximum capacity to be delivered to the circuit of 750W or larger model when the maximum current value of the circuit breaker is limited to 20A.

• For details of noise filters, refer to P.309, "Noise Filter" and P.311, "Driver and List of Applicable Peripheral Equipments (EC Directives)" of Supplement.

<Remarks>

- Select and use the circuit breaker and noise filter with matching capacity to those of the power source, considering the load conditions as well.
- Terminal block and protective earth terminal Use a copper conductor cable with temperature rating of 60˚C or higher. Protective earth terminal is M4 for A to D-frame, and M5 for E and F-frame. Larger tightening torque of the screw than the max. value ($M4 : 1.2 N·m$, $M5 : 2.0 N·m$) may damage the terminal block.
- Earth cable diameter should be 2.0mm² (AWG14) or larger for 50W to 2.0kW model, and 3.5mm² (AWG12) or larger for 2.5kW to 4.0kW, and 5.3mm² (AWG10) or larger for 4.5kW to 5kW model.
- Use the attached exclusive connectors for A to D-frame, and maintain the peeled off length of 8 to 9mm.
- Tightening torque of the screws for connector (CN X5) for the connection to the host to be 0.3 to 0.35 N•m. Larger tightening torque than these may damage the connector at the driver side.
System Configuration and Wiring

Wiring of the Main Circuit (A to D-frame)

- Wiring should be performed by a specialist or an authorized personnel.
- Do not turn on the power until the wiring is completed.

Tips on Wiring

1) Peel off the insulation cover of the cable. (Observe the dimension as the right fig. shows.)

Power
NFB

Yellow (X2)

supply

CN X1

1

L1C L3 $L₂$ L1

L2C

RB1 RB3 RB2 U V W

 $CN X2$

⊕

Æ

Œ

8 to 9mm

3) Connect the wired connector to the driver.

 $NF \perp \parallel MC$

L

1

U

V

W

E

2

3

4

Red

Blac Green/ Yellow

White

Surge absorber

 DC 24V

DC power supply

for brake

Motor

 Ω

Fuse (5A)

Check the name plate of the driver for power specifications.

Provide a circuit breaker, or a leakage breaker. The leakage breaker to be the one designed for "Inverter" and is equipped with countermeasures for harmonics.

 \circ Provide a noise filter without fail.

 \Box Provide a surge absorber to a coil of the Magnetic Contactor. **Never start/stop the motor with this Magnetic Contactor.**

Connect a fuse in series with the surge absorber. Ask the manufacturer of the Magnetic Contactor for the fuse rating.

Provide an AC Reactor.

- **Connect L1 and L1C, and L3 and L2C at single phase use (100V and 200V), and don't use L2.**
- Match the colors of the motor lead wires to those of the corresponding motor output terminals (U,V,W).

Don't disconnect the shorting cable between RB2 and RB3 (C and D frame type). Disconnect this only when the external regenerative register is used.

- **Avoid shorting and ground fault. Don't connect the main power.**
- Connect pin 3 of the connector on the amplifier **side with pin 1 of the connector on the motor side.**

Earth-ground this.

- \circ Connect the protective earth terminal (\oplus) of the driver and the protective earth (earth plate) of the control panel without fail to prevent electrical shock.
- Don't co-clamp the earth wires to the protective earth terminal (\bigoplus) . Two terminals are provided.

Don't connect the earth cable to other inserting For applicable wire, refer to P32 and 33. **Slot, nor make them touch.** Ground resistance : 100Ω max.

- Compose a duplex Brake Control Circuit so that the brake can also be activated by an external emergency stop signal.
- The Electromagnetic Brake has no polarity.
- For the capacity of the electromagnetic brake and how to use it, refer to P.47, "Specifications of Built-in Holding Brake".
- Provide a surge absorber.

Connect a 5A fuse in series with the surge absorber.

Preparation

Preparation

Wiring of the Main Circuit (E and F-frame)

- Wiring should be performed by a specialist or an authorized personnel.
- Do not turn on the power until the wiring is completed.

Tips on Wiring

- 1) Take off the cover fixing screws, and detach the terminal cover.
- 2) Make wiring

Use clamp type terminals of round shape with insulation cover for wiring to the terminal block. For cable diameter and size, rater to "Driver and List of Applicable Peripheral Equipments" (P.32 and 33).

3) Attach the terminal cover, and fix with screws. Fastening torque of cover fixed screw in less than 0.2 N•m.

System Configuration and Wiring

Wiring Diagram

Compose the circuit so that the main circuit power will be shut off when an error occurs.

System Configuration and Wiring

Wiring to the Connector, CN X6 (Connection to Encoder)

Tips on Wiring

[Preparation]

Wiring Diagram | In case of 17-bit absolute/incremental encoder

System Configuration and Wiring

Wiring to the Connectors, CN X3 and X4 (Connection to PC, Host or Console)

• This servo driver features 2 kinds of communication function, RS232 and RS485, and you can use in 3 connecting methods.

In Case of Communication with One Driver Using RS232

By connecting the PC and the driver via RS232, you can utilize the setup support software, "PANATERM®" (option). "PANATERM "offers useful functions such as monitoring of various status, setup/change of parameters and waveform graphic display and so on.

[How to connect]

In Case of Communication with Multiple Drivers Using RS232 and RS485

By connecting the host (PC and host controller) and one driver via RS232 and connecting other drivers via RS485 each other, you can connect multiple drivers..

In Case of Communication with Multiple Drivers Using RS485 Only

By connecting the host with all drivers via RS485 you can realize connection with multiple drivers.

• Set up the rotary switch (ID) to 1 to F.

<Notes>

- You can connect up to 15 drivers with the host.
- For details, refer to P.278, "Communication"of Supplement.

Connection with the Console

Preparation

Preparation

Wiring to the Connector, CN X5 (Connection to Host Controller)

• Tips on wiring

• For detailed information, refer to Wiring Diagram at each control mode, P.83 (Position control mode), P.127 (Velocity control mode), P.161 (Torque control mode) and P.192 (Full-closed control mode).

• Specifications of the Connector, CN X5

<Note>

For details, refer to P.312, "Options" of Supplement.

<Remarks>

 • Tightening torque of the screws for connector (CN X5) for the connection to the host to be 0.3 to 0.35N•m. Larger tightening torque than these may damage the connector at the driver side.

Timing Chart

<Cautions>

- The above chart shows the timing from AC power-ON to command input.
- Activate the external command input according to the above timing chart.
- *1. In this term Servo-ON input (SRV-ON) turns ON as a hard ware, but operation command can not be received.
- *2. S-RDY output will turn on when both conditions are met, initialization of micro computer has been completed and the main power has been turned on.
- *3. After Internal control power supply , protective functions are active from approx. 1.5 sec after the start of initializing microcomputer. Please set the signals, especially for protective function, for example overtravel inhibit input (CWL,CCWL) or external scale input, so as to decide their logic until this term.

When an Error (Alarm) Has Occurred (at Servo-ON Command)

<Cautions>

- *1. t1 will be a shorter time of either the setup value of Pr6B or elapsing time for the motor speed to fall below 30r/min.
	- t1 will be 0 when the motor is in stall regardless of the setup pf Pr6A.
- *2. For the action of dynamic brake at alarm occurrence, refer to an explanation of Pr68, "Sequence at alarm ("Parameter setup" at each control mode) as well.

When an Alarm Has Been Cleared (at Servo-ON Command)

Servo-ON/OFF Action While the Motor Is at Stall (Servo-Lock)

<Cautions>

- *1. t1 will be determined by Pr6A setup value.
- *2. For the dynamic brake action at Servo-OFF, refer to an explanation of Pr69, "Sequence at Servo-OFF ("Parameter setup" at each control mode) as well.
- *3. Servo-ON will not be activated until the motor speed falls below approx. 30r/min.

Servo-ON/OFF Action While the Motor Is in Motion

(Timing at emergency stop or trip. Do not repeat this sequence. During the normal operation, stop the motor, then make Servo-ON/OFF action.)

<Cautions>

- *1. t1 will be a shorter time of either the setup value of Pr6B or elapsing time for the motor speed to fall below 30r/min.
- *2. Even though the SRV-ON signal is turned on again during the motor deceleration, Servo-ON will not be activated until the motor stops.
- *3. For the action of dynamic brake at alarm occurrence, refer to an explanation of Pt69, "Sequence at Servo-OFF ("Parameter setup" at each control mode) as well.
- *4. Servo-ON will not be activated until the motor speed falls below approx. 30r/min.
- *5. For the motor energization during deceleration at Servo-OFF, refer to an explanation of Pr69, "Sequence at Serve-OFF ("Parameter setup" at each control mode) as well.

Built-in Holding Brake

In the applications where the motor drives the vertical axis, this brake would be used to hold and prevent the work (moving load) from falling by gravity while the power to the servo is shut off.

<Caution>

Use this built-in brake for "Holding" purpose only, that is to hold the stalling status. Never use this for "Brake" purpose to stop the load in motion.

Connecting Example

The following shows the example when the brake is controlled by using the brake release output signal (BRK-OFF) of the driver.

<Notes, Cautions>

- 1. The brake coil has no polarity.
- 2. Power supply for the brake to be provided by customer. Do not co-use the power supply for the brake and for the control signals (V_{DC}).
- 3. Install a surge absorber as the above Fig. shows to suppress surge voltage generated by ON/OFF action of the relay (RY). When you use a diode, note that the time from the brake release to brake engagement is slower than that of the case of using a surge absorber.
- 4. For a surge absorber, refer to P.323, "Recommended Components"of Supplement.
- 5. Recommended components are specified to measure the brake releasing time. Reactance of the cable varies depending on the cable length, and it might generate surge voltage. Select a surge absorber so that relay coil voltage (max. rating : 30V, 50mA) and terminal voltage may not exceed the rating.

Output Timing of BRK-OFF Signal

- For the brake release timing at power-on, or braking timing at Servo-OFF/Servo-Alarm while the motor is in motion, refer to P.42 , "Timing Chart".
- With the parameter, Pr6B (Setup of mechanical brake action while the motor is in motion), you can set up a time between when the motor enters to a free-run from energized status and when BRK-OFF signal turns off (brake will be engaged), when the Servo-OFF or alarm occurs while the motor is in motion.

<Notes>

- 1. The lining sound of the brake (chattering and etc.) might be generated while running the motor with builtin brake, however this does not affect any functionality.
- 2. Magnetic flux might be generated through the motor shaft while the brake coil is energized (brake is open). Pay an extra attention when magnetic sensors are used nearby the motor.

Specifications of Built-in Holding Brake

• Excitation voltage is DC24±10%.

• * Values represent the ones with DC-cutoff using a surge absorber for holding brake.

Values in () represent those measured by using a diode (V03C by Renesas Technology Corp.)

- Above values (except static friction torque, releasing voltage and excitation current) represent typical values.
- Backlash of the built-in holding brake is kept ±1˚ or smaller at ex-factory point.
- Permissible angular acceleration : 30000rad/s2 for MAMA series

10000rad/s2 for MSMD, MQMA, MSMA, MDMA, MHMA, MFMA and MGMA series

 • Service life of the number of acceleration/deceleration with the above permissible angular acceleration is more than 10 million times.

(Life end is defined as when the brake backlash drastically changes.)

Dynamic Brake

This driver is equipped with a dynamic brake for emergency stop. Pay a special attention to the followings.

<Caution>

1. Dynamic brake is only for emergency stop.

Do not start/stop the motor by turning on/off the Servo-ON signal (SRV-ON). Or it may damage the dynamic brake circuit of the driver.

The motor becomes a dynamo when driven externally, and shorting current runs while this dynamic brake is activated and might cause smoking or fire.

2. Dynamic brake is a short-duration rating, and designed for only emergency stop. Allow approx. 3 minutes pause when the dynamic brake is activated during high-speed running.

(Over-current protection (error code No. 14) may be activated when the dynamic brake circuit inside the F-frame amplifier has overheated.)

- You can activate the dynamic brake in the following cases.
	- 1) When the main power is turned off
	- 2) At Servo-OFF
	- 3) When one of the protective function is activated.
	- 4) When over-travel inhibit input (CWL, CCWL) of CN X5 is activated In the above cases from 1) to 4), you can select either activation of the dynamic brake or making the motor free-run during deceleration or after the stop, with parameter. Note that when the control power is off, the dynamic brake will be kept activated.

1) Setup of driving condition from deceleration to after stop by main power-off (Pr67)

Torque limit value at emergency stop will be that of Pr6E (Setup of torque at emergency stop) when the setup value is 8 or 9.

2) Setup of driving condition from deceleration to after stop by Servo-OFF (Pr69)

Torque limit value at emergency stop will be that of Pr6E (Setup of torque at emergency stop) when the setup value is 8 or 9.

3) Setup of driving condition from deceleration to after stop by activation of protective function (Pr68)

Deviation counter at activation of protective function will be cleared at alarm-clear.

4) Setup of driving condition from deceleration to after stop by validation of over-travel inhibit input (Pr66)

Torque limit value during deceleration will be that of Pr6E (Setup of torque at emergency stop) when the setup value is 2.

Changes will be validated after the control power is turned on.

Caution on Homing Operation

• In homing action by using the host controller, stop position might not be stabilized if the origin input (Zphase of the encoder) is entered while the motor is not decelerated enough after the proximity input is turned on. Set up the ON-positions of proximity input and the position of origin point, considering the necessary pulse counts for deceleration. Take the positioning action and homing action into account when you set put acceleration/deceleration time with parameter, since this affect these action as well. **For the details of homing, observe the instruction manual of the host controller.**

Example of Homing Action

Proximity dog on... .Decelerates at an entry of the proximity input, and stops at an entry of the first origin input (Z-phase)

Proximity dog off... .Decelerates at an entry of the proximity input, and stops at an entry of the first origin input (Z-phase) after the input is tuned off

Setup of Parameter and Mode

Outline of Parameter

This driver is equipped with various parameters to set up its characteristics and functions. This section describes the function and purpose of each parameter. Read and comprehend very well so that you can adjust this driver in optimum condition for your running requirements.

How to Set

- You can refer and set up the parameter with either one of the following.
	- 1) Front panel of the driver
	- 2) Combination of the setup support software, "PANATERM®" (Option, DV0P4460: English/Japanese version) and PC.
	- 3) Console (DV0P4420, option)

<Note>

For setup of the parameters on PC screen, refer to the instruction manual of the "PANATERM®".

How to Connect

<Remarks>

- Connect the console connector to the connector, CN X4 of the driver securely.
- Do not pull the cable to insert/unplug.

Preparation

Preparation

Setup of Parameter and Mode

Composition and List of Parameters

For details, refer to "Parameter Setup" of each control mode.

• In this document, following symbols represent each mode.

* When you select the combination mode of 3, 4 or 5, you can select either 1st or 2nd with control mode switching input (C-MODE).

 When C-MODE is open : 1st mode selection When C-Mode is closed : 2nd mode selection Do not enter the command 10ms before/after the switching.

Parameters for Functional Selection

• For parameters with suffix of "*1", change will be validated after the reset of the control power.

Parameters for Adjustment of Time Constant for Gains and Filters

 • For parameters which default values are parenthesized by "< >", default value varies automatically by the real-time auto-gain tuning function. Set up Pr21 (Setup of Real-time auto-gain tuning mode) to 0 (invalid) when you want to adjust manually.

Setup of Parameter and Mode

Parameters for Auto-Gain Tuning

*3 this parameter will be automatically set up when the adaptive filter is validated (Pr23, "Setup of adaptive filter mode" is "1", and you cannot set this up at your discretion. Set up Pr23, "Setup of adaptive filter mode" to "0" (invalid) to clear this parameter.

Parameters for Adjustment (2nd Gain Switching Function)

 • For parameters which default values are parenthesized by "< >", default value varies automatically by the real-time auto-gain tuning function. Set up Pr21 (Setup of Real-time auto-gain tuning mode) to 0 (invalid) when you want to adjust manually.

*** In this documentation, each mode is represented by the following symbols**

P : Position control, S : Velocity control, T : Torque control, F : Full-closed control, P/S : Position (1st),/ Velocity (2nd) control, P/T : Position (1st)/Torque (2nd) control, S/T : Velocity (1st)/Torque (2nd) control

Parameters for Position Control

• For parameters with suffix of "*1", change will be validated after the reset of the control power.

Parameters for Velocity/Torque control

*2 Defaults of Pr5E and Pr5F vary depending on the combination of the driver and the motor. Refer to P.57, "Setup of Torque Limit".

Setup of Parameter and Mode

Parameters for Sequence

Parameters for Full-Closed Control

• For parameters with suffix of "*1", change will be validated after the reset of the control power.

- *** In this documentation, each mode is represented by the following symbols**
- P : Position control, S : Velocity control, T : Torque control, F : Full-closed control, P/S : Position (1st),/ Velocity (2nd) control, P/T : Position (1st)/Torque (2nd) control, S/T : Velocity (1st)/Torque (2nd) control

Setup of Torque Limit

Torque limit setup range is 0 to 300 and default is 300 except the combinations of the motor and the driver listed in the table below.

 • The above limit applies to Pr5E, 1st torque limit setup, Pr5F, 2nd torque limit setup and Pr6E, Torque setup at emergency stop.

<Caution>

When you change the motor model, above max. value may change as well. Check and reset the setup values of Pr5E, Pr5F and Pr6E.

Cautions on Replacing the Motor

As stated above, torque limit setup range might change when you replace the combination of the motor and the driver. Pay attention to the followings.

1.When the motor torque is limited,

When you replace the motor series or to the different wattage motor, you need to reset the torque limit setup because the rated toque of the motor is different from the previous motor. (see e.g.1)

2.When you want to obtain the max. motor torque,

You need to reset the torque limiting setup to the upper limit, because the upper limit value might be different from the previous motor. (see e.g.2)

How to Use the Front Panel and Console

Setup with the Front Panel

Composition of Touch Panel and Display

Display LED (6-digit)

All of LED will flash when error occurs, and switch to error display screen. All of LED will flash slowly when warning occurs.

Shifting of the digit for data changing to higher digit. (Valid to the digit whose decimal point flashes.)

Press these to change display and data, select parameters and execute actions. (Change/Selection/Execution is valid to the digit which decimal point flashes.) Numerical value increases by pressing $, \widehat{A}$, decreases by pressing $\left(\blacktriangledown\right)$.

SET Button (valid at any time) Press this to switch SELECTION and EXECUTTION display.

Mode switching button (valid at SELECTION display) Press this to switch 5 kinds of mode.

- 1) Monitor Mode
- 4) Auto-Gain Tuning Mode
- 2) Parameter Set up Mode
- 3) EEPROM Write Mode 5) Auxiliary Function Mode

Setup with the Console

Composition of Touch Panel and Display

Display LED (6-digit)

All of LED will flash when error occurs, and switch to error display screen.

Displays ID No. (address) of selected driver (in 2 digits).

The value set in Pr00(address) is ID No. Parameter No. is displayed (2 digits) at parameter setup mode.

Press this to shift the digit for data change.

Press these to change data or execute selected action of parameter. Numerical value increases by pressing $, \mathbf{A}$,

decreases by pressing $\left(\blacktriangledown\right)$.

SET Button

Press this to shift each mode which is selected by mode switching button to EXECUTION display.

Mode Switching Button Press this to switch 6 kinds of mode.

-
- 1) Monitor mode 4) Normal auto-gain tuning mode
- 2) Parameter setup mode 5) Auxiliary function mode
	-
- 3) EEPROM write mode 6) Copy mode
-

Initial Status of the Front Panel Display (7 Segment LED)

Front panel display shows the following after turning on the power of the driver.

Initial Status of the Console Display (7 Segment LED)

Turn on the power of the driver while inserting the console connector to the driver main body, or inserting the console connector to CN X4 connector.

How to Use the Front Panel and Console

Structure of Each Mode

Use each button on the touch panel to select the structure and switch the mode.

How to Use the Front Panel and Console

After the writing completes, return to SELECTION display by referring to "Structure of each mode" (P.60 and 61).

<Remarks>

- $F555E$ will be displayed when you change the parameter setup which change will be validated only after the reset. Turn off the power of the driver, then reset it.
- When writing error occurs, repeat the writing. If the writing error persists, the console might be a failure.
- Do not shut down the power during EEPROM writing, otherwise wrong data might be written. In such case, set up all parameters again to write them again after full confirmation.
- Do not disconnect the console connector from the driver between $5 \epsilon R \epsilon E$ and ϵ is ightharpoonector is disconnected, insert the connector and repeat the procedure from the beginning.

[Preparation]

Monitor Mode

Preparation **Preparation**

How to Use the Front Panel and Console

Display of Position Deviation, Motor Rotational Speed and Torque Output

Display of I/O Signal Status

Displays the control input and output signal to be connected to CN X5 connector. Use this function to check if the wiring is correct or not.

• Signal No. and its title

Reference of Error Factor and History

• You can refer the last 14 error factors (including present one) Press $(\triangle)(\blacktriangledown)$ to select the factor to be referred.

<Note>

- Following errors are not included in the history.
	- 11:Under-voltage protection for control power 13:Under-voltage protection for main power 36:EEPROM parameter error protection 37:EEPROM check code error protection 38:Ocer-travel inhibition input protection 95:Automatic motor recognition error protection
- $E \mid J$ History 13 (oldest error)
- When one of the errors which are listed in error history occurs, this error and history o shows the same error No.
- When error occurs, the display flashes.

