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College of Engineering
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# Design and implementation of a Petit-four machine 

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By the guidance of our supervisor, and by the acceptance of all members in the testing committee, this project is delivered to Mechanical Engineering Department in the college of Engineering, to be as a partial fulfillment of the requirement of the department for the degree of B.sc .

Supervisor signature

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## List of contents:

List of Contents ..... II
List of Figures ..... IV
List of Tables ..... VI
Abstract ..... VI
الاهداء ..... VI
CHAPTER1 : Introduction ..... 1
1.1 Introduction ..... 2
1.2 Project idea and importance ..... 3
1.3 Recognition of the Need ..... 4
1.3.1 Need of petit-four for bakery sweet ..... 4
1.3.2 Quality of petit-four. ..... 4
1.4 Project Objectives ..... 5
1.5 Time schedule for the project ..... 5
1.6 Total Cost for the Project ..... 6
CHAPTER2 : Production of A Petit-Four ..... 7
2.1 Introduction ..... 8
2.2 Traditional method of production ..... 8
2.3 Automated method of production ..... 10
2.3.1 Loading Stage ..... 11
2.3.2 Pulling and pressing stage. ..... 12
2.3.3 Casting Stage. ..... 13
2.3.4 Transporting Stage. ..... 14
CHAPTER3 : Mechanical Design ..... 15
3.1 Proposal system description and specification ..... 16
3.2 Introduction. ..... 17
3.3 Conceptual Design ..... 18
3.4 Mechanical Design. ..... 18
3.4.1 The Container ..... 18
3.4.2 Pulling Cylinder System. ..... 21
3.4.3 Container Rod ..... 27
3.4.4 The Conveyor ..... 30
3.4.4.a Tray ..... 30
3.4.4.b Belt. ..... 30
3.4.4.c Mass of Conveyor ..... 34
3.4.5 Sliding system ..... 36
3.3.5.a Beam Design. ..... 36
3.3.5.b Cam Motor Calculation ..... 38
3.4.6 Machine Body ..... 40
3.4.7 Welding Design ..... 42
CHAPTER4 : PLC Programming ..... 45
4.1 Introduction ..... 46
4.2 PLC Characteristic ..... 46
4.3 PLC Graph ..... 50
CHAPTER5 : Electrical Design \& Protection ..... 52
5.1 Introduction ..... 53
5.2 Motors ..... 53
5.2.1 CAM Motor ..... 53
5.2.2 Conveyer Motor ..... 53
5.2.3 Pulling Motor. ..... 53
5.3 Voltage Frequency Driver ..... 54
5.3.1 CAM motor voltage frequency driver ..... 54
5.3.2 Conveyer Motor Voltage Frequency Driver ..... 54
5.4 Sensor ..... 55
5.5 (Power \& Control) Circuit ..... 56
5.6 Electrical Panel \& Protection ..... 57
5.6.1 Motor Overload ..... 57
5.6.2 Contactor ..... 57
5.6.3 Switches ..... 58
5.6.4 Klements ..... 58
5.6.5 LED ..... 59
CHAPTER6 : Experimental Result \& Recommendations ..... 60
6.1 Introduction ..... 61
6.2 Experimental Result. ..... 61
6.3 Recommendations ..... 62
6.4 Future Work ..... 62
Appendix A ..... 64
Appendix B ..... 69
Appendix C ..... 76
References ..... 86

## Lists of Figures:

Figure 1.1 Shapes of petit-four ..... 2
Figure 2.1 Preparation of the petit-four dough ..... 8
Figure 2.2 Forming the dough by handle dough mold ..... 9
Figure 2.3 Put pieces on the tray ..... 9
Figure 2.4 Petit-four presented in a beautiful shape ..... 9
Figure 2.5 Proposed design of the machine ..... 10
Figure 2.6 Container ..... 11
Figure 2.7 Pulling cylinder ..... 12
Figure 2.8 Molds ..... 13
Figure 2.9 Cast pieces on the tray ..... 13
Figure 2.10 Conveyor system ..... 14
Figure 2.11 Cam follower mechanism ..... 14
Figure 3.1 The machine in 3D. ..... 16
Figure 3.2 The machine in 2D. ..... 16
Figure 3.3 Dough container [mm] ..... 19
Figure 3.4 Pulling Cylinder. ..... 22
Figure 3.5 Cylinder section ..... 22
Figure 3.6 Cylinder section ..... 23
Figure 3.7 Container position. ..... 24
Figure 3.8 Power transition for pulling motor. ..... 25
Figure 3.9 Shear and Bending moment ..... 27
Figure 3.10 Deflection of container beam. ..... 28

Figure 3.11 Tray dimension. 30
Figure 3.12 Belt in 3D. 30
Figure 3.13 Double Conveyor in 2D. 32
Figure 3.14 Free body diagram of belt 32
Figure 3.15 Fraction between belt and conveyor frame. 33
Figure 3.16 Conveyor frame dimension[mm] and area. 34
Figure 3.17 Conveyor frame with Rolling tube. 35
Figure 3.18 Rolling tube section 35
Figure 3.19 Shaft section. 36
Figure 3.20 Conveyer beam 37
Figure 3.21 Beam dimension 37
Figure 3.22 Beam deflection 37
Figure 3.23 Cam system. 38
Figure 3.24 Machine body 40
Figure 3.25 Free body diagram of machine body. 41
Figure 3.26 Free body diagram for machine support. 41
Figure 3.27 Free body diagram for cutting beam 42
Figure 3.28 Beam section 42
Figure 3.29 Welding joint. 42
Figure 3.30 Weld pattern. 43
Figure 4.1 PLC Connection. 48
Figure 4.2 PLC Schneider TWDLCAA24DRF. 49
Figure 4.3 TwidoSuite micro/win64 program. 49
Figure 4.4 The state graph " Automatic Mode ". 50
Figure 4.5 The state graph " Manual Mode ". 51
Figure 5.1 CAM motor inverter. 54
Figure 5.2 Conveyer motor inverter. 54
Figure 5.3 Limit Switch. ..... 55
Figure 5.4 Electrical Panel. ..... 55
Figure 5.5 Power Circuit. ..... 56
Figure 5.6 Motor overload. ..... 57
Figure 5.7 Contactor. ..... 57
Figure 5.8 Emergence, Pushbutton, and Select Switch. ..... 58
Figure 5.9 Klements. ..... 58
Figure 5.10 LED. ..... 59
Figure 6.1 Pitie-Fore Sizes. ..... 61
Figure 6.2 The Final Machine. ..... 62

## Lists of Tables:

Table 1.1 Time schedule for the introduction project ..... 2
Table 1.2 Total cost of the project ..... 4
Table 3.1 Properties of Delrin material ..... 25
Table 3.2 Bearing coefficient factor ( $C_{t}$ ) ..... 26
Table 3.3 Pulling Motor characteristic ..... 27
Table 3.4 Properties of belt ..... 30
Table 3.5 Conveyor motor characteristic ..... 34
Table 3.6 Cam motor characteristic ..... 40
Table 4.1 PLC VS Microcontroller ..... 46
Table 4.2 Logic Allocation ..... $47 \& 48$


#### Abstract

Most Bakeries and Pastry shops in Palestine uses the traditional way of producing the Petit-four sweets, the traditional way has many disadvantages in terms of Inconsistency of a petit-four pieces, Effort and a long time in production, in addition a unhealthy product As a result of the use of human hands in production.

This project aimed to solving this problem by design and implementation of a Petitfour machine that producing the petit-four in automatic way. The machine was desired to reduce the time and effort that need for production and to ensure the healthy of the product.


## الاهداء

نهدي مشروعنا هذا اللى قدوتنا ومعلبنا وقائد امتنا حهد صلى الله عليه وسلم

للى مـ رعونا بنور تلبهم. .وحمونا بحكتنهم...وتدموا لنا حنانهم وتلبهم . إلى م~ سقونا وألطعونا وربونا وأبونا. . وونحونا
 قيود الظلام.. إلى بسبة الأمل ونبع الحنان إلى مـ هم بلسم روحنا إلى ورود حياتنا إلى مـ رعونا بحنانهم .. اليكم والدينا ..

،إلى می يحملون في عيونهم زكريات طفولتنا وشبابنا. ...إخوتنا وأخواتنا

إلى مح ضحوا بحريتهم مـ أجل حرية غيرهم....الأسرى والمعتُقلِن
إلى مـ هم أكرم منا مكانة....شهداء نلسطين

إلى شمعة أحرتت نغسها لتضيء لم هم حولها. .اليك يا وردة فاح عبيرها وطاب شذاها. .اليك يا وردة زاد بريقها ورونتها. .مازا بوسعنا أن نتول لقد هربت منا الكللات وتشتت شمل العبارات..لا ندري أي الكلام يفيدك حتّك. .بل أي العبارات تليق بمقامك.. نديـى الشكر الى مشرننا العزيز الدكتور بوسف السويطي الذي أنار لنا الطريق ولم يبخل علينا بتوجبهاته ونصائحه وللى معلبينا الذيـى لم يبخلوا علينا بعلهم والذي لولا جهددهم لـا وصلنا لـا خحى عليه الان كـا ونوجه شكـر خاص الى المخرطة الهندسية الميكانيكية ممثله بمديرها المهندس صاح دويك لجهودهم معنا في خراطة اجزاء الالة الميكانيكية ، ولكل مى ساهم بانجاز عبلنا هذا الذيـي لم يدخروا جهدا ني تُقديم المساعدة لنا مـ تونير المصادر والمراجع اللازمة وكل التُقير للذيـى منهونا كل التشجيع •

ولا ننسى أيضا أصدقائنا الذيـى وتنوا إلى جانبنا في السراء والضراء وخصوصا الذيـ كانوا اصدقاء أونياء ولم يتُددوا ني مد يد العون لنا سائلين الملى عز وجل بأن يجبعنا بهم في جنات الخلد ع الرسل والصديقينِ والشهداء والأبرار حيث لا يوجد نراق

## 1

## Chapter One

## Introduction to Petit-four machine

1.1 Introduction .
1.2 Project idea and importance .
1.3 Recognition of the Need .
1.4 Project Objectives .
1.5 Time schedule for the project .
1.6 Total Cost for the Project .

### 1.1 Introduction

Petit-Four is a French dish originally sweets, label taken from French society (Petit-Four as in figure 1.1) which Means "little oven", the Petit-Four usually eaten after meals or between as a dessert with tea or coffee. There are many types of it, There's even a salty Petit Four offers on special occasions.


Figure 1.1: Shapes of Petit-Four.
The Petit-Four is attend from flour, butter, egg yolks, sugar, baking powder and vanilla; And added to the pieces after baked decorative materials as Jam and Cream.

In Palestinian society the Petit-Four considered essential product with some people, where we have made the study of the local market and from this study found that $40 \%$ of people consume the Petit-Four on a daily basis.

The Petit-Four was produced at the first time in the eighteenth century by the traditional way, during the process of cooling oven "made of brick" after the use of fire in order to benefit from the heat latent within these furnaces.

## Types of Petit-Four :

There are three main types of the Petit-Four :-

1. Decorated or iced.
2. Salty, and is opening an appetite suppressant, so provides in concerts and buffets.
3. Dry, as Biscuit.

## Nutritional value of the Petit-Four product

A piece of a Petit-Four (about 30 grams) has the following nutritional values:

1. Calories: 83
2. Fat: 5
3. Saturated fat: 3
4. Cholesterol: 14
5. Carbohydrates: 8
6. Proteins: 1

### 1.2 Project idea and importance

The idea of the project is to design and implement a machine that makes a Petit-Four by an automatic way and is controlled by a programming PLC.

The importance of the project is summarized by the following points:-

1. Save the time needed to produce these types.
2. Reduce effort and number of workers.
3. Produce inconsistent types of petit-four that equal in weight and size.
4. Ensure you to get the health product.
5. Increase productivity and production of different types and varieties that difficult to make it by traditional methods.

### 1.3 Recognition of the Need.

### 1.3.1 A need of Petit-Four for bakery sweet use :

The research team made a questionnaire took (13) purposeful sample of bakery sweet who have Petit-Four, to decide if there is an important of the project, and if there is really a need for an automated Petit-Four machine.