•Error code No. and its content

How to Use the Front Panel and Console

<Cautions>

• You can not clear the each date of [PANATERM] and console to "0" with this operation.

• Since accumulation process of command pulse cannot be executed when the command pulse input prohibition is validated, during normal auto-gain tuning and while measuring function to frequency characteristics of [PANATERM] is used, actual pulse input counts may differ from the displayed value of command pulse total sum.

 $\overline{\bm{\mathit{\Pi}}}$

Initial display of LED of the selected driver will appear by pressing $(\frac{S}{n})$. $\boxed{E - - 485}$ will appear when you select the ID of not-selected driver.

67

How to Use the Front Panel and Console

Display of the Factor of No-Motor Running

Displays the factor of no-motor running in number.

Control mode

 E

•Explanation of factor No.

<Note>

* Motor might run even though the other number than 0 is displayed.

Operation at SELECTION display

Press (M) once after pressing (S) from initial status of LED to change the display to Parameter setup mode, $|\mathcal{P}|\mathcal{Q}|$

Parameter No. (Hexadecimal No.)

<Note>

For parameters which place is displayed with " \mathbf{r} ", the content changed and written to EEPROM becomes valid after turning off the power once.

Press (A) or (\forall) to select parameter No. to be referred/set.

Operation at EXECUTION display

Press $\left(\frac{S}{m}\right)$ to change to EXECUTION display of $|B\bar{B}|$

Parameter value **<Note>**

(1) You can change the decimal point with (\mathbf{A}) , then shift the digit for data change.

Each parameter has a limit in number of places for upper-shifting.

(2) Press (\triangle) or (\triangledown) to set up the value of parameter.

Value increases with (\triangle) decreases with (\blacktriangledown) .

After setting up parameters, return to SELECT mode, referring to structure of each mode (P.60 and 61).

<Remarks>

After changing the parameter value and pressing (\S) , the content will be reflected in the control. Do not extremely change the parameter value which change might affect the motor movement very much (especially velocity loop or position loop gains).

Preparation

Preparation
How to Use the Front Panel and Console

- When you change the parameters which contents become valid after resetting, $\lceil \cdot \rceil \leq \lceil \cdot \rceil$ will be displayed after finishing wiring. Turn off the control power once to reset.
- **Note 1)** When writing error occurs, make writing again. If the writing error repeats many times, this might be a failure.
- **Note 2)** Don't turn off the power during EEPROM writing. Incorrect data might be written. If this happens, set up all of parameters again, and re-write after checking the data.

Auto-Gain Tuning Mode

Normal Mode Auto-Gain Tuning Screen

<Remarks>

- For details of normal auto-gain tuning, refer to P.236, "Normal Auto-Gain Tuning" of Adjustment. Pay a special attention to applicable range and cautions.
- The motor will be driven in a preset pattern by the driver in normal auto-gain tuning mode. You can change this pattern with Pr25 (Setup of action at normal auto-gain tuning), however, shift the load to where the operation in this pattern may not cause any trouble, then execute this tuning.
- Depending on the load, oscillation may occur after the tuning. In order to secure the safety, use the protective functions of Pr26 (Setup of software limit), Pr70 (Setup of excess position deviation) or Pr73 (Setup of over-speed level).

Operation at SELECTION display

After setting up tuning, return to SELECT DISPLAY, referring to structure of each mode (P.60 and 61). **<Remarks>**

Don't disconnect the console from the driver between $\{5 \nmid \nmid R \nmid \nmid \mathbf{r} \mid \mathbf{r} \}$ **and** $\{6 \nmid \nmid \nmid R \nmid \nmid \nmid \nmid R \}$ Should the connector is pulled out, insert it again and repeat the procedures from the beginning. **<Note>** If the following status occurs during the tuning action, the tuning error occurs.

- (1) During the tuning action, 1) when an error occurs, 2) when turned to Servo-OFF, 3) even the deviation counter is cleared, 4) when the tuning is actuated close to the limit switch and 5) when the main power is shut off.
- (2) When the output torque is saturated because the inertia or load is too large.
- (3) When the tuning can not be executed well causing oscillation.

If the tuning error occurs, value of each gain returns to the previous value before the tuning. The driver does not trip except error occurrence. Depending on the load, the driver might oscillate without becoming tuning error. (not showing \sqrt{F} \sqrt{G} \sqrt{G}) Extra attention should be paid to secure the safety.

How to Use the Front Panel and Console

 L

Auxiliary Function Mode

Alarm Clear Screen

Protective function will be activated and release the motor stall status (error status).

After alarm cleaning, return to SELECTION display, referring to structure of each mode (P.60 and 61).

<Remarks>

Don't disconnect the console from the driver between $[52R + 12R + 12R]$. Should the connector is pulled out, insert it again and repeat the procedures from the beginning.

How to Use the Front Panel and Console

Automatic Offset Adjustment (Front Panel Only)

Automatically adjust the offset value of Pr52 (Velocity command offset) of analog velocity command input (SPR/TRQR).

$$
[B\,F_-\,\varpi\,F\,S]
$$

Operation at EXECUTION display

<Notes>

This function is invalid at position control mode.

You cannot write the data only by executing automatic offset adjustment.

Execute a writing to EEPROM when you need to reflect the result afterward.

Console

BABAAA

Trial Run (JOG Run)

You can make a trial run (JOG run) without connecting the Connector, CN X5 to the host controller such as PLC. <Remarks>

- Separate the motor from the load, detach the Connector, CN X5 before the trial run.
- Bring the user parameter setups (especially Pr11-14 and 20) to defaults, to avoid oscillation or other failure.

Inspection Before Trial Run

- (1) Inspection on wiring
	- Miswiring ?
		- (Especially power input and motor output)
	- Short or grounded ?
	- Loose connection ?
- Display LED (2) Confirmation of power supply and voltage • Rated voltage ? Power supply \circ \overline{O} O \circ \overline{O} \overline{O}
- $E \cdot$ \circ \circ (3) Fixing of the servo motor \circ • Unstable mounting ? \circ \circ \circ ∩ \bigcirc (4) Separation from the mechanical system \subset (5) Release of the brake CN X6 Machine HH | Motor ground
- (6) Turn to Servo-OFF after finishing the trial run by pressing $(\frac{S}{n})$.

How to Use the Front Panel and Console

Procedure for Trial Run

When you use the console, insert the console connector to CN X4 of the driver securely and turn on the driver power.

After the Servo-ON of preparation step 2 for trial run,

the motor runs at the preset speed with Pr3D (JPG speed) to CCW direction by pressing (A) CW by pressing (\blacktriangledown) .

The motor stops by pressing (\triangle) (\blacktriangledown) .

After finished trial running, return to SELECTION display, referring to structure of each mode (P.60 and 61). **<Notes>**

- Set up torque limit input invalidation (Pr03) to 1, run-inhibit input invalidation (Pr04) to 1 and ZEROSPD input (Pr06) to 0.
- If SRV-ON becomes valid during trial run, the display changes to \sqrt{F} \sim σ \sim which is normal run through external command.

<Caution>

If such trouble as disconnection of cable or connector occurs during trial run, the motor makes over-run for maximum 1 sec. Pay an extra attention for securing safety.

Clearing of Absolute Encoder

Only applicable to the system which uses absolute encoder. You can clear the alarm and multi-turn data of the absolute encoder.

After clearing of absolute encoder finishes, return to SELECTION display, referring to structure of each mode (P.60 and 61).

<Remarks>

Don't disconnect the console from the driver between $5 \nmid R \nmid t$ **to** $\lceil n \rceil$ **.** $5h$. Should the connector is pulled out, insert it again and repeat the procedures from the beginning.

How to Use the Front Panel and Console

After cleaning of External scale Error, return to SELECTION display, referring to the structure of each mode (P.60 and 61).

After copying finishes, return to SELECTION display, referring to structure of each mode (P.60 and 61)

<Remarks>

Don't disconnect the console from the driver between $\overline{PHB5E}$ to $\overline{PHB5E}$

Should the connector is pulled out, insert it again and repeat the procedures from the beginning. **<Note>**

If the error display repeats frequently, check the broken cable, disconnection of the connector, misoperation due to noise or failure of console.

How to Use the Front Panel and Console

After copying finishes, return to SELECTION display, referring to structure of each mode (P.60 and 61).

<Remarks>

Don't disconnect the console from the driver between $PHBSE I$ **to** $PHBSE J$ Should the connector is pulled out, insert it again and repeat the procedures from the beginning.

<Note>

If the error display repeats frequently, check the broken cable, disconnection of the connector, misoperation due to noise or failure of console.

[Connection and Setup of Position Control Mode]

Control Block Diagram of Position Control Mode 82

Control Block Diagram of Position Control Mode

Wiring Example to the Connector, CN X5

Wiring Example of Position Control Mode

Wiring to the Connector, CN X5

Interface Circuit

Input Circuit

SI Connection to sequence input signals

- Connect to contacts of switches and relays, or open collector output transistors.
- When you use contact inputs, use the switches and relays for micro current to avoid contact failure.
- Make the lower limit voltage of the power supply (12 to 24V) as 11.4V or more in order to secure the primary current for photo-couplers.

PI1 Connection to sequence input signals (Pulse train interface)

- (1) Line driver I/F (Input pulse frequency : max. 500kpps)
- This signal transmission method has better noise immunity. We recommend this to secure the signal transmission.
- (2)Open collector I/F (Input pulse frequency : max. 200kpps)
- The method which uses an external control signal power supply (V_{DC})
- Current regulating resistor R corresponding to VDC is required in this case.
- Connect the specified resister as below.

Specifications 1kΩ1/2W 2kΩ1/2W

(3)Open collector I/F (Input pulse frequency : max. 200kpps)

 • Connecting diagram when a current regulating resistor is not used with 24V power supply.

 $\#$ represents twisted pair.

VDC 12V 24V

> Max.input voltage : DC24V, Rated current : 10mA

Connection to sequence input signals PI2 (Pulse train interface exclusive to line driver)

Line driver I/F (Input pulse frequency : max. 2Mpps)

• This signal transmission method has better noise immunity. We recommend this to secure the signal transmission when line driver I/F is used.

AI Analog command input

- The analog command input goes through 3 routes, SPR/TRQR(Pin-14), CCWTL (Pin-16) and CWTL (Pin-18).
- Max. permissible input voltage to each input is ±10V. For input impedance of each input, refer to the right Fig.
- When you compose a simple command circuit using variable resistor(VR) and register R, connect as the right Fig. shows. When the variable range of each input is made as $-10V$ to +10V, use VR with 2kΩ, B-characteristics, 1/2W or larger, R with 200Ω, 1/2W or larger.
- A/D converter resolution of each command input is as follows. (1)ADC1 : 16 bit (SPR/TRQR), (including 1bit for sign), \pm 10V (2)ADC2 : 10 bit (CCWTL, CWTL), 0 to 3.3V

Output Circuit

SO1 SO2 Sequence output circuit

- The output circuit is composed of open collector transistor outputs in the Darlington connection, and connect to relays or photo-couplers.
- There exists collector to emitter voltage, VcE (SAT) of approx. 1V at transistor-ON, due to the Darlington connection of the output or. Note that normal TTL IC cannot be directly connected since it does not meet VIL.
- There are two types of output, one which emitter side of the output transistor is independent and is connectable individually, and the one which is common to – side of the control power supply (COM–).
- If a recommended primary current value of the photo-coupler is 10mA, decide the resistor value using the formula of the right Fig.

AM26LS32 or equivalent **AM26LS31 or**

OA-OA–

 \overline{OB}

equivalent

22 21

A

B

For the recommended primary current value, refer to the data sheet of apparatus or photo-coupler to be used.

PO1 Line driver (Differential output) output

- Feeds out the divided encoder outputs (A, B and Z-phase) in differential through each line driver.
- At the host side, receive these in line receiver. Install a terminal resistor (approx. 330Ω) between line receiver inputs without fail.
- These outputs are not insulated.

$\#$ represents twisted pair.

PO2 Open collector output

- Feeds out the Z-phase signal among the encoder signals in open collector. This output is not insulated.
- Receive this output with high-speed photo couplers at the host side, since the pulse width of the Z-phase signal is narrow.

 $\#$ represents twisted pair.

43 SP 1kΩ

42 IM

17 GND

1kΩ

Measuring instrument or external circuit

AO Analog monitor output

- There are two outputs, the speed monitor signal output (SP) and the torque monitor signal output (IM)
- Output signal width is $±10V$.
- The output impedance is 1kΩ. Pay an attention to the input impedance of the measuring instrument or the external circuit to be connected.

<Resolution>

- (1) Speed monitor output (SP)
- With a setup of 6V/3000r/min (Pr07=3), the resolution converted to speed is 8r/min/16mV. (2) Torque monitor output (IM)

With a relation of 3V/rated torque (100%), the resolution converted to torque is 0.4%/12mV.

Wiring to the Connector, CN X5

Input Signal and Pin No. of the Connector, CN X5

Input Signals (common) and Their Functions

[Connection and Setup of Position Control Mode]

Position Control Mode Connection and Setup of

Wiring to the Connector, CN X5

Input Signals (Pulse Train) and Their Functions

You can select appropriate interface out of two kinds, depending on the command pulse specifications. **• Pulse train interface exclusive for line driver**

• Pulse train interface

• Command pulse input format

uts of pulse ircuit. Refer P.84, "Input pulse train

- e train and sign, pulse ap tured at the rising edge.
- hase pulse, ill be capedge.

• Permissible max. input frequency of command pulse input signal and min. necessary time width

Wiring to the Connector, CN X5

Input Signals (Analog Command) and Their Functions

*Function becomes valid when the control mode with underline (\Box / \Box) **<Remark>**

Do not apply voltage exceeding ±10V to analog command input of SPR/TRQR.

[Connection and Setup of Position Control Mode]

*Function becomes valid when the control mode with underline ($\boxed{}$ / $\boxed{}$)

is selected while the switching mode is used in the control mode in table.

<Remark>

Do not apply voltage exceeding ±10V to analog command input of CWTL and CCWTL

Position Control Mode Connection and Setup of

Wiring to the Connector, CN X5

Output signal and Pin No. of the Connector, CN X5

Output Signals (Common) and Their Functions

• Selection of TCL and ZSP outputs

Output Signals (Pulse Train) and Their Functions

<Note>

• When the output source is the encoder

• If the encoder resolution $X \frac{Pr44}{Pr4F}$ is multiple of 4, Z-phase will be fed out synchronizing with A-phase. In other case, the Z-phase width will be equal to the encoder resolution, and will not synchronize with A-phase because of narrower width than that of A-phase. Pr45

• In case of the 5-wire, 2500P/r incremental encoder, the signal sequence might not follow the above fig. until the first Z-phase is fed out. When you use the pulse output as the control signal, rotate the motor one revolution or more to make sure that the Z-phase is fed out at least once before using.

Wiring to the Connector, CN X5

Output Signals (Analog) and Their Functions

Output Signals (Others) and Their Functions

Wiring to the Connector, CN X5

Connecting Example to Host Controller

Matsushita Electric Works, FPG-C32T

<Remark>

Matsushita Electric Works, FP2-PP2 AFP2430

Yokogawa Electric , F3NC11-ON

<Remark>

Yokogawa Electric , F3YP14-0N/F3YP18-0N

<Remark>

 \overrightarrow{a} represents twisted pair wire.

Omron, CS1W-NC113

<Remark>

Omron, CS1W-NC133

<Remark>

 \overrightarrow{a} represents twisted pair wire.

Omron, C200H-NC211

<Remark>

Mitsubishi, A1SD75/AD75P1

Trial Run (JOG run) at Position Control Mode

Trial Run by Connecting the Connector, CN X5

- (1) Connect the CN X5.
- (2) Enter the power (DC12 to 24V) to control signal (COM+, COM–)
- (3) Enter the power to the driver.
- (4) Confirm the default values of parameters.
- (5) Match to the output format of the host controller with Pr42 (Command pulse input mode setup).
- (6) Write to EEPROM and turn off/on the power (of the driver).
- (7) Connect the Servo-ON input (SRV-ON, CN X5, Pin-29) and COM– (CN X5, Pin-41) to bring the driver to Servo-ON status and energize the motor.
- (8) Enter low frequency from the host controller to run the motor at low speed.
- (9) Check the motor rotational speed at monitor mode whether, rotational speed is as per the setup or not, and

the motor stops by stopping the command (pulse) or not.

(10) If the motor does not run correctly, refer to P.68, "Display of Factor for No-Motor Running" of Preparation.

• Enter command pulses from the host controller.

Input signal status

Setup of Motor Rotational Speed and Input Pulse Frequency

<Note>

Defaults of Pr48 and Pr49 are both 0, and encoder resolution is automatically set up as numerators.Defaults of Pr48 and Pr49 are both 0, and encoder resolution is automatically set up as numerators.

<Remarks>

- Max. input pulse frequency varies depending on input terminals.
- You can set up any values to numerator and denominator, however, setup of an extreme division ratio or multiplication ratio may result in dangerous action. Recommended ratio is 1/50-20.

 60° Pulley ratio : Gear ratio : **Total reduct**

18

e.g.) When you want to rotate the motor by 60° with the load of total reduction ratio of 18/365.

*Refer to P.306 "Division Ratio for Parameters" of Supplement.
Real-Time Auto-Gain Tuning

Outline

The driver estimates the load inertia of the machine in real time, and automatically sets up the optimum gain responding to the result. Also the driver automatically suppress the vibration caused by the resonance with an adaptive filter.

Applicable Range

 • Real-time auto-gain tuning is applicable to all control modes.

Caution

Real-time auto-gain tuning may not be executed properly under the conditions described in the right table. In these cases, use the normal mode auto-gain tuning (refer to P.236 of Adjustment), or execute a manual gain tuning. (refer to P.240, of Adjustment)

How to Operate

- (1) Bring the motor to stall (Servo-OFF).
- (2) Set up Pr21 (Real-time auto-gain tuning mode setup) to 1- 7. Default is 1.

• When the varying degree of load inertia is large, set up 3 or 6.

• When the motor is used for vertical axis, set up 4-6.

- When vibration occurs during gain switching, set up 7.
- When resonance might give some effect, validate the setup of Pr23 (Setup of adaptive filter mode).
- (3) Set up Pr22 (Machine stiffness at real-time auto-gain tuning) to 0 or smaller value.
- (4) Turn to Servo-ON to run the machine normally.
- (5) Gradually increase Pr22 (Machine stiffness at real-time auto-gain tuning) when you want to obtain better response. Lower the value (0 to 3) when you experience abnormal noise or oscillation.
- (6) Write to EEPROM when you want to save the result.

Adaptive Filters

The adaptive filter is validated by setting up Pr23 (Setup of adaptive filter mode) to other than 0.

The adaptive filter automatically estimates a resonance frequency out of vibration component presented in the motor speed in motion, then removes the resonance components from the torque command by setting up the notch filter coefficient automatically, hence reduces the resonance vibration.

The adaptive filter may not operate property under the following conditions. In these cases, use 1st notch filter (Pr1D and 1E) and 2nd notch filter (Pr28-2A) to make measures against resonance according to the manual adjusting procedures. For details of notch filters, refer to P.246, "Suppression of Machine Resonance" of Adjustment.

<Note>

Even though Pr23 is set up to other than 0, there are other cases when adaptive filter is automatically invalidated. Refer to P.235, "Invalidation of adaptive filter" of Adjustment.

Parameters Which Are Automatically Set Up.

Following parameters are automatically adjusted. Also following parameters are automatically set up.

Position gain switching time 2nd mode of control switching

<Notes>

• When the real-time auto-gain tuning is valid, you cannot change parameters which are automatically adjusted.

35 36

• Pr31 becomes 10 at position or full closed control and when Pr21 (Setup of Real-Time Auto-Gain Tuning Mode) is 1 to 6, and becomes 0 in other cases.

Cautions

- (1) After the start-up, you may experience abnormal noise and oscillation right after the first Servo-ON, or when you increase the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning), until load inertia is identified (estimated) or adaptive filter is stabilized, however, these are not failures as long as they disappear immediately. If they persist over 3 reciprocating operations, take the following measures in possible order.
	- 1) Write the parameters which have given the normal operation into EEPROM.
	- 2) Lower the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning).
	- 3) Set up both Pr21 (Setup of real-time auto-gain tuning) and Pr23 (Setup of adaptive filter mode) to 0, then set up other value than 0. (Reset of inertia estimation and adaptive action)
	- 4) Invalidate the adaptive filter by setting up Pr23 (Setup of adaptive filter mode setup) to 0, and set up notch filter manually.
- (2) When abnormal noise and oscillation occur, Pr20 (Inertia ratio) or Pr2F (Adaptive filter frequency) might have changed to extreme values. Take the same measures as the above in these cases.
- (3) Among the results of real-time auto-gain tuning, Pr20 (Inertia ratio) and Pr2F (Adaptive filter frequency) will be written to EEPROM every 30 minutes. When you turn on the power again, auto-gain tuning will be executed using the latest data as initial values.
- (4) When you validate the real-time auto-gain tuning, Pr27 (Setup of instantaneous speed observer) will be invalidated automatically.
- (5) The adaptive filter is normally invalidated at torque control, however, when you select torque control while you set up Pr02 (Control mode setup) to 4 and 5, the adaptive filter frequency before mode switching will be held.
- (6) During the trial run and frequency characteristics measurement of "PANATERM®", the load inertia estimation will be invalidated.

20 0

Parameters for Functional Selection

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Standard default : < >

Parameter Setup

Standard default : < >

Standard default : < >

Parameters for Adjustment of Time Constants of Gains and Filters

Position Control Mode Connection and Setup of

**Connection and Setup of
Position Control Mode**

<Notes>

- For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.
- Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

Parameter Setup

Standard default : < >

Parameters for Auto-Gain Tuning

Standard default : < >

Standard default : < >

Position Control Mode Connection and Setup of

<Notes>

 • Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

Parameter Setup

Standard default : < >

<Notes>

- For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.
- Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

Parameters for Adjustment (2nd Gain Switching Function)

Standard default : < >

Parameter Setup

Standard default : < > **PrNo.** Title Setup range **range Title Function/Content** (setup You can setup the 35 | Switching time of $|0 - 10000|$ $< 20 >$ * e.g.) 166 166µs Kp1(Pr10)>Kp2(Pr18) position gain value $+1)$ step-by-step switching 166 166 x 166µs time to the position Kp1(Pr10) 0 bold line 3 1 loop gain only at gain Pr35= 0 $\sqrt{2}$ switching while the 1st $\overline{3}$ thin line 1 and the 2nd gain Kp2(Pr18) switching is valid. 1st gain 2nd gain 1st gain **<Caution>** The switching time is only valid when switching from small position gain to large position gain. 3D \bigcup JOG speed setup \bigcup 0 – 500 r/min You can setup the JOG speed. $<$ 300 $>$ Refer to P.75, "Trial Run"of Preparation.

Parameters for Position Control

40 * 0 to 1 < 0 Selection of command pulse input You can select either the photo-coupler input or the exclusive input for line driver as the command pulse input. **Setup value** ≤ 0 1 **Content** Photo-coupler input (X5 PULS1:Pin-3, PULS2:Pin-4, SIGN1:Pin-5, SIGN2:Pin-6) Exclusive input for line driver (X5 PULSH1:Pin-44, PULSH2:Pin-45, SIGNH1:Pin-46, SIGNH2:Pin-47) 41 * 42 * 0 to 1 < 0 0 to 3 <1> Command pulse rotational direction setup Setup of command pulse input mode You can set up the rotational direction against the command pulse input, and the command pulse input format. • Permissible max. input frequency, and min. necessary time width of command pulse input signal. **Pr41 setup value Pr42 setup value (Command pulse rotational direction setup) (Command pulse input mode setup) Signal title CCW command** -phase advances to A by 90 $^{\circ}$. B-phase delays from A by 90 **CW command Command pulse format** t1 A-phase B-phase t1 t1 t1 t1 t1 t1 t1 t2 t2 t2 t3 t2 t4 "H" "L" t4 t5 t6 t6 t6 t6 t6 t6 t5 A by 90 t1 A-phase B-phase <u>t1</u> t1___ | <u>t1 t</u>1 t1 t1 t1 t1 t2 t2 t2 t3 t2 t4 <u>"L" M</u> † "H" t4 t5 t6 t6 t6 t6 t6 t5 0 or 2 $\langle 0 \rangle$ $\begin{array}{ccc} \langle & \rangle & \langle & \rangle \end{array}$ 3 0 or 2 $\begin{array}{ccc} 1 & & \\ & 1 \end{array}$ 3 PULS SIGN PULS SIGN PULS SIGN PULS **SIGN** PULS SIGN PULS **SIGN** 90˚ phase difference 2-phase pulse $(A + B - b)$ CW pulse train + CCW pulse train pulse train + Signal 90˚ phase difference 2-phase pulse $(A + B$ -phase CW pulse train + CCW pulse train pulse train + Signal Line driver interface Open collector interface Pulse train interface exclusive to line driver Pulse train interface **Input I/F of PULS/SIGN signal Permissible max. input frequency** 2Mpps 500kpps 200kpps t1 500ns 2µs 5µs **Min. necessary time width** t2 250ns 1µs 2.5µs t3 250ns 1µs 2.5µs t4 250ns 1µs 2.5µs t₅ 250ns 1µs 2.5µs t6 250ns 1µs 2.5µs Make the rising/falling time of the command pulse input signal to $0.1\mu s$ or smaller. **PrNo.** Title Setup Setup **Function/Content** Standard default : < >

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Parameter Setup

Standard default : < >

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Parameters for Velocity and Torque Control

Standard default : < >

<Note>

 • For parameters which default. has a suffix of "*2", value varies depending on the combination of the driver and the motor.

Parameters for Sequence

Standard default : < >

[Connection and Setup of Position Control Mode]

Standard default : < >

<Notes>

[•] For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Parameter Setup

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Standard default : < >

Parameter Setup

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

page **[Connection and Setup of Velocity Control Mode]**

Control block diagram of velocity control mode

Wiring Example to the Connector CN X5

Wiring Example of Velocity Control Mode

Connection and Setup of **Connection and Setup of Velocity Control Mode elocity Control Mode**

Wiring to the connector, CN X5

Interface Circuit

Input Circuit

SI Connection to sequence input signals

- Connect to contacts of switches and relays, or open collector output transistors.
- When you use contact inputs, use the switches and relays for micro current to avoid contact failure.
- Make the lower limit voltage of the power supply (12 to 24V) as 11.4V or more in order to secure the primary current for photo-couplers.

AI Analog command input

- The analog command input goes through 3 routes, SPR/TRQR(Pin-14), CCWTL (Pin-16) and CWTL (Pin-18).
- Max. permissible input voltage to each input is ±10V. For input impedance of each input, refer to the right Fig.
- When you compose a simple command circuit using variable resistor(VR) and register R, connect as the right Fig. shows. When the variable range of each input is made as -10V to +10V, use VR with 2kΩ, B-characteristics, 1/2W or larger, R with 200Ω, 1/2W or larger.
- A/D converter resolution of each command input is as follows. (1)ADC1 : 16 bit (SPR/TRQR), (including 1bit for sign), \pm 10V (2)ADC2 : 10 bit (CCWTL, CWTL), 0 to 3.3V

Output Circuit

SO1 SO2 Sequence output circuit

- The output circuit is composed of open collector transistor outputs in the Darlington connection, and connect to relays or photo-couplers.
- There exists collector to emitter voltage, Vce (SAT) of approx. 1V at transistor-ON, due to the Darlington connection of the output or. Note that normal TTL IC cannot be directly connected since it does not meet VIL.
- There are two types of output, one which emitter side of the output transistor is independent and is connectable individually, and the one which is common to – side of the control power supply (COM–).
- If a recommended primary current value of the photo-coupler is 10mA, decide the resistor value using the formula of the right Fig.

AM26LS32 or equivalent **AM26LS31** or

equivalent

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For the recommended primary current value, refer to the data sheet of apparatus or photo-coupler to be used.

PO1 Line driver (Differential output) output

- Feeds out the divided encoder outputs (A, B and Z-phase) in differential through each line driver.
- At the host side, receive these in line receiver. Install a terminal resistor (approx. 330Ω) between line receiver inputs without fail. • These outputs are not insulated.
- A B Z 22 OA-OA– $\overline{074}$ $O₇$ \overline{OR} $\overline{OB} + \overline{O} + \overline{AB}$ -
23 **GND** \mathcal{L} 49 Connect signal ground of the host and the driver without fail. $#$ represents twisted pair.

PO2 Open collector output

- Feeds out the Z-phase signal among the encoder signals in open collector. This output is not insulated.
- Receive this output with high-speed photo couplers at the host side, since the pulse width of the Z-phase signal is narrow.

 $\#$ represents twisted pair.

AO Analog monitor output

• There are two outputs, the speed monitor signal output (SP) and the torque monitor signal output (IM)

• Output signal width is $±10V$.

• The output impedance is 1kΩ. Pay an attention to the input impedance of the measuring instrument or the external circuit to be connected.

<Resolution>

- (1) Speed monitor output (SP)
- With a setup of 6V/3000r/min (Pr07=3), the resolution converted to speed is 8r/min/16mV. (2) Torque monitor output (IM)

With a relation of 3V/rated torque (100%), the resolution converted to torque is 0.4%/12mV.

Wiring to the connector, CN X5

Input Signal and Pin No. of the Connector, CN X5

Input Signals (common) and Their Functions

[Connection and setup of velocity control mode]

• Selection of Internal Speed

Wiring to the connector, CN X5

Input Signals (Analog Command) and Their Functions

*Function becomes valid when the control mode with underline (\Box / \Box)

is selected while the switching mode is used in the control mode in table.

<Remark>

Do not apply voltage exceeding ±10V to analog command input of SPR

Wiring to the connector, CN X5

*Function becomes valid when the control mode with underline (\Box / \Box)

is selected while the switching mode is used in the control mode in table.

<Remark>

Do not apply voltage exceeding ±10V to analog command input of CWTL and CCWTL

Output signal and Pin No. of the Connector, CN X5

Output Signals (Common) and Their Functions

Ω 1 2 3 4 5 6 7 8 **X5 TLC : Output of Pin-40 X5 ZSP : Output of Pin-12 • Selection of TCL and ZSP outputs • Torque in-limit output (Default of X5 TLC Pr09)** The output transistor turns ON when the torque command is limited by the torque limit during Servo-ON. **• Zero-speed detection output (Default of X5 ZSP Pr0A)** The output transistor turns ON when the motor speed falls under the preset value with Pr61. **• Alarm signal output** The output transistor turns ON when either one of the alarms is triggered, over-regeneration alarm, overload alarm, battery alarm, fan-lock alarm or external scale alarm. **• Over-regeneration alarm** The output transistor turns ON when the regeneration exceeds 85% of the alarm trigger level of the regenerative load protection. **• Over-load alarm** The output transistor turns ON when the load exceeds 85% of the alarm trigger level of the overload alarm. **• Battery alarm** The output transistor turns ON when the battery voltage for absolute encoder falls lower than approx. 3.2V. **• Fan-lock alarm** The output transistor turns ON when the fan stalls for longer than 1s. **• External scale alarm** The output transistor turns ON when the external scale temperature exceeds 65°, or signal intensity is not enough (adjustment on mounting is required). Valid only at the full-closed control. **• In-speed (Speed coincidence) output** The output transistor turns ON when the difference between the actual motor speed and the speed command before acceleration/deceleration reaches within the preset range with Pr61. Valid only at the velocity and torque control. **Value of Pr09 or Pr0A**

Wiring to the connector, CN X5

Output Signals (Pulse Train) and Their Functions

<Note>

• When the output source is the encoder

• If the encoder resolution $X \frac{Pr44}{Pr4F}$ is multiple of 4, Z-phase will be fed out synchronizing with A-phase. Pr45

In other case, the Z-phase width will be equal to the encoder resolution, and will not synchronize with A-phase because of narrower width than that of A-phase.

• In case of the 5-wire, 2500P/r incremental encoder, the signal sequence might not follow the above fig. until the first Z-phase is fed out. When you use the pulse output as the control signal, rotate the motor one revolution or more to make sure that the Z-phase is fed out at least once before using.

Output Signals (Analog) and Their Functions

Output Signals (Others) and Their Functions

Trial Run (JOG run) at Velocity Control Mode

Inspection Before Trial Run

Trial Run by Connecting the Connector, CN X5

- 1) Connect the CN X5.
- 2) Enter the power (DC12-24V) to control signal (COM+, COM–)
- 3) Enter the power to the driver.
- 4) Confirm the default values of parameters.
- 5) Connect the Servo-ON input (SRV-ON, CN X5, Pin-29) and COM– (CN X5, Pin-14) to turn to Servo-ON and energize the motor.
- 6) Close the speed zero clamp input (ZEROSPD) and apply DC voltage between velocity command input , SPR (CN X5, Pin-14) and GND (CN X5, Pin-15), and gradually increase from 0V to confirm the motor runs.
- 7) Confirm the motor rotational speed in monitor mode.
	- Whether the rotational speed is per the setup or not.
	- Whether the motor stops with zero command or not.
- 8) If the motor does rotate at a micro speed with command voltage of 0, correct the command voltage referring to P.74, "Automatic offset adjustment" of Preparation.
- 9) When you want to change the rotational speed and direction, set up the following parameters again.

 Pr50 : Speed command input gain Pr51 : Speed command input reversal Refer to P.152, "Parameter Setup"

(Parameters for Velocity/Torque Control)

10)If the motor does not run correctly, refer to P.68, "Display of Factor for No-Motor Running" of Preparation.

Parameter Parameter

switch close, and Stop with open

In case of one-directional operation

In case of bi-directional operation (CW/CCW), provide a bipolar power supply, or use with $Pr06 = 3$.

Input signal status

**Connection and Setup of
Velocity Control Mode Connection and Setup of elocity Control Mode**

Real-Time Auto-Gain Tuning

Outline

The driver estimates the load inertia of the machine in real time, and automatically sets up the optimum gain responding to the result. Also the driver automatically suppress the vibration caused by the resonance with an adaptive filter.

Applicable Range

 • Real-time auto-gain tuning is applicable to all control modes.

Caution

Real-time auto-gain tuning may not be executed properly under the conditions described in the right table. In these cases, use the normal mode auto-gain tuning (refer to P.236 of Adjustment), or execute a manual gain tuning. (refer to P.240, of Adjustment)

How to Operate

- (1) Bring the motor to stall (Servo-OFF).
- (2) Set up Pr21 (Real-time auto-gain tuning mode setup) to 1- 7. Default is 1.

• When the varying degree of load inertia is large, set up 3 or 6.

• When resonance might give some effect, validate the setup of Pr23 (Setup of adaptive filter mode).

- (3) Set up Pr22 (Machine stiffness at real-time auto-gain tuning) to 0 or smaller value.
- (4) Turn to Servo-ON to run the machine normally.
- (5) Gradually increase Pr22 (Machine stiffness at real-time auto-gain tuning) when you want to obtain better response. Lower the value (0 to 3) when you experience abnormal noise or oscillation.
- (6) Write to EEPROM when you want to save the result.

Adaptive Filters

The adaptive filter is validated by setting up Pr23 (Setup of adaptive filter mode) to other than 0.

The adaptive filter automatically estimates a resonance frequency out of vibration component presented in the motor speed in motion, then removes the resonance components from the torque command by setting up the notch filter coefficient automatically, hence reduces the resonance vibration.

The adaptive filter may not operate property under the following conditions. In these cases, use 1st notch filter (Pr1D and 1E) and 2nd notch filter (Pr28-2A) to make measures against resonance according to the manual adjusting procedures. For details of notch filters, refer to P.246, "Suppression of Machine Resonance" of Adjustment.

<Note>

Even though Pr23 is set up to other than 0, there are other cases when adaptive filter is automatically invalidated. Refer to P.235, "Invalidation of adaptive filter" of Adjustment.

Parameters Which Are Automatically Set Up.

Following parameters are automatically adjusted. Also following parameters are automatically set up.

<Notes>

- When the real-time auto-gain tuning is valid, you cannot change parameters which are automatically adjusted.
- Pr31 becomes 10 at position or full closed control and when Pr21 (Setup of Real-Time Auto-Gain Tuning Mode) is 1 to 6, and becomes 0 in other cases.

Cautions

- (1) After the start-up, you may experience abnormal noise and oscillation right after the first Servo-ON, or when you increase the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning), until load inertia is identified (estimated) or adaptive filter is stabilized, however, these are not failures as long as they disappear immediately. If they persist over 3 reciprocating operations, take the following measures in possible order.
	- 1) Write the parameters which have given the normal operation into EEPROM.
	- 2) Lower the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning).

3) Set up both Pr21 (Setup of real-time auto-gain tuning) and Pr23 (Setup of adaptive filter mode) to 0, then set up other value than 0. (Reset of inertia estimation and adaptive action)

4) Invalidate the adaptive filter by setting up Pr23 (Setup of adaptive filter mode setup) to 0, and set up notch filter manually.

- (2) When abnormal noise and oscillation occur, Pr20 (Inertia ratio) or Pr2F (Adaptive filter frequency) might have changed to extreme values. Take the same measures as the above in these cases.
- (3) Among the results of real-time auto-gain tuning, Pr20 (Inertia ratio) and Pr2F (Adaptive filter frequency) will be written to EEPROM every 30 minutes. When you turn on the power again, auto-gain tuning will be executed using the latest data as initial values.
- (4) When you validate the real-time auto-gain tuning, Pr27 (Setup of instantaneous speed observer) will be invalidated automatically.
- (5) The adaptive filter is normally invalidated at torque control, however, when you select torque control while you set up Pr02 (Control mode setup) to 4 and 5, the adaptive filter frequency before mode switching will be held.
- (6) During the trial run and frequency characteristics measurement of "PANATERM®", the load inertia estimation will be invalidated.

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Parameters for Functional Selection

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Standard default : < >

Parameters for Adjustment of Time Constants of Gains and Filters

Standard default : < >

Parameters for Auto-Gain Tuning

Standard default : < >

Connection and Setup of
Velocity Control Mode **Connection and Setup of elocity Control Mode**

<Notes>

- For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.
- Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

25 Setup of an action $\begin{vmatrix} 0 & 1 \\ 0 & 0 \end{vmatrix}$ - < 0 at normal mode auto-gain tuning You can set up the action pattern at the normal mode auto-gain tuning. e.g.) When the setup is 0, the motor turns 2 revolutions to CCW and 2 revolutions to CW. **Setup value Number of revolution** < 0 1 2 3 4 5 6 7 2 [revolution] 1 [revolution] **Rotational direction** $CCW \rightarrow CW$ $CW \rightarrow CCW$ $CCW \rightarrow CCW$ $CW \rightarrow CW$ $CCW \rightarrow CW$ $CW \rightarrow CCW$ $CCW \rightarrow CCW$ $CW \rightarrow CW$ 27 Setup of | 0 to 1 | – $< 0 >$ * instantaneous speed observer With a high stiffness machine, you can achieve both high response and reduction of vibration at stall, by using this instantaneous speed observer. **Setup value** $< 0 >$ * 1 **Instantaneous speed observer setup** Invalid Valid You need to set up the inertia ratio of Pr20 correctly to use this function. If you set up Pr21, real-time auto-gain tuning mode setup, to other than 0 (valid), Pr27 becomes 0 (invalid) 23 Setup of adaptive $\begin{array}{|c|c|c|c|c|c|} \hline \end{array}$ 0 to 2 $\begin{array}{|c|c|c|c|c|c|} \hline \end{array}$ <1> filter mode You can set up the action of the adaptive filter. 0 : Invalid 1 : Valid 2 : Hold (holds the adaptive filter frequency when this setup is changed to 2.) **<Caution>** When you set up the adaptive filter to invalid, the adaptive filter frequency of Pr2F will be reset to 0. The adaptive filter is always invalid at the torque control mode. 22 Selection of \vert 0 to 15 \vert -A to C-frame: <4> D to F-frame: <1> machine stiffness at real-time auto-gain tuning You can set up the machine stiffness in 16 steps while the real-time autogain tuning is valid. **<Caution>** When you change the setup value rapidly, the gain changes rapidly as well, and this may give impact to the machine. Increase the setup gradually watching the movement of the machine. $low \leftarrow$ machine stiffness \rightarrow high $low \leftarrow$ servo gain \rightarrow high $low \leftarrow$ response \rightarrow high Pr22 0, 1- - - - - - - - - - - - 14, 15 **PrNo.** Title Setup range **range Title Function/Content Unit** 2A | Selection of | 0 to 99 | – < 0 2nd notch depth You can set up the 2nd notch depth of the resonance suppressing filter. Higher the setup, shallower the notch depth and smaller the phase delay you can obtain. 28 | 2nd notch | 100 to 1500 | Hz < 1500 frequency You can set up the 2nd notch width of the resonance suppressing filter in 5 steps. The notch filter function is invalidated by setting up this parameter to "1500". 29 | Selection of | 0 to 4 | – \langle 2> 2nd notch width You can set up the notch width of 2nd resonance suppressing filter in 5 steps. Higher the setup, larger the notch width you can obtain. Use with default setup in normal operation.

Standard default : < >

<Notes>

 • Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

Standard default : < >

Parameters for Adjustment (2nd Gain Switching Function)

Standard default : < >

<Notes>

 • Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

Parameters for Position Control

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Connection and Setup of elocity Control Mode

46 * 0 to 3 < 0 Reversal of pulse output logic You can set up the B-phase logic and the output source of the pulse output (X5 OB+ : Pin-48, OB– : Pin-49). With this parameter, you can reverse the phase relation between the A-phase pulse and the B-phase pulse by reversing the B-phase logic. *1 The output source of Pr46=2, 3 is valid only at full-closed control. **Setup value** - $< 0 > 0$, 2 1, 3 **A-phase (OA)** B-phase(OB) non-reversal B-phase(OB) reversal **at motor CCW rotation at motor CW rotation Pr46** < 0 1 2 *1 3 *1 **B-phase logic** Non-reversal Reversal Non-reversal Reversal **Output source** Encoder position Encoder position External scale position External scale position **PrNo.** Title Setup range **Function/Content** Standard default : < >

Parameters for Velocity and Torque Control

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Standard default : < >

Connection and Setup of elocity Control Mode

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Standard default : < >

<Notes>

- For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.
- For parameters which default. has a suffix of "*2", value varies depending on the combination of the driver and the motor.