The analysis of the questionnaire is attached in Appendix A. And here some of the results.
$15 \%$ of the participants who have Producing more than 150 kg of Petit-Four daily, as shown in Figure 1.2 . This is a large percentage, so we decide to work with them, and solve their problem.

Also according to the questioner results about $11 \%$ have 5 worker or larger, because of large quantity Figure 1.3 which the project come with the solution of it.

Figure 1.3. Number of workers.

As shown in Figure 1.4, 92.3\% says they are ready to buy the Petit-Four machine, and the other say yes but, if the cost was good.

Figure 1.2. Daily production of Petit-Four.



Figure 1.4.The desire to buy the machine.

### 1.3.2. Quality of Petit-Four

In Palestine and other Arab world countries, there's need for machine that gives a high quality of Petit-Four, our project will give higher quality than all current ways of traditional production methods, by using a modern method of production that will concerned cleanliness of the product and an elaborate form of the product.

According to the questionnaire the machine must have the following features:

1. Low noise.
2. Ease for use.
3. High safety factor, safe for worker.
4. Keeps clean \& healthy.

### 1.4 Project Objectives

1. To build an automated machine of Petit-Four for bakery sweet.
2. To introduce modern technology for the local market.
3. To make a combination from traditional and automated methods for Petit-Four .
4. To achieve high quality Petit-Four .

### 1.5 Time schedule for the introduction project

Table 1.1 Time schedule for the introduction project.

| Task No. Of Week | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Identification Of <br> Project Idea |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Drafting a Preliminary <br> Project Proposal |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Introduction About <br> Project <br> (Chapter 1) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| General Description <br> About Project <br> (Chapter 2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Mechanical Design <br> (Chapter 3) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

### 1.6 Total Cost for the Project

Table 1.2. Total cost of the project.

| Components | Price(NIS) | Quantity | Total <br> (NIS) |
| :--- | :--- | :--- | :--- |
| Cylinder Stainless Steel | 200 | 2 | 400 |
| Standees Steel Container | 300 | 1 | 300 |
| Bearing | 40 | 10 | 400 |
| Motor's And Gears | 900 | 3 | 2700 |
| Sheets Of Stainless Steel | 1000 | 1 | 1000 |
| Profile's Of Stainless Steel | 500 | - | 500 |
| PLC | 650 | 1 | 650 |
| Encoder | 600 | 1 | 600 |
| Sliders | 200 | 1 | 200 |
| Micro Switches | 20 | 5 | 100 |
| Gears | 300 | 3 | 900 |
| Bolts Of Stainless Steel | 150 | 1 | 150 |
| Trays | 150 | 2 | 300 |
| Belt Drives | 600 | 1 | 600 |
| Raw Materials | 2000 | 1 | 2000 |
| Lathing | 1500 | 1 | 1500 |
|  |  |  | 12300 |

## 2

# Chapter Two <br> Production of a Petit-Four 

2.1 Introduction .
2.2 Traditional Method Of Production .
2.3 Automated Method Of Production .

### 2.1 Introduction.

The production of a Petit-Four pieces has two methods, traditional method (manually) or modern method (automatically), since the Petit-Four is a foodstuff and is related to the health of the human we should follows the international standard of production, in this chapter we will show the stages of production of the Petit-Four.

### 2.2 Traditional Method Of Production.

Before we start explaining the automated stages of producing the Petit-Four, We have to recognize the traditional method of producing it, to evolve in our minds the principle that used for production the Petit-Four.

Petit-Four are produced in homes, bakeries and sweets shops, most of them used the traditional method of producing it by a manual way. Production of a Petit-Four by using this method passes through a multi stages :-

Step 1 : Preparation of the petit-four dough as shown in figure 2.1.


Figure 2.1: Preparation of the Petit-Four dough.

Step 2 :- Forming the dough by a handle dough mold as shown in figure 2.2 .


Figure 2.2: Forming the dough by handle dough mold.
Step3 :- Put the resulting pieces on the tray as shown in figure 2.3 .


Figure 2.3: Put pieces on the tray.
Step4 :- Put the tray after filling it by pieces in the oven and presented in beautiful shape after completion in the oven as shown in figure 2.4.


Figure 2.4 Petit-four presented in a beautiful shape.

Manual method in the production of Petit-Four take a long period of time and need a greater effort and human energy, also since the Petit-Four must be a healthy product and is not harmful to human health due to the pollution that results from hands and the human, we should replace this method by the automatic method (without Human intervention) that will show in the next section.

### 2.3 Automated Method Of Production

In our project we will show the new technology in produced of a Petit-Four using a full automated machine programmed with a PLC, which will allows the user to control the operation of the machine by an pushbutton installed on a machine body, This method of production will ensure to get healthy product and save the time and reduce the number of workers required to perform this task. The proposed machine is shown in the figure 2.5 .


Figure 2.5 : Proposed design of the machine.

In order to take an image in our minds about how the machine works and the manufacturing stages passes through it to get the final product, we divided the stages of production into four stages as shown in figure 2.5 :-

1. Loading stage
2.Pulling and pressing stage

## 3. Casting stage

## 4. Transporting system

These four stages are integrated with each other in order to get the final product, in the coming sections each stage will be explained in full details.

### 2.3.1 Loading Stage:

The Loading stage starting when the user put the dough into the container manually, in this stage we will describe the container that carries the dough.

## Stainless Steel Container

Because it concerns with the stuff food and in order to get a healthy product, the container material must be careful chosen, so stainless steel material's used after reviewing the specifications of this material as shown below:

1. High oxidation resistance at ambient temperature.
2. High corrosion resistance and staining.
3. High resistance attack from acids.
4. Relatively poor conductor of electricity.
5. Resistant to high temperatures.

According to these properties, the stainless steel is used as a material to make the container of the machine.


Figure 2.6: Container.
The container that shown in figure 2.6 has a volume of 52 liter and it can carries a 64 kg of dough, more details will be considered in chapter 3 .

### 2.3.2 Pulling And Pressing Stage

After the user load the dough to the container, the two cylinder driven by a motor will pull and press the dough into the molds, the dough will flow in each hole of molds to get its final form before casting in the tray.

## Pulling Cylinder :


a. Pulling cylinder.

b. Pulling cylinder with housing.

Figure 2.7 Pulling cylinder.
In order to get the force that need for pull and press the dough into molds, design two toothed cylinder as shown in figure 2.7.a that moves in opposite of each other with distance to pulling the dough from container into casting molds as shown in figure 2.7.b. The two cylinder which made from delrin material ${ }^{1}$ and the reason of chosen this material it have low density compared to steel and that give us a small weight. properties of this material can be summarized as :

1. Good dimensional stability.
2. Low moisture absorption.
3. Can operate in wet environments with little effect on performance or dimensions.
4. Excellent machinability.
5. High fatigue endurance.
6. High strength and stiffness properties.
7. Superior impact and creep resistance.
8. Chemical resistance to fuels and solvents.
9. Good wear and abrasion properties.

Typical property values and technical product data Sheet of these material is shown in Appendix B.

### 2.3.3 Casting Stage

Casting Process occurs by molds as shown in figure 2.8 after the pulling cylinder pull and press the dough into the holes of molds, have a Six pieces molds in our machine that made from delrin material, these molds able to make a 5 shapes of a Petit-Four.


Figure 2.8 : Molds.
Through compressive strength that results from the motion of pulling cylinders in opposite direction, the mold will cast the dough into the tray. The molds will cast a Six pieces of a Petit-Four at the same time as shown in figure 2.9 and this operation will continue until filling the tray which has sequential step wise motion controlled by PLC.


Figure 2.9: Cast pieces on the tray.

### 2.3.4 Transporting Stage

To transport the tray to fill it with a Petit-Four pieces that pouring from casting molds, we need a conveyor (Transporting System) driven by a motor as shown in figure 2.10


Figure 2.10: Conveyor system.
The conveyor system consist of two shafts, belt, and roller tube, one of the two shafts is driven by a motor and the other is follower.

The conveyor is moving up, down, right, and left to transport the tray and to complete the operation of filling the tray with the different shapes of Petit-Four pieces; This process is done by a cam follower mechanism that connected with a linear bearing to hold the base of conveyor and push up and down or left and right as commanded by the user of machine (shown in figure 2.11 ).The shafts and roller tube is made of stainless steel, and the belt is made from rubber metal.


Figure 2.11: Cam follower mechanism.

# 3 

## Chapter Three Mechanical Design

3.1 Proposal System Description And Specifications.
3.2 Introduction.
3.3 Conceptual Design.
3.4 Mechanical Design.
3.5 Welding Calculation.

### 3.1 Proposal System Description And Specifications.

The first step in mechanical design is to know the hole operation of the system and to know how the machine is bind as shown in figure 3.1 and figure 3.2.


Figure 3.1: The machine in 3D.


Figure 3.2 : The machine in 2D.

In the next sections the parts of the machine will be describe in full details .

### 3.2 Introduction

As explained before, the production of Petit-Four passes through four stages (prepare the dough, load the dough to container, pull the dough into molds, loaded the formed dough by molds into tray ).

The dough is prepared and loaded to the container manually, but the process of pulling the dough into the molds is done by two cylinders are moving contrary to each other, and moving them is done by an electric motor through a gearbox to get the opposite rotational movement to be pulling the dough inside the container to the casting molds.

After pulling the dough into casting molds, the dough is loaded to tray by the molds, this process is done through the pressure force that result from the weight of the dough and from the pulling force of the rotating pulling cylinder.

In this design the machine, is divided it into five parts, which are connected to each other to cover all stages needed, these parts are:-

1. Container.
2. Cylinders.
3. Conveyer.
4. Molds.
5. Machine body.

Since the machine is used for production of a foodstuff and in order to get a healthy and clean product, most of the machine parts are made of stainless steel that has resistance to corrosion and prevent food poisoning; And in order to obtain a good and simple design a set of parameters must be considered, these parameters are related to the machine itself such as: safety, portability, cost, design simplicity, availability, work space, easy to move, volume occupied by the machine. On the other hand, the design must be able to produce a high quality Petit-Four related into the international standard.

### 3.3 Conceptual Design

It is desired to design and produce a Petit-Four machine fully automated and controlled. The process starts when the user puts the Petit-Four dough in the container and press the start button, the dough will be transferred to the two cylinder which applying pressure to the dough and pulling it to the casting molds, then the molds loading the dough into the tray, we have a six casting molds which will produce a six pieces of Petit-Four at the same time, the process will repeated until the tray is filled.

The machines divided into four subsystems:-

1. loading system.
2. Pulling system.
3. Casting system.
4. Transporting system.

### 3.4 Mechanical Design

In this section each block will be explained in details, the used material for most parts in this machine is stainless steel (304L) suitable for food uses.

### 3.4.1 The Container

The first step in the whole operation start in the container as shown in figure 3.2 which designed to hold ( 64 kg ) of Petit-Four dough.

a. Top view

b. Overall view

c. Side View

d. Bottom View

f. Front view

Figure 3.3:Dough container [mm].

Need find the area of stainless steel that used for make the container, disassemble the container into multi section or parts needed, the parts shown at Figure 3.3.

First at figure 3.3(c) the area of this section divided to two part:
First rectangular area $\left(A_{1}\right)$ :
$A_{1}=t_{1} * \mathrm{~W}$

$$
\begin{equation*}
=5.0415 * 40=201.66 \mathrm{~cm}^{2} \tag{3.1}
\end{equation*}
$$

Second trapezoidal $\left(A_{2}\right)$ :
$A_{2}=\frac{H(b 1+b 2)}{2}$
$=\frac{29.9585(40+17)}{2}=853.81725 \mathrm{~cm}^{2}$

$$
\begin{equation*}
A=A_{1}+A_{2} \tag{3.3}
\end{equation*}
$$

By substitution Eq (3.1) and Eq (3.2) in Eq (3.3) can find the area of first rectangular :
$\mathrm{A}=201.66+853.81725=1055.47 \mathrm{~cm}^{2}$
$t_{1}$ : Width of rectangular at figure 3.3.c $(\mathrm{cm})$.
b1:Length of larger base of trapezoidal $(\mathrm{cm})$.
b2:Length small base trapezoidal (cm).
H :Hight of container (cm).

Second at figure 3.3(d) the area of this section divided to two part
Rectangular area $\left(A_{3}\right)$ :
$A_{3}=t_{2} * l$

$$
\begin{equation*}
=3 * 17=51 \mathrm{~cm}^{2} \tag{3.4}
\end{equation*}
$$

Rectangular area $\left(A_{4}\right)$ :

$$
\begin{align*}
& A_{4}=t_{2} * \mathrm{~L}  \tag{3.5}\\
& \quad=3 * 50=150 \mathrm{~cm}^{2}
\end{align*}
$$

$t_{2}$ :Width of rectangular at figure 3.3.d (cm).
L: Length of container (cm).
$l$ : Length of rectangular 3 at figure 3.3.d (cm).

Third at figure 3.3(f) the area of this section divided to two part
Rectangular area $\left(A_{5}\right)$ :

$$
\begin{align*}
A_{5} & =t_{3} * \mathrm{~L}  \tag{3.6}\\
& =32.09 * 50=1604.5 \mathrm{~cm}^{2}
\end{align*}
$$

Rectangular area $\left(A_{6}\right)$ :

$$
\begin{align*}
A_{6} & =t_{1} * \mathrm{~L}  \tag{3.7}\\
& =5.0415 * 50=252.075 \mathrm{~cm}^{2}
\end{align*}
$$

$t_{3}$ : Width of rectangular at figure 3.3.f ( cm ).

To find the area of stainless steel that need to make the container, should found the total area of the upper parts:-

$$
\begin{aligned}
\text { Total area } & =2 *\left(A+A_{3}+A_{4}+A_{5}+A_{6}\right) \\
& =2 *(1055.47+51+150+1604.5+252.075) \\
& =0.623 \mathrm{~m}^{2}
\end{aligned}
$$

In order to find the mass Petit-Four dough contains in the container first have to find the volume of container and the density of Petit-Four dough and for this we made an experiment by taking a Petit-Four dough and filling out in a can with a mass and volume known and find the density of the Petit-Four dough.

The volume of container :

$$
\begin{align*}
\mathrm{V} & =\mathrm{A} * \mathrm{~L}  \tag{3.8}\\
& =1055.47 * 50=52.77 * 10^{3} \mathrm{~cm}^{3}
\end{align*}
$$

The mass of Petit-Four dough:

$$
\begin{aligned}
\mathrm{M} & =\mathrm{V}^{*} \rho \\
& =0.05277 * 1200 \approx 64 \mathrm{Kg}
\end{aligned}
$$

L: Length of container (cm).
W :Width of container (cm).
$\rho$ : Density of petit-four dough $\left(\mathrm{Kg} / \mathrm{m}^{3}\right)$.
A: The side area of the container.

### 3.4.2 Pulling Cylinder System

The design of this stage must be suitable and able to break the Petit-Four dough including the slot, and produce a force that pull the dough into the molds. in order to determine the required force to pull the dough and design the cylinders. It is desirable to make an experiment on bread dough machine with different forces.

In order to find the force required to pulling the dough into molds, we make an experiment on the bread dough machine and we applied a different force from frequency inverter (device used for control of induction motor) to show at what value of force the cylinder starting to move and pulling the dough, first we applied a 75 N force but the cylinders still not move at this value, then we increase the force to 125 but the cylinder also still no move, and we increase the force until the cylinder is moving and pulling the dough into molds and this occurred at force 180 N .

From this experiment, the selected force for this stage to pull the whole Petit-Four dough including the slot was 180 N . The design chosen was two contacted cylinders rotated opposite to each other as shown in Figure 3-4.


Figure 3.4 Pulling Cylinder.
The length of the cylinders equal 50 cm , and the total length of cylinder including the set shaft of bearing and gearbox is equal to 65.9 cm as shown in figure 3.5 .

The pulling operation start when the start switch is pressed and the optical sensor give a signal to the controller that there is an Petit-Four dough in the container.

In order to select the suitable motor to drive the system with suitable gear box some calculations was made:-


Figure 3.5 Cylinder section

The weight of cylinder :
Part one" cylinder" :

$$
\begin{align*}
\mathrm{A}= & \pi r^{2}  \tag{3.10}\\
& =\pi * 0.0375^{2}=0.00415 \mathrm{~m}^{2}
\end{align*}
$$

$$
\begin{equation*}
\mathrm{V}=\mathrm{A} * \mathrm{~L} \tag{3.11}
\end{equation*}
$$

$$
\begin{align*}
\mathrm{M} & =\mathrm{V} * \rho  \tag{3.12}\\
& =0.0022 * 1419.9=2.83 \mathrm{~kg}
\end{align*}
$$

$$
=0.00415 * 0.5
$$

$$
=0.0022 \mathrm{~m}^{3}
$$

The cylinder section is shown un figure 3.5 .
V: Volume $\left(m^{3}\right)$.
L:Length (m)
A: $\operatorname{Area}\left(m^{2}\right)$.)
M:mass (kg)
$\rho$ : Density of Delrin material as shown in Table $3.1\left(\mathrm{Kg} / \mathrm{m}^{3}\right)$.


Figure 3.6:Cylinder section Part two flange stainless steel:

Area of flange $=$ Area of cylinder $=0.00415 \mathrm{~m}^{2}$
$\mathrm{V}=\mathrm{A} * \mathrm{~L}$

$$
\begin{equation*}
=0.00415 * 0.008=0.000033 \mathrm{~m}^{3} \tag{3.13}
\end{equation*}
$$

$\mathrm{M}=\mathrm{V} * \rho$
$=0.000033 * 7500=0.2475 \mathrm{~kg}$
Have two flange $2 * 0.2475=0.495 \mathrm{~kg}$. As shown in figure 3.4.
$\rho$ : Density of stainless steel $\left(\mathrm{Kg} / \mathrm{m}^{3}\right)$.
Part three stainless steel rod:

$$
\begin{align*}
A & =\pi r^{2}  \tag{3.15}\\
& =\pi * 0.015^{2} \\
& =0.000706 \mathrm{~m}^{2}
\end{align*}
$$

$$
\begin{aligned}
& \mathrm{V}=\mathrm{A} * \mathrm{~L} \\
& \quad=0.000706 * 0.659 \\
& \quad=0.0004652 \mathrm{~m}^{3} \\
& \mathrm{M}=\mathrm{V} * \rho \\
& =0.0004652 * 7500 \\
& =3.489 \mathrm{~kg}
\end{aligned}
$$

$$
\rho \text { : density of stainless steel }\left(\mathrm{Kg} / \mathrm{m}^{3}\right) \text {. }
$$

The total mass of three part $=2.83+0.465+3.489=6.784 \mathrm{Kg}$.
The system mass is equal to 66 Kg as mentioned above and the force produced from this mass is equal to 647.5 N .
Mass of tank $=$ Area of tank * thickness * density of stainless steel

$$
\begin{equation*}
=0.623 * 1.5 * 10^{-3} * 7500=7.1 \mathrm{Kg} \tag{3.18}
\end{equation*}
$$

Mass of cylinder housing equal 3 Kg , mass of Petit-Four dough equal 64 Kg from section 3.4.1 ,mass of Pulling Cylinder equal 13.6 kg from section 3.4 .2 , mass of dough mold equal 4 Kg and mass of gears equal 6 Kg .

Total mass $=7.1+3+64+13.6+4+6=97.7 \mathrm{Kg}$.


Figure3.7. Container position.
The chosen total mass above the beam equal 100 Kg include as shown in figure 3.7

Table 3.1 Properties of delrin material:

| Property | Astm test method | Units | Delrin |
| :--- | :--- | :--- | :--- |
| Density | D792 | Lbs/in^3 | 0.0513 |
| Tensile strength | D638 | Psi | 9000 |
| Water absorption | D570 | $\%$ | 0.25 |
| Heat deflection <br> temperature | D648 | F | 336 |
| Rock well hardness | D758 | M ® scale | M 94(120) |
| Wear Factor <br> Against Steel, 40 <br> psi, 50 FPM | D3702 | in3 x 1/hr PV | $55 \times 10-10$ |

The required force to pull the dough into the molds equal $90 \mathrm{~N}, \mathrm{n}=30 \mathrm{rev} / \mathrm{min}$.
Now, referring to figure 3.8 the calculation will be:


Figure 3.8.Power transition for pulling motor.
$\Sigma M_{o}=J_{o} \ddot{\theta}$
T-F.r- $C_{t} \dot{\theta}=J_{o} \ddot{\theta}$
$\mathrm{T}=J_{o} \ddot{\theta}+C_{t} \dot{\theta}+$ F.r
$\alpha=\ddot{\theta}, J_{o}=\frac{1}{2} m r^{2}$
$\mathrm{T}=\frac{1}{2} \mathrm{~m} r^{2} \alpha+C_{t} \omega+$ F. r
$\alpha=\frac{\Delta \omega}{\Delta t}=\frac{\omega_{2}-\omega_{1}}{t_{2}-t_{1}}$
$\omega_{2}=\frac{2 \pi n}{60}=\frac{2 . \pi \cdot 30}{60}=3.14 \mathrm{rad} / \mathrm{s}$
$t_{2}=0.5 \mathrm{sec}$
Free body diagram of cylinder
$\alpha=6.28 \mathrm{rad} / \mathrm{s}^{2}$
$\mathrm{T}=2 *\left(\frac{1}{2} * 6.78 * 0.035^{2} * 6.28\right)+4 *\left(1.5 * 10^{-3} * 3.14\right)+(90 * 2 * 0.085)$
$=0.0522+0.019+7.625 \approx 15.37 \mathrm{~N} . \mathrm{m}$

The value of the bearing fraction $\left(C_{t}\right)$ is taken from the Table 3.2
Table 3.2: Bearing coefficient factor ( $C_{t}$ )

| Bearing type | Friction factor $\mu \times 10^{-3}$ |
| :--- | :---: |
| Deep groove ball bearings | $1.0 \sim 1.5$ |
| Angular contact ball bearings | $1.2 \sim 1.8$ |
| Self-aligning ball bearings | $0.8 \sim 1.2$ |
| Cylindrical roller bearings | $1.0 \sim 1.5$ |
| Needle roller bearings | $2.0 \sim 3.0$ |
| Tapered roller bearings | $1.7 \sim 2.5$ |
| Self-aligning roller bearings | $2.0 \sim 2.5$ |
| Thrust ball bearings | $1.0 \sim 1.5$ |
| Thrust roller bearings | $2.0 \sim 3.0$ |

The chosen gear box has a reduction ratio equal to (1:30)has these specification

## Name Product :NMRV050 Speed Reducer Model

Size: NMRV50
Speed Ratio: 1/30
Color: Blue or silver


$$
\begin{align*}
\begin{aligned}
W_{\text {motor }} & =\frac{W_{\text {gear }}}{1 / 30} \\
& =3.14 * 30=94.2 \mathrm{rad} / \mathrm{s} \\
n_{\text {motor }} & =94.2 * \frac{60}{2 * \pi}=900 \mathrm{rpm} \\
T_{\text {motor }} & =\frac{W_{\text {gear }}}{30} \\
& =0.512 \mathrm{~N} . \mathrm{m}
\end{aligned} \tag{3.22}
\end{align*}
$$

$\mathrm{P}=T_{\text {motor }} * W$
$=0.512 * 94.2=48.3 \mathrm{Watt}$
$P^{\prime}=48.3 / 746$
$=0.065 \mathrm{hp}$
$P_{\text {motor }}=$ F.s $* P^{\prime}$
$=6 * 0.0324=0.4 \mathrm{hp}$
So the chosen motor will be a 0.5 hp because there is no motor with 0.4 hp
The motor with this characteristic has been chosen to fit the calculation of the pulling system.