Parameters for Sequence

Standard default : < >

**Connection and Setup of
Velocity Control Mode Connection and Setup of elocity Control Mode**

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Standard default : < >

Connection and Setup of elocity Control Mode

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Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

page **[Connection and Setup of Torque Control Mode]**

Control Block Diagram of Torque Control Mode

• when Pr5B (Torque command selection) is 0

• when Pr5B (Torque command selection) is 1

Connection and Setup of

Connection and Setup of

Wiring to the connector, CN X5

Interface Circuit

Input Circuit

SI Connection to sequence input signals

- Connect to contacts of switches and relays, or open collector output transistors.
- When you use contact inputs, use the switches and relays for micro current to avoid contact failure.
- Make the lower limit voltage of the power supply (12 to 24V) as 11.4V or more in order to secure the primary current for photo-couplers.

AI Analog command input

- The analog command input goes through 3 routes, SPR/TRQR(Pin-14), CCWTL (Pin-16) and CWTL (Pin-18).
- Max. permissible input voltage to each input is ±10V. For input impedance of each input, refer to the right Fig.
- When you compose a simple command circuit using variable resistor(VR) and register R, connect as the right Fig. shows. When the variable range of each input is made as -10V to +10V, use VR with 2kΩ, B-characteristics, 1/2W or larger, R with 200Ω, 1/2W or larger.
- A/D converter resolution of each command input is as follows. (1)ADC1 : 16 bit (SPR/TRQR), (including 1bit for sign), \pm 10V (2)ADC2 : 10 bit (CCWTL, CWTL), 0 to 3.3V

Output Circuit

SO1 SO2 Sequence output circuit

- The output circuit is composed of open collector transistor outputs in the Darlington connection, and connect to relays or photo-couplers.
- There exists collector to emitter voltage, VcE (SAT) of approx. 1V at transistor-ON, due to the Darlington connection of the output or. Note that normal TTL IC cannot be directly connected since it does not meet VIL.
- There are two types of output, one which emitter side of the output transistor is independent and is connectable individually, and the one which is common to – side of the control power supply (COM–).
- If a recommended primary current value of the photo-coupler is 10mA, decide the resistor value using the formula of the right Fig.

AM26LS32 or equivalent $\overline{AM26L}$ S31 or animal

OA-

GND

Connect signal ground of the host and the driver without fail.

Measuring instrument or external circuit

For the recommended primary current value, refer to the data sheet of apparatus or photo-coupler to be used.

PO1 Line driver (Differential output) output

• Feeds out the divided encoder outputs (A, B and Z-phase) in differential through each line driver. • At the host side, receive these in line receiver. Install a termi-

nal resistor (approx. 330Ω) between line receiver inputs with-

B Z 22 O_A $\overline{O7}$ OZ \overline{OR} \overline{OB} + \overline{OB} + \overline{AB} בל 24 49

21

equivalent

A

• These outputs are not insulated.

out fail.

$#$ represents twisted pair.

PO2 Open collector output

- Feeds out the Z-phase signal among the encoder signals in open collector. This output is not insulated.
- Receive this output with high-speed photo couplers at the host side, since the pulse width of the Z-phase signal is narrow.

 $#$ represents twisted pair.

43 SP 1kΩ

42 IM

 $17₁$ GND

1kΩ

AO Analog monitor output

- There are two outputs, the speed monitor signal output (SP) and the torque monitor signal output (IM)
- Output signal width is $±10V$.
- The output impedance is 1kΩ. Pay an attention to the input impedance of the measuring instrument or the external circuit to be connected.

<Resolution>

- (1) Speed monitor output (SP)
- With a setup of 6V/3000r/min (Pr07=3), the resolution converted to speed is 8r/min/16mV. (2) Torque monitor output (IM)

With a relation of 3V/rated torque (100%), the resolution converted to torque is 0.4%/12mV.

Wiring to the connector, CN X5

Input Signal and Pin No. of the Connector, CN X5

Input Signals (common) and Their Functions

[Connection and Setup of Torque Control Mode]

Wiring to the connector, CN X5

Input Signals (Analog Command) and Their Functions

*Function becomes valid when the control mode with underline (\Box / \Box) is selected while the switching mode is used in the control mode in table.

[Connection and Setup of Torque Control Mode]

*Function becomes valid when the control mode with underline ($\boxed{}$ / $\boxed{}$)

is selected while the switching mode is used in the control mode in table.

<Remark>

Do not apply more than ±10V to analog command inputs of SPR/TRQR/SPL

Do not apply more than ±10V to analog command input of TRQR.

Wiring to the connector, CN X5

Output signal and Pin No. of the Connector, CN X5

Output Signals (Common) and Their Functions

• Selection of TCL and ZSP outputs

Output Signals (Pulse Train) and Their Functions

<Note>

• When the output source is the encoder

• If the encoder resolution $X \frac{Pr44}{Pr4F}$ is multiple of 4, Z-phase will be fed out synchronizing with A-phase. In other case, the Z-phase width will be equal to the encoder resolution, and will not synchronize with Pr45

A-phase because of narrower width than that of A-phase.

• In case of the 5-wire, 2500P/r incremental encoder, the signal sequence might not follow the above fig. until the first Z-phase is fed out. When you use the pulse output as the control signal, rotate the motor one revolution or more to make sure that the Z-phase is fed out at least once before using.

Wiring to the connector, CN X5

Output Signals (Analog) and Their Functions

Output Signals (Others) and Their Functions

Trial Run by Connecting the Connector, CN X5

- 1) Connect the CN X5.
- 2) Enter the power (DC12-24V) to control signal (COM+, COM–)
- 3) Enter the power to the driver.
- 4) Confirm the default values of parameters.
- 5) Set a lower value to Pr56 (4th speed of speed setup).
- 6) Energize the motor by connecting the Servo-ON input (SRV-ON, CN X5, Pin-29) and COM– (Pin-41 of CN X5) to turn to Servo-ON status.
- 7) Confirm that the motor runs as per the setup of Pr56 by applying DC voltage (positive/negative) between the torque command input (Pin-14 of CN X5) and GND (Pin-41 of CN X5).
- 8) If you want to change the torque magnitude, direction and velocity limit value against the command voltage, set up the following parameters.

 Pr56 : 4th speed of speed setup Pr5C : Torque command input gain Pr5D : Torque command input reversal

Refer to P.183, "Parameter Setup-Parameters for Velocity and Torque Control".

9) If the motor does not run correctly, refer to P.68, "Display of factor for No-motor running" of Preparation.

Wiring Diagram Parameter Parameter Parameter

In case of one way running

For bi-directional running (CW/CCW), provide a bipolar power supply.

Input signal status

Real-Time Auto-Gain Tuning

Outline

The driver estimates the load inertia of the machine in real time, and automatically sets up the optimum gain responding to the result. Also the driver automatically suppress the vibration caused by the resonance with an adaptive filter.

Applicable Range

 • Real-time auto-gain tuning is applicable to all control modes.

Caution

Real-time auto-gain tuning may not be executed properly under the conditions described in the right table. In these cases, use the normal mode auto-gain tuning (refer to P.236 of Adjustment), or execute a manual gain tuning. (refer to P.240, of Adjustment)

How to Operate

- (1) Bring the motor to stall (Servo-OFF).
- (2) Set up Pr21 (Real-time auto-gain tuning mode setup) to 1- 7. Default is 1.

• When the varying degree of load inertia is large, set up 3.

- (3) Set up Pr22 (Machine stiffness at real-time auto-gain tuning) to 0 or smaller value.
- (4) Turn to Servo-ON to run the machine normally.
- (5) Gradually increase Pr22 (Machine stiffness at real-time auto-gain tuning) when you want to obtain better response. Lower the value (0 to 3) when you experience abnormal noise or oscillation.
- (6) Write to EEPROM when you want to save the result.

Parameters Which Are Automatically Set Up.

Following parameters are automatically adjusted. Also following parameters are automatically set up.

<Notes>

- When the real-time auto-gain tuning is valid, you cannot change parameters which are automatically adjusted.
- Pr31 becomes 10 at position or full closed control and when Pr21 (Setup of Real-Time Auto-Gain Tuning Mode) is 1 to 6, and becomes 0 in other cases.

Cautions

(1) After the start-up, you may experience abnormal noise and oscillation right after the first Servo-ON, or when you increase the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning), until load inertia is identified (estimated) or adaptive filter is stabilized, however, these are not failures as long as they disappear immediately. If they persist over 3 reciprocating operations, take the following measures in possible order.

1)Write the parameters which have given the normal operation into EEPROM.

2)Lower the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning).

3)Set up both Pr21 (Setup of real-time auto-gain tuning) and Pr23 (Setup of adaptive filter mode) to 0, then set up other value than 0. (Reset of inertia estimation and adaptive action)

4)Invalidate the adaptive filter by setting up Pr23 (Setup of adaptive filter mode setup) to 0, and set up notch filter manually.

- (2) When abnormal noise and oscillation occur, Pr20 (Inertia ratio) or Pr2F (Adaptive filter frequency) might have changed to extreme values. Take the same measures as the above in these cases.
- (3) Among the results of real-time auto-gain tuning, Pr20 (Inertia ratio) and Pr2F (Adaptive filter frequency) will be written to EEPROM every 30 minutes. When you turn on the power again, auto-gain tuning will be executed using the latest data as initial values.
- (4) When you validate the real-time auto-gain tuning, Pr27 (Setup of instantaneous speed observer) will be invalidated automatically.
- (5) The adaptive filter is normally invalidated at torque control, however, when you select torque control while you set up Pr02 (Control mode setup) to 4 and 5, the adaptive filter frequency before mode switching will be held.
- (6) During the trial run and frequency characteristics measurement of "PANATERM®", the load inertia estimation will be invalidated.

Parameters for Functional Selection

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Standard default : < >

Connection and Setup of Torque Control Mode

175

Parameters for Adjustment of Time Constants of Gains and Filters

Standard default : < >

<Notes>

- For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.
- Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.
Standard default : < >

Parameters for Auto-Gain Tuning

Standard default : < >

Standard default : < >

Parameters for Adjustment (2nd Gain Switching Function)

<Notes>

 • Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

Connection and Setup of Torque Control Mode

Standard default : < >

 $<300>$ Refer to P.75, "Trial Run" of Preparation.

Parameters for Position Control

Standard default : < >

<Notes>

- For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.
- Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

46 * 0 to 3 < 0 Reversal of pulse output logic You can set up the B-phase logic and the output source of the pulse output (X5 OB+ : Pin-48, OB– : Pin-49). With this parameter, you can reverse the phase relation between the A-phase pulse and the B-phase pulse by reversing the B-phase logic. *1 The output source of Pr46=2, 3 is valid only at full-closed control. **Setup value** ۰ $< 0 > 0$, 2 1, 3 **A-phase (OA)** B-phase(OB) non-reversal B-phase(OB) reversal **at motor CCW rotation at motor CW rotation Pr46** < 0 1 $2 *1$ 3 *1 **B-phase logic** Non-reversal Reversal Non-reversal Reversal **Output source** Encoder position Encoder position External scale position External scale position **PrNo.** Title Setup range **Function/Content** Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Parameters for Velocity and Torque Control

Standard default : < >

Standard default : < >

<Notes>

 • For parameters which default. has a suffix of "*2", value varies depending on the combination of the driver and the motor.

Parameters for Sequence

Standard default : < >

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Standard default : < >

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Outline of Full-Closed Control

What Is Full-Closed Control ?

In this full-closed control, you can make a position control by using a linear scale mounted externally which detects the machine position directly and feeds it back.. With this control, you can control without being affected by the positional variation due to the ball screw error or temperature and you can expect to achieve a very high precision positioning in sub-micron order.

We recommend the linear scale division ratio of $\frac{1}{20} \le$ Linear scale division ratio \le 20

Cautions on Full-Closed Control

- (1) Enter the command pulses making the external scale as a reference. If the command pulses do not match to the external scale pulses, use the command division/multiplication function (Pr48-4B) and setup so that the command pulses after division/multiplication is based on the external scale reference.
- (2) A4-series supports the linear scale of a communication type. Execute the initial setup of parameters per the following procedures, then write into EEPROM and turn on the power again before using this function.

<How to make an initial setup of parameters related to linear scale >

- 1) Turn on the power after checking the wiring.
- 2) Check the values (initial) feedback pulse sum and external scale feedback pulse sum with the front panel or with the setup support software, PANATERM .
- 3) Move the work and check the travel from the initial values of the above 2).
- 4) If the travel of the feedback sum and the external scale feedback pulse sum are reversed in positive and negative, set up the reversal of external scale direction (Pr7C) to 1.
- 5) Set up the external scale division ratio (Pr78-7A) using the formula below,

External scale division ratio = $\frac{\text{Total variation of external scale feedback pulse}}{\text{Total strain}}$

Total variation of feedback pulse sum

$$
= \frac{\text{Pr78} \times 2^{\text{Pr79}}}{\text{Pr7A}}
$$

* If the design value of the external scale division ratio is obtained, set up this value.

- 6) Set up appropriate value of hybrid deviation excess (Pr7B) in 16 pulse unit of the external scale resolution, in order to avoid the damage to the machine.
	- * A4-series driver calculates the difference between the encoder position and the linear scale position as hybrid deviation, and is used to prevent the machine runaway or damage in case of the linear scale breakdown or when the motor and the load is disconnected.

If the hybrid deviation excess range is too wide, detection of the breakdown or the disconnection will be delayed and error detection effect will be lost. If this is too narrow, it may detect the normal distortion between the motor and the machine under normal operation as an error.

When the external scale division ration is not correct, hybrid deviation excess error (Err25) may occur especially when the work travels long distance, even though the linear scale and the motor position matches.

In this case, widen the hybrid deviation excess range by matching the external scale division ratio to the closest value.

Wiring to the Connector, CN X5

Wiring Example to the Connector, CN X5

Wiring example of full-closed control mode

Interface Circuit

Input Circuit

SI Connection to sequence input signals

- Connect to contacts of switches and relays, or open collector output transistors.
- When you use contact inputs, use the switches and relays for micro current to avoid contact failure.
- Make the lower limit voltage of the power supply (12 to 24V) as 11.4V or more in order to secure the primary current for photo-couplers.

4 PULS2 220Ω
SIGN1 <u>d SIGN2</u> 13 é
⊿GND 2200

3) PULS1 4¦PULS2 SIGN₁

 $\frac{1}{2200}$

(¥

 VDC 13 GND 220Ω SIGN2 6

> 1 OPC1 2.2kΩ PULS2 \cap

220Ω

2.2kΩ

∉

 $\overline{2200}$

ໍ່ YGND SIGN2

VDC

H İΤ 5

Ħ

13

5

H/L PULS

 H/I SIGN

> \overline{H} PULS

 L/H **SIGN**

L/H PULS

 L/H **SIGN**

AM26LS31 or equivalent 3 PULS1

R

R

H/L

(1)

(2)

(3)

 H/I

ON/OFI

ON/OFF

ON/OFF

ON/OFF

PI1 Connection to sequence input signals (Pulse train interface)

(1) Line driver I/F (Input pulse frequency : max. 500kpps)

- This signal transmission method has better noise immunity. We recommend this to secure the signal transmission.
- (2)Open collector I/F (Input pulse frequency : max. 200kpps)
- The method which uses an external control signal power supply (V_{DC})
- Current regulating resistor R corresponding to V_{DC} is required in this case.
- Connect the specified resister as below.

(3)Open collector I/F (Input pulse frequency : max. 200kpps)

 • Connecting diagram when a current regulating resistor is not used with 24V power supply.

 $\#$ represents twisted pair.

VDC 12V 24V

> Max.input voltage : DC24V, Rated current : 10mA

 $#$ represents twisted pair.

Connection to sequence input signals PI2 (Pulse train interface exclusive to line driver)

Line driver I/F (Input pulse frequency : max. 2Mpps)

• This signal transmission method has better noise immunity. We recommend this to secure the signal transmission when line driver I/F is used.

AI Analog command input

- The analog command input goes through 3 routes, SPR/TRQR(Pin-14), CCWTL (Pin-16) and CWTL (Pin-18).
- Max. permissible input voltage to each input is ± 10 V. For input impedance of each input, refer to the right Fig.
- When you compose a simple command circuit using variable resistor(VR) and register R, connect as the right Fig. shows. When the variable range of each input is made as $-10V$ to +10V, use VR with 2kΩ, B-characteristics, 1/2W or larger, R with 200Ω, 1/2W or larger.
- A/D converter resolution of each command input is as follows. (1) ADC1 : 16 bit (SPR/TRQR), (including 1bit for sign), \pm 10V (2)ADC2 : 10 bit (CCWTL, CWTL), 0 – 3.3V

Wiring to the Connector, CN X5

Output Circuit

SO1 SO2 Sequence output circuit

- The output circuit is composed of open collector transistor outputs in the Darlington connection, and connect to relays or photo-couplers.
- There exists collector to emitter voltage, VcE (SAT) of approx. 1V at transistor-ON, due to the Darlington connection of the output or. Note that normal TTL IC cannot be directly connected since it does not meet VIL.
- There are two types of output, one which emitter side of the output transistor is independent and is connectable individually, and the one which is common to – side of the control power supply (COM–).
- If a recommended primary current value of the photo-coupler is 10mA, decide the resistor value using the formula of the right Fig.

AM26LS32 or equivalent AM26LS31 or

OA+ OA–

OZ+ OZ–

GND

Connect signal ground of the host and the driver without fail.

Measuring instrument or external circuit

OB+ \overline{OB} + \overline{OB} + \overline{AB} equivalent

22 21

23

49

 24

A

B

Z

For the recommended primary current value, refer to the data sheet of apparatus or photo-coupler to be used.

PO1 Line driver (Differential output) output

- Feeds out the divided encoder outputs (A, B and Z-phase) in differential through each line driver.
- At the host side, receive these in line receiver. Install a terminal resistor (approx. 330Ω) between line receiver inputs without fail.
- These outputs are not insulated.

 $#$ represents twisted pair.

PO2 Open collector output

- Feeds out the Z-phase signal among the encoder signals in open collector. This output is not insulated.
- Receive this output with high-speed photo couplers at the host side, since the pulse width of the Z-phase signal is narrow.

 $#$ represents twisted pair.

- There are two outputs, the speed monitor signal output (SP) and the torque monitor signal output (IM)
- Output signal width is $±10V$.
- The output impedance is 1kΩ. Pay an attention to the input impedance of the measuring instrument or the external circuit to be connected.

<Resolution>

(1) Speed monitor output (SP)

 With a setup of 6V/3000r/min (Pr07=3), the resolution converted to speed is 8r/min/16mV. (2) Torque monitor output (IM)

With a relation of 3V/rated torque (100%), the resolution converted to torque is 0.4%/12mV.

43 SP 1kΩ

42 IM

 $17 \mid$ GND

1kΩ

Input Signal and Pin No. of the Connector, CN X5

Input Signals (common) and Their Functions

Full-Closed Control Mode

Wiring to the Connector, CN X5

[Connection and Setup of Full-closed Control]

Input Signals (Pulse Train) and Their Functions

You can select appropriate interface out of two kinds, depending on the command pulse specifications. **• Pulse train interface exclusive for line driver**

• Pulse train interface

• Permissible max. input frequency of command pulse input signal and min. necessary time width

*Function becomes valid when the control mode with underline (\Box / \Box)

is selected while the switching mode is used in the control mode in table.

<Remark>

Do not apply voltage exceeding ±10V to analog command inputs of SPR/TRQR/SPL.

Wiring to the Connector, CN X5

*Function becomes valid when the control mode with underline (\Box / \Box) is selected while the switching mode is used in the control mode in table.

<Remark>

Do not apply voltage exceeding ±10V to analog command input of CWTL and CCWTL.

Output signal and Pin No. of the Connector, CN X5

Output Signals (Common) and Their Functions

Ω 1 2 3 4 5 6 7 8 **X5 TLC : Output of Pin-40 X5 ZSP : Output of Pin-12 • Selection of TCL and ZSP outputs • Torque in-limit output (Default of X5 TLC Pr09)** The output transistor turns ON when the torque command is limited by the torque limit during Servo-ON. **• Zero-speed detection output (Default of X5 ZSP Pr0A)** The output transistor turns ON when the motor speed falls under the preset value with Pr61. **• Alarm signal output** The output transistor turns ON when either one of the alarms is triggered, over-regeneration alarm, overload alarm, battery alarm, fan-lock alarm or external scale alarm. **• Over-regeneration alarm** The output transistor turns ON when the regeneration exceeds 85% of the alarm trigger level of the regenerative load protection. **• Over-load alarm** The output transistor turns ON when the load exceeds 85% of the alarm trigger level of the overload alarm. **• Battery alarm** The output transistor turns ON when the battery voltage for absolute encoder falls lower than approx. 3.2V. **• Fan-lock alarm** The output transistor turns ON when the fan stalls for longer than 1s. **• External scale alarm** The output transistor turns ON when the external scale temperature exceeds 65°, or signal intensity is not enough (adjustment on mounting is required). Valid only at the full-closed control. **• In-speed (Speed coincidence) output** The output transistor turns ON when the difference between the actual motor speed and the speed command before acceleration/deceleration reaches within the preset range with Pr61. Valid only at the velocity and torque control. **Value of Pr09 or Pr0A**

Full-Closed
Control Mode **Control Mode Full-Closed**

Wiring to the Connector, CN X5

Output Signals (Pulse Train) and Their Functions

<Note>

• When the output source is the encoder

• If the encoder resolution $X \frac{Pr44}{Pr4F}$ is multiple of 4, Z-phase will be fed out synchronizing with A-phase. Pr45

In other case, the Z-phase width will be equal to the encoder resolution, and will not synchronize with A-phase because of narrower width than that of A-phase.