Table 3.3 Pulling motor characteristic :

| Output |  | Frame <br> Size | Type Designation | Speed <br> (rpm) | Current <br> (A) | Torque$(\mathrm{kgm})$ | Efficency \% |  |  | Powerf Fator |  |  | STA | StI | POT | $\begin{gathered} 60^{2} \\ \left(\mathrm{kgm}^{2}\right) \end{gathered}$ | Wt.$(\mathrm{kg})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| KW | HP |  |  |  |  |  | Fl | 3/4L | 122 | Fl | 3/41 | 1/2L |  |  |  |  |  |
| 0.37 | 0.50 | 80 | 2H52080-06 | 915 | 1.02 | 0.39 | 69.4 | 69.4 | 65.0 | 0.73 | 0.62 | 0.50 | 5.0 | 2.0 | 2.3 | 0.0049 | 15 |

### 3.4.3 Container Rod

In this section we will show the calculation of the rod that carry the container with the cylinder .
The calculation include reaction, dimension and deflection :

## Stress analysis :

The force produced from the container has a shear effect on the rod that carry the container and to find it we make the following calculation :
$\Sigma F_{y}=0$
$R_{A}-875.9 * 0.56=0$
$R_{A}=490.5 \mathrm{~N}$
$\Sigma M_{A}=0$
$M_{A}+875.9 * 0.38^{*} 0.56=0$
$M_{A}=-186.4 \mathrm{~N} . \mathrm{m}$
Shear diagram from Figure 3.9 can find $V_{A}, V_{C}$ :
$V_{A}=R_{A}=490.5 \mathrm{~N}$
$V_{C}=V_{A}-875.9 * 0.56=0$
Area of shear diagram :

$$
\begin{aligned}
A_{\mathrm{A}-\mathrm{B}} & =0.1 * 490.5 \\
& =49.05 \mathrm{~N} . \mathrm{m} \\
A_{\mathrm{B}-\mathrm{C}} & =0.5 * 0.56 * 490.5 \\
& =137.35 \mathrm{~N} . \mathrm{m}
\end{aligned}
$$

Bending moment from Figure 3.9 can find $M_{A}, M_{B}$ :
$M_{A}=-186.4 \mathrm{~N} . \mathrm{m}$


Figure 3.9 : Shear and Bending moment
$M_{B}=M_{A}+A_{\text {A-B }}$
$=-186.4+49.05=-137.35 \mathrm{~N} . \mathrm{m}$

$$
\begin{aligned}
M_{c} & =M_{B}+A_{\mathrm{B}-\mathrm{C}} \\
& =-137.35+137.35=0
\end{aligned}
$$

To find the diameter make the following calculation :
$\left|M_{\max }\right|=M_{A}=186.4 \mathrm{~N} . \mathrm{m}$
$\sigma_{\text {req }}=\frac{M_{\text {max }} \cdot C}{I}$
$\mathrm{I}=\frac{\pi \mathrm{D}^{4}}{64}$
$\mathrm{C}=\frac{D}{2}$
The chosen safety factor equal 2 and the chosen material of beam it a Chromium it has allowable stress ${ }^{1}$ equal 689 MPa .
$n_{f}=\frac{\sigma_{\text {all }}}{\sigma_{\text {req }}}$
$\sigma_{\text {req }}=\frac{\sigma_{\text {all }}}{n_{f}}$

$$
\begin{equation*}
=\frac{689}{2}=344.5 \mathrm{MPa} \tag{3.33}
\end{equation*}
$$

Now by substitution Eq (3.30) , Eq (3.31) and Eq (3.33) in Eq (3.29) we can found the required diameter of the rod.
$\sigma_{r e q}=\frac{186.4 * \frac{D}{2}}{\frac{\pi \mathrm{D}^{4}}{64}}$
D $\approx 18 \mathrm{~mm}$

## Deflection analysis :

Using a superposition the given loading can be obtained by superposition the loading shown in the following picture equation figure 3.10.


Figure 3.10. Deflection of container beam.

[^0]For each of the loading | and || we now determine deflection at B.
Loading | :
$\left(y_{B}\right)_{\mid}=-\frac{w L^{4}}{8 E I}$
Loading || :
$\left(\theta_{c}\right)_{\|}=+\frac{w(L-0.56)^{3}}{6 E I}$
$\left(y_{C}\right)_{\|}=+\frac{w(L-0.56)^{4}}{8 E I}$
In portion CB ,the bending moment for loading $\|$ is zero and thus the elastic carve is a straight line .
$\left(y_{B}\right)_{\|}=\left(y_{C}\right)_{\|}+\left(\Theta_{C}\right)_{\|} \cdot(L-0.56)$
Deflection at B

$$
\begin{align*}
y_{B} & =\left(y_{B}\right)_{I}+\left(y_{B}\right)_{\|}  \tag{3.38}\\
& =-\frac{w L^{4}}{8 E I}+\left(y_{C}\right)_{\|}+\left(\Theta_{c}\right)_{\|} \cdot(L-0.56) \\
& =-\frac{w L^{4}}{8 E I}+\frac{w(L-0.56)^{4}}{8 E I}+\left(\frac{w(L-0.56)^{3}}{6 E I}\right) \cdot(L-0.56)
\end{align*}
$$

Now we substitute $w=875.9 \mathrm{~N} / \mathrm{m}, \mathrm{L}=0.66 \mathrm{~m}$ and modules of elasticity $(\mathrm{E})=294 \mathrm{GPa}$.
$y_{B}=-\frac{875.9(0.66)^{4}}{8 * 294 * 10^{9} * I}+\frac{875.9(0.66-0.56)^{4}}{8 * 294 * 10^{9} * I}+\left(\frac{8759(0.66-0.56)^{3}}{6 * 294 * 10^{9} * I}\right) \cdot(0.66-0.56)$
$y_{B}=-\frac{7 * 10^{-11}}{I}$
The acceptable deflection for our part is 1 mm as maximum .
$\mathrm{I}=\frac{\pi \mathrm{D}^{4}}{64}=\frac{-7 * 10^{-11}}{-1 * 10^{-3}}$
$\mathrm{D}=34.56 \mathrm{~mm}$
By stress analyses gave a beam diameter equal 18 mm and from deflection analyses have a rod diameter equal 34.56 mm there for we will choose the biggest one .

Rod diameter $\approx 35 \mathrm{~mm}$

### 3.4.4 The conveyer

### 3.4.4.a Tray

We found that the used tray in the bakery has a fixed dimension (50x70) as shown in figure 3.11 and 5.25 kg so we will used this tray to appropriate the market demand.


Figure 3.11.Tray dimension .
As talk in perverse chapter the number of the shape mold is six and the number of units produce in the tray is 48 units with a 50 g for each units .

Mass of petit-four units = Number of units * Mass of each units

$$
\begin{equation*}
=48 * 50=2.4 \mathrm{~kg} \tag{3.40}
\end{equation*}
$$

Mass $1=$ Mass of tray + Mass of petite four units $=5.25+2.4=7.65 \mathrm{~kg}$.

### 3.4.4.b Belt

From the above section the tray must choose suitable belt to appropriate the tray with the conveyer so we use a belt with the following dimensions in figure 3.14 and properties as in table 3.4 .


Figure 3.12. Belt in 3D.

Table 3.4 Properties of belt ${ }^{2}$ :

| Properties | Value |
| :--- | :--- |
| Material conveying side | Polyvinylchloride $(\mathrm{PVC})$ |
| Colour conveying side | Green |
| Total thickness | $2,5 \mathrm{~mm}(+/-0,1 \mathrm{~mm})$ |
| Belt weight | $2,8 \mathrm{~kg} / \mathrm{m}^{2}$ |
| Maximum tensile force | $120 \mathrm{~N} / \mathrm{mm}$ |
| Standard production width | 2.000 mm |
| Friction coefficient on slider bed of steel | 0.35 |

From the table 3.4 the weight factor is equal $2.8 \mathrm{~kg} / \mathrm{m}^{2}$. the belt is shown in the figure 3.14
The area of one belt $=\mathrm{L} * \mathrm{~W}$

$$
\begin{align*}
& =15 * 10^{-2} * 270 * 10^{-2}  \tag{3.41}\\
& =0.405 \mathrm{~m}^{2}
\end{align*}
$$

The weight of one belt $=$ Weight factor * Area

$$
\begin{equation*}
=2.8 * 0.405=1.134 \mathrm{~kg} \tag{3.42}
\end{equation*}
$$

For two belt the total weight is:
Mass * $2=2.268 \mathrm{~kg}$
The total mass $(M)=$ Mass $1+$ Mass 2

$$
\begin{equation*}
=7.65+2.268=9.92 \mathrm{~kg} \tag{3.43}
\end{equation*}
$$

The force produce from this mass $=\mathrm{M}^{*} \mathrm{~g}$

$$
=9.92 * 9.81=97.3 \mathrm{~N}
$$

Use a motor with a speed of 1400 rpm and to have a low speed equal 14 rpm we choose a gear box is $1: 100$ to reduce the speed, and the reason of not choose a motor with a speed of 900 rpm is there is no gear box ratio gave me 14 rpm .

The chosen gear box has a reduction ratio equal to (1:100)has these specification

Name Product :NMRV050 Speed Reducer Model
Size: NMRV50
Speed Ratio: 1/100
Color: Blue or silver
${ }^{2}$ - Appendix B


Figure 3.13. Double Conveyor in 2D .
In the figure 3.13 its show how the system work and in the figure 3.14 its show the free body diagram of the force that the motor is effect by.

By substitution in $\mathrm{Eq}(3.19)$ the belt motor torque found:
$\Sigma M_{o}=J_{o} \ddot{\theta}$
T-F.r- $C_{t} \dot{\theta}=J_{o} \ddot{\theta}$
$\mathrm{T}=J_{o} \ddot{\theta}+C_{t} \dot{\theta}+$ F.r
$\alpha=\ddot{\Theta} \quad, J_{o}=\frac{1}{2} \mathrm{~m} r^{2}$
$\mathrm{T}=\frac{1}{2} \mathrm{~m} r^{2} \alpha+C_{t} \omega+$ F. r


Figure 3.14. Free body diagram of belt

By substitution in $\mathrm{Eq}(3.20)$ the acceleration and speed found:
$\alpha=\frac{\Delta \omega}{\Delta t}=\frac{\omega_{2}-\omega_{1}}{t_{2}-t_{1}}$
$\omega_{2}=\frac{2 \pi n}{60}=\frac{2 . \pi \cdot 14}{60}=1.46 \mathrm{rad} / \mathrm{s}$
$t_{2}=0.5 \mathrm{sec}$
$\alpha=2.92 \mathrm{rad} / \mathrm{s}^{2}$
By substitution in $\mathrm{Eq}(3.21)$ the polar inertia found:
$J_{o}=\frac{1}{2} m r^{2}$
To find the mass of roller tube

Have two roller tube then the mass is 1 kg

$$
\begin{aligned}
J_{o} & =\frac{1}{2} * 1^{*} 0.51^{2} \\
& =0.13 \mathrm{~kg} \cdot \mathrm{~m}^{2}
\end{aligned}
$$

From the table 3.3 friction coefficient on slider bed of steel is 0.35 ,then the fraction force between belt and conveyor frame.

$$
\begin{align*}
\mathrm{F}_{\text {fraction }} & =\text { Force } * \text { Fraction coefficient }  \tag{3.47}\\
& =97.3 * 0.35=34 \mathrm{~N}
\end{align*}
$$

$$
\mathrm{T}=(0.13 * 2.92)+4 *\left(1.5 * 10^{-9} * 1.46\right)+(34 * 0.51)
$$

$$
=0.38+8.7 * 10^{-9}+17.3 \approx 17.7 \mathrm{~N} . \mathrm{m}
$$

$$
\begin{equation*}
T_{\text {motor }}=\frac{T_{\text {gear }}}{100} \tag{3.48}
\end{equation*}
$$

$$
=\frac{17.7}{100}=0.177 \mathrm{~N} . \mathrm{m}
$$

$$
\begin{equation*}
W_{\text {motor }}=\frac{1.46}{1 / 100}=146 \mathrm{rad} / \mathrm{s} \tag{3.49}
\end{equation*}
$$



Figure 3.15: Fraction between belt and conveyor frame.
$n_{\text {motor }}=146 * \frac{60}{2 * \pi}=1396 \mathrm{rpm}$

$$
\begin{align*}
\mathrm{P} & =T_{\text {motor }} * \mathrm{~W}  \tag{3.51}\\
& =0.177 * 146=25.8 \mathrm{Watt}
\end{align*}
$$

$$
\begin{align*}
& \mathrm{m}=\rho^{*} \mathrm{~V}  \tag{3.44}\\
& \mathrm{~V}=\mathrm{A} \text { * }  \tag{3.45}\\
& A=\frac{\pi\left(D_{0}-D_{i}\right)^{2}}{4} \\
& =\frac{\pi(0.102-0.08)^{2}}{4} \\
& =3.8 * 10^{-4} \mathrm{~m}^{2} \\
& \text { length }(1)=0.15 \mathrm{~m} \\
& \mathrm{~V}=3.8 * 10^{-4 *} 0.15 \\
& =5.7^{*} 10^{-5} \mathrm{~m}^{3} \\
& \mathrm{~m}=8000^{*} 5.7^{*} 10^{-5} \\
& \approx 0.5 \mathrm{~kg}
\end{align*}
$$

$$
\mathrm{P}=25.8 / 746=0.0346 \mathrm{hp}
$$

The chosen power factor is 3 so the motor power will be 0.10 hp because there is no motor with 0.10 hp . The motor has some characteristic in the table 3.5

Table 3.5 Conveyor motor characteristic :

| Framesize | $\begin{aligned} & \text { Power } \\ & (\mathrm{KW}) \end{aligned}$ | Current (A) |  |  | Current (A) |  |  | Curent (A) |  |  | Pmen(inin) | EH. <br> (\%) | Power factor <br> ( $\operatorname{Cos} \phi$ ) | $\begin{aligned} & \mathrm{C} \delta \\ & \mathrm{Cn} \end{aligned}$ | Cmax Cn | $\begin{aligned} & \mathrm{Cn} \\ & (\mathrm{Nm}) \end{aligned}$ | ls An | $\mathrm{dB}(\mathrm{A})$ | Weight ( Kg ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 220 V | 360 V | 660 V | 230 V | 400 V | 690 V | 240 V | 415 V | 720V |  |  |  |  |  |  |  |  |  |
| MS 562-4 | 009 | 088 | 0.47 | 027 | 0.78 | 045 | 026 | 0.75 | 0.43 | 025 | 1360 | 52 | 0.59 | 23 | 24 |  | 4 | 50 | 320 |

### 3.4.4.C Mass Of Conveyor

Need to calculate the total mass of conveyer, to determine the force that effect on the cam, the conveyer shown in the figure 3.1 .

## Conveyer part:

Mass of conveyer frame :


Figure 3.16: Conveyor frame dimension $[\mathrm{mm}]$ and area.
Mass of conveyer frame $=$ Volume of conveyer frame $*$ Density of aluminum
Volume of conveyer frame $=$ Area* ${ }^{*}$ Thickness

$$
\begin{equation*}
=0.132 * 0.02=2.64 * 10^{-3} \mathrm{~m}^{3} \tag{3.53}
\end{equation*}
$$

Density for aluminum $=2700 \mathrm{Kg} / \mathrm{m}^{3}$
Mass of conveyer frame $=2.64 * 10^{-3} * 2700=7.13 \mathrm{Kg}$
We have 4 conveyer frame as in the figure 3.16 then the mass will be $7.13 * 4=28.52 \mathrm{Kg}$


Figure 3.17: Conveyor frame with Rolling tube .

## Mass of roller tube in figure 3.17 :

Mass of Roller tube $=$ Volume of Roller tube * Density for Steel
Area of Roller tube $=\frac{\pi}{4}\left(D_{o}-D_{i}\right)^{2}$

$$
\begin{align*}
& =\frac{\pi}{4}(0.102-0.08)^{2}  \tag{3.55}\\
& =3.8 * 10^{-4} \mathrm{~m}^{2}
\end{align*}
$$

The Length of roller tube is 0.15 m
$D_{o}$ : Outer dimension [mm] in figure 3.18.
$D_{i}$ : Inner dimension [mm] in figure 3.18.
Volume of roller tube $=$ Area of roller tube $*$ Length

$$
\begin{align*}
& =3.8 * 10^{-4} * 0.15  \tag{3.56}\\
& =5.7 * 10^{-5} \mathrm{~m}^{3}
\end{align*}
$$

Density for Steel $=8000 \mathrm{Kg} / \mathrm{m}^{3}$
Mass of Roller tube $=5.7 * 10^{-5} * 8000$

$$
=0.456 \mathrm{Kg}
$$

Have Four Roller then the mass will be 1.85 Kg .


Figure3.18.Rollering tube section

## Mass of the Shaft in figure 3.17 :

Mass of Shaft $=$ Volume of Shaft * $\rho_{\text {steel }}$
Volume of Shaft = Area of Shaft * length

$$
\begin{aligned}
& =\frac{\pi}{4} D^{2} * \mathrm{~L} \\
& =\frac{\pi}{4} \cdot 025^{2} * 0.65 \\
& =3.19 * 10^{-4} \mathrm{~m}^{3}
\end{aligned}
$$

D: Diameter [mm] in figure 3.19.

$$
\begin{aligned}
\text { Mass of Shaft } & =3.19 * 10^{-4} * 8000 \\
& =2.5 \mathrm{Kg}
\end{aligned}
$$

Have two shaft so the mass will be 5 Kg .


Figure 3.19. Shaft section.

## Mass of motor and gear box :

From the data sheet of motor and gear box we find the mass of motor is 6.2 and mass of gear box is 3.8 , the total mass will be 10 Kg .

## Mass of the conveyer belt and Tray :

From the section 3.4.4.b the mass of belt equal to 2.268 Kg and From the section 3.4.4.a the mass of Tray equal to 7.65 kg .

Total Mass Of Conveyer Equal :

$$
\begin{aligned}
\text { Mass } & =28.25+1.85+5+10+2.268+7.65 \\
& =55 \mathrm{Kg}
\end{aligned}
$$

### 3.4.5 Sliding System

In this section will discuss the force that effect on beam that carrying the conveyer and will calculate the motor needs for carry the hole system rise and decline.

### 3.4.5.A Beam Design

The function of the beam as shown in figure 3.20 is to carry the conveyer system and the dimension of the beam that have a chosen dimension ( $20 \mathrm{~mm} \times 40 \mathrm{~mm}$ ) so there is must to cheek the maximum deflection according to this dimension and disease if allowable or not.


Figure 3.20: Conveyer beam.
The maximum deflection ${ }^{3}$ from figure 3.22 :
$y_{\max }=\frac{F a^{2}}{6 E I}(\mathrm{a}-3 \mathrm{~L})$
$\mathrm{F}=\frac{\text { mass of conveyer } * 9.81 \mathrm{~m} / \mathrm{s}^{2}}{2}$

$$
=\frac{55 * 9.81}{2}=270 \mathrm{~N}
$$

$\mathrm{a}=41 \mathrm{~mm}$ from figure 3.22
$\mathrm{L}=75 \mathrm{~mm}$ from figure 3.22 .
$\mathrm{E}=207 \mathrm{GPa}$ (modules of elasticity )

$$
\begin{align*}
\mathrm{I} & =\frac{0.04^{3} * 0.02}{12}  \tag{3.61}\\
& =1.07 * 10^{-7} \mathrm{~m}^{4}
\end{align*}
$$

I: Moment of inertia in figure 3.21

$$
\begin{aligned}
y_{\max } & =\frac{270 * 0.41^{2}}{6 * 270 * 10^{9} * 1.07 * 10^{-7}}(0.41-3 * 0.75) \\
& =-\frac{83.512}{173340} `=0.5 \mathrm{~mm}
\end{aligned}
$$



Figure 3.22: Beam deflection

### 3.4.5.B Cam Motor Calculation

[^1]The motor are affected by the force produced from the hole system mass, so must choose a motor meat this effect as in figure 3.23.


Figure 3.23.Cam system.
The system mass is equal to 66 Kg as we mentioned in section 3.4.5.a and the force produced from this mass is equal to 647.5 N . with velocity 1400 rpm and gear box with ratio of 1:50.
$\Sigma M_{o}=J_{o} \ddot{\theta}$
T-F.r- $C_{t} \dot{\theta}=J_{o} \ddot{\theta}$
$\mathrm{T}=J_{o} \ddot{\theta}+C_{t} \dot{\theta}+$ F.r
$\alpha=\ddot{\theta} \quad, J_{o}=\frac{1}{2} \mathrm{~m} r^{2}$
$\mathrm{T}=\frac{1}{2} \mathrm{~m} r^{2} \alpha+C_{t} \omega+$ F.r
$\alpha=\frac{\Delta \omega}{\Delta t}=\frac{\omega_{2}-\omega_{1}}{t_{2}-t_{1}}$
$\omega_{2}=\frac{2 . \pi .28}{60}=2.93 \mathrm{rad} / \mathrm{s}$
$t_{2}=0.5 \mathrm{sec}$
$\alpha=5.86 \mathrm{rad} / \mathrm{s}^{2}$
Area of cam $=\frac{\pi D^{2}}{4}$

$$
\begin{equation*}
=\frac{\pi * 0.12^{2}}{4}=0.011 \mathrm{~m}^{2} \tag{3.64}
\end{equation*}
$$

Volume of cam = Area of cam * Thickness of cam

$$
\begin{align*}
& \qquad=0.011 * 0.02=2.2 * 10^{-4} \mathrm{~m}^{3} \\
& \text { Mass of cam }=\text { Volume of cam * Density of steel } \\
& =2.2 * 10^{-4} * 8000=1.76 \mathrm{Kg} \\
& J_{o}=\frac{1}{2} \mathrm{~m} r^{2}  \tag{3.67}\\
& =\frac{1}{2} * 1.76 * 0.06^{2}=3.168 * 10^{-3} \mathrm{Kg} . \mathrm{m}^{2} \\
& \mathrm{~T}=3.168 * 10^{-3} * 5.86+1.5 * 10^{-3} * 2.93+640.8 * 0.0475 \\
& =0.018+0.0043+30.72=30.7 \mathrm{~N} . \mathrm{m}
\end{align*}
$$

The chosen gear box has a reduction ratio equal to (1:50) has these specification

```
Name Product :NMRV050 Speed Reducer Model
Size: NMRV50
Speed Ratio: 1/50
Color: Blue or silver
```

$W_{\text {befor }}=\frac{W_{\text {after }}}{1 / 50}$

$$
=2.93 * 50=146.5 \mathrm{rad} / \mathrm{s}
$$

$$
\begin{equation*}
n_{\text {befor }}=146.5 * \frac{60}{2 * \pi}=1400 \mathrm{rpm} \tag{3.69}
\end{equation*}
$$

$$
\begin{equation*}
T_{\text {befor }}=\frac{T_{\text {after }}}{50}=0.614 \mathrm{~N} . \mathrm{m} \tag{3.70}
\end{equation*}
$$

$$
\begin{align*}
\mathrm{P} & =T_{\text {motor }} * \mathrm{~W}  \tag{3.71}\\
& =0.614 * 146.5=89.9 \mathrm{Watt}
\end{align*}
$$

$$
\mathrm{P}=263.7 / 746
$$

$$
=0.354 \mathrm{hp}
$$

Safety factor equal to 2.5

$$
\begin{aligned}
\mathrm{p} & =\mathrm{p} * 6 \\
& =0.354 * 2.5=0.88 \mathrm{hp} .
\end{aligned}
$$

So the chosen motor will be a 1 hp because there is no motor with 0.88 hp
The motor with this characteristic has been chosen to fit the calculation of the Cam system.

Table 3.6 Cam Motor characteristic :

| Framesize | Power (KW) | Curent (A) |  |  | Current (A) |  |  | Current (A) |  |  | Pan.(ntin) | Ef. <br> (\%) | Power factor ( $\operatorname{Cos} \phi$ ) | $\begin{aligned} & \mathrm{C} \otimes \\ & \mathrm{Cn} \end{aligned}$ | Cmaxd Cn | $\begin{aligned} & \mathrm{Cn} \\ & (\mathrm{Nm}) \end{aligned}$ | lesin | $\mathrm{dB}(\mathrm{A})$ | Woight ( Kg ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 220 V | 380 V | 860 V | 230 V | 400V | 690 V | 240 V | 415 V | 720V |  |  |  |  |  |  |  |  |  |
| MS 802-4 | 0.75 | 350 | 2.90 | 1.17 | 3.34 | 003300 | 1.11 | 321 | 1.36 | 107 | 1380 | 22 | 076 | 22 | 24. | 527 | 6 | 58 | 210 |

### 3.4.6 Machine Body

To know if the machine support will be able to carry the weight of the machine frame, so there must be some calculation to verify that the support can carry. the support are describe in figure 3.24 .


Figure 3.24 : Machine body.

Now the resultant force of each part in the machine body was calculate in the previous sections and this force are describe in the Figure 3.25 .