• In case of the 5-wire, 2500P/r incremental encoder, the signal sequence might not follow the above fig. until the first Z-phase is fed out. When you use the pulse output as the control signal, rotate the motor one revolution or more to make sure that the Z-phase is fed out at least once before using.

• When output source is the external scale,

- When the external scale is the output source, Z-phase pulse will not be fed out until the absolute position crosses 0 (000000000000h).
- Z-phase pulse after its crossing of the absolute position 0, will be fed out synchronizing with A-phase in every A-phase pulses which are set with Pr47 (External scale Z-phase setup)

Output Signals (Analog) and Their Functions

Output Signals (Others) and Their Functions

Wiring to the Connector, CN X7

Connector, CN X7

Power supply for the external scale shall be prepared by customer, or use the following power supply output for the external scale (250mA or less).

<Note>

EXOV of the external scale power supply output is connected to the control circuit ground which is connected to the Connecter, CN X5.

<Remark>

Do not connect anything to other Pin numbers descried in the above table (Pin-3 and 4).

Cautions

(1) Following external scale can be used for full-closed control.

- AT500 series by Mitutoyo (Resolution 0.05 [µm], max. speed 2[m/s])
- ST771 by Mitutoyo (Resolution 0.5[µm], max. speed 2[m/s])

(2) **Recommended external scale ratio is 1/20<External scale ratio<20**

If you set up the external scale ratio to smaller value than 50/position loop gain (Pr10 and 18), you may not be able to control per 1 pulse unit. Setup of larger scale ratio may result in larger noise.

Wiring to the External Scale, Connector, CN X7

Wire the signals from the external scale to the external scale connector, CN X7.

- 1) Cable for the external scale to be the twisted pair with bundle shielding and to having the twisted core wire with diameter of 0.18mm2.
- 2) Cable length to be max. 20m. Double wiring for 5V power supply is recommended when the wiring length is long to reduce the voltage drop effect.
- 3) Connect the outer film of the shield wire of the external scale to the shield of the junction cable. Also connect the outer film of the shield wire to the shell (FG) of CN X7 of the driver without fail.
- 4) Separate the wiring to CN X7 from the power line (L1, L2, L3, L1C, L2C (t), U, V. W, \oplus) as much as possible (30cm or more). Do not pass these wires in the same duct, nor bundle together.
- 5) Do not connect anything to the vacant pins of CN X7.
- 6) Cut away the amplifier's CN X7 cover.

Please cut it out with nippers etc.

Real-Time Auto-Gain Tuning

Outline

The driver estimates the load inertia of the machine in real time, and automatically sets up the optimum gain responding to the result. Also the driver automatically suppress the vibration caused by the resonance with an adaptive filter.

Applicable Range

 • Real-time auto-gain tuning is applicable to all control modes.

Caution

Real-time auto-gain tuning may not be executed properly under the conditions described in the right table. In these cases, use the normal mode auto-gain tuning (refer to P.236 of Adjustment), or execute a manual gain tuning. (refer to P.240, of Adjustment)

How to Operate

- (1) Bring the motor to stall (Servo-OFF).
- (2) Set up Pr21 (Real-time auto-gain tuning mode setup) to 1- 7. Default is 1.

• When the varying degree of load inertia is large, set up 3 or 6.

• When the motor is used for vertical axis, set up 4-6.

- When vibration occurs during gain switching, set up 7.
- When resonance might give some effect, validate the setup of Pr23 (Setup of adaptive filter mode).
- (3) Set up Pr22 (Machine stiffness at real-time auto-gain tuning) to 0 or smaller value.
- (4) Turn to Servo-ON to run the machine normally.
- (5) Gradually increase Pr22 (Machine stiffness at real-time auto-gain tuning) when you want to obtain better response. Lower the value (0 to 3) when you experience abnormal noise or oscillation.
- (6) Write to EEPROM when you want to save the result.

Adaptive Filters

The adaptive filter is validated by setting up Pr23 (Setup of adaptive filter mode) to other than 0.

The adaptive filter automatically estimates a resonance frequency out of vibration component presented in the motor speed in motion, then removes the resonance components from the torque command by setting up the notch filter coefficient automatically, hence reduces the resonance vibration.

The adaptive filter may not operate property under the following conditions. In these cases, use 1st notch filter (Pr1D and 1E) and 2nd notch filter (Pr28-2A) to make measures against resonance according to the manual adjusting procedures. For details of notch filters, refer to P.246, "Suppression of Machine Resonance" of Adjustment.

<Note>

Even though Pr23 is set up to other than 0, there are other cases when adaptive filter is automatically invalidated. Refer to P.235, "Invalidation of adaptive filter" of Adjustment.

Parameters Which Are Automatically Set Up.

Following parameters are auto

2F Adaptive filter frequency

Inertia ratio

<Notes>

- When the real-time auto-gain tuning is valid, you cannot change parameters which are automatically adjusted.
- Pr31 becomes 10 at position or full closed control and when Pr21 (Setup of Real-Time Auto-Gain Tuning Mode) is 1 to 6, and becomes 0 in other cases.

Cautions

- (1) After the start-up, you may experience abnormal noise and oscillation right after the first Servo-ON, or when you increase the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning), until load inertia is identified (estimated) or adaptive filter is stabilized, however, these are not failures as long as they disappear immediately. If they persist over 3 reciprocating operations, take the following measures in possible order.
	- 1) Write the parameters which have given the normal operation into EEPROM.
	- 2) Lower the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning).
	- 3) Set up both Pr21 (Setup of real-time auto-gain tuning) and Pr23 (Setup of adaptive filter mode) to 0, then set up other value than 0. (Reset of inertia estimation and adaptive action)
	- 4) Invalidate the adaptive filter by setting up Pr23 (Setup of adaptive filter mode setup) to 0, and set up notch filter manually.
- (2) When abnormal noise and oscillation occur, Pr20 (Inertia ratio) or Pr2F (Adaptive filter frequency) might have changed to extreme values. Take the same measures as the above in these cases.
- (3) Among the results of real-time auto-gain tuning, Pr20 (Inertia ratio) and Pr2F (Adaptive filter frequency) will be written to EEPROM every 30 minutes. When you turn on the power again, auto-gain tuning will be executed using the latest data as initial values.
- (4) When you validate the real-time auto-gain tuning, Pr27 (Setup of instantaneous speed observer) will be invalidated automatically.
- (5) The adaptive filter is normally invalidated at torque control, however, when you select torque control while you set up Pr02 (Control mode setup) to 4 and 5, the adaptive filter frequency before mode switching will be held.
- (6) During the trial run and frequency characteristics measurement of "PANATERM®", the load inertia estimation will be invalidated.

Parameters for Functional Selection

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Standard default : < >

Full-Closed
Control Mode **Control Mode Full-Closed**

Standard default : < >

Standard default : < >

Parameters for Adjustment of Time Constants of Gains and Filters

<Notes>

- For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.
- Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

Full-Closed Control Mode

Full-Closed
Control Mode

Standard default : < >

Parameters for Auto-Gain Tuning

Standard default : < >

<Notes>

 • Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

Full-Closed
Control Mode **Control Mode Full-Closed**
Parameter Setup

Parameters for Adjustment (2nd Gain Switching Function)

Standard default : < >

<Notes>

 • Parameters which default values have a suffix of "*" will be automatically set up during real time auto-gain tuning. When you change manually, invalidate the real-time auto-gain tuning first then set, referring to P.239, "Release of Automatic Gain Adjusting Function" of Adjustment.

Full-Closed
Control Mode **Control Mode Full-Closed**

Parameters for Position Control

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Standard default : < >

Parameter Setup

Standard default : < >

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Parameters for Velocity and Torque Control

Standard default : < >

<Note>

 • For parameters which default. has a suffix of "*2", value varies depending on the combination of the driver and the motor.

Parameters for Sequence

Standard default : < >

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Full-Closed Control Mode

Parameter Setup

Standard default : < >

Standard default : < >

<Notes>

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

Full-Closed Control Mode

Parameter Setup

Standard default : < >

 \langle >

Parameters for Full-Closed Control

<Notes>

*

*

• For parameters which No. have a suffix of "*", changed contents will be validated when you turn on the control power.

a reversed signed position data with the setup of 1.

[Adjustment]

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page

Gain Adjustment

Purpose

It is required for the servo driver to run the motor in least time delay and as faithful as possible against the commands from the host controller. You can make a gain adjustment so that you can run the motor as closely as possible to the commands and obtain the optimum performance of the machine.

<e.g. : Ball screw>

Type

<Remarks>

 • Pay extra attention to safety, when oscillation (abnormal noise and vibration) occurs, shut off the main power, or turn to Servo-OFF.

Real-Time Auto-Gain Tuning Mode

Outline

Estimates the load inertia of the machine in real time and sets up the optimum gain automatically responding to the result.

Applicable Range

Real time auto-gain tuning is applicable to all control modes.

Caution

Real-time auto-gain tuning may not be executed properly under the conditions described in the table below. In these cases, use the normal mode auto-gain tuning (refer to P.236 of Adjustment), or execute the manual auto-gain tuning (refer to P.240).

How to Operate

1) Bring the motor to stall (Servo-OFF).

2) Set up Pr21 (Setup of real-time auto-gain tuning mode) to 1-7.

When the changing degree of load inertia is large, set up 3 or 6.

When the motor is used for vertical axis, set up 4-6.

When vibration occurs during gain switching, set up 7.

- 3) Set up Pr22 (Machine stiffness at real-time auto-gain tuning) to 0 or smaller value.
- 4) Turn to Servo-ON to run the machine normally.
- 5) Gradually increase Pr22 (Machine stiffness at real-time auto-gain tuning, machine) when you want to obtain a better response. Lower the value (0-3) when you experience abnormal noise or oscillation.
- 6) Write the result to EEPROM when you want to save it.

Real-Time Auto-Gain Tuning

Parameters Which Are Automatically Set

Following parameters are automatically adjusted. Also following parameters are automatically set up.

<Notes>

- When the real-time auto-gain tuning is valid, you cannot change the parameters which are automatically adjusted.
- Pr31 becomes 10 at position or full closed control and when Pr21 (Setup of real-time auto-gain tuning) is 1 to 6, and becomes 0 in other cases.

Caution

- (1) After the start-up, you may experience abnormal noise and oscillation right after the first Servo-ON, or increase of Pr22 (Selection of machine stiffness at real-time auto-gain tuning) until the load inertia is identified (estimated) or the adaptive filter is stabilized, however, these are not failures as long as they disappear immediately. If they persist over 3 reciprocating operations, take the following measures in possible order.
	- 1) Write the parameters which have given the normal operation into EEPROM.
	- 2) Lower the setup of Pr22 (Selection of machine stiffness at real time auto-gain tuning).
	- 3) Set up the notch filter manually.
- (2) When abnormal noise and oscillation occur, Pr20 (Inertia ratio) or Pr2F (Adaptive filter frequency) might have changed to extreme values. Take the same measures as the above in these cases.
- (3) Among the results of real-time auto-gain tuning, Pr20 (Inertia ratio) and Pr2F (Adaptive filter frequency) will be written to EEPROM every 30 minutes. When you turn on the power again, the auto-gain tuning will be executed using the latest data as initial values.
- (4) When you validate the real-time auto-gain tuning, Pr27 (Setup of instantaneous speed observer) will be invalidated (0) automatically.
- (5) During the trial run and frequency characteristics measurement of "PANATERM®", the load inertia estimation will be invalidated.

Fit-Gain function

Outline

MINAS-A4 series features the Fit-gain function which executes the automatic setup of stiffness corresponding to the machine while the real time auto-gain tuning is used at position control. This function automatically searches the optimum stiffness setup by repeating reciprocating movement at position control.

Applicable Range

This function can be applicable when the following conditions are satisfied in addition to the applicable conditions for real time auto-gain tuning.

Caution

This function may not work properly under the following conditions in addition to the conditions for real time auto-gain tuning. In these cases, use the normal real-time auto-gain tuning.

Real-Time Auto-Gain Tuning

Before Operation

Before the start-up of the Fit-Gain function, set up the followings with the Fit-Gain screen and parameter setup mode of the front panel, or the Console or the Setup Support Software, "PANATERM®".

How to Operate

display (1) Bring the front panel display to EXECUTION display of the Fit-Gain screen.

(For operation of the front panel, refer to P.72 of Preparation.)

- (2) Start up the Fit-Gain function by pressing (\vee) for approx. 3sec after lowering the stiffness to 0 while the dot " . " on the right lower corner flashes.
- (3) Enter the position command which satisfies the action pattern condition of P.228, "Applicable Range".

<Caution 1>

The Fit-Gain movement requires max. 50 reciprocating movements. The Fit-gain function finishes when the optimum real-time stiffness No. is found in normal case.

(4) $\overline{F \cdot a \cdot 5h}$ will be displayed when the Fit-Gain function finishes normally, and $\overline{[\varepsilon \cdot \sigma \cdot \sigma \cdot]}$ will be displayed when this finishes with error. (You can clear ϵ ϵ ϵ α c) display by operating

any key.)

<Caution 2>

 $\overline{\xi \cdot$ $\overline{\zeta \cdot \zeta \cdot \zeta}}$ will be displayed in the following cases.

- No chattering of COIN signal and real-time stiffness NO. without micro vibration, have been found.
- One of the keys of the front panel has been operated during the Fit-Gain action, or applicable condition have not been satisfied.

Result of Fit-Gain

 $\overline{F \cdot a \cdot 5h}$ will be displayed when the Fit-Gain finishes normally, and $\overline{E \cdot a \cdot b}$ will be displayed when it finishes with some error. Write the result to EEPROM when you want to apply the result after the power reset.

[EXECUTION display] Writing of the result from the Fit-Gain screen

Press (\blacktriangledown) for approx.3sec to save the present setup to EEPROM.

Parameters Which Are Automatically Set

Following parameters are automatically adjusted. Also following parameters are automatically set up.

Caution

During the Fit-Gain movement, you may experience some noise and vibration, however, these do not give any trouble since the gain is automatically lowered. If noise and vibration persist, interrupt the Fit-Gain by pressing one of the switches of the front panel.

Adaptive Filter

Outline

Estimates the resonance frequency out of vibration component presented in the motor speed in motion, then removes the resonance component from the torque command by setting up the notch filter coefficient automatically, hence reduces the resonance vibration.

Applicable Range

This function works under the following condition.

Caution

The adaptive filter may not work properly under the following conditions. In these cases, take measures to resonance according to the manual adjustment procedures, using the 1st notch filter (Pr1D and 1E) and the 2nd notch filter (Pr28 to 2A).

How to Operate

1) Validate the adaptive filter by setting up Pr23 (Setup of adaptive filter) to 1.

Adaptive filter automatically estimates the resonance frequency out of vibration component presented in the motor speed in motion, then removes the resonance components from the torque command by setting up the notch filter coefficient automatically, hence reduces the resonance vibration.

When adaptation finishes (Pr2F does not change), and resonance point seems not change, set up the value to 2.

2) Write the result to EEPROM when you want to save it.

Caution

- (1) After the start-up, you may experience abnormal noise and oscillation right after the first Servo-ON, or when you increase the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning), until the load inertia is identified (estimated) or the adaptive filter is stabilized, however, these are not failures as long as they disappear immediately. If they persist over 3 reciprocating operations, take the following measures in possible order.
	- 1) Write the parameters which have given the normal operation into EEPROM.
	- 2) Lower the setup of Pr22 (Selection of machine stiffness at real-time auto-gain tuning).
	- 3) Invalidate the adaptive filter by setting up Pr23 (Setup of adaptive filter mode) to 0.
	- (Reset of inertia calculation and adaptive action)
	- 4) Set up the notch filter manually.
- (2) When abnormal noise and oscillation occur, Pr2F (Adaptive filter frequency) might have changed to extreme values. Take the same measures as the above in these cases.
- (3) Pr2F (Adaptive filter frequency) will be written to EEPROM every 30 minutes. When you turn on the power again, adaptive action will be executed using the latest data as initial values.
- (4) The adaptive filter is normally invalidated at torque control, however, when you select torque control while you set up Pr02 (Control mode setup) to 4 and 5, the adaptive filter frequency before mode switching will be held.

Invalidation of Adaptive Filter

When you set up Pr23 (Setup of adaptive filter) to 0, the adaptive filter function which automatically follows the load resonance will be invalidated.

If you invalidate the adaptive filter which have been working correctly, noise and vibration may occur due to the effect of resonance which have been suppressed.

Therefore, execute the copying function of the setup of adaptive filter (Pr2F) to the 1st notch frequency (Pr1D) from the Fit-Gain screen of the front panel (refer to P.72, "Fit-Gain Screen" of Preparation), or set up Pr1D (1st notch frequency) manually by using the table below, then invalidate this filter.

*Set up 1500 to Pr1D (1st notch frequency) in case of " invalid " of the above table.

Normal Mode Auto-Gain Tuning

Outline

The motor will be driven per the command with a pattern generated by the driver automatically. The driver estimates the load inertia from the necessary torque, and sets up an appropriate gain automatically.

Applicable Range

This function works under the following condition.

<Remarks>

Set up the torque limit selection (Pr03) to 1. When you set up other than 1, driver may not act correctly.

Caution

Normal mode auto-gain tuning may not be work properly under the following conditions. In these cases, set up in manual gain tuning

- Tuning error will be triggered when an error, Servo-OFF, the main power shutdown, validation of overtravel inhibition, or deviation counter clear occurs during the normal mode auto-gain tuning.
- If the load inertia cannot be calculated even though the normal mode auto-gain tuning is executed, gain value will not change and be kept as same as that of before the execution.
- The motor output torque during the normal auto-gain tuning is permitted to the max. torque set with Pr5E (Setup of torque limit).

Pay an extra attention to the safety. When oscillation occurs, shut off the main power or turn to Servo-OFF immediately. Bring back the gain to default with parameter setup. Refer to cautions of P.71, "Auto-Gain Tuning Mode" of Preparation as well.

Auto-Gain Tuning Action

(1) In the normal mode auto-gain tuning, you can set up the response with machine stiffness No..

Machine stiffness No.

- Represents the degree of machine stiffness of the customer's machine and have values from o to 15. You can set a higher No. to the high stiffness machine and set up a higher gain.
- Usually start setting up with a lower value and increase gradually to repeat auto-gain tuning in the range where no oscillation, no abnormal noise, nor vibration occurs.
- (2) This tuning repeats max. 5 cycles of the action pattern set with Pr25 (Normal mode auto-gain tuning action). Action acceleration will be doubled every one cycle after third cycle. Tuning may finish, or action acceleration does not vary before 5th cycle depending on the load, however, this is nor an error.

How to Operate

- (1) Set up the action pattern with Pr25.
- (2) Shift the load to the position where no hazard is expected even though the action pattern which is set with Pr25 is executed.
- (3) Prohibit the command entry.
- (4) Turn to Servo-ON.
- (5) Start up the auto-gain tuning. Use the front panel or the "PANATERM®". For the operation of the front panel, refer to P.71, "Auto-Gain Tuning Mode" of Preparation.
- (6) Adjust the machine stiffness to the level at which no vibration occurs and obtain the required response.
- (7) Write the result to EEPROM, if it is satisfactory.

Parameters Which Are Automatically Set

Table of auto-gain tuning

represents parameters with fixed value. Default for A to C-frame is 4, and 1 for D to F-frame.

*1 Stiffness value is 10 for position control and full-closed control, and 0 for velocity control and torque control.

*2 Lower limit for stiffness value is 10 for 17-bit encoder, and 25 for 2500P/r encoder.

Normal Mode Auto-Gain Tuning

by pressing $(\frac{S}{n})$. (4) Operation at MONITOR/EXECUTION mode

Keep pressing (A) until the display changes to $5E$ F F

 • Pin-29 of the connector, CN X5 to be Servo-ON status.

Keep pressing (A) for approx.3sec, then bar increase as the right fig. shows.

The motor starts rotating.

 For approx. 15 sec, the motor repeats max. 5 cycles of CCW/CW rotation, 2 revolutions each direction per one cycle. Tuning may finish before 5th cycles, however, this is not an error.

(5) Write the gain value to EEPROM to prevent them from being lost due to the power shut off.

<Caution>

Do not use the normal mode auto-gain tuning with the motor and driver alone. Pr20 (Inertia ratio) becomes to 0.

normally

<Notes>

Outline

Cautions are described when you want to invalidate the real time auto-gain tuning of default or the adaptive filter.

Caution

Execute the release of the automatic adjusting functions while all action stop (Servo-OFF)

Invalidation of Real-Time Auto-Gain Tuning

You can stop the automatic calculation of Pr20 (Inertial ratio) and invalidate the real-time auto-gain tuning by setting up Pr21 (Real-time auto-gain tuning setup) to 0.

Note that the calculation result of Pr20 (Inertia ratio) will be held, and if this parameter becomes abnormal value, use the normal mode auto-gain tuning or set up proper value manually obtained from formula or calculation.

Invalidation of Adaptive Filter

When you set up Pr23 (Setup of adaptive filter) to 0, adaptive filter function which automatically follows the load resonance will be invalidated.

If you invalidate the adaptive filter which have been working correctly, noise and vibration may occur due to the effect of resonance which have been suppressed.

Therefore, execute the copying function of the setup of adaptive filter (Pr2F) to the 1st notch frequency (Pr1D) from the Fit-gain screen of the front panel (refer to P.72, "Fit-Gain Screen" of Preparation), or set up Pr1D (1st notch frequency) manually by using the table below, then invalidate this filter.

*Set up 1500 to Pr1D (1st notch frequency) in case of " invalid " of the above table.

Manual Gain Tuning (Basic)

As explained previously, MINAS-A4 series features the automatic gain tuning function, however, there might be some cases where this automatic gain tuning cannot be adjusted properly depending on the limitation on load conditions. Or you might need to readjust the tuning to obtain the optimum response or stability corresponding to each load.

Here we explain this manual gain tuning method by each control mode and function.

Before Making a Manual Adjustment

You can adjust with the sound or motor (machine) movement by using the front panel or the console, however, you can adjust more securely by using wave graphic function of the setup support software, PANATERM®, or by measuring the analog voltage waveform using a monitoring function.

1. Analog monitor output

You can measure the actual motor speed, commanded speed, torque and deviation pulses by analog voltage level by using an oscilloscope. Set up the types of the signals or the output voltage level with Pr07 (Selection of speed monitor) and Pr08 (Selection of torque monitor).

For details, refer to P.41, "Wiring to the Connector, CN X5" of Preparation, and "Parameter Setup" of each control mode.

2. Waveform graphic function of the PANATERM®

You can display the command to the motor, motor movement (speed, torque command and deviation pulses) as a waveform graphic on PC display. Refer to P.276, "Outline of the Setup Support Software, PANATERM®" of Supplement.

Adjustment in Position Control Mode

Position control of MINAS-A4 series is described in Block diagram of P.82. Make adjustment in position control per the following procedures.

(2) Enter the inertia ratio of Pr20. Measure the ratio or setup the calculated value.

(3) Make adjustment using the standard values below.

Adjustment in Velocity Control Mode

Velocity control of MINAS-A4 series is described in Block Diagram of P.126 of Velocity Control Mode. Adjustment in velocity control is almost same as that in position control described in "Adjustment in Position Control Mode", and make adjustments of parameters per the procedures except the gain setup of position loop and the setup of velocity feed forward.

Manual Gain Tuning (Basic)

Adjustment in Torque Control Mode

Torque control of MINAS-A4 series is described in P.160, "Block Diagram" of Torque Control Mode. This torque control is based on velocity control while making the 4th speed of speed setup of Pr56 or SPR/ SPL input as a speed limit. Here we explain the setup of speed limiting value.

• Setup of speed limiting value

Setup the speed limiting value to the 4th speed of speed setup (Pr56) (when torque command selection (Pr5B) is 0.) or to the analog speed command input (SPR/TRQR/SPL) (when torque command selection (Pr5B) is 1).

- When the motor speed approaches to the speed limiting value, torque control following the analog torque command shifts to velocity control based on the speed limiting value which will be determined by the 4th speed of speed setup (Pr56) or the analog speed command input (SPR/TRQR/SPL).
- In order to stabilize the movement under the speed limiting, you are required to set up the parameters according to the above-mentioned "Adjustment in Velocity Control Mode".
- When the speed limiting value = 4th speed of speed setup (Pr56) , the analog speed command input is too low or the velocity loop gain is too low, or when the time constant of the velocity loop integration is 1000 (invalid), the input to the torque limiting portion of the above fig. becomes small and the output torque may not be generated as the analog torque command.

Adjustment in Full-Closed Control Mode

Full-closed control of MINAS-A4 series is described in Block diagram of P.191 of Full-Closed Control.

Adjustment in full-closed control is almost same as that in position control described in P.241 "Adjustment in Position Control Mode", and make adjustments of parameters per the procedures except cautions of P.190,

"Outline of Full-Closed Control" (difference of command unit, necessity of position loop unit conversion and difference of electronic gear).

Here we explain the setup of external scale ratio, hybrid deviation excess and hybrid control at initial setup of full-closed control.

1) Setup of external scale ratio

Setup the external scale ratio using the numerator of external scale division (Pr78), the multiplier for numerator of external scale division (Pr79) and denominator of external scale division (Pr7A).

 • Check the encoder pulse counts per one motor revolution and the external scale pulse counts per one motor revolution, then set up the numerator of external scale division (Pr78), the multiplier for numerator of external scale division (Pr79) and denominator of external scale division so that the following formula can be established.

 $Pr78$ 1 x 2 $Pr79$ ^[17] Pr7A 5000 Number of encoder pulses per motor rotation Number of external scale pulses per motor rotation

- If this ratio is incorrect, a gap between the position calculated from the encoder pulse counts and that of calculated from the external scale pulse counts will be enlarged and hybrid deviation excess (Err.25) will be triggered when the work or load travels a long distance.
- When you set up Pr78 to 0, the encoder pulse counts will be automatically set up.

2) Setup of hybrid deviation excess

Set up the minimum value of hybrid deviation excess (Pt78) within the range where the gap between the motor (encoder) position and the load (external scale) position will be considered to be an excess.

• Note that the hybrid deviation excess (Error code No.25) may be generated under other conditions than the above 1), such as reversed connection of the external scale or loose connection of the motor and the load.

Caution

- (1) Enter the command pulses based on the external scale reference.
- (2) The external scales to used for full-closed control are as follows. • AT500 series by Mitutoyo (Resolution 0.05 [µm], max. speed 2[m/s])
	- ST771 by Mitutoyo (Resolution 0.5 [µm], max. speed 2[m/s])
- (3) To prevent the runaway and damage of the machine due to the setup of the external scale, setup the hybrid deviation excess (Pr7B) to the appropriate value, in the unit of external scale resolution.
- (4) We recommend the external scale as 1/20 \leq external scale ratio \leq 20.

If you setup the external scale ratio to smaller value than 50/position loop gain (Pr10 and 18), you may not be able to control by one pulse unit. If you set up too large external scale ratio, you may expect larger noise in movement.

Gain Switching Function

At manual gain tuning, you can set 2nd gain manually in addition to 1st gain and you can switch the gain depending on the various requirements of the action such cases as,

- you want to increase the response by increasing the gain in motion
- you want to increase the servo-lock stiffness by increasing the gain at stopping
- switch to the optimum gain according to the action mode
- lower the gain to suppress the vibration at stopping.

<Example>

Following is the example when you want to reduce the noise at motor in stall (Servo-Lock), by setting up to lower gain after the motor stops.

• Make adjustment referring to the auto-gain tuning table (P.237) as well.

Setup of Gain Switching Condition

• Positing control mode, Full-closed control mode (\circ : Corresponding parameter is valid, $-$: invalid)

• Velocity control mode

• Torque control mode

*1 Delay time (Pr32 and 37) will be valid only when returning from 2nd to 1st gain.

*2 Hysteresis is defined as the fig. below shows.

*3 When you make it a condition that there is 10% torque variation during 166µs, set up the value to 200. $10\%/166\,\text{us} = \text{Setup value}$ 200 x [0.05%/166s]

*4 Designate with either the encoder resolution or the external scale resolution depending on the control mode.

*5 When you make it a condition that there is speed variation of 10r/min in 1s, set up the value to 1.

*6 When Pr31=10, the meanings of delay time, level and hysteresis are different from the normal. (refer to Fig. G)

[Adjustment]

<Caution>

Above Fig. does not reflect a timing lag of gain switching due to hysteresis (Pr34 and 39).

Suppression of Machine Resonance

In case of a low machine stiffness, you cannot set up a higher gain because vibration and noise occur due to oscillation caused by axis distortion or other causes. You can suppress the resonance using two types of filter in these cases.

1. Torque command filter (Pr14 and Pr1C)

Sets up the filter time constant so as to damp the frequency at vicinity of resonance frequency You can obtain the cut off frequency of the torque command filter in the following formula. Cut off frequency (Hz) fc = $1/(2\pi x)$ parameter setup value x 0.00001)

2. Notch filter

• Adaptive filter (Pr23, Pr2F)

MINASA-4 series feature the adaptive filter. With this filter you can control vibration of the load which resonance points vary by machine by machine and normal notch filter or torque filter cannot respond. The adaptive filter is validated by setting up Pr23 (Adaptive filter mode setup) to 1.

• 1st and 2nd notch filter (Pr1D, 2E, 28, 29 and 2A)

MINASA-4 series feature 2 normal notch filters. You can adjust frequency and width with the 1st filter, and frequency, width and depth with the 2nd filter.

How to Check the Resonance Frequency of the Machine

- (1) Start up the Setup Support Software, "PANATERM® " and bring the frequency characteristics measurement screen.
- (2) Set up the parameters and measurement conditions. (Following values are standard.)
	- Set up Pr11 (1st gain of velocity loop) to 25 or so. (to lower the gain and make it easy to identify the resonance frequency)
	- Set up the amplitude to 50 (r/min) or so. (not to saturate the torque)
	- Make the offset to 100 (r/min) or so. (to increase the speed detecting data and to avoid the measurement error in the vicinity of speed-zero)
	- Polarity is made CCW with "+" and CW with "-".
	- Setup the sampling rate to 0. (setup range to be 0-7.)
- (3) Execute the frequency characteristic analysis.

<Remarks>

• Make sure that the revolution does not exceed the travel limit before the measurement.

Standard revolutions are,

Offset (r/min) x 0.017 x (sampling rate $+1$)

Larger the offset, better measurement result you can obtain, however, revolutions may be increased.

• Set up Pr23 (Setup of adaptive filter mode) to 0 while you make measurement.

<Notes>

- When you set a larger value of offset than the amplitude setup and make the motor run to the one direction at all time, you can obtain a better measurement result.
- Set up a smaller sampling rate when you measure a high frequency band, and a larger sampling rate when you measure a low frequency band in order to obtain a better measurement result.
- When you set a larger amplitude, you can obtain a better measurement result, but noise will be larger. Start a measurement from 50 [r/min] and gradually increase it.

Relation of Gain Adjustment and Machine Stiffness

In order to enhance the machine stiffness,

- (1) Install the base of the machine firmly, and assemble them without looseness.
- (2) Use a coupling designed exclusively for servo application with high stiffness.
- (3) Use a wider timing belt. Belt tension to be within the permissible load to the motor shaft.
- (4) Use a gear reducer with small backlash.
- Inherent vibration (resonance frequency) of the machine system has a large effect to the gain adjustment of the servo.

You cannot setup a higher response of the servo system to the machine with a low resonance frequency (machine stiffness is low).

Manual Gain Tuning (Basic)

Automatic Gain Setup Function

Outline

This function initializes control parameters and gain switching parameters to the gain setups corresponding to the stiffness during auto-gain tuning, before executing a manual tuning.

Caution

When you execute the automatic gain setup function, stop the action first then make a change.

How to Use

Refer to P.72, "Fit-Gain Screen" of Preparation.

- (1) Stop the action first.
- (2) Start up the automatic gain setup function from the fit-gain screen of the front panel.
- (3) $\begin{bmatrix} F & I & I \end{bmatrix}$ will be displayed when the automatic gain setup completes normally, and $\begin{bmatrix} F & I & I \end{bmatrix}$ will be displayed when it completes with error.

(This display can be cleared by pressing any key.)

(4) If you want to store the measurement, write it to EEPROM.

Parameters Which Are Automatically Set

Parameters Which Are Automatically Set

Parameters Which Setup Values Are Automatically Fixed

*1 In case of position and full-closed control, this becomes 10, and 0 in case of velocity and torque control.

Manual Gain Tuning (Application)

Instantaneous Speed Observer

Outline

This function enables both realization of high response and reduction of vibration at stopping, by estimating the motor speed using a load model, hence improving the accuracy of the speed detection.

Applicable Range

This function can be applicable only when the following conditions are satisfied.

Caution

This function does not work properly or no effect is obtained under the following conditions.

How to Use

(1) Setup of inertia ratio (Pr20)

Set up as exact inertia ratio as possible.

- When the inertia ratio (Pr20) is already obtained through real-time auto-gain tuning and is applicable at normal position control, use this value as Pr20 setup value.
- When the inertia ratio is already known through calculation, enter this calculated value.
- When the inertia ration is not known, execute the normal mode auto-gain tuning and measure the inertia ratio.

(2) Adjustment at normal position control

Refer to P.241, "Adjustment at Position Control Mode".

(3) Setup of instantaneous velocity observer (Pr27)

- You can switch the velocity detecting method to instantaneous velocity observer by setting up Pr27 (Setup of instantaneous speed observer) to 1.
- When you experience a large variation of the torque waveform or noise, return this to 0, and reconfirm the above cautions and (1).
- When you obtain the effect such as a reduction of the variation of the torque waveform and noise, search an optimum setup by making a fine adjustment of Pr20 (Inertia ratio) while observing the position deviation waveform and actual speed waveform to obtained the least variation. If you change the position loop gain and velocity loop gain, the optimum value of the inertia ratio (Pr20) might have been changed, and you need to make a fine adjustment again.
Manual Gain Tuning (Application)

Damping Control

Outline

This function reduces the vibration by removing the vibration frequency component from the command when the load end of the machine vibrates.

Applicable Range

This function can only be applicable when the following conditions are satisfied.

Caution

 When you change the parameter setup or switch with VS-SEL, stop the action first then execute.

This function does not work properly or no effect is obtained under the following conditions.

How to Use

(1) Setup of damping frequency (1st : Pr2B, 2nd : Pr2D))

Measure the vibration frequency of the front edge of the machine. When you use such instrument as laser displacement meter, and can directly measure the load end vibration, read out the vibration frequency from the measured waveform and enter it to Pr2B or Pr2D (Damping frequency).

(2) Setup of damping filter (1st : Pr2C, 2nd : Pr2E))

First, set up 0.

You can reduce the settling time by setting up larger value, however, the torque ripple increases at the command changing point as the right fig. shows. Setup within the range where no torque saturation occurs under the actual condition. If torque saturation occurs, damping control effect will be lost.

<Remark>

Limit the damping filter setup with the following formula. 10.0 $[$ Hz $]$ – Damping frequenc \equiv Damping filter setup \leq Damping frequency

(3) Setup of damping filter switching selection (Pr24) You can switch the 1st or the 2nd damping filter depending on the vibration condition of the machine.

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What to Check ?

Protective Function (What is Error Code ?)

- Various protective functions are equipped in the driver. When these are triggered, the motor will stall due to error, according to P.43, "Timing Chart (When error occurs)"of Preparation, and the driver will turn the Servo-Alarm output (ALM) to off (open).
- Error status ands their measures
	- During the error status, the error code No. will be displayed on the front panel LED, and you cannot turn Servo-ON.
	- You can clear the error status by turning on the alarm clear input (A-CLR) for 120ms or longer.
	- When overload protection is triggered, you can clear it by turning on the alarm clear signal (A-CLR) 10 sec or longer after the error occurs. You can clear the time characteristics by turning off the connection between L1C and L2C or r and t of the control power supply of the driver.
	- You can clear the above error by operating the front panel keys. (Refer to P.73, "Alarm Clear Mode" of Preparation.)
	- You can also clear the above error by operating the "PANATERM®".

<Remarks>

 • When the protective function with a prefix of "*" in the protective function table is triggered, you cannot clear with alarm clear input (A-CLR). For resumption, shut off the power to remove the cause of the error and re-enter the power.

Protective Function (Detail of Error Code)

• Software Limit Function

1)Outline

You can make an alarm stop of the motor with software limit protection (Error code No.34) when the motor travels exceeding the movable range which is set up with Pr26 (Set up of software limit) against the position command input range.

You can prevent the work from colliding to the machine end caused by motor oscillation.

2) Applicable range

This function works under the following conditions.

3) Cautions

- This function is not a protection against the abnormal position command.
- When this software limit protection is activated, the motor decelerates and stops according to Pr68 (Sequence at alarm).

The work (load) may collide to the machine end and be damaged depending on the load during this deceleration, hence set up the range of Pr26 including the deceleration movement.

 • This software limit protection will be invalidated during the trial run and frequency characteristics functioning of the PANATERM®.

4) Example of movement

(1) When no position command is entered (Servo-ON status),

The motor movable range will be the travel range which is set at both sides of the motor with Pr26 since no position command is entered. When the load enters to the Err34 occurrence range (oblique line range), software limit protection will be activated.

(2) When the load moves to the right (at Servo-ON),

When the position command to the right direction is entered, the motor movable range will be expanded by entered position command, and the movable range will be the position command input range + Pr26 setups in both sides.

(3) When the load moves to the left (at Servo-ON),

When the position command to the left direction, the motor movable range will be expanded further.

5) Condition under which the position command input range is cleared

The position command input range will be 0-cleared under the following conditions.

- when the power is turned on.
- while the position deviation is being cleared (Deviation counter clear is valid, Pr66 (Sequence at overtravel inhibition) is 2 and over-travel inhibition input is valid.)
- At the starting and the finishing of the normal auto-gain tuning.

Troubleshooting

Motor Does Not Run When the motor does not run, refer to P.68, "Display of Factor of No-Motor Running" of Preparation as well.

Unstable Rotation (Not Smooth)

Motor Runs Slowly Even with Speed Zero at Velocity Control Mode

Positioning Accuracy Is Poor

Origin Point Slips

Abnormal Motor Noise or Vibration

Troubleshooting

Overshoot/Undershoot | Overheating of the Motor (Motor Burn-Out) |

Motor Speed Does Not Reach to the Setup Motor Revolutions (Travel) Is Too Large or Small

Parameter Returns to Previous Setup

Display of "Communication port or driver cannot be detected" Appears on the Screen While Using the PANATERM®.

[Supplement]

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Absolute System

Outline of Absolute System

When you compose an absolute system using an absolute encoder, you are not required to carry out homing operation at the power-on, and this function suits very well to such an application as a robot.

Connect the host controller with the Minas A4 with absolute specifications. (motor with absolute encoder and driver with absolute spec) and set up the parameter, Pr0B to 0, then connect the battery for absolute encoder to compose an absolute system with which you can capture the exact present position information after the power-ON.

Shift the system to origin once after installing the battery and clear the multi-turn data by clearing the absolute encoder, then you can detect the absolute position without carrying out homing operation. Via RS232 or RS485 communication, the host controller can connect up to 16 MINAS-A4 and capture the present position information as serial data to obtain the absolute position of each axis by processing. each

Applicable Mode

data.

You can use all of MINAS A4 series driver in absolute specifications by setting up parameter. Use the motor which 8th place (designated for rotary encoder specifications) is "S" (7-wire type).

M M S

^{8th place ______} Rotary encoder specifications

Absolute Specifications

There are 3 connecting methods of the host controller and MINAS-A4 driver as described below, and select a method depending on the interface of the host controller specs or number of axis to be connected. Designate a module ID to RSW of each MINAS-A4 driver when you connect multiple MINAS-A4 in communication to one host controller as shown below.

Module ID (RSW)

- When you connect each MINAS-A4 to the host separately with RS232 and switch the communication individually, designate 0 to F to each MINAS-A4. (Max. 16 axis are connectable.)
- When you connect one MINAS-A4 to the host with RS232 and connect each MINAS-A4 with RS485, designate 0 to the MINAS-A4 connected with the host, and designate 1 to F to other MINAS-A4.
- When you connect MINAS-A4 to the host with RS485, the host is given module ID of 0, and designate 1 to F to MINAS-A4. (Max 15 axis are connectable.)

M * DD driver

[Supplement]

Absolute System Configuration with RS232 Communication

Motor

Л

Battery for
absolute encoder

Absolute System Configuration with RS485 Communication

CN_{X6}

absolute encoder Positioning controller

 \overline{CN} X5

* Battery for absolute encoder is required to store the multi-turn data into the encoder. Connect the battery between BAT+ and BAT– of the motor.

Battery (for Backup) Installation

First Installation of the Battery

After installing and connecting the back-up battery to the motor, execute an absolute encoder setup. Refer to P.271, "Setup (initialization) of Absolute Encoder ".

It is recommended to perform ON/OFF action once a day after installing the battery for refreshing the battery.

A battery error might occur due to voltage delay of the battery if you fail to carry out the battery refreshment.

Replacement of the Battery

It is necessary to replace the battery for absolute encoder when battery alarm occurs.

Replace while turning on the control power. Data stored in the encoder might be lost when you replace the battery while the control power of the driver is off.

After replacing the battery, clear the battery alarm. Refer to P.275, "How to Clear the Battery Alarm".

<Caution>

When you execute the absolute encoder with the front panel (refer to P.77 of Preparation), or via communication (refer to P.302), all of error and multi-turn data will be cleared together with alarm, and you are required to execute "Setup (Initialization) of absolute encoder" (refer to P.271).

How to Replace the Battery

1) Refresh the new battery.

Connector with lead wire of the battery to CN601 and leave of 5 min. Pull out the connector from CN601 5 min after.

2) Take off the cover of the battery box.

3) Install the battery to the battery box.

Place the battery with + facing downward. The connect the connect the connector.

4) Close the cover of the battery box.