Figure 3.25 : Free body diagram of machine body.
The resultant force as shown in figure 3.26, are equal to the force from the weight of container and pulling system. weight of conveyer, weight of back side of machine and weight of steel pleat.
$\mathrm{R}=980+647.5+196.2+912=2735.7 \mathrm{~N}$.
$M_{o}=\mathrm{F} * \mathrm{R}$
$M_{o}=980 * 0.38+647.5 * 0.41+196.2 * 0.1$
$=372.4+265.5+19.62=657.52 \mathrm{~N} . \mathrm{m}$
The machine have two support so the moment must be divided by tow.
$\mathrm{R} * \mathrm{~d}=M_{o}$
2735.7 * $\mathrm{d}=657.52$
$\mathrm{d}=0.24 \mathrm{~m}=240 \mathrm{~mm}$
$\sum M_{b}=0$
$1.030 * \mathrm{Ra}-\frac{\mathrm{R}}{2} * 0.520=0$
$\mathrm{Ra}=690.56 \mathrm{~N}$


Figure 3.26:Free body diagram for machine support.

By cutting the beam at point o as shown in figure 3.27 :
$\sum M_{o}=0$
$M_{c}+0.750 * \mathrm{Ra}-\mathrm{R} * 0.24=0$
$M_{c}+0.750 * 690.56-\frac{2735.7}{2} * 0.24=0$
$M_{c}=189.64 \mathrm{~N} . \mathrm{m}$

Calculate safety factor
$\sigma_{\text {req }}=\frac{M_{c} . C}{I}$


Figure 3.27:Free body diagram for cutting beam.
$\mathrm{I}=\frac{1}{12}(0.080)(0.040)^{3}-\frac{1}{12}(0.076)(0.036)^{3}$

$$
=1.4 * 10^{-7}
$$

I: Moment inertia of figure 3.28.
$\mathrm{C}=\frac{80}{2}=40 \mathrm{~mm}$.

$$
\begin{aligned}
\sigma_{r e q} & =\frac{189.64 * .040}{1.4 * 10^{-7}} \\
& =54.2 * 10^{6} \\
& =54.2 \mathrm{MPa}
\end{aligned}
$$

The chosen material of beam is steel and it has allowable stress equal 380 MPa

$$
n_{f}=\frac{\sigma_{\text {all }}}{\sigma_{\text {req }}}
$$

$$
=\frac{380 * 10^{6}}{54.2 * 10^{6}}=7
$$

So can use this standard of beam to carry the machine body.

### 3.5 The Welding Design

The welding is needed to connect the conveyer beam with the sliding system. Figure 3.29 shows the welding joints. Filler metal rods and wires are designated by a system established by the American Welding Society (AWS). AWS designation is E60XX .


Figure 3.29 : Welding joint.
From the weld design tables the area of welding is :
$\mathrm{A}=1.414 \mathrm{hd}$
$=1414 * \mathrm{~h} * 0.81=1.1455 \mathrm{~h}$
$M=F^{*} L$

Where,
h: Height of welding as in Figure 3.30.
d: Length of the part that the welding is on .
F: Force effect on the beam as in figure 3.30.
L: Length of the beam .
$\mathrm{M}=16.7$ * $0.0606=1.012$ Kip.in.


Figure 3.30.Weld pattern.

The polar moment of area of the weld group per throat length $\left(J_{u}\right)$ is selected from the weld design tables.

$$
\begin{align*}
J_{u} & =\frac{d\left(3 b^{2}+d^{2}\right)}{6}  \tag{3.83}\\
& =\frac{0.81\left(31.63^{2}+0.81^{2}\right)}{6}=1.1646
\end{align*}
$$

This value needs to represent the value of (J) in the equation (3.84)
$\mathrm{J}=0.707 \mathrm{~J}_{u}$
The leg weld (h) needs to be designed.
The primary shear is :

$$
\begin{align*}
\tau & =\frac{F}{A}  \tag{3.85}\\
& =\frac{0.0606}{1.145 h}=\frac{0.052}{h}
\end{align*}
$$

The second shear is :

$$
\begin{align*}
\tau^{\prime \prime}{ }_{x} & =\frac{M r_{y}}{J}  \tag{3.86}\\
& =\frac{(1.012)(0.815)}{0.82 h}=\frac{1}{h} \\
\tau^{\prime \prime}{ }_{y} & =\frac{M r_{x}}{J}  \tag{3.87}\\
& =\frac{(1.012)(0.405)}{0.82 h}=\frac{0.49}{h} \\
\tau & =\sqrt{\tau^{\prime \prime}{ }_{x}+\tau^{\prime \prime}{ }_{y}} \\
& =\sqrt{\left(1 / h^{2}+(0.49) / h\right)^{2}}=\frac{1.7}{h} \mathrm{Kpsi}
\end{align*}
$$

Member: structured steel ; A. $36 \rightarrow s_{y}=36$ Kips

Attachment: AISI 1018 HR steel $\rightarrow s_{y}=32$ Kips
Allowable stress: Attachment : $\tau_{\text {all }=0.4} s_{y}=0.4(32)=12.8 \mathrm{Kips}$

$$
\begin{equation*}
\text { Member : } \tau_{\text {all }=0.4} s_{y}=0.4(36)=14.4 \mathrm{Kips} \tag{3.88}
\end{equation*}
$$

Note that the Attachment is weaker than the member. It is the critical part. therefore, select an electrode not weaker than the attachment and the chosen electrode is E60XX .
$\tau_{\text {all,electode }}=0.3 \mathrm{~S}_{u t}=0.3^{*} 60=18 \mathrm{Kips}$ which is greater than 12.8 Kips

$$
\begin{equation*}
\tau_{\text {all }}=\operatorname{Min}(12.8,14.4,18.0)=12.8 \text { Kips } \tag{3.90}
\end{equation*}
$$

Setting $\tau_{\max }=\tau_{\text {all }}$, the value of the leg length (h) is considered 3 mm with two lines where the total length for each line is 20 mm .

## 4

## Chapter Four

## PLC Programming

4.1 Introduction.
4.2 PLC Characteristic .
4.3 PLC Graph .

### 4.1 Introduction

As it has been mentioned before the pitit-fore machine is fully automated and the process is performed sequentially, this can be perform by using PLC (programmable logic controller). This made adding automation capability and safety precautions possible, which is explained through this chapter.

The PLC is chosen to be used on the machine rather than the microcontroller because of its ability to operate with the voltage used at workshop (220v) without the need of other component, where the microcontroller can operate only with 5 v and needs other component which has a high cost, A comparison between PLC and microcontroller is made in the table-4.1.

|  | PLC | Microcontroller |
| :--- | :---: | :---: |
| Less Initial Cost |  | $\checkmark$ |
| Ease In Programming | $\checkmark$ |  |
| Work At 220V | $\checkmark$ |  |
| Build In Modules | $\checkmark$ |  |
| Faster Response |  | $\checkmark$ |
| Less Total Cost | $\checkmark$ |  |

Table 4.1 : PLC VS Microcontroller

### 4.2 PLC Characteristic

Programmable Logic Controller (PLC) is a digital computer used for automation of electromechanical process, such as control of machinery on factory assembly lines, PLCs are used in many industries and machine. Unlike general-purpose computers, the PLC is designed for multiple inputs and output arrangements, extended temperature ranges, immunity to electrical noise, and resistance to vibration and impact. programs to control machine operation are typically stored in battery backedup or non- volatile memory .

A PLC is an example of a hard real time system since output results must be produced in response to input conditions within a limited time otherwise unintended operation will result. In our controlling design it is desirable to use a PLC with 13
input and 6 outputs mention in the table 4.2 below, It must be compatible to use with 220 volt .

The PLC connection are shown in the figure 4.1.
Table 4.2 : logic allocation

| Input | Symbol | Logic allocation | address |
| :---: | :---: | :--- | :---: |
| Start(NO) | START | START = 1, Operation is run. <br> /CAM motor is run on manual. | I 0.0 |
| Stop(NC) | STOP | STOP = 0, Operation is stop. | I 0.1 |
| Encoder | ENCODER | Cont pulse at Rising edge. | I 0.2 |
| Emergency switch(NC) | EMG | Turn off all process. | I 0.3 |
| Limit switch 1 | CAM_UP | CAM_UP = 1, Conveyer is ready <br> for casting. | I 0.4 |
| Limit switch 2 | CAM_DOWN | CAM_Down = 1, Conveyer is <br> ready for moving the tray. | I 0.5 |
| Limit switch 3 | TRAY_READY | TRAY_READY = 1, The tray is <br> on the casting position. | I 0.6 |
| Push bottom 1(NO) | TYPE1 | TYPE1 = 1, Shape one is selected <br> /Cylinder motor is run in manual. | I 0.7 |
| Push bottom 2(NO) | TYPE2 | TYPE2 $=1$, Shape second is <br> selected / conveyer motor is run <br> in manual. | I 0.8 |
| Select switch | AUTOMATIC | If the select switch in the right <br> position the operation mode is <br> automatic. | I 0.9 |
| Select switch | MANUAL | If the select switch in the left <br> position the operation mode is <br> manual. | I 0.10 |


| Output | Symbol | Logic allocation | address |
| :---: | :---: | :---: | :---: |
| Cam Motor | CAM_MOTOR_M1 | CAM_MOTOR_M1=1, <br> The cam motor is run. | Q0.0 |
|  | CAM_MOTOR_M4 | CAM_MOTOR_M4=1, <br> The output frequency from <br> the inverter is 25 Hz. | Q0.1 |
|  | CAM_MOTOR_M5 | CAM_MOTOR_M5=1, <br> The output frequency from <br> the inverter is 35 Hz. | Q0.2 |
| Conveyer Motor | CONVEYER_MOTOR | CONVEYER_MOTOR=1, <br> The conveyer motor is run. | Q0.3 |
| Cylinder Motor | CYLINDER_MOTOR | CYLINDER_MOTOR=1, <br> The cylinder motor is run. | Q0.4 |
| Red Led | STOP_LED | STOP_LED=1, <br> The red led is light. | Q0.5 |
| Green Led | START_LED | START_LED=1, <br> The green led is light. | Q0.6 |



Figure 4.1 : PLC Connection.

The used PLC is Schneider TWDLCAA24DRF as shown in figure 4.2 ,with 14 inputs and 10 outputs and the data sheet is shown in the appendix


Figure 4.2 : PLC Schneider TWDLCAA24DRF.
The software for TWDLCAA24DRF is the program TwidoSuite micro/win64 as shown in the figure 4.3 .


Figure 4.3: TwidoSuite micro/win64 program .

### 4.3 PLC Graph

The machine will has two operation mode manual mode and automatic mode. The manual mode is added for increasing the safety of the machine with the addition of the emergency switch and to allow the user to clean the machine. the selection between two modes can be made by using the switch, the transformation between the two modes can be implemented at any stage if an errors are happened. The state graph shown in figure 4.4 " Automatic mode " and figure 4.5 " Manual Mode ".


Figure 4.4 : The state graph" Automatic Mode ".


Figure 4.5 : The state graph" Manual Mode ".

The ladder code ${ }^{1}$ is obtained from the state graph .

## 5

## Chapter Five Electrical Design \& Protection

5.1 Introduction.
5.2 Motors.
5.3 Voltage Frequency Driver.
5.4 Sensors.
5.5 (Power \& Control) Circuit.
5.6 Electrical Panel \& Protection.

### 5.1 Introduction

This chapter contain the electrical component specifications ( motor, inverters, sensor, overload, ... etc) , power \& control circuit, and protection.

### 5.2 Motors:

In this project there are three AC motors ( CAM Motor, Conveyer Motor, Casting Motor).