<Caution>

Use the following battery for absolute encoder. Part No. : DV0P2990 (Lithium battery by Toshiba Battery Co., Ltd. ER6V, 3.6V 2000mAh)

<Cautions>

- Be absolutely sure to follow the precautions below since improper use of the battery can cause electrolyte to leak from the battery, giving rise to trouble where the product may become corroded, and/or the battery itself may rupture.
	- 1) Insert the battery with its " $+$ " and " $-$ " electrodes oriented correctly.
	- 2) Leaving a battery which has been used for a long period of time or a battery which is no longer usable sitting inside the product can cause electrolyte leakage and other trouble. For this reason, ensure that such a battery is replaced at an early date. (As a general guideline, it is recommended that the battery be replaced every two years.)
		- The electrolyte inside the battery is highly corrosive, and if it should leak out, it will not only corrode the surrounding parts but also give rise to the danger of short-circuiting since it is electrically conductive. For this reason, ensure that the battery is replaced periodically.
	- 3) Do not disassemble the battery or throw it into a fire.
		- Do not disassemble the battery since fragments of the interior parts may fly into your eyes, which is extremely dangerous. It is also dangerous to throw a battery into a fire or apply heat to it as doing to may cause it to rupture.
	- 4) Do not cause the battery to be short-circuited. Under no circumstances must the battery tube be peeled off.
		- It is dangerous for metal items to make contact with the " + " and " " electrodes of the battery since such objects may cause a high current to flow all at once, which will not only reduce the battery performance but also generate considerable heat, possibly leading to the rupture of the battery.
	- 5) This battery is not rechargeable. Under no circumstances must any attempt be made to recharge it.
- The disposal of used batteries after they have been replaced may be subject to restrictions imposed by local governing authorities. In such cases, ensure that their disposal is in accordance with these restrictions.

Absolute System

<Reference>

Following example shows the life calculation of the back-up battery used in assumed robot operation. 2000[mAh] of battery capacity is used for calculation. Note that the following value is not a guaranteed value, but only represents a calculated value. The values below were calculated with only the current consumption factored in. The calculations do not factor in electrolyte leakage and other forms of battery deterioration. Life time may be shortened depending on ambient condition.

1) 2 cycles/day

a : Current consumption in normal mode 3.6[µA] b : Current consumption at power failure timer mode 280[µA]

 * Power failure timer mode...Action mode in time period when the motor can respond to max. speed even the power is off (5sec).

c : Current consumption at power failure mode 110[µA]

Annual consumption capacity = $(10h \times a + 0.0014h \times b + 2h \times c) \times 2 \times 313$ days + 24h x c x 52 days = 297.8[mAh] Battery life = 2000[mAh] $/297.8$ [mAh] = 6.7 (6.7159) [year]

2) 1 cycle/day

(2nd cycle of the above 1) is for rest.

Annual consumption capacity = $(10h \times a + 0.0014h \times b + 14h \times c) \times 313$ days + 24h x c x 52 days = 640.6[mAh]) Battery life = 2000 [mAh] /630.6[mAh] = 3.1 (3.1715) [year]

When you make your own cable for 17-bit absolute encoder

When you make your own cable for 17-bit absolute encoder, connect the optional battery for absolute encoder, DV0P2060 or DV0P2990 as per the wiring diagram below. Connector of the battery for absolute encoder shall be provided by customer as well.

<Cautions>

Install and fix the battery securely. If the installation and fixing of the battery is not appropriate, it may cause the wire breakdown or damage of the battery.

Refer to the instruction manual of the battery for handling the battery.

• Installation Place

- 1) Indoors, where the products are not subjected to rain or direct sun beam.
- 2) Where the products are not subjected to corrosive atmospheres such as hydrogen sulfide, sulfurous acid, chlorine, ammonia, chloric gas, sulfuric gas, acid, alkaline and salt and so on, and are free from splash of inflammable gas, grinding oil, oil mist, iron powder or chips and etc.
- 3) Well-ventilated and humid and dust-free place.
- 4) Vibration-free place

Wiring Diagram

Setup (Initialization) of Absolute Encoder

Execute the setup of absolute encoder in the following cases.

- Initial setup of the machine
- When absolute system down error protection (alarm No. 40) occurs
- When the encoder cable is pulled out

In the above setup, it is required to make multi-turn data to 0 after clearing the encoder error by clearing absolute encoder while the machine stops at the origin position with homing operation. Clear the absolute encoder with the front panel operation or with the PANATERM operation. After the clearing, turn off the power and turn on the power again.

Setup Operation of Absolute Encoder

- (Auxiliary function mode) Mode Selection \leftarrow Execution (1) Turn on the power to bring he machine to origin position Automatic offset adjustment mode by homing operation. (2) Make the front panel to Motor trial run mode ដ ច ដ ប់ចប់ auxiliary function mode and bring EXECUTION Alarm clear mode display of "Absolute encoder clear mode". Refer Absolute encoder to P.51, "Setup of Paraclear mode meter and Mode" of Preparation.
- (3) Execute the following key operation at EXECUTION DISPLAY

Note) In case of incremental encoder, $\overline{\xi \cdot \zeta \cdot \zeta}$ display appears when absolute encoder clear starts.

(4)Turn off the control power once, then re-enter the power.

Transmission and Reception Sequence of Absolute Data

Servo-Ready output will be turned on 2sec. after the control power is turned on. Capture the absolute data in the following communication protocol while the Servo-Ready output is on and the fix the motor with brake by Servo-Off (when the motor is at complete stall.).

RS232 Communication Protocol

Refer to the instruction manual of the host for the transmission/reception method of command.

Data of *1 and *2 are determined by the setup of RSW (ID) of the front panel.

Check sum becomes OK'ed when the lower 8-bit of the sum of the received absolute data (15 characters) is 0.

Enter the RSW value of the driver to which you want to communicate from the host to axis (*1 data) of the command block, and transmit the command according to the RS232 communication protocol. For details of communication, refer to P.278, "Communication".

- **Allow 500ms or longer interval for axis switching when you want to capture multiple axes data.**
- **It is recommended for you to repeat the above communication more than 2 times to confirm the absolute data coincide, in order to avoid mis-operation due to unexpected noise.**

RS485 Communication Protocol

Refer to the instruction manual of the host for the transmission/reception method of command. Following shows the communication example of the driver to RSW (ID).

Data of *1 and *2 are determined by the setup of RSW (ID) of the front panel.

Check sum becomes OK'ed when the lower 8-bit of the sum of the received absolute data (15 characters) is 0.

Command from the host will be transmitted to the desired driver based on RS485 transmission protocol. For details of communication, refer to P.278, "Communication".

- **Allow 500ms or longer interval for axis switching when you want to capture multiple axes data.**
- **It is recommended for you to repeat the above communication more than 2 times to confirm the absolute data coincide, in order to avoid mis-operation due to unexpected noise.**

Absolute System

Composition of Absolute Data

Absolute data consists of singe-turn data which shows the absolute position per one revolution and multiturn data which counts the number of revolution of the motor after clearing the encoder.

Single-turn data and multi-turn data are composed by using 15-character data (hexadecimal binary code) which are received via RS232 or RS485.

• Details of multi-turn data

<Remark>

If the multi-turn data of the above fig. is between 32768 and 65535, convert it to signed date after deducting 65536.

• Encoder status (L)-----1 represents error occurrence.

• Encoder status (L)-----1 represents error occurrence.

ttery error e of the following has occurred. ttery alarm, multi-turn error, counter overflow, counter error, full absolute status, Counter overflow multi-turn error, battery error or battery alarm

• Transmit the absolute data while fixing the motor with brake by turning to Servo-Off.

<Note>

For details of the above error protection, refer to P.252, "Protective Function" of When in Trouble, and for contents of alarms, refer to the following "Display of Battery Alarm".

Display of Battery Alarm

Following alarm will be displayed when making the front panel to alarm execution mode of monitor mode.

How to Clear the Battery Alarm

Replace the battery for absolute encoder when battery alarm occurs according to P.268, "How to Replace the Battery". After replacement, clear the battery alarm in the following 3 methods.

- (a) "CN X5" Connecting Alarm clear input (A-CLR) to COM– for more than 120ms.
- (b) Executing the alarm clear function in auxiliary function mode by using the console (option).
- (c) Click the "Battery warning" Clear button, after select the "Absolute encoder" tab in the monitor display window by using the PANATERM (option).

Outline of Setup Support Software, "PANATERM®"

Outline of PANATERM®

With the PANATERM®, you can execute the followings.

- (1) Setup and storage of parameters, and writing to the memory (EEPROM).
- (2) Monitoring of I/O and pulse input and load factor.
- (3) Display of the present alarm and reference of the error history.
- (4) Data measurement of the wave-form graphic and bringing of the stored data.
- (5) Normal auto-gain tuning
- (6) Frequency characteristic measurement of the machine system.

How to Connect

Install the "PANATERM®" to Hard Disc

you log on "PANATERM®".

<Cautions/Notes>

- 1. 15MB capacity of hard disc is required. OS to be Window® 98, Windows® 2000, Windows® Me or Windows® XP.
- 2. Install the "PANATERM®" to a hard disc, using the setup disc according to the procedures below to log on.
- 3. Part No. of the "PANATERM[®]" may be changed based on the version up. Refer to the catalog for the latest part No.

Procedure of install

- 1) Turn on the power of the computer to log on the supporting OS. (Exit the existing logged on software.)
- 2) Insert the setup disc of the "PANATERM®" to CD-ROM drive.
- 3) The window opens automatically so click the name of the file required. * If the window fails to appear automatically, start up Explorer, and run the targeted setup file.
- 4) Operate according to the guidance of the setup program.
- 5) Click \Box OK \Box on the installation verification window to start the setup.
- 6) Exit all applications and log on Windows® again.

"PANATERM®" will be added on program menu when you log on again.

Log on of the "PANATERM®" .

<Cautions/Notes>

- 1. Once the "PANATERM®" is installed in the hard disc, you do not need to install every time you log on.
- 2. Connect the driver to a power supply, the motor and encoder before you log on. Refer to the instruction manual of supporting OS for start.

Procedure of log on

- 1) Turn on the power of the computer and log on the supporting OS.
- 2) Turn on the power of the driver.
- 3) Click the start bottom of the supporting OS.
- (Refer to the instruction manual of supporting OS for start.)
- 4) Select the "PANATERM®" with program \blacktriangleright and click.
- 5) The screen turns to "PANATERM®" after showing opening splash for approx. 2sec.

For more detailed information for operation and functions of the "PANATERM®", refer to the instruction manual of the Setup Support Software, "PANATERM®".

Communication

Outline of Communication

You can connect up to 16 MINAS-A4 series with your computer or NC via serial communication based on RS232 and RS484, and can execute the following functions.

- (1) Change over of the parameters
- (2) Referring and clearing of alarm data status and history
- (3) Monitoring of control conditions such as status and I/O.
- (4) Referring of the absolute data
- (5) Saving and loading of the parameter data

Merits

- You can write parameters from the host to the driver in batch when you start up the machine.
- You can display the running condition of machine to improve serviceability.
- You can compose multi-axis absolute system with simple wiring.

Following application software and cables are prepared as options. For the operation of the "PANATERM®, refer to the instruction manual of the PANATERM®.

Communication Specifications

Connection of Communication Line

MINAS-A4 series provide 2 types of communications ports of RS232 and RS485, and support the following 3 types of connection with the host.

• RS232 communication

Connect the host and the driver in one to one with RS232, and communicate according to RS232 transmission protocol.

• Set up the module ID of MINAS-A4 to RSW of the front panel. In the above case, you can set any value of 0 to F. You can set the same module ID as long as the host has no difficulty in control.

• RS232 and RS485 communication

When you connect one host to multiple MINAS-A4s, connect the host to connector $|X4|$ of one driver with RS232 communication, and connect each MINAS-A4 with RS485 communication. Set up the RSW of the driver to 0 which is connected to the host, and set up 1 to F to other drivers each.

• RS485 communication

Connect the host to multiple MINAS-A4s with RS485 communication, set up the RSW of each front panel of MINAS-A4 to 1 to F.

Allow 500ms or longer interval for switching the axes while capturing data of multiple axes.

Communication

• Connection to the host with RS485

Communication Method

 • Set up the RS232 communication baud rate with Pr0C, and RS485 communication baud rate with Pr0D. The change of these parameters will be validated after the control power entry. For details, refer to the following list of parameters related to communication.

List of User Parameters for Communication

• Required time for data transmission per 1 byte is calculated in the following formula in case of 9600[bps].

$$
1000 / 9600 \times (1 + 8 + 1) = 1.04 [ms/byte]
$$

Start bit ________ 25top bit

Data

Note that the time for processing the received command and time for switching the line and transmission/ reception control will added to the actual communication time.

• Handshake code

Following codes are used for line control.

ENQ ... The module (host or driver) sends out ENQ when it has a block to send.

EOT The module (host or driver) sends out EOT when it is ready to receive a block. The line enters to a transmission mode when ENQ is transmitted and EOT is received.

ACK When the received block is judged normal, the module (host or driver) will send out ACK.

NAK.... When the received block is judged abnormal, NAK will be sent. A judgment is based on checksum and timeout.

<Caution>

1 byte of module recognition is added to ENQ and EOT at RS485 communication.

Module recognition byte... Make the RSW value of the front panel as a module ID, and data which makes its bit7 as 1, becomes a module recognition byte.

Module ID : The module ID of the host side will be 0 in case of RS485 communication, therefore set up RSW of MINAS-A4 to 1- F.

Transmission Sequence

• Transmission protocol

• In case of RS232

• In case of RS485

• Line control

Decides the direction of transmission and solves the contention.

Reception mode... From when the module (host or driver) returns EOT after receiving ENQ. Transmission mode... From when the module (host or driver) receives EOT after transmitting ENQ. At contention of transmission and reception... Slave side will enter to reception mode when it receives ENQ while waiting for EOT after transmitting ENQ, by giving priority to ENQ (of master side).

• Transmission control

On entering to transmission mode, the module transmits the command block continuously and then waits for ACK reception. Transmission completes at reception of ACK.. ACK may not be returned at transmission failure of command byte counts. If no ACK is received within T2 period, or other code than NAK or ACK is received, sequence will be retried. Retry will start from ENQ.

• Reception control

On entering to reception mode, the module receives the transmitted block continuously. It will receive the command byte counts from the first byte, and continuously receive extra 3 bytes. It will return ACK when the received data sum becomes 0, by taking this status as normal. In case of a check sum error or a timeout between characters, it will return NAK.

• Data Block Composition

Below shows the composition of data block which is transmitted in physical phase.

N : Command byte counts (0 to 240)

Shows the number of parameters which are required by command.

- axis : Sets up the value of RSW of the front panel (Module ID,
- command : Control command (0 to 15)
- mode : Command execution mode (0 to 15)
	- Contents vary depending on the mode.

check sum : 2's complement of the total number of bytes, ranging from the top to the end of the block

• Protocol Parameter

Following parameters are used to control the block transmission. You can set any value with the INIT command (described later).

- T1 Permissible time interval for this driver to receive the consecutive character cods which exists between the module recognition bytes and ENQ/EOT, or in the transmission/reception data block. Time out error occurs and the driver returns NAK to the transmitter when the actual reception time has exceeded this setup time
- T2 Permissible time interval for the driver to transmit ENQ and to receive EOT. If the actual reception time exceeds this setup, this represents that the receiver is not ready to receive, or it has failed to receive ENQ code in some reason, and the driver will re-transmit ENQ code to the receiver. (retry times)
	- Permissible time interval for the driver to transmit EOT and to receive the reception of the 1st character code. The driver will return NAK and finishes the reception mode if the actual reception has exceeded this setup time.
	- Permissible time interval for the module to transmit the check sum bytes and to receive ACK. The module will re-transmit ENQ code to the receiver in the same way as the NAK reception, if the actual reception time exceeds this setup time.
- RTY Maximum value of retry times. Transmission error occurs if the actual retry has exceeds this setup value.
- M/S Switching of master and slave. When contention of ENQ has occurred, the module decides which is to be given priority.

Priority is given to the transmitter which is set up as a master. (0: Slave mode, 1 : Master mode)

Example of Data Communication

• e.g. Reference of Absolute Data

When you connect the host to one driver with RS232 communication, and connect multiple MINAS-A4s with RS485 communication. Following flow chart describes the actual flow of the communication data when you want to capture the absolute data of the module ID=1.

e.g. of capturing the absolute data

Following shows the communication data in time series when you want to capture the absolute data. Data is presented in hexadecimals.

Supplement **Supplement**

Allow 500ms or longer interval for switching the axis while capturing data of multiple axes.
• Example of Parameter Change

Following shows the communication data in time series when you change parameters. Communication in general will be carried out in sequence of (1) Request for capturing of execution right, (2) Writing of individual parameter, and (3) Writing to EEPROM when saving of data is required, and (4) Release of execution right. Here the hardware connection shows the case that the driver (user ID=1) is directly connected to the host with RS232C. Date is presented in hexadecimals.

<Caution>

For details of command, refer to P.290, "Details of Communication Command".

Status Transition Chart

• RS232 Communication

• RS485 Communication

<Caution>

Above time represents a period from the rising edge of the stop bit.

List of Communication Command

• Use the above commands only. If you use other commands, action of the driver cannot be guaranteed.

 • When the reception data counts are not correct in the above command, transmission byte1 (Error code only) will be returned regardless of communication command.

Details of Communication Command

4 bit of the upper data as 0.)

• Version will be displayed in figures from 0 to 9. (e.g. Version 3.1 will be upper data 30h, lower data 13h.)

[Supplement]

- RTY is 4-bit, and M/S is 1-bit.
- Unit... T1 : 0.1s, T2 : 1s

• RTY is 4-bit, and M/S is 1-bit.

• Capture the execution right to prevent the conflict of the operation via communication and that with the front panel.

• Enquires for the capture of the execution right at parameter writing and EEPROM writing, and release the execution right after the action finishes.

• mode = 1 : Enquires for the capture of the execution right mode = 0 : Enquires for the release of the execution right

• You cannot operate with the front panel at other than monitor mode while the execution right is captured via communication.

• When the module fails to capture the execution right, it will transmit the error code of in use.

[Supplement]

command pulses)

• Counter value in 32 bit.

• Counter value will be "-" for CW and "+" for CCW.

• Module returns the present position of feedback pulse counter in absolute coordinates from the staring point.

• Counter value will be "–" for CW and "+" for CCW.

• Feedback pulse counter is the total pulse counts of the encoder and represents the actual motor position traveled

• Output value in 16 bit

• Torque command will be "–" value for CW and "+" value for CCW.

[Supplement]

and 26 (mode = 6).

• External scale FB pulse sum will return the present position of the external scale counter in absolute coordinates from the starting point.

3 2 1 0

FB pulse sum (H)

external scale deviation

 (H) error code checksum

(L)

• External scale FB pulse sum will be "-" for CW and "+" for CCW.

6 5 4

Command error RS485 error

Error code

bit7 0 : Normal 1 : Error

• External scale deviation becomes "+" when the external scale is positioned at CW direction against position command, and "–" when it is positioned at CCW direction.

• If the parameter No. is not within the range of 0 x 00 to 0 x 7F, No. error will be returned.

• This command change parameters only temporarily. If you want to write into EEPROM, execute the parameter writing to $EPPROM$ (mode = 4).

• Set up parameters not in use to 0 without fail, or it leads to data error. Data error also occurs when the parameter value exceeds the setup range.

• When under-voltage occurs, error code of control LV will be returned instead of executing writing.

[Supplement]

• You can read out last 14 error events.

[Supplement]

• Designate 0 to 7 to page No. and read out 16 parameters from each specified page. • No. error will be returned when other No. than 0 to 7 is entered to page No.

Supplement **Supplement**

• Designate 0 to 7 to page No. and write 16 parameters from each specified page.

• Set up o to parameters not in use without fail, or data error will occur. Data error will also occurs when data exceeding the setup range is transmitted.

• No. error will be returned when other No. than 0 to 7 is entered to page No.

MEMO

Division Ratio for Parameters

Relation between Electronic Gear and Position Resolution or Traveling Speed

Here we take a ball screw drive as an example of machine.

A travel distance of a ball screw M \lceil mm \rceil corresponding to travel command P1 \lceil P \rceil , can be described by the following formula (1) by making the lead of ball screw as $L \upharpoonright mm$]

M = P1 x (D/E) x (1/R) x L (1)

therefore, position resolution (travel distance ∆M per one command pulse) will be described by the formula (2) ∆M = (D/E) x (1/R) x L (2)

modifying the above formula (2), electronic gear ratio can be found in the formula (3).

D = (∆M x E x R) x L(3)

Actual traveling velocity of ball screw, V[mm/s] can be described by the formula (4) and the motor rotational speed, N at that time can be described by the formula (5).

V = F x (D/E) x (1/R) x L (4)

N = F x (D/E) x 60(5)

modifying the above formula (5), electronic gear ratio can be found in the formula (6).

D = (N x E)/ (F x 60) (6)

<Notes>

4)

- 1) Make a position resolution, ∆M as approx. 1/5 to 1/10 of the machine positioning accuracy, $\Delta \epsilon$, considering a mechanical error.
- 2) Set up Pr48 and Pr4B to any values between 1 to 10000.
- 3) You can set up any values to a numerator and denominator, however, action by an extreme division ratio or multiplication ratio cannot be guaranteed. Recommended range is 1/50 to 20 times.

[Supplement]

Conformity to EC Directives and UL Standards

EC Directives

The EC Directives apply to all such electronic products as those having specific functions and have been exported to EU and directly sold to general consumers. Those products are required to conform to the EU unified standards and to furnish the CE marking on the products.

However, our AC servos meet the relevant EC Directives for Low Voltage Equipment so that the machine or equipment comprising our AC servos can meet EC Directives.

EMC Directives

MINAS Servo System conforms to relevant standard under EMC Directives setting up certain model (condition) with certain locating distance and wiring of the servo motor and the driver. And actual working condition often differs from this model condition especially in wiring and grounding. Therefore, in order for the machine to conform to the EMC Directives, especially for noise emission and noise terminal voltage, it is necessary to examine the machine incorporating our servos.

Conformed Standards

IEC : International Electrotechnical Commission

- EN : Europaischen Normen
- EMC : Electromagnetic Compatibility

UL : Underwriters Laboratories

CSA : Canadian Standards Association

<Precautions in using options>

Use options correctly after reading operation manuals of the options to better understand the precautions. Take care not to apply excessive stress to each optional part.

Peripheral Equipments

Installation Environment

Use the servo driver in the environment of Pollution Degree 1 or 2 prescribed in IEC-60664-1 (e.g. Install the driver in control panel with IP54 protection structure.)

Power Supply

- (1) This product is designed to be used at over-voltage category (Installation category) II of EN 50178:1997. If you want to use this product un over-voltage category (Installation category) III, install a surge absorber which complies with EN61634-11:2002 or other relevant standards at the power input portion.
- (2) Use an insulated power supply of DC12 to 24V which has CE marking or complies with EN60950

Circuit Breaker

Install a circuit breaker which complies with IEC Standards and UL recognizes (Listed and ω_0 marked) between power supply and noise filter.

Noise Filter

When you install one noise filter at the power supply for multi-axes application, contact to a manufacture of the noise filter.

L

Conformity to EC Directives and UL Standards

Surge Absorber

Provide a surge absorber for the primary side of noise filter.

<Remarks>

Take off the surge absorber when you execute a dielectric test to the machine or equipment, or it may damage the surge absorber.

Noise Filter for Signal Lines *

Install noise filters for signal lines to all cables (power cable, motor cable, encoder cable and interface cable) * In case of D-frame, install 3 noise filters at power line.

<Caution> Fix the signal line noise filter in place to eliminate excessive stress to the cables.

Grounding

- (1) Connect the protective earth terminal (\bigoplus) of the driver and the protective earth terminal (PE) of the control box without fail to prevent electrical shocks.
- (2) Do not make a joint connection to the protective earth terminals (\oplus). 2 terminals are provided for protective earth.

Ground-Fault Breaker

Install a type B ground fault breaker (RCD) at primary side of the power supply.

<Note>

For driver and applicable peripheral equipments, refer to P.32 "Driver and List of Applicable Peripheral Equipments" of Preparation.

Driver and List of Applicable Peripheral Equipments (EC Directives)

Refer to P.28 to 41, "System Configuration and Wiring"

Conformity to UL Standards

Observe the following conditions of (1) and (2) to make the system conform to UL508C (File No. E164620).

- (1) Use the driver in an environment of Pollution Degree 2 or 1 prescribed in IEC60664-1. (e.g. Install in the control box with IP54 enclosure.)
- (2) Install a circuit breaker or fuse which are UL recognized (LISTED ω marked) between the power supply and the noise filter without fail.

For the rated current of the circuit breaker or fuse, refer to P.32, "Driver and List of Applicable Peripheral Equipments" of Preparation.

Use a copper cable with temperature rating of 60˚C or higher.

Tightening torque of more than the max. values (M4:1.2N• m, M5: 2.0N•m) may break the terminal block. (3) Over-load protection level

Over-load protective function will be activated when the effective current exceeds 115% or more than the rated current based on the time characteristics. Confirm that the effective current of the driver does not exceed the rated current. Set up the peak permissible current with Pr5E (Setup of 1st torque limit) and Pr5F (Setup 2nd torque limit).

Options

Specifications of for Motor Connector

• Pin disposition for encoder connector

• Pin disposition for motor/brake connector (with brake)

• Pin disposition for motor/brake connector (without brake)

1kW, 1.5kW, 2kW MSMA	MSMA 3kW, 4kW, 5kW	MFMA 400W, 1.5kW	MFMA 2.5kW, 4.5kW
1kW, 1.5kW, 2kW MDMA	MDMA 3kW, 4kW, 5kW		
MHMA 500W, 1kW, 1.5kW	2kW,3kW,4kW,5kW MHMA		
MGMA 900W	MGMA 2kW, 3kW, 4.5kW		
Ď \overline{A} $\frac{1}{B}$ ်ီ	Ď. Ā $\frac{1}{B}$ \mathbf{C}	Ĥ G B \oplus^{F} \oplus \oplus Ē Ď $\tilde{\mathbf{S}}$	B С $\overline{\oplus}$ F ⊕ \oplus \mathbf{S} Ĥ
JL04V-2E20-4PE-B-R	JL04V-2E22-22PE-B-R	JL04V-2E20-18PE-B-R	JL04V-2E24-11PE-B-R
(by Japan Aviation	(by Japan Aviation	(by Japan Aviation	(by Japan Aviation
Electronics or equivalent)	Electronics or equivalent)	Electronics or equivalent)	Electronics or equivalent)
PIN No. Content	PIN No. Content	PIN No. Content	PIN No. Content
Α U-phase	A U-phase	G NC.	NC. Α
B V-phase	B V-phase	H NC	B NC
$\overline{\mathsf{c}}$ W-phase	$\overline{\mathrm{c}}$ W-phase	NC Α	\overline{C} NC.
D Earth	D Earth	F U-phase	D U-phase
		V-phase	E V-phase
		в W-phase	F W-phase
		Ē Earth	G Earth
		D Earth	Н Earth
		C NC	NC.

Do not connect anything to NC pins.

Table for junction cable by model of MINAS A4 series

Options

Junction Cable for Encoder

MFECA00EAE** Fig. 2-1

MFECA00EAD**

Note) Battery for absolute encoder is an option.

MSMD 50W to 750W, MQMA100W to 400W, MAMA 100W to 750W 17-bit incremental encoder without battery holder

MSMD 50W to 750W, MQMA 100W to 400W, MAMA 100W to 750W

(14)

 (4) (14) (4)

MSMA, MDMA, MHMA, MGMA, MFMA

Fig. 2-4

17-bit absolute encoder with battery holder

Note) Battery for absolute encoder is an option.

MSMA, MDMA, MHMA, MGMA, MFMA

17-bit incremental encoder without battery holder, 2500P/r encoder

Junction Cable for Motor (ROBO-TOP® 105˚C 600V• DP)

ROBO-TOP® is a trade mark of Daiden Co.,Ltd.

MFMCA00EED** MSMD 50W to 750W, MQMA 100W to 400W, MAMA 100W to 750W

Fig. 3-1

MFMCD02ECD** Fig. 3-2

MSMA 1.0kW to 1.5kW, MDMA 1.0kW to 1.5kW MHMA 500W to 1.5kW, MGMA 900W

MFMCD02ECT**

Fig. 3-3

MFECA03ECT**

Fig. 3-4

MSMA 3.0kW to 5.0kW, MDMA 3.0kW to 5.0kW MHMA 2.0kW to 5.0kW, MGMA 2.0kW to 4.5kW

MSMA 2.0kW, MDMA 2.0kW

MFMA 400W to 1.5kW

MFMCD03ECT**

MFMA 2.5kW to 4.5kW

Fig. 3-6

Supplement **Supplement**

Options

Junction Cable for Motor with Brake (ROBO-TOP® 105˚C 600V• DP)

MFMCA02FCD**

Fig. 4-1

MSMA 1.0kW to 1.5kW, MDMA 1.0kW to 1.5kW MHMA 500W to 1.5kW, MFMA 400W to 1.5kW MGMA 900W

ROBO-TOP® is a trade mark of Daiden Co.,Ltd.

MFMCA02FCT**

MSMA 2.0kW, MDMA 2.0kW

MSMA 3.0kW to 5.0kW, MDMA 3.0kW to 5.0kW

Fig. 4-2

MHMA 2.0kW to 5.0kW, MFMA 2.5kW to 4.5kW MGMA 2.0kW to 4.5kW

Junction Cable for Brake (ROBO-TOP® 105˚C 600V• DP)

MSMD 50W to 750W MQMA 100W to 400W MAMA 100W to 750W

ROBO-TOP® is a trade mark of Daiden Co.,Ltd.

Connector Kit for External Peripheral Equipments

1) Par No. **DV0P4350**

3) Pin disposition (50 pins) (viewed from the soldering side)

<Cautions>

- 1) Check the stamped pin-No. on the connector body while making a wiring.
- 2) For the function of each signal title or its symbol, refer to the wiring example of the connector CN I/F.
- 3) Check the stamped pin-No. on the connector body while making a wiring.

Interface Cable

1) Par No. **DV0P4360**

2) Dimensions

<Remarks>

Color designation of the cable e.g.) Pin-1 Cable color : Orange (Red1) : One red dot on the cable

Communication Cable (for connection to PC)

Par No. **DV0P1960 (DOS/V machine)**

Mini-DIN 8P MD connector

 \Rightarrow $\boxed{\circ}$

Communication Cable (for RS485)

Setup Support Software "PANATERM®"

1) Part No. **DV0P4460 (English/Japanese version)**

2) Supply media : CD-ROM

<Caution>

For setup circumstance, refer to the Instruction Manual of [PANATERM®].

Options

Connector Kit for Motor/Encoder Connection

These are required when you make your own encoder and motor cables.

Options

Mounting Bracket

<Caution>

For E and F-frame, you con make a front end and back end mounting by changing the mounting direction of L-shape bracket (attachment).

Console

Part No. **DV0P4420**

Reactor

Harmonic restraint

On September, 1994, "Guidelines for harmonic restraint on heavy consumers who receive power through high voltage system or extra high voltage system" and "Guidelines for harmonic restraint on household electrical appliances and general-purpose articles" established by the Agency for Natural Resources and Energy of the Ministry of Economy, Trade and Industry (the ex-Ministry of International Trade and Industry). According to those guidelines, the Japan Electrical Manufacturers' Association (JEMA) have prepared technical documents (procedure to execute harmonic restraint: JEM-TR 198, JEM-TR 199 and JEM-TR 201) and have been requesting the users to understand the restraint and to cooperate with us. On January, 2004, it has been decided to exclude the general-purpose inverter and servo driver from the "Guidelines for harmonic restraint on household electrical appliances and general-purpose articles". After that, the "Guidelines for harmonic restraint on household electrical appliances and general-purpose articles" was abolished on September 6, 2004.

We are pleased to inform you that the procedure to execute the harmonic restraint on general-purpose inverter and servo driver was modified as follows.

- 1.All types of the general-purpose inverters and servo drivers used by specific users are under the control of the "Guidelines for harmonic restraint on heavy consumers who receive power through high voltage system or extra high voltage system". The users who are required to apply the guidelines must calculate the equivalent capacity and harmonic current according to the guidelines and must take appropriate countermeasures if the harmonic current exceeds a limit value specified in a contract demand. (Refer to JEM-TR 210 and JEM-TR 225.)
- 2. The " Guidelines for harmonic restraint on household electrical appliances and general-purpose articles"
was abolished on September 6, 2004. However, based on conventional guidelines, JEMA applies the
technical document was abolished on September 6, 2004. However, based on conventional guidelines, JEMA applies the technical documents JEM-TR 226 and JEM-TR 227 to any users who do not fit into the "Guidelines for harmonic restraint on heavy consumers who receive power through high voltage system or extra high voltage system" from a perspective on enlightenment on general harmonic restraint. The purpose of these guidelines is the execution of harmonic restraint at every device by a user as usual to the utmost extent.
Options

External Regenerative Resistor

Manufacturer : Iwaki Musen Kenkyusho

* Power with which the driver can be used without activating the built-in thermostat.

DV0P4280, DV0P4281 DV0P4282,DV0P4283

05

0220

100

100

100

thermostat
(light vellow x2)

 \sim

<Remarks>

Thermal fuse is installed for safety. Compose the circuit so that the power will be turned off when the thermostat is activated. The thermal fuse may blow due to heat dissipating condition, working temperature, supply voltage or load fluctuation.

Make it sure that the surface temperature of the resistor may not exceed 100°C at the worst running conditions with the machine, which brings large regeneration (such case as high supply voltage, load inertia is large or deceleration time is short) Install a fan for a forced cooling if necessary.

Regenerative resistor gets very hot.

Take preventive measures for fire and burns.

Avoid the installation near inflammable objects, and easily accessible place by hand.

Battery For Absolute Encoder

Battery

- (1) Part No. **DV0P2990**
- (2) Lithium battery by Toshiba Battery Co. ER6V, 3.6V 2000mAh

<Caution>

This battery is categorized as hazardous substance, and you may be required to present an application of hazardous substance when you transport by air (both passenger and cargo airlines).

Recommended components

Surge Absorber for Motor Brake

**List of Peripheral Equipments (and in the case of the conduction of the case of the conduction *

* The above list is for reference only. We may change the manufacturer without notice.

Dimensions (Driver)

[Supplement]

Dimensions (Driver)

• MAMA 100W to 750W

<Cautions>

• MSMD 50W to 100W

<Cautions>

<Cautions>

• MQMA 100W to 400W

<Cautions>

• MSMA 1.0kW to 2.0kW

<Cautions>

• MSMA 3.0kW to 5.0kW

<Cautions>

• MDMA 1.0kW to 1.5kW

Supplement **Supplement**

<Cautions>

• MDMA 2.0kW to 3.0kW

<Cautions>

• MDMA 4.0kW to 5.0kW

<Cautions>

• MGMA 900W to 2.0kW

<Cautions>

<Cautions>

• MFMA 400W to 1.5kW

MFMA series (Middle inertia) MFMA | 04 * P1 * | 04 * S1 * | 15 * P1 * | 15 * S1 * 400W 1.5kW 120 145 55 19 145 110 130 165 6 12 84 118 9 45 42 6h9 6 15.5 65 35 200 114.3 176 233 3.2 18 84 143 13.5 55 50 10h9 8 30 120 145 4.7 6.7 4.7 6.7 11.0 14.0 11.0 14.0 145 170 145 170 L R S L A L B L C L D L E L F L G L H L Z L W L K K W K H R H Refer to P.312, "Options". Motor model Motor output Mass (kg) Connector/Plug specifications Rotary encoder specifications Without brake With brake Without brake With brake L L Key way
dimensions dimensions 2500P/r Incremental 17-bit 17-bit
Absolute/Incremental 2500P/r Incremental Absolute/Incre Absolute/Incremental

<Cautions>

• MFMA 2.5kW to 4.5kW

* Dimensions are subject to change without notice. Contact us or a dealer for the latest information.

<Cautions>

• MHMA 500W to 1.5kW

<Cautions>

• MHMA 2.0kW to 5.0kW

<Cautions>

Permissible Load at Output Shaft

Radial load (P) direction Thrust load (A and B) direction

Unit : N (1kgf=9.8N)

<Note>

When the load point varies, calculate the permissible radial load, P (N) from the distance of the load point, L (mm) from the mounting flange based on the formula of the right table, and make it smaller than the calculated result.

Motor Characteristics (S-T Characteristics) [Supplement]

- Note that the motor characteristics may vary due to the existence of oil seal or brake.
- Continuous torque vs. ambient temperature characteristics have been measured with an aluminum flange attached to the motor (approx. twice as large as the motor flange).

- These are subject to change. Contact us when you use these values for your machine design.
- Ratio to the rated torque at ambient temperature of 40˚C is 100% in case of without oil seal, without brake.

speed

Motor Characteristics (S-T Characteristics)

* These are subject to change. Contact us when you use these values for your machine design.

* Ratio to the rated torque at ambient temperature of 40˚C is 100% in case of without oil seal, without brake.

[Supplement]

* These are subject to change. Contact us when you use these values for your machine design.

Supplement

Supplement

Motor Characteristics (S-T Characteristics)

* These are subject to change. Contact us when you use these values for your machine design.

0 10 20 30 40

ambient temp. [˚C]

50

ý, ratio

15 (9.54)

(28.5)

0

speed [r/min]

1000 2000 3000 (2200)

Peak running range Continuous running range

[Supplement]

* These are subject to change. Contact us when you use these values for your machine design.

Supplement **Supplement**

Motor Characteristics (S-T Characteristics)

* These are subject to change. Contact us when you use these values for your machine design.

0 10 20 30 40

 $\overline{0}$

 (42.9)

1000 2000

Continuous running range

speed [r/min] speed [r/min]

ratio vs.

0 10 20 30 40

speed [r/min] ambient temp. [°C]

ratio[,]

 $\overline{0}$

1000 2000

Continuous running range

Combination of Driver and Motor with Gear Reducer

This driver is designed to be used in the combination with the specified motor model. Check the series name, rated output and voltage specifications and the encoder specifications of the applicable motor.

Incremental Specifications, 2500P/r

<Remark>

Do not use the driver and the motor with gear reducer in other combinations than the one in the following table.

• Incremental specifications, 2500P/r

• Absolute/Incremental specifications, 17bit

<Note>

• "*" of the model No. represents the structure of the motor.

Motor with Gear Reducer

 $(\text{unit} \cdot \text{mm})$

Permissible Load at Output Shaft

Radial load (P) direction Thrust load (A and B) direction

Unit : N (1kgf=9.8N)

Remarks on installation

- (1) Do not hit the output shaft of the gear reducer when attaching a pulley or sprocket to it. Or it may cause an abnormal noise.
- (2) Apply the load of the pulley or the sprocket to as close to the base of the output shaft as possible.
- (3) Check the mounting accuracy and strength of the stiff joint, when you use it.
- (4) The encoder is built in to the motor. If an excessive impact is applied to the motor while assembling it to the machine, the encoder might be damaged. Pay an extra attention at assembly.

Characteristics of Motor with Gear Reducer [Supplement]

Dotted line represents the torque at 10% less supply voltage.

Block Diagram of Driver

Block Diagram by Control Mode

Position Control Mode

• when Pr02 (Setup of control mode) is $\overline{0}$ when Pr02 (Setup of control mode) is $\overline{3}$ and 1st control mode when Pr02 (Setup of control mode) is $|4|$ and 1st control mode

Velocity Control Mode

• when Pr02 (Setup of control mode) is $|1|$ when Pr02 (Setup of control mode) is $\overline{3}$ and 2nd control mode when Pr02 (Setup of control mode) is $\overline{5}$ and 1st control mode

Torque Control Mode

• when Pr02 (Setup of control mode) is $\boxed{2}$.

when Pr02 (Setup of control mode) is $\overline{4}$ and 2nd control mode

when Pr02 (Setup of control mode) is $\overline{5}$ and 2nd control mode

Full-closed Control Mode

• when Pr02 (Setup of control mode) is $|6|$,

Supplement **Supplement**
Specifications

Hit & Stop" Homing and "Press & Hold" Control

Homing with Hit & Stop

You can set up the homing position with "Hit & Stop" where it is not easy to install a sensor due to environment.

- (1) when you make a point where the work (load) hits as an origin
- (2) when you stop the work (load) using Z-phase after making a hitting point as a starting point, then make that stopping point as an origin.

<Remarks>

Make the Pin-27 H (Off=Open) after the Hit & Stop Homing is completed.

[Supplement]

0

Press & Hold Control

MEMO

Motor Company, Matsushita Electric Industrial Co.,Ltd.Marketeing Group

Repair

Consult to a dealer from whom you have purchased the product for details of repair.

When the product is incorporated to the machine or equipment you have purchased, consult to the manufacture or the dealer of the machine or equipment.

Cautions for Proper Use

- This product is intended to be used with a general industrial product, but not designed or manufactured to be used in a machine or system that may cause personal death when it is failed.
- •Install a safety equipments or apparatus in your application, when a serious accident or loss of property is expected due to the failure of this product.
- Consult us if the application of this product is under such special conditions and environments as nuclear energy control, aerospace, transportation, medical equipment, various safety equipments or equipments which require a lesser air contamination.
- We have been making the best effort to ensure the highest quality of the products, however, application of exceptionally larger external noise disturbance and static electricity, or failure in input power, wiring and components may result in unexpected action. It is highly recommended that you make a fail-safe design and secure the safety in the operative range.
- If the motor shaft is not electrically grounded, it may cause an electrolytic corrosion to the bearing, depending on the condition of the machine and its mounting environment, and may result in the bearing noise. Checking and verification by customer is required.
- Failure of this product depending on its content, may generate smoke of about one cigarette. Take this into consideration when the application of the machine is clean room related.
- •Please be careful when using in an environment with high concentrations of sulphur or sulphuric gases, as sulphuration can lead to disconnection from the chip resistor or a poor contact connection.
- Take care to avoid inputting a supply voltage which significantly exceeds the rated range to the power supply of this product. Failure to heed this caution may result in damage to the internal parts, causing smoking and/or a fire and other trouble.

Technical information

Electric data of this product (Instruction Manual, CAD data) can be downloaded from the following web site. http://industrial.panasonic.com/ww/i_e/25000/motor_fa_e/motor_fa_e.html

MEMO (Fill in the blanks for reference in case of inquiry or repair.)

Motor Company Matsushita Electric Industrial Co., Ltd.

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