### 5.2.1 CAM motor

Three phase AC motor( to control it using inverter ) (1HP:0.75KW), REM Germany Electric Machine Co.

| Framesize | Power (KW) | Curent (A) |  |  | Current (A) |  |  | Current (A) |  |  | Pren(intin) | Eft <br> (\%) | Power factor <br> $(\operatorname{Cos} \phi)$ | $\begin{aligned} & \mathrm{C} \delta \\ & \mathrm{Cn} \end{aligned}$ | Cmax Cn | $\begin{aligned} & \mathrm{Cn} \\ & (\mathrm{Nm}) \end{aligned}$ | lsin | $\mathrm{dB}(\mathrm{A})$ | Weight ( Kg ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 220 V | 380 V | 660 V | 230 V | 400 V | 690 V | 240 V | 415V | 720V |  |  |  |  |  |  |  |  |  |
| MS 802-4 | 0.75 | 350 | 2000 | 1.17 | 3.34 | 0233.00 | 1.11 | 321 | 1.36 | 197 | 1380 | 22 | $0 \%$ | 22 | 24 | 527 | 6 | 58 | 919 |

### 5.2.2 Conveyer motor

Three phase AC motor ( to control it using inverter ) ( $0.12 \mathrm{HP}: 0.09 \mathrm{KW}$ ) ,REM Germany Electric Machine Co.

| Framesize | Power(KW) | Curent ( $A$ ) |  |  | Current (A) |  |  | Current (A) |  |  | Pran(min) | Ef. <br> (\%) | Power factor ( $\operatorname{Cos} \phi$ ) | $\begin{aligned} & \mathrm{Cs} \\ & \mathrm{Cn} \end{aligned}$ | Cmax$\mathrm{Cn}$ | $\begin{aligned} & \mathrm{Cn} \\ & (\mathrm{Nm}) \end{aligned}$ | l /fn | $\mathrm{dB}(\mathrm{A})$ | Weight $(\mathrm{Kg})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 220 V | 380 V | 660 V | 230 V | 400 V | 690 V | 240 V | 415V | 720V |  |  |  |  |  |  |  |  |  |
| MS 562-4 | 009 | 088 | 0.47 | 027 | 0.78 | 0.45 | 025 | 075 | 0.43 | 025 | 1360 | 52 | 0.59 | 23 | 2.4 |  | 4 | 50 | 320 |

### 5.2.3 Pulling motor

Single phase AC motor ( $230 \mathrm{~V}, 50 \mathrm{~Hz}$ ) ( $0.5 \mathrm{HP}: 0.37 \mathrm{KW}$ ) ,REM Germany Electric Machine Co.

| Model | Power (KW) | Speed (rimin) | EH: <br> (*) | Power Factor (Con¢) | Cumme (A) |  |  | THITs (Times) | Tmin (Times) | $T-1 T_{0}$ <br> (Times) | Lat(Times) | Noise dex(A) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 230 V | 400 V | 680 V |  |  |  |  |  |
| MSBCCL712-4 | 0.37 | 1370 | 65 | 0.74 | 1.92 | 1.11 | 0.64 | 22 | 2.4 | 1.7 | 6 | 55 |

### 5.3 Voltage Frequency Driver

### 5.3.1 CAM motor voltage frequency driver

The purpose of using the voltage frequency driver is to control the speed of CAM motor by using multifunction speed, the type of CAM Motor driver is Delta model VFD015EL21A shown in figure 5.1

The VFD-EL series is multiple function new generation micro type AC drive, high precision current detection, overload protection, and a built in keypad.

## Specifications

Nominal Input VAC: 208;240 Volts AC
Input Range VAC: 200 to 240 Volts AC
Input Phase: 1
HP (CT): 2 Horsepower
Amps (CT): 7.5 Amps
Max. Frequency: 600 Hertz


Figure 5.1: CAM motor inverter.

### 5.3.2 Conveyer motor voltage frequency driver

The purpose of using the voltage frequency driver is to control the speed of conveyer motor by using multifunction speed, the type of conveyer Motor driver is Delta model VFD007L21A shown in figure 5.2

## Specifications

Input :1PH/9.7A 3PH/5.1A 200-240A 50-60HZ
Output:3PH 0-240V 4.2A 1.6kVA 1HP
Input Phase: 1
HP (CT): 1 Horsepower
Max. Frequency: 600 Hertz


Figure 5.2: Conveyer motor inverter.

### 5.4 Sensor

Limit switch is a switch operated by the motion of a machine part or presence of an object. They are used for control of a machine.

In this project there is 3 limit switches, 2 to check the position of cam during machine running and the other one is to check the presence of tray on the conveyer.

The limit switches used in this project has a model number Z-15GW2-B shown in figure 5.3.


Figure 5.3: Limit Switch.

## 5.5 (Power \& Control) Circuit

The shown in figure 5.4 an it is contain:


Figure 5.4: Electrical Panel.

## 5.5 (Power \& Control) Circuit



Figure 5.5 Power Circuit.

### 5.6 Electrical Panel \& Protection

### 5.6.1 Motor Overload

Overload relays are intended to protect motors against excessive heating due to prolonged motor over currents up to and including locked motor currents. Protection of the motor due to short circuits or grounds, is a function of circuit breakers, or motor short-circuit protectors.

The motor overload used for cylinder motor, and in this project used a META-MEC Series MMS-32S (2.5A) overload as shown in figure 5.6.


Figure 5.6: Motor overload

### 5.6.2 Contactors

A contactor is an eclectically controlled switch used for switching a power circuit, similar to a relay except with higher current ratings.

A contactor is controlled by a circuit which has a much lower power level than the switched circuit.

Contactors come in many forms with varying capacities and features. Unlike a circuit breaker, a contactor is not intended to interrupt a short circuit current. Contactors range from those having a breaking current of several amperes to thousands of amperes and 24 V DC to many kilovolts. The physical size of contactors ranges from a device small enough to pick up with one hand to large devices approximately a meter (yard) on a side. Contactors are used to control electric motors, lighting, heating, capacitor banks, thermal evaporators, and other electrical loads.

In this project used a one contactors for a cylinder motor and the contactor shown in figure 5.7.


Figure5.7:contactor.

### 5.6.3 Switches

The emergence switch are used to stop the machine immediately when something wrong happened with the machine as shown in the figure 5.8.a. The pushbutton are used to select the betit-fore type as shown in the figure 5.8.b .The selector switch used to select automatic or manual as shown in the figure 5.8.c .

C. Selector Switch

Figure 5.8: Emergence, Pushbutton, and select switch.

### 5.6.4 Klements

Used to connect wires and a rang the connections as shown in figure 5.9.


Figure 5.9: Klements.

### 5.6.5 LED

The led as shown in figure 5.10 are singed the machine operation mode .


Figure 5.10: LED.

## 6

## Chapter Six

## Experimental Result \& Recommendations

6.1 Introduction
6.2 Experimental Result
6.3 Recommendations
6.4 Future Work

### 6.1 Introduction

This chapter provides experimental result and some recommendations from the work learn for this project. In this chapter we are listing some goals hope to be accomplished or _at least_ under attention .

### 6.2 Experimental Result

We made some experiments on parts of our project and these are some of results :

1. Transporting system: before get the dough from molds, tried to check the operation of conveyer, so putting the tray on the conveyer unit and it run successfully and moving the tray under casting molds to starting the casting operation.
2. Cylinder and molds system: put a small quantity of a petit-four dough on the container ( 2 kg ) and the dough is passing through the cylinder into the molds, so the cylinder and molds system work successfully.
3. Cam system: the conveyer unit goes up or down when the cam motor run, so the cam motor run successfully.

At the first experiment we note that the final product of petit-fore has a large size so we reduce the casting time to make to achieve the desired size of petit-fore piece as shown in figure 6.1.


Figure 6.1: petit-Fore Sizes.

The experiment as shown in figure 6.2.


Figure 6.2: The Final Machine.

### 6.3 Recommendations

These recommendations are recorded to people who can create opportunities for student to make something new and useful, in order to make difference in our country Palestine:

1. Such projects should be handled among different departments according to the project nature (we had lots of electrical problems that might solve without having enough previous knowledge).
2. Once the university administration financially supported graduation projects, this support must be provided at the beginning of the project work, to enable students to do their projects according to the time plan, and to test them at the proper time.
3. The university should provide the proper toolsets, which enable the student to assemble his project and to test it the university campus, so he could get benefit of experiences in the university.

### 6.4 Future Work

The following tasks are suggested as future works:

1. Testing and evaluating the machine with different types of dough.
2. Compare the improvement of our product with other product by public bakery

## Appendix A

## Questionnaire Analysis

A.1.1. The amount of daily production.
A.1.2. Number of the worker.
A.1.3. Number of work hours.
A.1.4. Number of shapes.
A.1.5. Buy the machine.
A.1.6. Price of the machine.

This questionnaire took (13) bakery that production Petit-Fore.
The results of the questionnaire :

## -Q1: Do produce the petit-fore in your bakery?

All of the bakeries are produce a Petit-Fore in their shops.

## -Q2:What is the method that you are us in your bakery?

All of the bakeries are produce a Petit-Fore in the traditional method that depends on labor.

## -Q3: What is the size of the daily consumption of the product?

About $\% 54$ of bakeries are sell about 50 Kg of Petit-Fore, and the others are sell less as shown in the figure A.1.1


Figure A.1.1:The amount of daily production .

## -Q4:How many workers does it take to production this product?

About $\% 70$ of bakeries are use 3 or less worker to produce this product, and the other are more than that as shown in figure A.1.2.


Figure A.1.2:Number of the worker.

## -Q5: How much time needs of production this product?

About $\% 68$ of bakeries that produce 50 Kg it take 3-4 hour to produce that amount and the
 other amounts are shown in figure A.1.3.

Figure A.1.3: Number of work hours .

## -Q6: The number of shapes that can be produced in the traditional way?

According to figure A.1.4 more than the half of bakeries are produce between 11-20 shape of the petit-fore.


Figure A.1.4: Number of shapes.
-Q7: If you have been offered to you a machine industry Petit-Fore in automatic way are you going to buy it?
Most of the bakeries are said yes if the cost was acceptable according to figure A.1.5.


Figure A.1.5: Buy the machine.
-Q8: What is the expected price that will you pay for this machine?
About $\% 80$ of them were expected to pay around $10,000 \$$ as you see in figure A.1.6.


Figure A.1.6: Price of the machine.
-Q9: Is the manual " traditional " production covers the need of the market?
Almost agree that the traditional not cover the need of the market.
-Q10: How important is the machine for you, and whether you expect it would be economically?

Some of them are excited to this machine and expect that will be economically.


> .1. هل تقوم بإنتاج البيتيفور في محلك ؟
> أ. نعـ لا
> Y. ما هي الطريقة التي تستخفمها في انتاج البيتيفور ؟
$\qquad$
「. مـا هو حجم الاستهلاك اليومي من منتج البيتيفور ؟
$\qquad$
؛. كم هو عدد العمال الذي يتطبه انتاج هذا الصنف ؟
$\qquad$
-. كم يحتّاج من الوقت انتاج هذا الصنف ؟
$\qquad$
\. عدد الاشكال التّي يمكن انتاجها بالطريقة اليـويةّ؟

## V. الذا عرضت عیيك ملكة تقوم بصناعة البيتيفور بشكل الي وبدون الحاجة المى عملل هل ستقوم بشرائها ؟

^.. مـا هو السعر المتّوقِع والمقبول والأي من الممكن ان تدفعه لشُراء مثل هذه الالةّ ؟
$\qquad$
9. هل الاتّاج اليّوي يغطي حاجة السوق
$\qquad$

- • . ما مدى اهمبة الماكنة بالنسبة لك و هل ستتّوقع انها سنكون ذات جدوى اقتّصادية ؟ ...................................................................................................................


## Appendix B

B. 1 Delrin Properties.
B. 2 Belt Properties.
B. 3 Mechanical Properties of stainless steel.
B. 4 Mechanical Properties of steel 1020.

## ENSINGER-HYDE <br> ASK. THINK. SUCCEED.

## DELRIN ${ }^{\circledR}$ <br> (Acetal Homopolymer)

DELRIN ${ }^{\text {® }}$ is a crystalline plastic which offers an excellent balance of properties that bridge the gap between metals and plastics. DELRIN ${ }^{\circledR}$ possesses high tensile
strength, creep resistance and toughness. It also exhibits low moisture absorption. It is chemically resistant to hydrocarbons, solvents and neutral chemicals. These
properties along with its fatigue endurance make DELRIN ${ }^{\text {® }}$ ideal for many industrial applications.


## - Good dimensional stability

- Low moisture absorption

DELRIN ${ }^{\oplus}$ can operate in wet environments with little effect on performance or dimensions.

- Excellent machinability
- High fatigue endurance
- High strength and stiffness properties
- Superior impact and creep resistance
- Chemical resistance to fuels and solvents
- Natural grade is FDA, NSF and USDA compliant
- Good wear and abrasion properties

With its low coefficient of friction and hard and resilient surface,
DELRIN® is the material of choice in many wear applications.

[^2]
## TYPICAL PROPERTY VALUES

|  | PROPERTIES | $\begin{aligned} & \text { ASTM } \\ & \text { Test } \\ & \text { Method } \end{aligned}$ | Units | Delrin® 150 |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \frac{1}{\mathbf{d}} \\ & \frac{2}{0} \\ & \frac{2}{x} \end{aligned}$ | Density <br> Specific Gravity <br> Water Absorption, @24 hours, $73^{\circ} \mathrm{F}$ @Saturation, $73^{\circ} \mathrm{F}$ | $\begin{aligned} & \text { D792 } \\ & \text { D792 } \\ & \text { D570 } \\ & \text { D570 } \end{aligned}$ | $\begin{gathered} \mathrm{lbs} / \mathrm{ln}^{3} \\ \mathrm{~g} / \mathrm{cc} \\ \% \\ \% \end{gathered}$ | $\begin{gathered} 0.0513 \\ 1.42 \\ 0.25 \\ 0.9 \end{gathered}$ |
| $\begin{aligned} & \frac{1}{6} \\ & 0 \\ & \frac{0}{2} \\ & \frac{1}{3} \\ & \frac{11}{2} \end{aligned}$ | Tensile Strength @ Yield, $73^{\circ} \mathrm{F}$ <br> Tensile Modulus <br> Elongation @ Break, $73^{\circ} \mathrm{F}$ <br> Flexural Strength, $73^{\circ} \mathrm{F}$ <br> Flexural Modulus, $73^{\circ} \mathrm{F}$ <br> Compressive Strength <br> Izod Impact Strength, $73^{\circ} \mathrm{F}$ <br> Rockwell Hardness, $73^{\circ} \mathrm{F}$ <br> Shure Hardness <br> Wear Factor Against Steel, 40 psi, 50 fpm <br> Static Coefficient of Friction <br> Dynamic Coefficient of Friction, $40 \mathrm{psi}, 50 \mathrm{fpm}$ | D638 <br> D639 <br> D638 <br> D790 <br> D790 <br> D695 <br> D256 <br> D785 <br> D3702 <br> D3702 <br> D3702 | $\begin{gathered} \text { psi } \\ \text { psi } \\ \% \\ \text { psi } \\ \text { psi } \\ \text { psi } \\ \text { ft-lbs/in } \\ \text { M (R) Scale } \\ \text { D Scale } \\ \frac{\mathrm{in}}{}{ }^{3} \times \frac{1}{\mathrm{hr}} \times \frac{1}{\mathrm{PV}} \end{gathered}$ | $\begin{gathered} 9,000 \\ 350,000 \\ 25 \\ 11,500 \\ 420,000 \\ 5,200 \\ 1.5 \\ \text { M } 94(120) \\ - \\ 55 \times 10^{10} \\ - \\ - \\ 0.2 \end{gathered}$ |
| $\begin{gathered} \frac{1}{4} \\ \frac{8}{7} \\ \frac{\pi}{7} \\ \hline \end{gathered}$ | Heat Deflection Temperature @ 66 psi @264 psi <br> Coefficient of Linear Thermal Expansion <br> Maximum Servicing Temperature, Intermittent Long Term <br> Specific Heat <br> Thermal Conductivity <br> Vicate Softening Point <br> Melting Point <br> Flammability | D648 D648 D696 <br> UL746B <br> D2133 <br> UL94 | $\begin{gathered} { }^{\circ} \mathrm{F} \\ { }^{\circ} \mathrm{F} \\ \mathrm{in} / \mathrm{in} /{ }^{\circ} \mathrm{F} \\ { }^{\circ} \mathrm{F} \\ { }^{\circ} \mathrm{F} \\ \mathrm{BTU} / \mathrm{lb} \cdot{ }^{\circ} \mathrm{F} \\ \hline \\ { }^{\circ} \mathrm{F} \\ { }^{\circ} \mathrm{F} \end{gathered}$ | $\begin{gathered} 336 \\ 257 \\ 6.8 \times 10^{5} \\ 300 \\ 185 \\ 0.35 \\ - \\ - \\ 347 \\ H B(1.47) \end{gathered}$ |
|  | Surface Resistivity <br> Volume Resistivity <br> Dielectric Strength | D257 <br> D257 <br> D149 <br> D150 <br> D150 <br> D150 <br> D150 <br> D150 | ohm/square ohm-cm V/mil | $\begin{gathered} - \\ 10^{15} \\ 500 \\ 3.7 \\ 3.7 \\ - \\ -\quad . \\ 0.005 \end{gathered}$ |

This information is only to assist and advise you on current technical knowledge and is given without obligation or liability. All trade and patent rights should be observed. All rights reserved. Data obtained from extruded shapes material.

MATERIAL AVAILABILITY

Rods: Diameters: $43 / 4$ ", $10^{\prime}$ length
Length: $5^{\prime \prime}$ and greater diameter, $5^{\prime}$ length
Primary Specification (Resin) (Typical)
ASTM-D-4181 POM110B34330

Plates: $1 / 4^{\prime \prime}$ to $2^{\prime \prime}$ thickness inclusive are $2^{\prime} \times 4^{\prime}, 4^{\prime} \times 8^{\prime}, 4^{\prime} \times 10^{\prime}$ $2-1 / 4^{\prime \prime}$ to $4^{\prime \prime}$ thickness inclusive are $2^{\prime} \times 4^{\prime}$

Shapes Specification (Typical)
ASTM-D-6100 S-POM0111

## B. 2 Belt Properties :




## B. 3 Mechanical Properties of Stainless steel :

Table A-5<br>' unen prererrea.<br>Physical Constants of Materials

| Material | Modulus of Elasticity E |  | Modulus of Rigidity $\mathbf{G}$ |  | Poisson's Ratio $\nu$ | Unit Weight w |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mpsi | GPa | Mpsi | GPa |  | $\mathrm{lbf} / \mathrm{in}^{3}$ | lbf/ft ${ }^{3}$ | $\mathbf{k N} / \mathrm{m}^{\mathbf{3}}$ |
| Aluminum (all alloys) | 10.4 | 71.7 | 3.9 | 26.9 | 0.333 | 0.098 | 169 | 26.6 |
| Beryllium copper | 18.0 | 124.0 | 7.0 | 48.3 | 0.285 | 0.297 | 513 | 80.6 |
| Brass | 15.4 | 106.0 | 5.82 | 40.1 | 0.324 | 0.309 | 534 | 83.8 |
| Carbon steel | 30.0 | 207.0 | 11.5 | 79.3 | 0.292 | 0.282 | 487 | 76.5 |
| Cast iron (gray) | 14.5 | 100.0 | 6.0 | 41.4 | 0.211 | 0.260 | 450 | 70.6 |
| Copper | 17.2 | 119.0 | 6.49 | 44.7 | 0.326 | 0.322 | 556 | 87.3 |
| Douglas fir | 1.6 | 11.0 | 0.6 | 4.1 | 0.33 | 0.016 | 28 | 4.3 |
| Glass | 6.7 | 46.2 | 2.7 | 18.6 | 0.245 | 0.094 | 162 | 25.4 |
| Inconel | 31.0 | 214.0 | 11.0 | 75.8 | 0.290 | 0.307 | 530 | 83.3 |
| lead | 5.3 | 36.5 | 1.9 | 13.1 | 0.425 | 0.411 | 710 | 111.5 |
| Magnesium | 6.5 | 44.8 | 2.4 | 16.5 | 0.350 | 0.065 | 112 | 17.6 |
| Molybdenum | 48.0 | 331.0 | 17.0 | 117.0 | 0.307 | 0.368 | 636 | 100.0 |
| Monel metal | 26.0 | 179.0 | 9.5 | 65.5 | 0.320 | 0.319 | 551 | 86.6 |
| Nickel silver | 18.5 | 127.0 | 7.0 | 48.3 | 0.322 | 0.316 | 546 | 85.8 |
| Nickel steel | 30.0 | 207.0 | 11.5 | 79.3 | 0.291 | 0.280 | 484 | 76.0 |
| Phosphor bronze | 16.1 | 111.0 | 6.0 | 41.4 | 0.349 | 0.295 | 510 | 80.1 |
| Stainless steel (18-8) | 27.6 | 190.0 | 10.6 | 73.1 | 0.305 | 0.280 | 484 | 76.0 |
| Titanium alloys | 16.5 | 114.0 | 6.2 | 42.4 | 0.340 | 0.160 | 276 | 43.4 |

## B. 4 Mechanical properties of Steel 1020 :

## Table A-20

Deterministic ASTM Minimum Tensile and Yield Strengths for Some HotRolled (HR) and Cold-Drawn (CD) Steels [The strengiths listed are estimated ASTM minimum values in the size range 18 to $32 \mathrm{~mm}\left(\frac{3}{4}\right.$ to $1 \frac{1}{4}$ in). These strengths are suitable for use with the design factor defined in Sec. 1-10, provided the materials conform to ASTM A6 or A568 requirements or are required in the purchase specifications. Remember that a numbering system is not a specification.] Sounce: 1986 SAE Handbook, p. 2.15.

| 1 UNS No. | $\begin{gathered} 2 \\ \text { SAE and/or } \\ \text { AISI No. } \end{gathered}$ | 3 <br> Processing | 4 <br> Tensile Strength, MPa (kpsi) | 5 <br> Yield <br> Strength, MPa (kpsi) | Elongation in $2 \mathrm{in}, \%$ | Reduction in Area, \% | $\begin{gathered} 8 \\ \text { Brinell } \\ \text { Hardness } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| G10060 | 1006 | HR | 300 (43) | 170 (24) | 30 | 55 | 86 |
|  |  | CD | 330 (48) | 280 (41) | 20 | 45 | 95 |
| G10100 | 1010 | HR | 320 (47) | 180 (26) | 28 | 50 | 95 |
|  |  | CD | 370 (53) | 300 (44) | 20 | 40 | 105 |
| G10150 | 1015 | HR | 340 (50) | 190 [27.5] | 28 | 50 | 101 |
|  |  | CD | 390 (56) | 320 (47) | 18 | 40 | 111 |
| G10180 | 1018 | HR | 400 (58) | 220 (32) | 25 | 50 | 116 |
|  |  | CD | 440 (64) | 370 (54) | 15 | 40 | 126 |
| G10200 | 1020 | HR | 380 (55) | 210 (30) | 25 | 50 | 111 |
|  |  | CD | 470 (68) | 390 (57) | 15 | 40 | 131 |
| G10300 | 1030 | HR | 470 (68) | 260 [37.5] | 20 | 42 | 137 |
|  |  | CD | 520 (76) | 440 (64) | 12 | 35 | 149 |
| G10350 | 1035 | HR | 500 (72) | 270 [39.5] | 18 | 40 | 143 |
|  |  | CD | 550 (80) | 460 (67) | 12 | 35 | 163 |
| G10400 | 1040 | HR | 520 (76) | 290 (42) | 18 | 40 | 149 |
|  |  | CD | 590 (85) | 490 (71) | 12 | 35 | 170 |
| G10450 | 1045 | HR | 570 (82) | 310 (45) | 16 | 40 | 163 |
|  |  | CD | 630 (91) | 530 (77) | 12 | 35 | 179 |
| G10500 | 1050 | HR | 620 (90) | 340 [49.5] | 15 | 35 | 179 |
|  |  | CD | 690 (100) | 580 (84) | 10 | 30 | 197 |
| G10600 | 1060 | HR | 680 (98) | 370 (54) | 12 | 30 | 201 |
| G10800 | 1080 | HR | 770 (112) | 420 [61.5] | 10 | 25 | 229 |
| G10950 | 1095 | HR | 830 (120) | 460 (66) | 10 | 25 | 248 |

## Appendix C

## Programming Code

C. 1 Ladder Code.
C. 1 Ladder Code :





|c|c|c|

Rung 4





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[^0]:    ${ }^{1}$ - Appendix B

[^1]:    ${ }^{3}$ - Appendix B

[^2]:    DELRIN ${ }^{\ominus}$ s overall combination of physical, tribological and environmental properties make it ideal for many industrial wear and mechanical applications. Parts exposed to a moist or wet environment, such as pump and valve components, are especially appropriate. Other common uses for DELRIN ${ }^{\circledR}$ include gears, bearings, bushings, rollers, fittings and electrical insulator parts.

